Folder

Form C-122
Revised 9-1-65

EW MEXICO OIL CONSERVATION CO SSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 10-1-80	
Company: ~~JACK~~ MC CLELLAN Oil Corp	Connection: TO AIR			
Pool: ~~UNDESIGNATED~~ Kemnitz Ranch Abo	Formation: ABO		Unit: NONE	
Completion Date: 9-28-80	Total Depth: 7,921	Plug Back TD: ~~4,620~~ 4800	Elevation: 3,971 GROUND 3,982 K.B.	Farm or Lease Name: TRES AMIGO
Csg. Size: 4.5 / Wt.: 10.5 / d: 4.052 / Set At: 4,620		Perforations: From ~~4,502~~ 4500 To ~~4,603~~ 4544		Well No.: 1
Tbg. Size: 2.375 / Wt.: 4.7 / d: 1.995 / Set At: 4,450		Perforations: From OPEN To ENDED		Unit: L / Sec.: 9 / Twp.: 19S / Rge.: 23E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: 4,450		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 100@ 4,452	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
4,450	4,450	.7699	.1545	.0587	-0-	2"		

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					1231		PACKER		SI 168 HRS
1.	2" X 1/8	85		98	1013	60			1 HR.
2.	2" X 1/8	240		110	925	60			1 HR.
3.	2" X 1/8	360		110	825	60			1 HR.
4.	2" X 1/8	380		108	720	60			1 HR.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.2648		98.2	.9653	1.140	1.008	28.8
2.	.2648		253.2	.9551	1.140	1.019	74.4
3.	.2648		373.2	.9551	1.140	1.027	110.5
4.	.2648		393.2	.9568	1.140	1.029	116.9
5.							

NO.	P_t	Temp. °R	T_r	Z
1	.140	558	1.48	.985
2.	.362	570	1.51	.964
3.	.533	570	1.51	.948
4.	.562	568	1.51	.945
5.				

Gas Liquid Hydrocarbon Ratio: DRY Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: 0 Deg.
Specific Gravity Separator Gas: 7699 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 700 P.S.I.A. 700 P.S.I.A.
Critical Temperature: 377 R 377 R

P_c 1465 P_c^2 2,146

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1297	1682	464
2		1231	1515	631
3		1165	1357	789
4		1124	1263	883
5	SIP	1465		

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.4304$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.4304$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 284.4$

Absolute Open Flow: 284.4 Mcfd @ 15.025 Angle of Slope θ: 55° Slope, n: 1.000

Remarks:

Approved By Commission:	Conducted By:	Calculated By: DON BENNETT	Checked By: