UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

AUG 1 7 2018

FORM APPROVED OMB NO. 1004-0137

Expires: January 31, 2018

5. Lease Serial No. NMNM40659

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill or to DESTRICT HEARTESIA O.C.D.

abandoned well. Use form 3160-3 (APD) for such practice of the first of t

		-,	SEE MANAGE	rici	I VIIICE	
	TRIPLICATE - Other inst	tructions on	page 20CI) Arte	7 If Unit or CA/Agreen	nent, Name and/or No.
1. Type of Well Oil Well Gas Well Oth	ner				8. Well Name and No. IRIDIUM MDP1 28-	21 FEDERAL COM 11H
Name of Operator OXY USA INC	Contact: E-Mail: david_stew	DAVID STEV vart@oxy.com	VART	_	9. API Well No. 30-015-45073	
3a. Address P.O. BOX 50250 MIDLAND, TX 79710		3b. Phone No Ph: 432-68	o. (include area code) 35-5717		10. Field and Pool or Ex INGLE WELLS B	ploratory Area ONE SPRING
4. Location of Well (Footage, Sec., T	., R., M., or Survey Description,)			11. County or Parish, St	ate
Sec 28 T23S R31E SWSW 43 32.269362 N Lat, 103.789196					EDDY COUNTY,	NM
12. CHECK THE AI	PPROPRIATE BOX(ES)	TO INDICA	TE NATURE O	F NOTICE,	REPORT, OR OTHI	ER DATA
TYPE OF SUBMISSION			TYPE OF	ACTION		
Notice of Intent	☐ Acidize	☐ Dee	pen	☐ Product	ion (Start/Resume)	■ Water Shut-Off
Cubacquent Banad	☐ Alter Casing	☐ Hyd	Iraulic Fracturing	□ Reclam	ation	■ Well Integrity
☐ Subsequent Report	□ Casing Repair	☐ Nev	v Construction	☐ Recomp	olete	Other
☐ Final Abandonment Notice	☐ Change Plans	Plug	g and Abandon	□ Tempor	arily Abandon	Change to Original A PD
	☐ Convert to Injection	Plug	g Back	☐ Water I	Disposal	
13. Describe Proposed or Completed Ope If the proposal is to deepen directions Attach the Bond under which the wor following completion of the involved testing has been completed. Final Ab- determined that the site is ready for fi OXY USA Inc. respectfully requ 1. Amend the TMD, TVD, see	ally or recomplete horizontally, rick will be performed or provide operations. If the operation resondonment Notices must be file inal inspection. Juests to amend the APD attached.	give subsurface the Bond No. oults in a multipl ed only after all with the follor	locations and measure file with BLM/BIA le completion or recording the requirements, including the changes.	red and true ve . Required sul mpletion in a r ing reclamation	ertical depths of all pertine beguent reports must be fi new interval a Form 3160.	nt markers and zones. led within 30 days 4 must be filed once d the operator has
Amend the surface, interme contingency intermediate casi OXY requests the option to ruronly if severe hole conditions will only occur if OXY elects to for the three string primary cast.	ng string and annular cleant the 7.625" Intermediate dictate an additional casing run a second intermedia	arance reques Il as a contin	st, see attached. Igency casing street intermediate II of	SE ing Objective cement iob	E ATTACHED TIONS OF AP	FOR PROVAL
14. I hereby certify that the foregoing is	Electronic Submission #4	(Y USA INC,	sent to the Carlsba	ad	-	
Name (Printed/Typed) DAVID ST		•	•	SULATORY	v	
						- · · · · · · · · · · · · · · · · · · ·
Signature (Electronic S	ubmission)		Date 08/06/20)18		
	THIS SPACE FO	R FEDERA	L OR STATE (OFFICE U	SE	
Approved By Muster School Approved By Conditions of approval, if any, are attached certify that the applicant holds legal or equ			Petro Carlst		Engineer eld Office	Date 08-15-2018
which would entitle the applicant to condu	ct operations thereon.	Sauject icase	Office			
Title 18 U.S.C. Section 1001 and Title 43 States any false, fictitious or fraudulent s	U.S.C. Section 1212, make it a tatements or representations as	crime for any pe	rson knowingly and	willfully to ma	ke to any department or ag	gency of the United

Additional data for EC transaction #430030 that would not fit on the form

32. Additional remarks, continued

Annular Clearance Variance Request as per the agreement reached in the Oxy/BLM meeting on Feb 22, 2018, Oxy requests permission to allow deviation from the 0.422" annular clearance requirement from Onshore Order #2 under the following conditions:

a. Annular clearance to meet or exceed 0.422" between intermediate casing ID and production casing coupling only on the first 500' overlap between both casings.

b. Annular clearance less than 0.422" is acceptable for the curve and lateral portions of the production open hole section.

2. Amend the cementing program and add bradenhead squeeze stage, see attached.

OXY requests to pump a two stage cement job on either the intermediate II or production casing string with the first stage being pumped conventionally with the calculated TOC @ the Brushy Canyon and the second stage performed as a bradenhead squeeze with planned cement from the Brushy Canyon to surface.

3. Amend BOP program and add BOP Break Testing request, see attached.

BOP Break Testing Request As per the agreement reached in the Oxy/BLM meeting on Feb 22, 2018, Oxy requests permission to allow BOP Break Testing under the following conditions:

a. After a full BOP test is conducted on the first well on the pad.

- b. When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.
- c. Full BOP test will be required prior to drilling any production hole.
- 4. Amend the mud program, depth and type, see attached.
- 5. Amend the drilling conditions, see attached.

1. Geologic Formations

A. Cheminate I. of the graceours			
TVD of target	9970'	Pilot Hole Depth	N/A
MD at TD:	20441'	Deepest Expected fresh water:	432'

Delaware Basin

Formation	TVD - RKB	Expected Fluids
Rustler	432	
Salado	789	
Castile	2,724	
Lamar/Delaware	4,176	
Bell Canyon	4,211	Water (inj zone)
Cherry Canyon	5,097	
Brushy Canyon	6,396	
Bone Spring	8,000	Oil/Gas/Water
1st Bone Spring	8,762	Oil/Gas/Water
2nd Bone Spring	9,316	Oil/Gas/Water

^{*}H2S, water flows, loss of circulation, abnormal pressures, etc.

2. Casing Program Primary Plan:

Buoyant Buoyant

Hole	Casing	Casing Interval	Csg.	Weight		_	SF ·	SF	Body SF	Joint SF
Size (in)	From (ft)	To (ft)	Size (in)	(lbs)	Grade	Conn.	Collapse	Burst	Tension	Tension
17.5	0	483 590	13.375	54.5	J-55	BTC	1.125	1.2	1.4	1.4
12.25	0	4,227	9.625	43.5	L-80	BTC	1.125	1.2	1.4	1.4
8.5	0	20,441	5.5	20	P-110	DQX	1.125	1.2	1.4	1.4
							SF	Values w	ill meet or Ex	ceed

Contingency Plans

Buoyant Buoyant

Hole	Casing Interval		Csg.	Weight			SF	SF	Body SF	Joint SF
Size (in)	From (ft)	To (ft)	Size (in)	(lbs)	Grade	Conn.	Collapse	Burst	Tension	Tension
17.5	0	483 5A 3	13.375	54.5	J-55	BTC	1.125	1.2	1.4	1.4
12.25	0	4,227	9.625	43.5	L-80	BTC	1.125	1.2	1.4	1.4
0.5	0	4,000	7.625	26.4	HCL-80	SF	1.125	1.2	1.4	1.4
8.5	4,000	8,500	7.625	26.4	HCL-80	FJ	1.125	1.2	1.4	1.4
6.75	0	20,441	5.5	20	P-110	DQX	1.125	1.2	1.4	1.4
-							SF	Values w	ill meet or Ex	ceed

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

"Oxy requests the option to run the 7.625" Intermediate II as a contingency string to be run only if severe hole conditions dictate an additional casing string necessary.

*Oxy requests the option to set casing shallower yet still below the salts if losses or hole conditions require this. Cement volumes may be adjusted if casing is set shallower and a DV tool may be run in case hole conditions merit pumping a second stage cement job to comply with permitted top of cement. If cement circulated to surface during first stage we will drop a cancelation cone and not pump the second stage.

Annular Clearance Variance Request	
As per the agreement reached in the Oxy	/BLM meeting on Feb 22, 2018, Oxy requests
	.422" annular clearance requirement from Onshore
Order #2 under the following conditions	
	0.422" between intermediate casing ID and production
casing coupling only on the first 500	
	s acceptable for the curve and lateral portions of the
production open hole section.	

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	Y
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	Y
If yes, are the first three strings cemented to surface?	Y
Is 2 nd string set 100' to 600' below the base of salt?	Y
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

3. Cementing Program

Primary Plan:

Casing	Slurry	#Sks	Wt. (Lb/gal)	Yld ft3/sack	H20 gal/sk	500# Comp. Strength	Slurry Description
Surface	Tail	491	14.8	1.33	6.365	5:26	Accelerator
	Lead	1,028	12.9	1.88	10.13	7:32	Retarder, Extender, Dispersant
Intermediate	Tail	141	14.8	1.33	6.42	6:31	Retarder, Dispersant, Salt
1st Stage	Lead	234	13.2	1.65	6.686	3:49	Extender. Accelerator, Dispersant
Production	Tail	1,814	13.2	1.65	6.686	3:49	Extender. Accelerator, Dispersant
2nd Stage Production	Tail	359	12.9	1.88	9.356	9:49	Retarder, Dispersant, Fluid Loss Control, Extender

