| Form 3160-5<br>(August 2007)  | UNITED STATE<br>DEPARTMENT OF THE I<br>BUREAU OF LAND MANA  | INTERIOR OLD AN   | esia OMB M<br>Expires   | 1 APPROVED<br>NO. 1004-0135<br>5: July 31, 2010                     |  |
|---|---|---|---|---|--|
|   | NDRY NOTICES AND REPO   |   | 5. Lease Serial No.<br>NMNM055737   | 1   |  |
| Do not<br>abandoi   | use this form for proposals to<br>ned well. Use form 3160-3 (AF   | <ul> <li>drill or to re-enter an</li> <li>D) for such proposals.</li> </ul>   | 6. If Indian, Allottee  | or Tribe Name   |  |
| SUBMIT  | IN TRIPLICATE - Other instru  | 7. If Unit or CA/Agr  | 7. If Unit or CA/Agreement, Name and/or   |   |  |
| <ol> <li>Type of Well</li> <li>Oil Well Gas Wel</li> </ol>  | I D Other   | 8. Well Name and No<br>AAO FEDERAL  |   |   |  |
| 2. Name of Operator<br>APACHE CORPORAT  | Contact:  | SORINA FLORES<br>res@apachecorp.com   | 9. API Well No.<br>30-015-42359-  | -00-X1  |  |
| 3a. Address<br>303 VETERANS AIRP<br>MIDLAND, TX 79705   | ARK LANE SUITE 3000   | 3b. Phone No. (include area cod<br>Ph: 432-818-1167   | e) 10. Field and Pool, o<br>RED LAKE  | er Exploratory  |  |
|   | e, Sec., T., R., M., or Survey Description  | n)  | 11. County or Parish  | , and State   |  |
| Sec 1 T18S R27E NE<br>32.462812 N Lat, 104.   | SW 1960FSL 2063FWL<br>140220 W Lon  |   | EDDY COUNT  | Ϋ́, ΝΜ  |  |
| 12 <sup>½</sup> CHEC  | K APPROPRIATE BOX(ES) T   | O INDICATE NATURE OF  | NOTICE, REPORT, OR OTHE   | ER DATA   |  |
| TYPE OF SUBMISSIC   | DN  | ТҮРЕ (  | OF ACTION   |   |  |
| Notice of Intent  | <ul> <li>Acidize</li> <li>Alter Casing</li> </ul>   | <ul><li>Deepen</li><li>Fracture Treat</li></ul>   | Production (Start/Resume) Reclamation   | Water Shut  |  |
| Subsequent Report   | Casing Repair   | New Construction  | Recomplete  | 🕅 Other   |  |
| 🗖 Final Abandonment N   | Iotice         Change Plans           Convert to Injection  | <ul> <li>Plug and Abandon</li> <li>Plug Back</li> </ul>   | <ul> <li>Temporarily Abandon</li> <li>Water Disposal</li> </ul>   | Change to Ori<br>PD   |  |
| following completion of the<br>testing has been completed.<br>determined that the site is re<br>BLM-CO-1463 NATIO<br>Apache request to cha<br>IN THE EVENT CMT I<br>CSG PROG: All csg is<br>HOLE DEPTH OD<br>MW RATE/SF RAT | NWIDE/NMB000736<br>ange CSG/CMT/BOP program as<br>S CIRC TO SURF ON PRIMAR<br>new & API appvd<br>WT GRADE COLLAR DESIG<br>TE/SF RATE/SF | esults in a multiple completion or re<br>iled only after all requirements, inclu<br>s follows:<br>Y CMT JOB FOR SURF CSC<br>,<br>GN COLPS BURST TEN | completion in a new interval, a Form 31<br>iding reclamation, have been completed<br>Accepted f<br>NMO<br>a:<br>SEE ATTACHE | ion-4 shall be filed of<br>and the operator has<br>ior record<br>CD |  |
| 17-1/2" 0-350' 13-3/8"<br>4.625 7.06 22.15<br>7-7/8" 0-4630' 5-1/2"<br>4600'TVD   |   | si 1730psi 322000#<br>osi 5320psi 247000#   | <b>NM OIL</b><br>AR   | - CONSERVA  |  |
| 14. I hereby certify that the for   | Electronic Submission<br>For APACH<br>Committed to AFMSS for pro  | #249333 verified by the BLM W<br>IE CORPORATION, sent to the<br>ocessing by CATHY QUEEN or  | Carlsbad<br>06/12/2014 (14CQ0438SE)   | RECEIVED  |  |
| Name(Printed/Typed) SC  | DRINA FLORES  | Title SUBM  |   |   |  |
| Signature (El   | ectronic Submission)  | Date 06/11/   | 2014 APPKU  |   |  |
|   | THIS SPACE F  | OR FEDERAL OR STATE   |   | 2014  |  |
| Approved By   | re attached. Approval of this notice doe  |   | BAREAU OF VAND M<br>CARLSPID FIEL   | ANAGEMENT   |  |
| Conditions of approval, if any, and   |   |   |   |   |  |

\*\* BLM REVISED \*\*

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### Additional data for EC transaction #249333 that would not fit on the form

#### 32. Additional remarks, continued

\*\*Calc safety factors based on: Burst -Full evacuation of annulus & csg filled with mud. Collapse -Mud in annulus & full evacuation of csg. Tension -Annulus & csg filled with mud.

#### CMT PROGRAM:

13-3/8" Surf (cmt to surf/100% excess cmt) Single slurry: 420sx Cl C w/1% CaCL2+0.25% R38 (18.8wt,1.34yld,6.33gal/sk) Comp Strength: 12hr-813psi 24hr-1205psi \*If lost circ is encountered while drig, 17-1/2" hole, 200sx CI C Thixotropic cmt (14.4wt,1.55yld,6.65gal/sk) may be pmpd ahead of cmt slurry shown above.

