

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

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C-122*

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Type Test <input type="checkbox"/> Initial <input type="checkbox"/> Annual <input checked="" type="checkbox"/> Special			Test Date 10-11-73		OCT 23 1973		
Company Monsanto Company			Connection Transwestern Pipeline Company			O. C. C.	
Pool Burton Flat (Morrow)			Formation Morrow			Unit ARTESIA, OFFICE V	
Completion Date 3-25-73		Total Depth 11,546		Plug Back TD 11,472		Elevation 3223 DF	
Farm or Lease Name Burton Flat Unit			Well No. 3- 11				
Csg. Size 7"	Wt. 26#	d 6.276	Set At 11,546	Perforations: From 11,244 To 11,438		Unit Sec. Twp. Rge. V 3 21-S 27-E	
Tbg. Size 2 7/8 EUE	Wt. 6.5	d 2.441	Set At 10,810	Perforations: From To			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual				Packer Set At 10,800		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 164 @ 11,546		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State New Mexico							
L 11,341	H 11341	Gg .582	% CO ₂ .81	% N ₂ .47	% H ₂ S 0	Prover 0	Meter Run X
FLOW DATA			TUBING DATA			CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Duration of Flow
SI						3559	63
1.	4"	2"	860	17	78	2774	67
2.	4"	2"	865	28	74	2338	70
3.	4"	2"	870	42	77	1876	73
4.	4"	2"	870	59	75	1409	75
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mc/d
1	19.81	121.83	873.2	.9831	1.0153	1.062	2559
2	19.81	156.81	878.2	.9868	1.0153	1.064	3312
3	19.81	192.60	883.2	.9840	1.0153	1.065	4060
4	19.81	226.98	883.2	.9859	1.0153	1.065	4821
5							
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ 991 _____ Mcf/bbl.		
					A.P.I. Gravity of Liquid Hydrocarbons _____ 57.2 _____ Deg.		
1.	1.30	538	1.54	.886	Specific Gravity Separator Gas _____ .582 _____		X X X X X X X X
2.	1.29	534	1.53	.884	Specific Gravity Flowing Fluid _____ X X X X X _____		
3.	1.31	537	1.53	.882	Critical Pressure _____ 672 _____ P.S.I.A.		672 P.S.I.A.
4.	1.31	535	1.53	.882	Critical Temperature _____ 350 _____ R		354 R
5.							
P _c 3572.2		P _c ² 12761					
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_i^2 - P_w^2} = \frac{12761}{10474}$		
1		2800.7	7844	4917	(2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1.199846$		
2		2375.6	5643	7118			
3		1931.8	3732	9029			
4		1512.2	2287	10474	AOF = Q $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 5784$		
5							
Absolute Open Flow _____ 5784 _____ Mc/d @ 15.025				Angle of Slope @ _____ 47.3 _____		Slope, n _____ .922 _____	
Remarks:							
Approved By Commission:		Conducted By: W. T. Hagler		Calculated By: H. L. Hagler		Checked By:	