2nd Stage Production cement will be pumped from surface as a bradenhead squeeze

Casing String	Top of Lead (ft)	Bottom of Lead (ft)	Top of Tail (ft)	Bottom of Tail (ft)	% Excess Lead	% Excess Tail
Surface	N/A	N/A	0	483	N/A	100%
Intermediate	0	3727	3727	4227	75%	20%
1st Stage Production	6396	8000	8000	20441	5%	5%
2nd Stage Production	N/A	N/A	372T 0	6396	N/A	25%

Contingency Plan: 500# Wt. Yld H20 Slurry **Casing** Slurry #Sks Comp. (Lb/gal) ft3/sack gal/sk Description Strength N/A N/A N/A N/A N/A N/A Lead Surface Class C Cement, Tail 491 14.8 1.33 6.365 5:26 Accelerator Retarder. 10.13 7:32 Extender, Lead 1028 12.9 1.88 Dispersant Intermediate I Retarder, 6.42 6:31 141 14.8 1.33 Tail Dispersant, Salt Retarder, Lead 54 13.2 1.65 6.686 3:49 Dispersant, Salt Intermediate II Retarder, 1st Stage 3:49 Tail 29 13.2 1.65 6.69 Dispersant, Salt Intermediate II 2nd Stage (Tail Slurry) to be pumped as Bradenhead Squeeze from surface, down the Intermediate annulus Lead N/A N/A N/A N/A N/A N/A Intermediate II Extender. 2nd Stage 377 12.8 9.38 9:49 Accelerator, Tail 1.76 Dispersant Lead N/A N/A N/A N/A N/A N/A Retarder, Production Dispersant, Fluid 911 6.686 3:49 Tail 13.2 1.38 Loss Control, Extender

Casing String	Top of Lead (ft)	Bottom of Lead (ft)	Top of Tail (ft)	Bottom of Tail (ft)	% Excess Lead	% Excess Tail
Surface	N/A	N/A	0	483	N/A	100%
Int I	0	3727	3727	4227	75%	20%
Int II (1st Stage)	6896	8000	8000	8500	25%	5%
Int II (2nd Stage)	N/A	N/A	0	6896	N/A	5%
Production	N/A	N/A	8000	20441	N/A	20%

"Contingency design will only be employed if Oxy elects to run 7.625" Intermediate II string.

4. Pressure Control Equipment

BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Туре		~	Tested to:			
			Annular		✓	70% of working pressure			
12.25" Hala	13-5/8"	.5/8" 5M	Blind R	am	✓				
12.25" Hole	13-3/8	13-3/6	13-3/6 31/1		Pipe Ra	Pipe Ram		250/5000:	
		ŀ	Double F	Ram	✓	250/5000psi			
			Other*						

^{*}Specify if additional ram is utilized.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Formation integrity test will be performed per Onshore Order #2.

On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.

A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.

Y Are anchors required by manufacturer?

A multibowl or a unionized multibowl wellhead system will be employed. The wellhead and connection to the BOPE will meet all API 6A requirements. The BOP will be tested per Onshore Order #2 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. We will test the flange connection of the wellhead with a test port that is directly in the flange. We are proposing that we will run the wellhead through the rotary prior to cementing surface casing as discussed with the BLM on October 8, 2015. See attached schematics.

BOP Break Testing Request

As per the agreement reached in the Oxy/BLM meeting on Feb 22, 2018, Oxy requests permission to allow BOP Break Testing under the following conditions:

- After a full BOP test is conducted on the first well on the pad.
- When skidding to drill an intermediate section that does not penetrate into the Wolfcamp.
- Full BOP test will be required prior to drilling any production hole.

5. Mud Program

Dej	oth	T	Weight	Viscosity	Water Loss
From (ft)	To (ft)	Type	(ppg)	Viscosity	Water Loss
0	483	Water-Based Mud	8.6-8.8	40-60	N/C
483	4227	Saturated Brine- Based Mud	9.8-10.0	35-45	N/C
4227	20441	Water-Based or Oil- Based Mud	8.0-9.5	38-50	N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times. The following is a general list of products: Barite, Bentonite, Gypsum, Lime, Soda Ash, Caustic Soda, Nut Plug, Cedar Fiber, Cotton Seed Hulls, Drilling Paper, Salt Water Clay, CACL2. Oxy will use a closed mud system.

What will be used to monitor the loss or gain	PVT/MD Totco/Visual Monitoring
of fluid?	