5-1/2" Prod (Cmt to surf/20% excess cmt) Lead: 410sx(35:65)Poz C w/5%Salt+ 0.25% R38+ 6% Bentonite(12.4wt,2.1yld, 10.57gal/sk) Comp Strength: 12hr-589psi 24hr-947psi Tail: 270sx (50:50) Poz C w/5% Salt + 0.25% R38 + 2% Bentonite(14.2wt, 1.28vld, 5.88gal/sk) Comp Strengths: 12hr-1379psi 24hr-2332psi

#### PROPOSED CONTROL EQUIP

An 11" 3M psi WP BOP stack consisting of an annular bag type preventer, middle pipe rams, & bottom blind rams will be nippled up on the 13-3/8" surf csg head & tested to 70% of csg burst. BOP will be utilized continuously until TD is reached. Max surf pressure is not expected to exceed 2000psi. BHP is calc to be approx 2024psi. All BOPs & associated equip will be tested per BLM Drilling Ops Order #2. BOP will be operated & checked each 24-hr period & blind rams will be operated & checked when the drill pipe is out of the hole. Function tests will be documented on the daily driller's log. A 3000psi choke manifold with a 3" panic line will be installed. A full opening stabbing valve & kelly cock will be on the derrick floor in case of need. No abnormal pressures or temps are expected in this well. No nearby wells have encountered any well control problems.

IN THE EVENT CMT IS NOT CIRC TO SURF ON PRIMARY CMT JOB FOR SURF CSG: HOLE DEPTH OD WT GRADE COLLAR DESIGN COLPS BURST TENSION MW RATE/SF RATE/SF RATE/SF 17-1/2" 0-350' 13-3/8" 48# H40 STC 8.8ppg 770psi 1730psi 322000# 2" 0-350 13-370 407 1112 211 7.06 22.15 0-400' 8-5/8" 24# J55 STC 8.8ppg 1370psi 2950psi 244000# 7.486 10.54 29.37 7.486 10.54 29.37 4.625 11" 4600'TVD 7-7/8" 0-4630' 5-1/2" 17# j55 LTC 10.0ppg 4910psi 5320psi 247000# 4600'TVD 2.054 2.23 3.67 \*\*Calc safety factors based on: Burst -Full evacuation of annulus & csg filled with mud. Collapse -Mud in annulus & full evacuation of csg. Tension -Annulus & csg filled with mud.

#### CMT PROGRAM

13-3/8" Surf (cmt to surf/100% excess cmt) Single slurry: 420sx Cl C w/1% CaCL2+0.25% R38 (18.8wt,1.34yld,6.33gal/sk) Comp Strength: 12hr-813psi 24hr-1205psi If lost circ is encountered while drlg, 17-1/2" hole, 200sx CI C Thixotropic cmt (14.4wt,1.55yld,6.65gal/sk) may be pmpd ahead of cmt slurry shown above.

\*\*\*Rest of CMT PROGRAM & PROPOSED CONTROL EQUIP on attachment due to lack of space. Have also added a new directional plan.\*\*\*

## Apache proposes to change the casing/cement/BOP program as shown below.

## In the event that cement IS circulated to surface on the primary cement job for the surface casing:

| HOLE<br>SIZE | DEPTH                   | OD<br>CSG | WEIGHT | GRADE | COLLAR | DESIGN<br>MW | COLLAPSE<br>Rating/SF* | BURST<br>Rating/SF* | TENSION<br>Rating/SF* |
|--------------|-------------------------|-----------|--------|-------|--------|--------------|------------------------|---------------------|-----------------------|
| 17-1/2"      | 0' - 350!               | 13-3/8"   | 48#    | H-40  | SŤC    | 8.8 ppg      | 770 psi<br>4.625       | 1730 psi<br>7.06    | 322000 lbs<br>22.15   |
| 7-7/8″       | 0′-4630′<br>(4600′ TVD) | 5-1/2"    | 17#    | J-55  | LTC ·  | 10.0 ppg     | 4910 psi<br>2.054      | 5320 psi<br>2.23    | 247000 lbs<br>3.70    |

1. Casing Program: All casing is new & API approved

\*Calculated Safety Factors based on:

Burst: Full evacuation of annulus and casing filled with mud Collapse: Mud in annulus and full evacuation of casing Tension: Annulus and casing filled with mud

#### 2. CEMENT PROGRAM:

#### A. <u>13-3/8" Surface (Cmt to surf / 100% excess cmt):</u>

<u>Single Slurry</u>: 420 sx Class C w/ 1% CaCl2 + 0.25% R38 (14.8 wt, 1.34 yld, 6.33 gal water/sk) Comp Strengths : **12 hr** – **8**13 psi **24 hr** – **1**205 psi

If lost circulation is encountered while drilling the 17-1/2" hole, 200 sx Class C thixotropic cement (14.4 wt, 1.55 yld, 6.65 gal water/sk) may be pumped ahead of the cement slurry shown above.

### B. <u>5-1/2</u> Production (Cmt to surf / 20 % excess cmt):

Lead: 410 sx (35:65) Poz C w/ 5% Salt + 0.25% R38 + 6% Bentonite (12.4 wt, 2.1 yld, 10.57 gal water/sk) Compressive Strengths: **12 hr** - 589 psi **24 hr** - 947 psi

Tail: 270 sx (50:50) Poz C w/ 5% Salt + 0.25% R38 + 2% Bentonite (14.2 wt, 1.28 yld, 5.88 gal water/sk) Compressive Strengths: 12 hr – 1379 psi 24 hr – 2332 psi

#### 3. PROPOSED CONTROL EQUIPMENT

An 11" 3M psi WP BOP stack consisting of an annular bag type preventer, middle pipe rams, and bottom blind rams will be nippled up on the 13-3/8" surface casing head and tested to 70% of casing burst. The BOP will be utilized continuously until TD is reached. The maximum surface pressure is not expected to exceed 2000 psi. BHP is calculated to be approximately 2024 psi. All BOPs and associated equipment will be tested per BLM *Drilling Operations Order #2*. The BOP will be operated and checked each 24-hour period and the blind rams will be operated and checked when the drill pipe is out of the hole. Function tests will be documented on the daily driller's log. A 3000 psi choke manifold with a 3" panic line will be installed. A full opening stabbing valve & kelly cock will be on the derrick floor in case of need. No abnormal pressures or temperatures are expected in this well. No nearby wells have encountered any well control problems.

