Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

30-015-33222

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

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Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: MEWBOURNE OIL		Lease or Unit Name: DINERO 20 FED	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date:	Well No.: 1
Completion Date	Total Depth: 12650	Plug Back TD: 12567	Elevation: 3065 GL
Unit Ltr - Sec - TWP - Rge: P 20 22S 28E			
Csg. Size: 5 1/2 / Wt.: 20# / d: 4.778 / Set At: 12650	Perforations: From: 12410 To: 12420	County: EDDY	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At: 11911	Perforations: From: 11997 To: 12196	Pool: DUBLIN RANCH	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At: 11897	Formation: MORROW	
Producing Thru: TUBING	Reservoir Temp.: 181	Mean Annual Temp.: 60	Baro. Press.-P_a: 13.2
Connection: SALES			

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
10506	10506	0.61	0.806	0.27	N/A	N/A	3.067	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					1996		PKR		24 HRS
1	3.067 X 1.375	552	91.16	86	700		"		24 HRS
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							1966
2							
3	TOTAL	FLOW	METER				
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2	TOTAL	FLOW	METER	
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	DRY GAS		Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	DRY		Deg.
Specific Gravity Separator Gas	0.574		XXXXXXX
Specific Gravity Flowing Fluid	XXXXX		N/A
Critical Pressure	675 P.S.I.A.	N/A	P.S.I.A.
Critical Temperature	342 R.	N/A	R

P_c 2009.2 P_c^2 4036.9

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		751.7	508.7	3471.8
2				
3				
4				
5				

(1) $\dfrac{P_c^2}{P_c^2 - P_w^2} =$ 1.163 (2) $\left[\dfrac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.163

AOF = Q $\left[\dfrac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 2.286

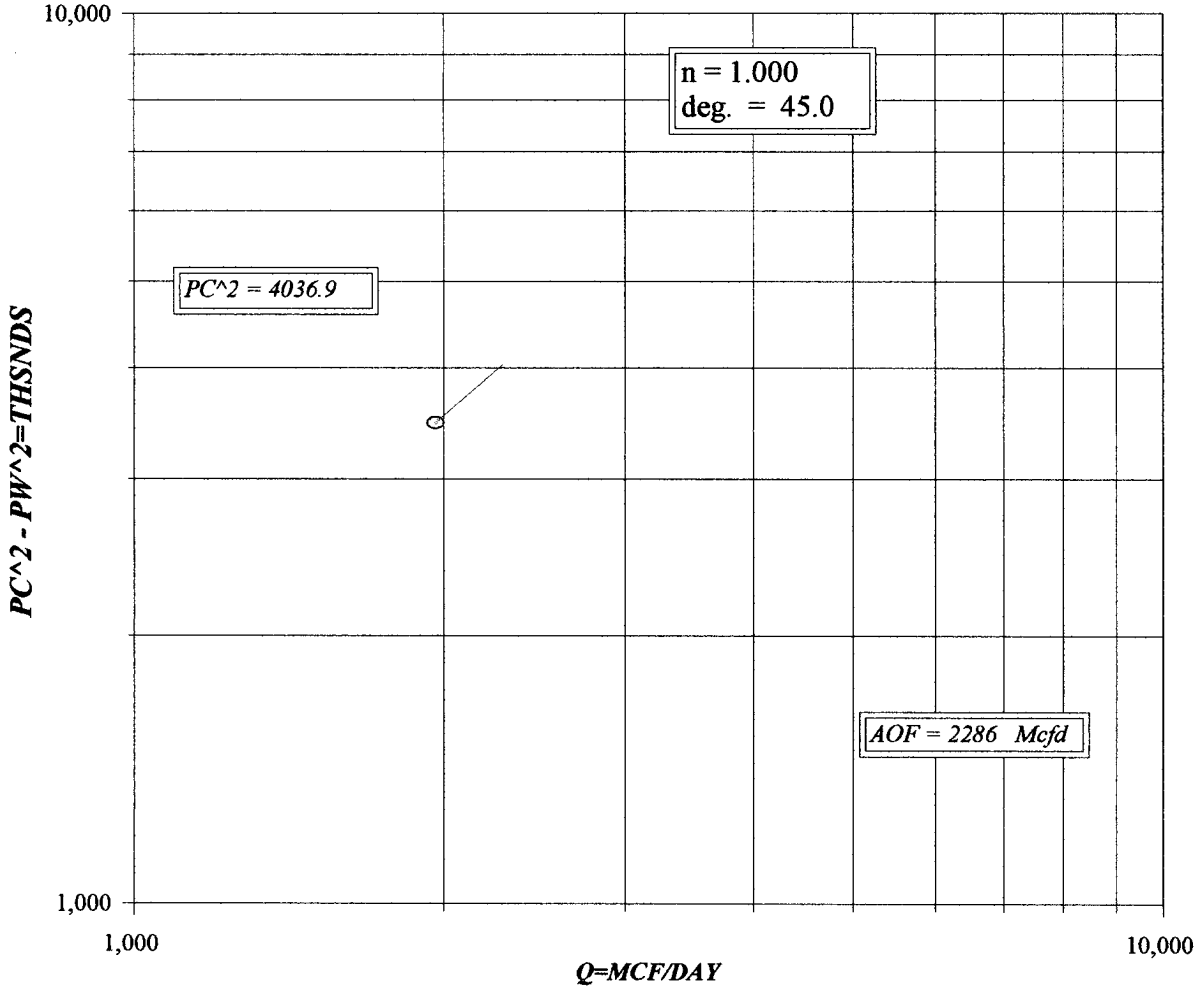
Absolute Open Flow 2.286 Mcfd @ 15.025 | Angle of Slope Q: 45 | Slope, n: 1.000