6. Logging and Testing Procedures

Logg	ing, Coring and Testing.					
Yes	Will run GR from TD to surface (horizontal well – vertical portion of hole). Stated logs					
	run will be in the Completion Report and submitted to the BLM.					
No	Logs are planned based on well control or offset log information.					
No	Drill stem test? If yes, explain					
No	Coring? If yes, explain					

Addi	tional logs planned	Interval
No	Resistivity	
No	Density	
No	CBL	
Yes	Mud log	ICP - TD
No	PEX	

7. Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	6222 psi
Abnormal Temperature	No
BH Temperature at deepest TVD	160°F

Pump high viscosity sweeps as needed for hole cleaning. The mud system will be monitored visually/manually as well as with an electronic PVT. The necessary mud products for additional weight and fluid loss control will be on location at all times. Appropriately weighted mud will be used to isolate potential gas, oil, and water zones until such time as casing can be cemented into place for zonal isolation.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

N H2S is present

H2S Plan attached

8. Other facets of operation

	Yes/No
Will the well be drilled with a walking/skidding operation? If yes, describe.	Yes
We plan to drill the two well pad in batch by section: all surface sections,	1
intermediate sections and production sections. The wellhead will be	
secured with a night cap whenever the rig is not over the well.	
Will more than one drilling rig be used for drilling operations? If yes, describe.	Yes
Oxy requests the option to contract a Surface Rig to drill, set surface	
casing, and cement for this well. If the timing between rigs is such that	
Oxy would not be able to preset surface, the Primary Rig will MIRU and	
drill the well in its entirety per the APD. Please see the attached document	
for information on the spudder rig.	

Total estimated cuttings volume: 1517.9 bbls.

9. Company Personnel

Name	<u>Title</u>	Office Phone	Mobile Phone
Garrett Granier	Drilling Engineer	713-513-6633	832-265-0581
Randy Neel	Drilling Engineer Supervisor	713-215-7987	713-517-5544
Simon Benavides	Drilling Superintendent	713-522-8652	281-684-6897
John Willis	Drilling Manager	713-366-5556	713-259-1417

Schlumberger

Oxy Iridium MDP1 28-21 Federal Com 11H Rev3 APS 24Jul18 Proposal **Geodetic Report**



(Def Plan)

Client: Field:

July 24, 2018 - 01:33 PM

Structure / Slot:

Well:

UWI / API#: Survey Name:

Survey Date: Tort / AHD / DDI / ERD Ratio: Coordinate Reference System: Location Lat / Long:

Location Grid N/E Y/X: CRS Grid Convergence Angle:

Grid Scale Factor: Version / Patch:

NM Eddy County (NAD 83)

Oxy Iridium MDP1 28-21 Federal Com 11H / Iridium MDP1 28-21 Federal Com 11H Iridium MDP1 28-21 Federal Com 11H

Unknown / Unknown

Oxy Indium MDP1 28-21 Federal Com 11H Rev3 APS 24Jul18

July 17, 2018 114.539 * / 11312.810 ft / 8,424 / 1.135

NAD83 New Mexico State Plane, Eastern Zone, US Feet N 32" 16' 9.70272", W 103" 47' 21.10569" N 482153.250 RUS, E 709519.680 RUS

0.99994149 2.10.740.0

Survey / DLS Computation: Vertical Section Azimuth: Vertical Section Origin:

TVD Reference Datum:

TVD Reference Elevation: Seabed / Ground Elevation: Magnetic Declination: **Total Gravity Field Strength:**

Gravity Model: Total Magnetic Field Strength: Magnetic Dip Angle: Magnetic Declination Model:

North Reference:
Grid Convergence Used:
Total Corr Mag North->Grid North: Local Coord Referenced To: Minimum Curvature / Lubinski 358.125 * (Grid North) 0.000 ft, 0.000 ft

RKR=30'