#### In the event that cement IS NOT circulated to surface on the primary cement job for the surface casing:

| HOLE<br>SIZE | DEPTH                   | OD<br>CSG | WEIGHT | GRADE | COLLAR | DESIGN<br>MW | COLLAPSE<br>Rating/SF* | BURST<br>Rating/SF* | TENSION<br>Rating/SF* |
|--------------|-------------------------|-----------|--------|-------|--------|--------------|------------------------|---------------------|-----------------------|
| 17-1/2"      | 0' - 350'               | 13-3/8"   | 48#    | H-40  | STC    | 8.8 ppg      | 770 psi<br>4.625       | 1730 psi<br>9.77    | 322000 lbs<br>22.15   |
| 11″          | 0' - 400'               | 8-5/8"    | 24#    | J-55  | STC    | 8.8 ppg      | 1370 psi<br>7.486      | 2950 psi<br>10.54   | 244000 lbs<br>29.37   |
| 7-7/8"       | 0'-4630'<br>(4600' TVD) | 5-1/2"    | 17#    | J-55  | LTC    | 10.0 ppg     | 4910 psi<br>2.054      | 5320 psi<br>2.23    | 247000 lbs<br>3.70    |

#### 1. Casing Program: All casing is new & API approved

\*Calculated Safety Factors based on:

Burst: Full evacuation of annulus and casing filled with mud Collapse: Mud in annulus and full evacuation of casing Tension: Annulus and casing filled with mud

AAO FEDERAL #27

#### 2. CEMENT PROGRAM:

### A. <u>13-3/8" Surface (Cmt to surf / 100% excess cmt):</u>

<u>Single Slurry</u>: 420 sx Class C w/ 1% CaCl2 + 0.25% R38 (14.8 wt, 1.34 yld, 6.33 gal water/sk) Comp Strengths : **12 hr - 8**13 psi **24 hr -** 1205 psi

If lost circulation is encountered while drilling the 17-1/2" hole, 200 sx Class C thixotropic cement (14.4 wt, 1.55 yld, 6.65 gal water/sk) may be pumped ahead of the cement slurry shown above.

#### B. <u>8-5/8" Intermediate (Cmt to surf / 50% excess cmt):</u>

<u>Single Slurry</u>: 220 sx Class C w/ 1% CaCl2 +<sup>(</sup>0.25% R38 (14.8 wt, 1.34 yld, 6.33 gal water/sk) Comp Strengths : **12 hr** – **8**13 psi **24 hr** – **1**205 psi

#### C. <u>5-1/2" Production (Cmt to surf / 20 % excess cmt):</u>

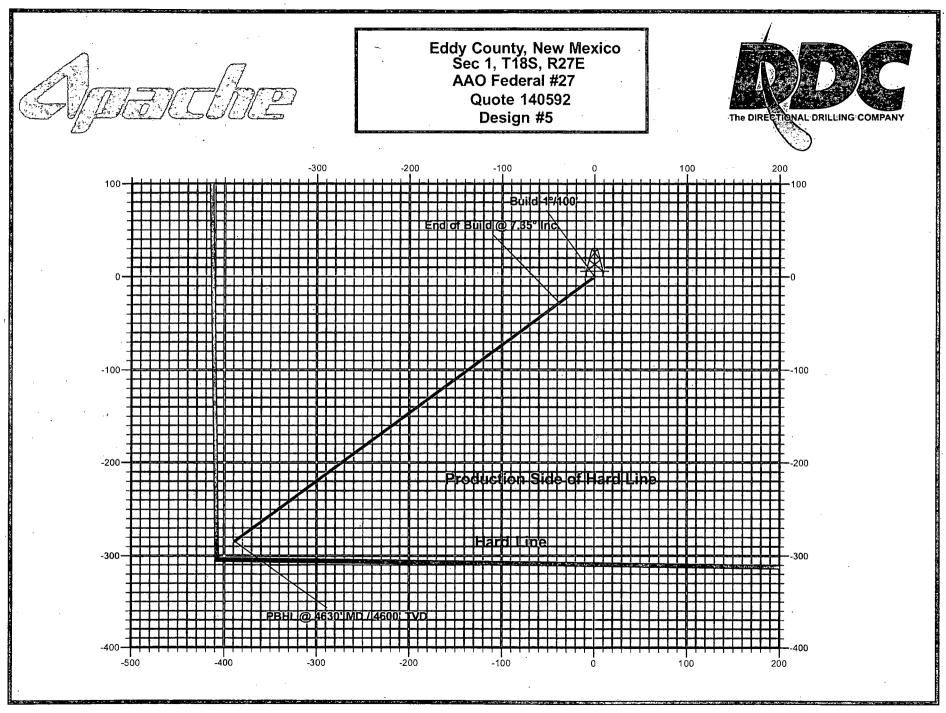
Lead: 310 sx (35:65) Poz C w/ 5% Salt + 0.25% R38 + 6% Bentonite (12.4 wt, 2.1 yld, 10.57 gal water/sk) Compressive Strengths: 12 hr – 589 psi 24 hr – 947 psi

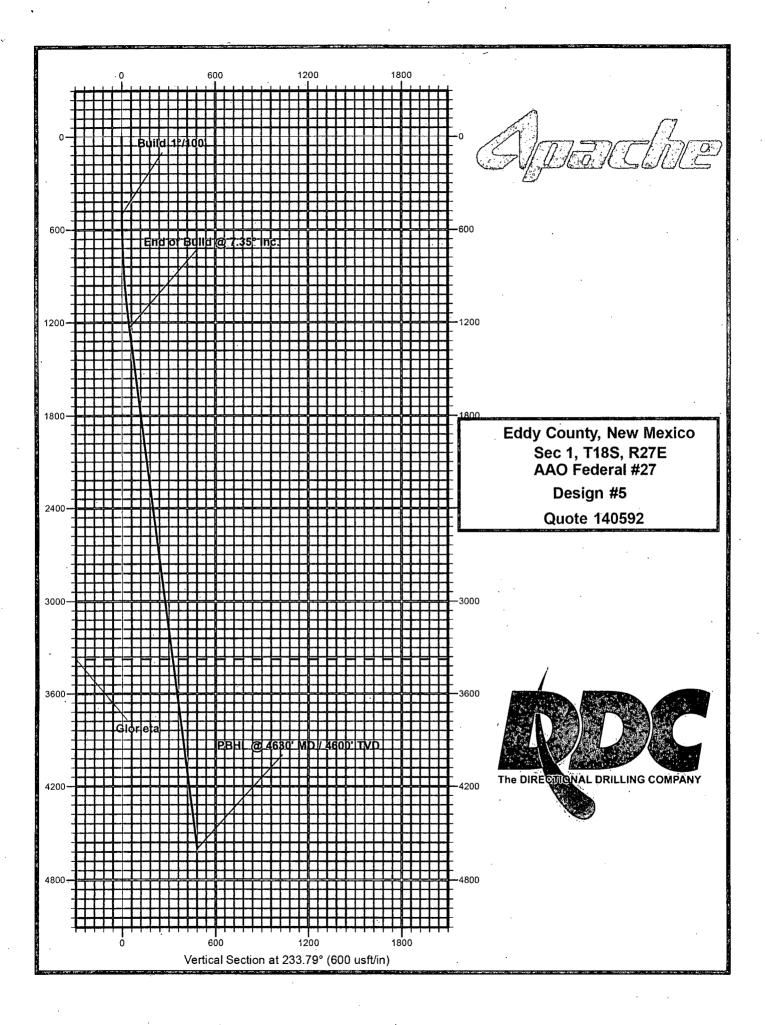
<u>Tail:</u> 270 sx (50:50) Poz C w/ 5% Salt + 0.25% R38 + 2% Bentonite (14.2 wt, 1.28 yld, 5.88 gal water/sk) Compressive Strengths: **12 hr** – 1379 psi **24 hr** – 2332 psi