Remarks: NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	MEWBOURNE OIL	MERV BUECKER	BM

MEWBOURNE OIL

DINERO 20 FED #1



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL		LEASE :	DINERO 20 FED	WELL NO. :	1			Pc =	2009.2	Pc2 =	4036.9
UNIT :	P		SECTION :	,20	TOWNSHIF :	,22S						
L :	11911	H :	11911	L/H :	1	G/GMIX :	0.574		Pt2 =	508.7	Pw =	751.7
%CO2 :	1.239	%N2 :	,180	H2S :		DATE :				0.0		#DIV/0!
d :	2.441	Fr :	0.010763	GH :	8197.0	RANGE :	,28E			0.0		#DIV/0!
										0.0		#DIV/0!
VOL 1 :	1966	PSIA 1 :	713.2			RESV.TEMP	193.0		Pc2-Pw2=	3471.8	Pw2 =	565.1
VOL 2 :		PSIA 2 :								#DIV/0!		#DIV/0!
VOL 3 :		PSIA 3 :				SHUT-IN PRE =	2009.2			#DIV/0!		#DIV/0!
VOL 4 :		PSIA 4 :								#DIV/0!		#DIV/0!
			PCR :	675						n =	1.000	
			TCR :	342								
									Pc2/(Pc2-Pw2) =		1.163	
											#DIV/0!	
											#DIV/0!	

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		`1ST	`2ND	`1ST	``2ND	`1ST	`2ND	`1ST	`2ND
1	QM	1.966	1.966	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	653.0	653.0	653.0	653.0	653.0	653.0	653.0	653.0
4	T	593.5	593.5	593.5	593.5	593.5	593.5	593.5	593.5
	PR (est)	1.06		0.00		0.00		0.00	
5	Z(est)	0.917	0.907	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	544.1	538.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	15.065	15.232	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.759	1.770	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.432	0.435	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	713.2	713.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	508.7	508.7	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.856	5.792	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	11.51	11.39	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	132.6	129.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	57.21437	56.42496	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	565.9	565.1	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	995.5	1000.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	997.8	1000.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	855.5	856.7	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	1.27	1.27	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.74	1.74	1.74	1.74	1.74	1.74	1.74	1.74
23	Z	0.907	0.907	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

[Pc2/Pc2-Pw2]n = 1.163

AOF= Q 2.286

FORM C122-D

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30-015-33512

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Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator	Lease or Unit Name
MEWBOURNE OIL	DINERO 20 FED

Type Test	Test Date	Well No.
☑ Initial ☐ Annual ☐ Special	12/7/2004	2

Completion Date	Total Depth	Plug Back TD	Elevation	Unit Ltr - Sec - TWP - Rge
9/11/2004	12530	12404	3066 GL	H 20 22S 28E

Csg. Size	Wt.	d	Set At	Perforations:			County
5 1/2	17	4.892	12530	From: 12302	To:	12370	EDDY

Tbg. Size	Wt.	d	Set At	Perforations:		Pool
2 7/8	6.5	2.441	11538	From:	To:	DUBLIN RANCH

Type Well-Single-Bradenhead-G.G. or G.O. Multiple	Packer Set At	Formation
SINGLE	11528	MORROW

Producing Thru	Reservoir Temp.	Mean Annual Temp.	Baro. Press.-P_a	Connection
TUBING	181	60	13.2	SALES

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
11538	11538	0.602	1.375	5.185	N/A	N/A	3.067	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					3900		PKR		24 HRS
1	3.067 X 1.000	529	3.06	73	700		"		24 HRS
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1							254
2							
3	TOTAL	FLOW	METER				
4							
5							

No.	P_r	Temp. R	T_r	Z
1				
2	TOTAL	FLOW	METER	
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	DRY GAS		Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	DRY		Deg.
Specific Gravity Separator Gas	0.602		XXXXXXX
Specific Gravity Flowing Fluid	XXXXX		N/A
Critical Pressure	666	P.S.I.A.	N/A P.S.I.A.
Critical Temperature	343	R.	N/A R

P_c 3913.2 P_c^2 15313.1

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		530	280.9	15032.2
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 1.019 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.019