3400,300 ft above MSL 3370.300 ft above MSL

6.909 °

999.4510mgn (9.80665 Based) GARM

48031.552 nT 60.018 * July 17, 2018 HDGM 2018 Grid North 0.2905

6.6184 * Well Head

Comments	MD	incl	Azim Grid	TVD	VSEC	NS	EW	DLS	Northing	Easting	Latitude	Longitude
Comments	(ft)	O	(*)	(ft)	(ft)	(ft)	(ft)	(°/100ft)	(ftUS)	(ftUS)	(N/S " ' ")	(E/W * ' ")
SHL	0.00	0.00	0.00	0.00	0,00	0.00	0.00	N/A	462153.25	709519.68		
Rustler	432.00	0.00	190.90	432.00	0.00	0.00	0.00	0.00	462153.25	709519.68		
Salado	789.00	0.00	190.90	789.00	0.00	0.00	0.00	0.00	462153.25		V 3216 9.70 W	
Castile	2724.00	0.00	190.90	2724.00	0.00	0.00	0.00	0.00	462153.25	709519.68		
Lamar	4176.00	0.00	190.90	4176.00	0.00	0.00	0.00	0.00	462153.25	709519.68	V 32 16 9.70 V	/ 103 47 21.11
Bell Canyon	4211.00	0.00	190.90	4211.00	0.00	0.00	0.00	0.00	482153.25	709519.68	V 32 16 9.70 V	/ 103 47 21.11
Cherry Canyon	5097.00	0.00	190,90	5097.00	0.00	0.00	0.00	0.00	482153.25	709519.68		/ 103 47 21,11
Build 2"/100"	5640.00	0.00	190.90	5640.00	0.00	0.00	0.00	0.00	462153.25	709519.68	N 32 16 9.70 V	V 103 47 21.11
Hold Tangent	6239.88	12.00	190,90	6235.51	-61.03	-81.45	-11,84	2.00	462091.80	709507.84	N 32 16 9.10 V	V 103 47 21.25
Brushy Canyon	6403.96	12.00 '	190.90	6396.00	-94.29	-94.94	-18.29	0.00	482058.32	709501.39	V 32 16 8.76 V	V 103 47 21.32
Bone Spring	8043.78	12.00	190.90	8000.00	-426.72	-429.66	-82.76	0.00	461723.62	709436.92	V 32 16 5.48 V	/ 103 47 22.09
Turn 2°/100°	8443.79	12.00	190.90	8391.27	-507.81	-511.31	-98.49	0.00	481841.97	709421.20	N 32 16 4.65 V	V 103 47 22.28
First Bone	8819.00	5.65	219.12	8762.00	-559.86	-564.00	-117.54	2.00	461589.28	700402 15	V 32 16 4.13 V	/ 103 47 22 51
Spring	0019.00	3.03	218.12	0702.00	-338.00	1304.00	-111.54	2.00	401308,20	100402.13	1 32 10 4.13 V	103 47 22.37
Second Bone	9375.68	8.53	320.78	9318.00	-547.67	-553.23	-181.07	2.00	461600.05	709358.62	V 32 18 4.24 V	V 103 47 23 01
Spring	3 373.00	0.55	020.70	3070.00	-547.57	-555.25	-707.07	1.00	407000.00	100000.02	V 02 10 4.24 V	7 705 47 25.07
Build/Tum	9567.02	12.00	330.00	9504.26	-518.83	-525.00	-180.00	2.00	461628.28	709339.69	N 32 18 4.52 V	V 103 47 23 23
10*/100	6307.02	12.00	330.00	5504.20	-510.00	-020.00	- 100.00	2.00	401020.20	700550.00	14 32 10 4.32 1	1 105 41 25.25
Build/Tum	9903.53	45.00	346.75	9796.25	-368.95	-374,55	-226.09	10.00	461778.72	709293.60	N 32 16 601 V	V 103 47 23.76
10*/100												
Landing Point	10367.79	90.00	359.64	9970.00	49.02	40.30	-267.47	10.00	462193.54	709252.23	N 32 18 10.11 V	V 103 47 24.22
Iridium MDP1 28-												
21 Federal Com	20440.66	90.00	359.64	9970.00	10118.39	10112.97	-331.04	0.00	472265.61	709188.66	N 32 17 49.79 V	V 103 47 24.38

Survey Type:

11H PBHL

Survey Error Model:

ISCWSA Rev 0 *** 3-D 95.000% Confidence 2.7955 sigma

Description	Part	MD From (ft)	MD To (ft)	EOU Freq (ft)	Hole Size Casi (in)	ing Diameter (in)	Expected Max Inclination (deg)	Survey Tool Type	Borehole / Survey
	1	0.000	30.000	1/100.000	30.000	30.000		NAL_NSG+MSHOT-Depth Only	Original Borehole / Oxy Iridium MDP1 28-21 Federal Com 11H
	1 .	30.000	500.000	1/100.000	30.000	30.000		NAL_NSG+MSHOT	Original Borehole / Oxy Iridium MDP1 28-21 Federal Com 11H
	1	500.000	20440.661	1/100.000	30,000	30.000		NAL_MWD_PLUS_0.5_DEG	Original Borehole / Oxy Iridium MDP1 28-21 Federal Com 11H