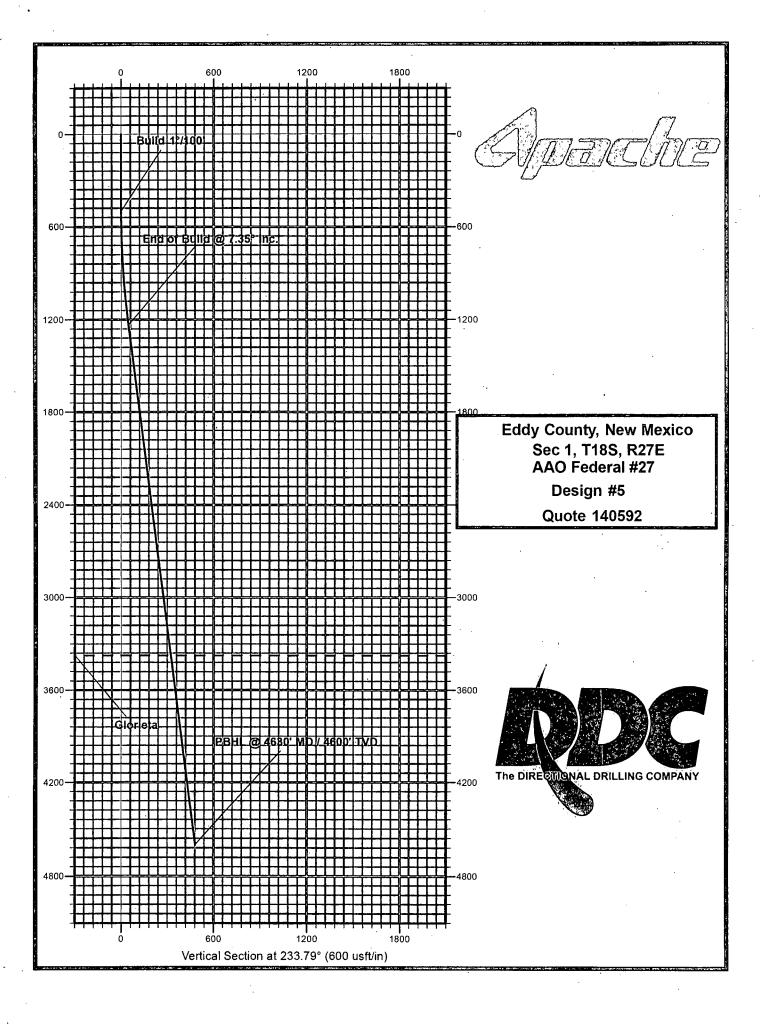
#### 3. PROPOSED CONTROL EQUIPMENT

An 11" 3M psi WP BOP stack consisting of an annular bag type preventer, middle pipe rams, and bottom blind rams will be nippled up on the 13-3/8" surface casing head and tested to 70% of casing burst. After intermediate casing is set and cemented the BOP will be nippled up on the casing spool and tested to 2000 psi. The BOPE will be utilized continuously until TD is reached. The maximum surface pressure is not expected to exceed 2000 psi. BHP is calculated to be approximately 2024 psi. All BOP's and associated equipment will be tested per BLM *Drilling Operations Order #2*. The BOP will be operated and checked each 24-hour period and the blind rams will be operated and checked when the drill pipe is out of the hole. Function tests will be documented on the daily driller's log. A 3000 psi choke manifold with a 3" panic line will be installed. A full opening stabbing valve & kelly cock will be on the derrick floor in case of need. No abnormal pressures or temperatures are expected in this well. No nearby wells have encountered any well control problems.

