OIL CONSERVATION DIVISION

MULTIPOINT ... ONE POINT BACK PRESSURE TEST FOR GAS WELL

SF
File:
122file

RECEIVED
JAN 14 1977
O. C. C.
ARTESIA, OFFICE

Type Test: [x] Initial [ ] Annual [ ] Special — Test Date: 1-10-77

Company: Monsanto Company	Connection: None	Unit	
Pool: ~~Undesignated~~ Cemetary Morrow	Formation: Morrow		

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
1-10-77	9556	9467	3503 Gr.	Albert Federal Com.

Csg. Size	Wt.	d	Set At	Perforations	Well No.
5.50"	20.00#	4.778"	9566	From 9282 To 9315	1

Tbg. Size	Wt.	d	Set At	Perforations	Unit	Sec.	Twp.	Rge.
2.875EUE	6.50#	2.441"	9177	From To	0	32	19S	25E

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
Single Completion	9177	Eddy

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
Tubing	156 @ 9299	60	13.2	New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
9299	9299	0.595	0.00	0.00	0.00		X	

NO.	FLOW DATA: Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						2999	22			282
1.	3.00	1.75	500	6.00"	70	2669	58			1.00 Hr.
2.	3.00	1.75	500	13.00"	64	2245	63			1.00 Hr.
3.	3.00	1.75	500	18.00"	66	2030	66			1.00 Hr.
4.	3.00	1.75	500	20.00"	69	1990	59			1.00 Hr.
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	15.61	55.491	513.2	.9905	1.296	1.040	1156
2.	15.61	81.68	513.2	.9962	1.296	1.043	1717
3.	15.61	96.112	513.2	.9943	1.296	1.041	2012
4.	15.61	101.311	513.2	.9915	1.296	1.044	2122
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	.76	530	1.50	.924
2.	.76	524	1.48	.920
3.	.76	526	1.49	.922
4.	.76	519	1.47	.918
5.				

Gas Liquid Hydrocarbon Ratio: None Produced Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Seperator Gas: .595 | XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX | .595
Critical Pressure: 672 P.S.I.A. | 672 P.S.I.A.
Critical Temperature: 354 R | 354 R

P_c ____ P_c^2 ____

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2697.9	7279	1794
2		2264.6	5128	3945
3		2052.9	4214	4859
4		2038.3	4155	4918
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.84486$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.61298$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 3424$

POSTED
ID-2 BOOK
1-21-77

Absolute Open Flow: 3424 Mcfd @ 15.025 | Angle of Slope θ: 52° 1' | Slope, n: .781

Remarks:

Approved By Commission:	Conducted By:	Calculated By: H.L. Hagler	Checked By:
	West Texas Con. Serv.	West Texas Con. Serv.	E.M. Scholl