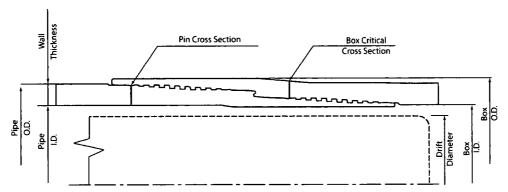
Schlumberger

OXY



Borehole: Well: Field: Structure: iridium MDP1 28-21 Federal Com 11H NM Eddy County (NAD 83) Oxy Indium MDP1 28-21 Federal Com 11H Original Borehole Miscellaneous bidium MDP1 28-Slot: 21 Federal Com NAD83 New Mexico State Plane, Eastern Zone, US Feet N 32 16 8.70 462153,25RUS 0.2805 HDGM 2018 Dip: 60,018* 11H Oxy Iridium MDP1 28-21 Federal Com 11H Rev3 APS 24Juj18 48031 552nT W 103 47 21.11 709819.68NUS Ozy tridigm MDP1 23-21 Federal Com 171H STe1 Rev1 APS 45Jul 1 **Critical Points** INCL AZIM TVD DLS Critical Point MD VSEC N(+)/S(-) E(+)/W(-) Oxy Iridium MDP1 28-21 Federal Com 11H Rev3 APS 24Jul18 10500 SHL 0,00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 432.00 0.00 0.00 Leas Iridium MDP1 28-21 Federal Com 11/9 PBH Rustler 432,00 190.90 0.00 0.00 10000 789.00 0.00 190.90 789.00 0.00 0.00 0.00 0.00 Iridium MDP1 28-21 Federal Com 11H PB Castile 2724.00 0.00 190.90 2724.00 0.00 0.00 0.00 0.00 20441 MD 9970 TVD 90.00 ' incl 359.64 ' az 4176.00 0.00 190,90 4176,00 0,00 0.00 0,00 0.00 Lamai N=10113 E=-331 Bell Canyon 4211,00 0.00 190.90 4211 00 0.00 0.00 0.00 0.00 0.00 5097.00 0.00 5097.00 190,90 0.00 0.00 0.00 Cherry Canyon 9000 Build 2°/100' 5640.00 0.00 190.90 5640.00 0,00 0.00 0.00 0.00 6235.51 -61.03 -81.45 2.00 Hold Tangent 6239.88 12.00 190.90 -11.84 6500 Brushy Canyon 6403.96 12,00 190,90 6396,00 -94,29 -18,29 Bone Spring 8043.78 12.00 190.90 8000.00 426.72 429.66 -82.76 0.00 ם Turn 2º/100 8443.79 12.00 190.90 8391.27 -507.81 -511.31 -98.49 0.00 8000 Line First Bone Spring 8819 00 5 65 219 12 8762 00 -559 86 -564 00 -117 54 2 00 9375.88 8.53 320.78 9316.00 -547,67 -553.23 -161.07 2.00 Second Bone Spring 7500 Build/Turn 10°/100' 9567 02 12 00 330 00 9504.26 -518.83 -525 00 -180.00 2.00 Build/Turn 10*/100* 9903.53 45.00 346.75 9796.25 -366.95 -374.55 -226.09 10,00 00 7000 10387.79 90.00 359.64 9970.00 49.02 40,30 -267.47 10,00 Landing Point Iridium MDP1 28-21 Federal 9970.00 10118.39 10112.97 -331.04 20440.66 90.00 359.64 0.00 NOT CROSS Com 11H PBHL 6500 O MID O TVID 0.00 i Grid 6000 Rustler (432 TVD) Mag <u>ease</u> 5500_Z (<u>2</u> Salado (789 TVD) Grid North 1500 ine -Tot Corr (M->G 6.618°) Lease Line - DO NOT CROS ĕ 4500g Mag Dec (6.909°) 2000 Grid Conv (0.291°) 8 2500 4000 NO Castile (2724 TVD) **H** 3000 3500 CROSS 3500 3000 4000 Lamar (4176 TVD) Beli Canyon (4211 TVD) 1.1900,000(ft) 2500 Build 2*/100* Line - DO NOT 4500 5640 MD 5640 TVD 0.00 * incl 190,90 * az Sort of . 0 vsec 2000 Cherry Canyon (5097 TVD) Hold Tangent 6240 MD 6236 TVD 12,00 ° incl 190,90 ° -61 vsec € 5500 1500 Hard Landing Point 10368 MD 9970 TVD 0.00 * incl 359.64 * az N=40 E=-267 6000 0 MD 0 TVC 1000 0.00 incl 0 00 * az N=0 E=0 Brushy Canyon (6396 TVD) 6500 Turn 2"/100" 8444 MD 8391 TVD Build 2 1100 500 5640 ftD 5540 TVD 0.00 1 nci 190,90 1 sz N=0 E=0 12.00 ° incl 190.90 ° sz -508 vsec 7000 9904 MD 9796 TVD 45,00 ° incl 348,75 ° az N=-375 E=-226 Hold Tangen 0 6240 ND 6256 TVD Build/Turn 10°/100' 9567 MD 9504 TVD 12.00 * incl 330.00 * az 7500 12.00 incl 190.90 * az N=-51E=-12 Build/Turn 10*/100* 9567 MD 9504 TVD 12.00 * incl 330.00 * az N=-525 E=-180 519 vsec Turn 2*/100 -500 8444 MD 8291 TVD 12,00 ' incl 190,90 ° 8000 Bone Spring (8000 TVD) Build/Turn 10*/100* N=-511 E=-98 8500 45,00 ° incl 346.75 ° az -2000 -1500 -1000 -500 og Sher MDP1 33-4 Federal Com: 51 til Rev4 APS 23.4418 Ony Senting Sher MDP1 23-4 F EW (ft) Scale = 1:1600.00(ft) -367 vsec -3500 -3000 500 First Bone Spring (8762 TVD) al Com 1rl Revel APS 23Jan18 9000 tridium MDP1 28-21 Federal Com 11H PBHL 20441 MD 9970 TVD 10368 MD 9970 TVD 90.00 * incl 359.64 * az Second Bane Spring (9316 TV) 90.00 * incl 359.64 * az 10116 vsec 10000 Iridium MDP1 28-21 Federal Com 11H PBHL A Oxy Iridium MDP1 28-21 Federal Com 11H Rev3 APS 24Jul13 10500 -20001500 -1000 1500 2000 2500 3000 3500 4000 4500 5000 5500 6000 6500 7000 7500 8000 8500 8000 9500 10000 10500 11000 11500 -500 1000 Vertical Section (ft) Azim = 358.13* Scale = 1:1900.00(ft) Origin = 0N/-S, 0E/-W