#### AAO FEDERAL #27









# **Apache Corporation**

Eddy County, New Mexico Sec 1, T18S, R27E AAO Federal #27

Wellbore #1

Plan: Design #5

# **DDC Well Planning Report**

10 June, 2014



Apparche

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## DDC

Well Planning Report



| D   | a takan managarakan menungkat kerikat                                     |   | The second second second   | CALIFORNIA CALIFORNIA   |   |   |  |   |   |
|---|---|---|--|---|---|---|--|---|---|
| Database:<br>Company:<br>Project:<br>Site:<br>Well:<br>Wellbore:<br>Design:   | Apacha<br>Eddy Co<br>Sec 1, 1<br>AAO Fe<br>Wellbor<br>Design              | #5,   | Xico   |   | Local Co-ordinate Refe<br>TVD Reference:<br>MD Reference;<br>North Reference;<br>Survey, Calculation Me   | thod:   | Well AAO Fédéra<br>WELL @ 3615 0u<br>WELL @ 3615 0u<br>Grid<br>Minimum Curvatu                                       | isti (Capstar #1<br>isti (Capstar #1                  | 18)   |
| Project   | Eddy Co   | unty: New Mexi  | ico  | ر بالا بالم من الم  | al your and their grant to we   | مارين ميندون مريديد معين مير<br>مسرد ميندون مريديد والساسي  | rdanti   | مستشفين فليتنا والمست                                 | And the second second   |
| Map System:<br>Geo Datum:<br>Map Zone:  | NAD 1927  | Plane 1927 (Ex<br>(NADCON CO<br>to East 3001  |  |   | System Datum:   | Me  | ean Sea Level  |   |   |
| Site  | Sec 1, T  | 18S, R27E   |  |   |   |   |  | ·····   |   |
| Site Position:  |   |   | Northing   |   | 645,438.80 usft   | Latitude:   |  | · · · · · · · · · · · · · · · · · · ·                 | 32° 46' 27,708 N  |
| From:   | Мар   |   | Easting:   | •   | 530,705.90 usft   | Latitude:<br>Longitude:   |  |   | 104° 14' 0.354 W  |
| Position Uncer  | •   | 0.0 เ   | -  | lus:  | 13-3/16 "   | Grid Converg  | ence:  |   | 0.05 °  |
| Well  | AAO Fed   | eral #27  | ىرىمى بۇرۇپ يىرىغى بىرىيى<br>يابىر بىرى بىرى بىرىيى بىرىيى بىرىيى  |   | مىرى بىلىمىكى بىلىمىرى بىلىمىرى بىرى بىرى بىرى بىلى بىلى بىلى<br>   | 1   | ىدۇنىرىدىيى بەرەپىيە بىرىسىيە مەرەپىيە<br>سەردىت ، ھىمدە ھەدىمە ، مەرەپىيە   |   | and any and a second |
|   |   |   | الأركى فسلامتنا الشبر المحاد متراسمية التعقدين   |   |   |   |  |   |   |
| Well Position   | +N/-S   |   | usft North   | ina:  | ********  |   |  |   | 32° 46' 27,708 N  |
| Well Position   | +N/-S<br>+E/-W  | 0.0   |  | -   | 645,438.80  | Dusft Lati  | tude:  |   |   |
| Well Position<br>Position Uncer   | +E/-W   | 0.0<br>0.0  | usft Easti   | -   | 645,438.80<br>530,705.90  | Dusft Lati<br>Dusft Lon   |  |   | 104° 14' 0.354 W  |
| Position Uncer<br>Wéllbore  | +E/-W<br>tainty   | 0.0<br>0.0<br>0.0   | usft Eastli<br>usft Wellh  | ng:<br>head Elevation   | 645,438.80<br>530,705.90  | ) usft Lati<br>) usft Lon<br>Gro  | tude:<br>igitude:<br>und Level:  | Field Str   | 104° 14' 0.354 W<br>3,604.0 usf   |
| Position Uncer  | +E/-W<br>tainty   | 0.0<br>0.0<br>0.0<br>#1   | usft Eastli<br>usft Wellh<br>Sample D  | ng:<br>nead Elevation   | 645,438.80<br>530,705.90<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:   | Dusft Lati<br>Dusft Lon   | tude:<br>igitude:<br>und Level:<br>ngle,   | ېلېنې کې          | 104° 14' 0.354 W<br>3,604.0 usfi  |
| Position Uncer<br>Wéllbore  | +E/-W<br>tainty   | 0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample D  | ng:<br>head Elevation   | 645,438.80<br>530,705.90<br>:<br>Declination  | Dusft Lati<br>Dusft Lon<br>Gro  | tude:<br>igitude:<br>und Level:<br>ngle,   |   | 104° 14' 0.354 W<br>3,604.0 usf   |
| Position Uncer<br>Wéllbore  | +E/-W<br>tainty<br>Wellbore<br>Mode                                       | 0.0<br>0.0<br>0.0<br>#1   | usft Eastli<br>usft Wellh<br>Sample D  | ng:<br>nead Elevation<br>ate<br>/9/2014   | 645,438.80<br>530,705.90<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:   | Dusft Lati<br>Dusft Lon<br>Gro  | tude:<br>igitude:<br>und Level:<br>ingje,<br>))<br>60.51   |   |   |
| Position Uncer<br>Weilbore<br>Mägnetics   | +E/-W<br>tainty<br>Wellbore<br>Mode                                       | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample D  | ng:<br>nead Elevation<br>ate<br>/9/2014   | 645,438.80<br>530,705.90<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:<br>:   | Dusft Lati<br>Dusft Lon<br>Gro  | tude:<br>igitude:<br>und Level:<br>ingje,<br>))<br>60.51   |   | 104° 14' 0.354 W<br>3,604.0 usft<br>angith:   |
| Position Uncer<br>Wëlibore<br>Magnetics<br>Design   | +E/-W<br>tainty<br>Wellbore<br>Mode                                       | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample D  | ng:<br>nead Elevation<br>ate<br>/9/2014   | 645,438.80<br>530,705.90<br>:<br>Declination<br>(*)<br>7.57   | Dusft Lati<br>Dusft Lon<br>Gro  | tude:<br>igitude:<br>und Level:<br>ingje,<br>))<br>60.51   | (jî ĵ)  | 104° 14' 0.354 W<br>3,604.0 usf   |
| Position Uncer<br>Weilbore<br>Magnetics<br>Design<br>Audit Notes:   | +E/-W<br>tainty<br>Wellbore<br>Modi                                       | 0.0<br>0.0<br>0.0<br>1.#1<br>I.Name<br>IGRF2010   | usft Eastli<br>usft Wellh<br>Sample D<br>6,  | ng:<br>nead Elevation<br>ate<br>/9/2014<br>PLAI   | 645,438.80<br>530,705.90<br>:<br>Decilination<br>(°)<br>7.57<br>N Tio   | Dusft Lati  | tude:<br>igitude:<br>und Level:<br>ingle,<br>))<br>60.51<br>0<br>Direc   | (jî î)<br>.0<br>țlon                                  | 104° 14' 0.354 W<br>3,604.0 usft<br>angith:   |
| Position Uncer<br>Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:   | +E/-W<br>tainty<br>Wellbore<br>Modi                                       | 0.0<br>0.0<br>0.0<br>1.#1<br>I.Name<br>IGRF2010   | usft Eastli<br>usft Wellh<br>Sample D<br>6<br>Phase:<br>Dth From (TVD)   | ng:<br>nead Elevation<br>ate<br>/9/2014<br>PLAI   | 645,438.8(<br>530,705.9(<br>:<br>Decilination<br>(°))<br>7.57<br>N Tir<br>+N/;S +H<br>(usft)) (L  | 0 usft Lati<br>0 usft Lon<br>Gro<br>Dip/A<br>(1)<br>(1)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2)<br>(2        | tude:<br>igitude:<br>und Level:<br>ingle<br>60.51  | ((nī)<br>.0<br>.1(loīn')<br>.),                       | 104° 14' 0.354 W<br>3,604.0 usf   |
| Position Uncer<br>Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Sectio  | +E/-W<br>tainty<br>Wellbore<br>Modi                                       | 0.0<br>0.0<br>0.0<br>1.#1<br>I.Name<br>IGRF2010   | usft Eastin<br>usft Wellh<br>Sample D<br>6,<br>Phase:<br>2th From (TVD)<br>(usft)  | ng:<br>nead Elevation<br>ate<br>/9/2014<br>PLAI   | 645,438.8(<br>530,705.9(<br>:<br>Decilination<br>(°))<br>7.57<br>N Tir<br>+N/;S +H<br>(usft)) (L  | Dusft Lati<br>Dusft Lon<br>Gro<br>Dip/A<br>(2)<br>Con<br>Depth:<br>2/W/<br>(2)  | tude:<br>igitude:<br>und Level:<br>igie,<br>)<br>60.51<br>0<br>Direc<br>(*   | ((nī)<br>.0<br>.1(loīn')<br>.),                       | 104° 14' 0.354 W<br>3,604.0 usf   |
| Position Uncer<br>Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Sectio  | +E/-W<br>tainty<br>Wellbore<br>Mode<br>(Design #                          | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample:D<br>6,<br>Phase:<br>5th/From.(TVD)<br>(Usft)<br>0.0                                   | ng:<br>nead Elevation<br>ate<br>/9/2014<br>PLAI<br>PLAI   | 645,438.8(<br>530,705.9(<br>:<br>Decilination<br>(°))<br>7.57<br>N Tir<br>+N/;S +H<br>(usft)) (L  | Dusft Lati<br>Dusft Lon<br>Gro<br>Dip/A<br>(2)<br>Con<br>Depth:<br>2/W/<br>(2)  | tude:<br>igitude:<br>und Level:<br>igie,<br>)<br>60.51<br>0<br>Direc<br>(*   | ((nī)<br>.0<br>.1(loīn')<br>.),                       | 104° 14' 0.354 V<br>3,604.0 usf   |
| Position Uncer<br>Weilbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Vertical Sections<br>Measured<br>Depth                           | +E/-W<br>tainty<br>(Wellbore<br>Modi<br>(Design.#                         | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample D<br>6,<br>Phase:<br>5th From (TVD)<br>(usft)<br>0.0                                   | ng:<br>nead Elevation<br>ate<br>/9/2014<br>PLAI<br>PLAI   | 645,438.80<br>530,705.90<br>:<br>Declination<br>(*)<br>7.57<br>N The<br>+N//S +ti<br>(usft)) (i<br>0.0 (<br>)<br>Doglegi<br>+E/-W) Rate                                     | Dusft Lati<br>Dusft Lon<br>Gro<br>Dip)A<br>(f<br>c<br>c<br>on Depth:<br>E/W/<br>(sti))<br>D.0<br>Builid<br>Rate                     | tude:<br>igitude:<br>und Level:<br>ingle<br>))<br>60.51<br>0.<br>Direc<br>(°<br>233)<br>Turn.<br>Rate                | (fi ī)<br>0<br>flon'<br>);<br>79<br>TEO               | 104° 14' 0.354 V<br>3,604.0 usi   |
| Position Uncer<br>Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Vertical Section<br>Plan Sections<br>Measured<br>Depth<br>(usft)                     | +E/-W<br>tainty<br>(Wellbore<br>Mode<br>(Design #<br>10<br>10<br>10<br>10 | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0  | usft Eastli<br>usft Wellh<br>Sample D<br>6,<br>Phase:<br>5th From (TVD)<br>(üsft)<br>0.0                                   | ng:<br>iead Elevation<br>jate<br>/9/2014<br>PLAI<br>PLAI<br>+N/-S<br>(usft)).                   | 645,438.8(<br>530,705.9(<br>:<br>Declination<br>(°)<br>7.57<br>N Th<br>+N/:S +t<br>((usft)) (t<br>0.0 (<br>)Dogleg)<br>+E/-W Rate<br>(usft)) (*/100usft)                    | ) usft Lati<br>) usft Lon<br>Gro<br>Dip/A<br>(<br>c<br>e On Depth:<br>E/-W/<br>(sft))<br>).0<br>Builid<br>(Rate)<br>(;/100usft))    | tude:<br>igitude:<br>und Level:<br>ingle<br>igle<br>60.51<br>0<br>Direc<br>(*<br>233<br>Turn.<br>Rate<br>(*/100usft) | ((i) T)<br>.0<br>(lon'<br>);<br>.79<br>TEO'<br>(())   | 104° 14' 0.354 V<br>3,604.0 usf   |
| Position Uncer<br>Wellbore<br>Magnetics<br>Design<br>Audit Notes:<br>Version:<br>Vertical Section<br>Plan:Sections<br>Measured<br>Depthi<br>(usft)<br>0.0 | +E/-W<br>tainty<br>Wellbore<br>Mode<br>(Design #                          | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>1<br>5<br>1<br>1<br>0.0<br>5<br>2<br>2<br>1<br>0.0<br>0<br>0.0<br>0<br>0.0<br>0<br>0.0 | usft Eastli<br>usft Wellh<br>Sample D<br>6,<br>Phase:<br>Dth From (T/VD)<br>(usft)<br>0.0<br>//ertical<br>(Usft)<br>(usft) | ng:<br>nead Elevation<br>hate<br>/9/2014<br>/9/2014<br>PLAI<br>PLAI<br>+N/-S<br>(ustt)).<br>0.0 | 645,438.8(<br>530,705.9(<br>:<br>Declination<br>(°)<br>7.57<br>N Tiu<br>+N/S +f<br>((usft)) (t<br>0.0 (0<br>+€/-W) Rate<br>(usft); Rate<br>(usft); (*/100usft);<br>0.0 0.00 | 0 usft Lati<br>0 usft Lon<br>Gro<br>DipA<br>()<br>e On Depth:<br>:://W/<br>(sft))<br>0.0<br>Build<br>(Rate)<br>(;/100usft))<br>0.00 | tude:<br>igitude:<br>und Level:<br>ingle<br>)<br>60.51<br>0.<br>Direc<br>(*<br>233<br>                               | (nT)<br>.0<br>(lion)<br>)<br>79<br>TEO<br>(()<br>0.00 | 104° 14' 0.354 W<br>3,604.0 usf   |