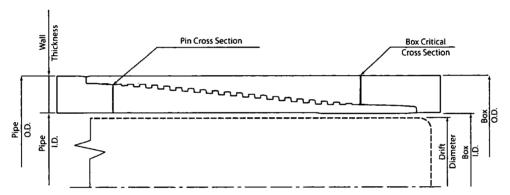
TUBULAR PARAMETERS		PIPE BODY PROPERTIES	
Nominal OD, (inch)	7.625	PE Weight, (lbs/ft)	25.56
Wall Thickness, (inch)	0.328	Nominal Weight, (lbs/ft)	26.40
Pipe Grade	L80 HC	Nominal ID, (inch)	6.969
Drift	Standard	Drift Diameter, (inch)	6.844
CONNECTION PARAMETERS		Nominal Pipe Body Area, (sq inch)	7.519 601
Connection OD (inch)	7.79	Min. Internal Yield Pressure, (psi)	6 020
Connection ID, (inch)	6.938	Collapse Pressure, (psi)	3 910
Make-Up Loss, (inch)	6.029	,	
Connection Critical Area, (sq inch)	5.948	to take w	•
Yield Strength in Tension, (klbs)	533		
Yeld Strength in Compression, (klbs)	533		
Tension Efficiency	89%	100-MPI 3C1 / Ed	
Compression Efficiency	89%		-
Min. Internal Yield Pressure, (psi)	6 020	The second secon	#:
Collapse Pressure, (psi)	3 910	Compression	luncon]
Uniaxial Bending (deg/100ft)	42.7		
MAKE-UP TORQUES			
Yield Torque, (ft-lb)	22 600	W.	
Minimum Make-Up Torque, (ft-lb)	15 000		
Optimum Make-Up Torque, (ft-lb)	16 500		= :-
Maximum Make-Up Torque, (ft-lb)	18 200		



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TUBULAR PARAMETERS		PIPE BODY PROPERTIES	
Nominal OD, (inch)	7.625	PE Weight, (lbs/ft)	25.56
Wall Thickness, (inch)	0.328	Nominal Weight, (lbs/ft)	26.40
Pipe Grade	L80 HC	Nominal ID, (inch)	6.969
Drift	Standard	Drift Diameter, (inch)	6.844
CONNECTION PARAMETERS		Nominal Pipe Body Area, (sq inch)	7.519
Connection OD (inch)	7.63	Yield Strength in Tension, (klbs)	601
Connection ID, (inch)	6.975	Min. Internal Yield Pressure, (psi)	6 020 3 910
Make-Up Loss, (inch)	4.165	Collapse Pressure, (psi)	3 910
Connection Critical Area, (sq inch)	2.520	to us	
Yield Strength in Tension, (klbs)	347		[
Yeld Strength in Compression, (klbs)	347		() () () () () () () () () ()
Tension Efficiency	58%	100 (MPISC), ISCH	7
Compression Efficiency	58%		- 計 - : = =
Min. Internal Yield Pressure, (psi)	6 020	the state of the s	
Collapse Pressure, (psi)	3 910	('soppessedt	Tens' n
Uniaxial Bending (deg/100ft)	28.0		/
MAKE-UP TORQUES			
Yield Torque, (ft-lb)	22 200		Vr
Minimum Make-Up Torque, (ft-lb)	12 500	and the state of t	
Optimum Make-Up Torque, (ft-lb)	13 900	t to the second	= ::- ^
Maximum Make-Up Torque, (ft-lb)	15 300		