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## DDC

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Well Planning Report

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| Database:<br>Compañy:         |                              | EDM 500011.S                              | ration                            |  | Local Co<br>TVD/Ref        | ordinate)Refer     |   | Véll AAO Feder<br>WELL @ 3615 0 |                             | 118)  |
|-------------------------------|------------------------------|---|-----------------------------------|--|----------------------------|--------------------|---|---------------------------------|-----------------------------|---|
| Project:<br>Site:             |                              | Eddy County I<br>Sec 1: T18S F            | at a start a mar have been a find |  | MD Refe                    | rence:<br>ference: |   | WELL @ 3615.0<br>Grid           | iusft (Capstar #            |   |
| Wéll:<br>Wellbore:<br>Design: |                              | AAO'Federal #<br>Wellbore #1<br>Design #5 | 27                                |  | Survey                     | alculation Meth    | iod:  | Ainimum Curval                  | ure;                        |   |
| Planned/Si                    | urvey                        |   |                                   | an a | all denies all             |                    |   | 2 13 fr                         |                             | and and a second se<br>Second second |
|                               | easured<br>Depth)<br>(usft)) | Inclination<br>(9)                        | Azimuth)                          | Vertical)<br>(Depth)<br>(usft))          | +Ň/ <u>\$</u> \$<br>(ùsft) | +Ē∕₊₩              | Section   | Doğleg<br>Rate<br>//100usft) (% | Build<br>Rate<br>(100usft)) | 'Turn)<br>Rate<br>≬/100usft)  |
|                               | 0.0<br>100.0                 | 0.00<br>0.00                              | 0.00<br>0.00                      | 0.0<br>100.0                             | 0:0<br>0.0                 | 0.0<br>0.0         | 0.0<br>0.0  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 200.0                        | 0.00                                      | 0.00                              | 200.0                                    | 0.0                        | 0.0                | 0.0   | 0.00                            | 0.00                        | 0.00  |
|                               | 300.0<br>400.0               | 0.00<br>0.00                              | 0.00<br>0.00                      | 300.0<br>400.0                           | 0.0<br>0.0                 | 0.0<br>0.0         | 0.0<br>0.0  | 0.00<br>0.00                    | 0.00<br>0,00                | 0.00<br>0.00  |
|                               | uild 1°/100<br>500.0         | 0.00                                      | 0.00                              | 500.0                                    | (余 <i>令) (金融</i> )<br>0.0  | 0.0                | 0.0   | 0.00                            | 0.00                        | 0.00  |
|                               | 600.0                        | 1.00                                      | 233.79                            | 600.0                                    | -0.5                       | -0.7               | 0.9   | 1.00                            | 1.00                        | 0.00  |
|                               | 700.0<br>800.0               | 2.00<br>3.00                              | 233.7 <b>9</b><br>233.79          | 700.0<br>799.9                           | -2.1<br>-4.6               | -2.8<br>-6.3       | 3.5<br>7.9  | 1.00<br>1.00                    | 1.00<br>1.00                | 0.00<br>0.00  |
|                               | 900.0                        | 4.00                                      | 233.79                            | 899.7                                    | -4.0                       | -0.3               | 14.0  | 1.00                            | 1.00                        | 0.00  |
|                               | 1,000.0                      | 5.00                                      | 233.79                            | 999.4                                    | -12.9                      | -17.6              | 21.8  | 1.00                            | 1.00                        | 0.00  |
|                               | 1,100.0<br>1,200.0           | 6.00<br>7.00                              | 233.79<br>233.79                  | 1,098.9<br>1,198.3                       | -18.5<br>-25.2             | -25.3<br>-34.5     | 31.4<br>42.7  | 1.00<br>1.00                    | 1.00<br>1.00                | 0.00<br>0.00  |
| Ē                             |                              | 7.35°/inc.7                               | 233.15<br>Sec. 15                 | 1,150.0                                  | 20.2                       | -54.5              | 44.1<br>146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 - 146 | 1.00 K                          |                             |   |
|                               | 1,235.1                      | 7.35                                      | 233.79                            | 1,233.1                                  | -27.8                      | -38.0              | 47.1  | 1.00                            | 1.00                        | 0.00  |
|                               | 1,300.0                      | 7.35                                      | 233.79                            | 1,297.5                                  | -32.7                      | -44.7              | 55.4  | 0.00                            | 0.00                        | 0.00  |
|                               | 1,400.0<br>1,500.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 1,396.6<br>1,495.8                       | -40.3<br>-47.8             | -55.0<br>-65.3     | 68.2<br>81.0  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00  |
|                               | 1,600.0                      | 7.35                                      | 233.79                            | 1,595.0                                  | -55.4                      | -75.7              | 93.8  | 0.00                            | 0.00                        | 0.00  |
|                               | 1,700.0<br>1,800.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 1,694.2<br>1,793.3                       | -63.0<br>-70.5             | -86.0<br>-96.3     | 106.6<br>119.4  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 1,900.0                      | 7.35                                      | 233.79                            | 1,892.5                                  | -78.1                      | -106.6             | 132.2   | 0.00                            | 0.00                        | 0.00  |
|                               | 2,000.0                      | 7.35                                      | 233.79                            | 1,892.5                                  | -85.6                      | -117.0             | 132.2   | 0.00                            | 0.00                        | 0.00  |
|                               | 2,100.0                      | 7.35                                      | 233.79                            | 2,090.9                                  | -93.2                      | -127.3             | 157.8   | 0.00                            | 0.00                        | 0.00  |
|                               | 2,200.0<br>2,300.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 2,190.1<br>2,289.2                       | -100.7<br>-108.3           | -137.6<br>-147.9   | 170 <i>.</i> 6<br>183.3   | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               |                              |   |                                   |  |                            |                    |   |                                 |                             |   |
|                               | 2,400.0<br>2,500.0           | 7.35                                      | 233.79<br>233.79                  | 2,388.4<br>2,487.6                       | -115.9<br>-123.4           | -158.3<br>-168.6   | 196.1<br>208.9  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 2,600.0                      | 7.35                                      | 233.79                            | 2,586.8                                  | -131.0                     | -178.9             | 221.7   | 0.00                            | 0.00                        | 0.00  |
|                               | 2,700.0                      | 7.35<br>7.35                              | 233.79<br>233.79                  | 2,685.9                                  | -138.5                     | -189.2             | 234.5   | 0.00                            | 0.00                        | 0.00  |
|                               | 2,800.0                      |   |                                   | 2,785.1                                  | -146.1                     | -199.6             | 247.3   |                                 | 0.00                        | 0.00  |
|                               | 2,900.0<br>3,000.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 2,884.3<br>2,983.5                       | -153.7<br>-161.2           | -209.9<br>-220.2   | 260.1<br>272.9  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 3,100.0                      | 7.35                                      | 233.7 <b>9</b>                    | 3,082.7                                  | -168.8                     | -230.5             | 285.7   | 0.00                            | 0.00                        | 0.00  |
|                               | 3,200.0                      | 7.35                                      | 233.79                            | 3,181.8                                  | -176.3                     | -240.9             | 298.5   | 0.00                            | 0.00                        | 0.00  |
|                               | 3,300.0                      | 7,35                                      | 233.79                            | 3,281.0                                  | -183.9                     | -251.2             | 311.3   | 0.00                            | 0.00                        | 0.00  |
| G                             | lorieta<br>3,394.8           | 7.35                                      | 233.79                            | 3,375.0                                  | -191.0                     | -261.0             | 323.4   | 0.00                            | 0.00                        | 0.00  |
|                               | 3,400.0                      | 7.35                                      | 233.79                            | 3,380.2                                  | -191.4                     | -261.5             | 324.1   | 0.00                            | 0.00                        | 0.00  |
| 1                             | 3,500.0                      | 7.35                                      | 233.79                            | 3,479.4                                  | -199.0                     | -271.8             | 336.9   | 0.00                            | 0.00                        | 0.00  |
|                               | 3,600.0<br>3,700.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 3,578.5<br>3,677.7                       | -206.6<br>-214.1           | -282.2<br>-292.5   | 349.7<br>362.5  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 3,800.0                      | 7.35                                      | 233.79                            | 3,776.9                                  | -221.7                     | -302.8             | 375.3   | 0.00                            | 0.00                        | 0.00  |
|                               | 3,900.0                      | 7.35                                      | 233. <b>79</b>                    | 3,876.1                                  | -229.2                     | -313.1             | 388.1   | 0.00                            | 0.00                        | 0.00  |
|                               | 4,000.0                      | 7.35                                      | 233.79                            | 3,975.3                                  | -236.8                     | -323.5             | 400.9   | 0.00                            | 0.00                        | 0.00  |
|                               | 4,100.0<br>4,200.0           | 7.35<br>7.35                              | 233.79<br>233.79                  | 4,074.4<br>4,173.6                       | -244.3<br>-251.9           | -333.8<br>-344.1   | 413.7<br>426.5  | 0.00<br>0.00                    | 0.00<br>0.00                | 0.00<br>0.00  |
|                               | 4,300.0                      | 7.35                                      | 233.79                            | 4,272.8                                  | -259.5                     | -354.4             | 439.3   | 0.00                            | 0.00                        | 0.00  |
|                               | 4,400.0                      | 7.35                                      | 233.79                            | 4,372.0                                  | -267.0                     | -364.8             | 452.1   | 0.00                            | 0.00                        | 0.00  |
| 1                             | 4,500.0                      | 7.35                                      | 233.79                            | 4,471.1                                  | -274.6                     | -375.1             | 464.8   | 0.00                            | 0.00                        | 0.00  |
| 5                             | 4,600.0                      | 7.35<br>0' MD / 4600'-TVI                 | 233.79                            | 4,570.3                                  | -282.1                     | -385.4             | 477.6   | 0.00                            | 0.00                        | 0.00  |
| <u> </u>                      | 4,629.9                      | 7.35                                      | 2. 233.79                         | 4,600.0                                  | -284.4                     | -388.5             | 481.5   | 0.00                            | 0.00                        | 0.00  |

6/10/2014 12:11:07PM

COMPASS 5000.1 Build 72

## CONDITIONS OF APPROVAL

| OPERATOR'S NAME:      | Apache Corporation                  |
|-----------------------|-------------------------------------|
| LEASE NO.:            | NMNM-0557371                        |
| WELL NAME & NO.:      | AAO Federal 27                      |
| SURFACE HOLE FOOTAGE: | 1960' FSL & 2063' FWL               |
| BOTTOM HOLE FOOTAGE   | 1670' FSL & 1670' FWL               |
| LOCATION:             | Section 01, T. 18 S., R 27 E., NMPM |
| COUNTY:               | Eddy County, New Mexico             |
| API:                  | 30-015-42359                        |

## The original COAs still stand with the following drilling modifications:

## I. DRILLING

## A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)

## **Eddy County**

Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822

- A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the Yates formation. As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.
- Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.
- 3. The record of the drilling rate along with the GR/N well log run from TD to surface shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies.

## B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) time prior to drilling out for a primary cement job will be a minimum 18 hours for a water basin, 24 hours in the potash area, or 500 pounds compressive strength, whichever is greater for all casing strings. DURING THIS WOC TIME, NO DRILL PIPE, ETC. SHALL BE RUN IN THE HOLE. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. IF OPERATOR DOES NOT HAVE THE WELL SPECIFIC CEMENT DETAILS ONSITE PRIOR TO PUMPING THE CEMENT FOR EACH CASING STRING, THE WOC WILL BE 30 HOURS. See individual casing strings for details regarding lead cement slurry requirements.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Possible water flows in the Artesia Group and Queen. Possible lost circulation in the Artesia Group, Grayburg, and San Andres.

<u>A MINIMUM OF TWO CASING STRINGS CEMENTED TO SURFACE IS</u> <u>REQUIRED IN HIGH CAVE/KARST AREAS.</u> THE CEMENT MUST BE IN A SOLID SHEATH. THEREFORE, ONE INCH OPERATIONS ARE NOT SUFFICIENT TO PROTECT CAVE KARST RESOURCES. A CASING DESIGN THAT HAS A ONE INCH JOB PERFORMED DOES NOT COUNT AS A SOLID SHEATH.

WHERE THE SURACE CASING HAD A SUCCESSFUL CEMENT JOB; IF LOST CIRCULATION (TOTAL LOSS) OCCURS WHILE DRILLING THE 7-7/8" PRODUCTION HOLE, THE CEMENT PROGRAM FOR THE 5-1/2" PRODUCTION CASING WILL NEED TO BE MODIFIED AND <u>THE BLM IS TO BE CONTACTED PRIOR TO RUNNING THE CASING.</u> A DV TOOL WILL BE REQUIRED.

- 1. The **13-3/8** inch surface casing shall be set at approximately **350** feet and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - **b.** Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

## **Contingency intermediate casing:**

- 2. The **8-5/8** inch intermediate casing shall be set at approximately **400** feet and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.

- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:

Cement to surface. If cement does not circulate, contact the appropriate BLM office. Excess calculates to 21% - Additional cement may be required.

4. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

## C. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **2000** (**2M**) psi (**Installing 3M system, testing to 2,000 psi**).
- 3. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
  - b. The tests shall be done by an independent service company utilizing a test plug **not a cup or J-packer**.
  - c. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
  - d. The results of the test shall be reported to the appropriate BLM office.
  - e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.

f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

## D. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

## E. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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