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PERFORMANCE DATA

TWK UP DQX Technical Data Sheet

Nom Pipe Body Area

5.500 in 20.00 lbs/ft

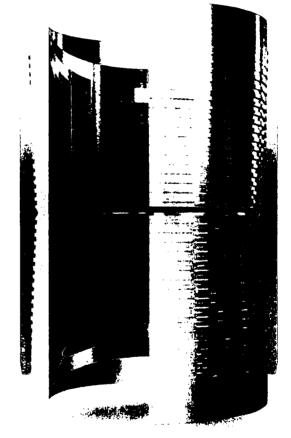
P-490

Tubular Parameters					
Size	5.500	in	Minimum Yield	110,000	psi
Nominal Weight	20 00	lbs/ft	Minimum Tensile	125,000	psi
Grade	P-110	}	Yield Load	641.000	lbs
PE Weight	19.81	lbs/ft	Tensite Load	729,000	lbs
Wall Thickness	0.361	in	Min. Internal Yield Pressure	12,600	psı
Nominal ID	4.778	in	Collapse Pressure	11.100	psi
Drift Diameter	4.653	ın			•

Connection Parameters		
Connection OD	6.050	in
Connection ID	4 77 8	in
Make-Up Loss	4.122	in
Critical Section Area	5.828	in²
Tension Efficiency	100.0	3/0
Compression Efficiency	100.0	%
Yield Load In Tension	641 000	lbs
Min Internal Yield Pressure	12.600	psı
Collapse Pressure	11.100	psi

Make-Up Torques		
Min Make-Up Torque	11.600	ft-lbs
Opt_Make-Up Torque	12 900	ft-lbs
Max Make-Up Torque	14.100	ft-lbs
Yield Torque	a0.600	ft-lbs

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PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME: OXY USA Inc

LEASE NO.: NMNM40659

WELL NAME & NO.: | Iridium MDP1 28-21 Fed Com 11H

SURFACE HOLE FOOTAGE: 430'/S & 648'/W

BOTTOM HOLE FOOTAGE | 180'/N & 380'/W, sec. 7

LOCATION: | Sec. 28, T. 23 S, R. 31 E

COUNTY: | Lea County

Potash	None	C Secretary	€ R-111-P
Cave/Karst Potential	€ Low		← High
Variance	None	Flex Hose	Other
Wellhead	Conventional	Multibowl ■ Multi	
Other	☐4 String Area	☐Capitan Reef	□WIPP

All previous COAs still apply except for the following:

A. CASING

Primary Design:

- 1. The 13 3/8 inch surface casing shall be set at approximately 590 feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - d. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 2. The minimum required fill of cement behind the 9 5/8 inch intermediate casing is:

- Cement to surface. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to potash.
- 3. The minimum required fill of cement behind the 5 1/2 inch production casing is:
 - Cement to surface. Operator shall provide method of verification.

Operator has proposed to pump down 9 5/8" X 5 1/2" annulus. Operator must run a CBL from the TD of the 5 1/2" casing to 9 5/8" casing shoe.

Casing Design Confingency

- 4. The 13 3/8 inch surface casing shall be set at approximately 590 feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface.
 - e. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - f. Wait on cement (WOC) time for a primary cement job will be a minimum of **24 hours in the Potash Area** or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)
 - g. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
 - h. If cement falls back, remedial cementing will be done prior to drilling out that string.
- 5. The minimum required fill of cement behind the 9 5/8 inch first intermediate casing is:
 - Cement to surface. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to potash.

Second intermediate casing must be kept fluid filled to meet BLM minimum collapse requirement.

- 6. The minimum required fill of cement behind the 7 5/8 inch second intermediate casing is:
 - Cement to surface. If cement does not circulate, contact the appropriate BLM office.

Operator has proposed to pump down 9 5/8" X 7 5/8" annulus. Operator must run a CBL from the TD of the 7 5/8 casing to 9 5/8" casing shoe.

- 7. The minimum required fill of cement behind the 5 1/2 inch production casing is:
 - Cement as proposed. Operator shall provide method of verification. Excess calculates to 19% additional cement might be required.

MHH 08152018

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - \(\text{Chaves and Roosevelt Counties} \)
 \(\text{Call the Roswell Field Office, 2909 West Second St., Roswell NM 88201.} \)
 \(\text{During office hours call (575) 627-0272.} \)
 \(\text{After office hours call (575)} \)
 - Eddy County
 Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822
 - ✓ Lea CountyCall the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575)393-3612

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- 2. Wait on cement (WOC) for Potash Areas: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log.
- 3. Wait on cement (WOC) for Water Basin: After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements.

- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.
- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.