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 0.259

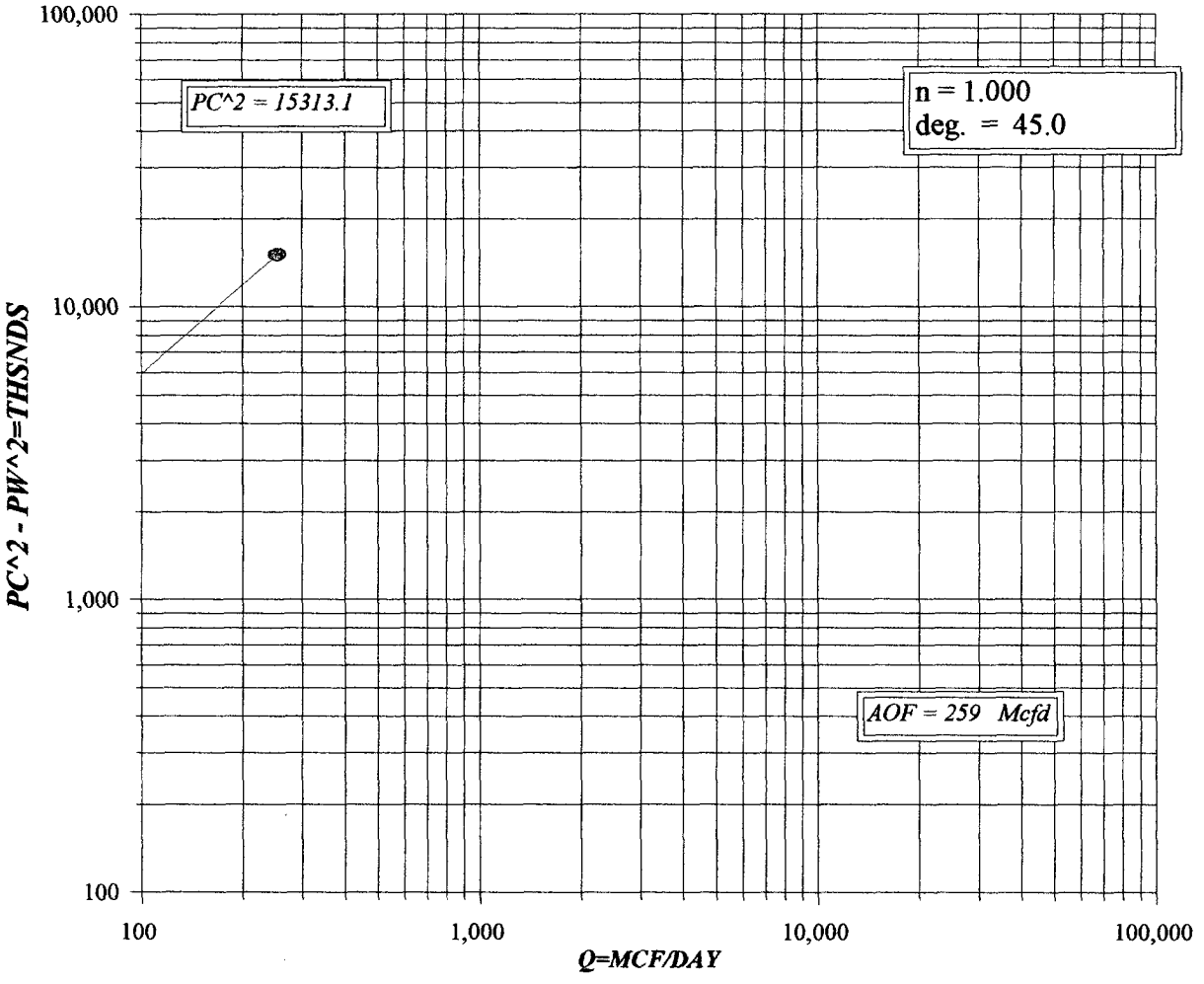
Absolute Open Flow	Mcfd @ 15.025	Angle of Slope Θ:	Slope, n:
259		45	,1.000

Remarks: NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	MEWBOURNE OIL	MERV BUECKER	BM

MEWBOURNE OIL

DINERO 20 FED # 2



COMPANY :	MEWBOURNE OIL			LEASE :	DINERO 20 FED		WELL NO. :	2				Pc =	3913.2	Pc2 =	15313.1				
UNIT :	H			SECTION :	20		TOWNSHIP :	22S											
L :	11538	H :	11538	L/H :	1	G/GMIX :	0.602					Pt2 =	280.1	Pw =	530.0				
%CO2 :	1.315	%N2 :	5.185	H2S :			DATE :	12/7/04					0.0		#DIV/0!				
d :	2.441	Fr :	0.010763	GH :	6945.9		RANGE :	28E					0.0		#DIV/0!				
													0.0		#DIV/0!				
VOL 1 :	254	PSIA 1 :	529.2			RESV.TEMP	189.4					Pc2-Pw2=			15032.2	Pw2 =	280.9		
VOL 2 :		PSIA 2 :											#DIV/0!			#DIV/0!			
VOL 3 :		PSIA 3 :				SHUT-IN PRI =	3913.2						#DIV/0!			#DIV/0!			
VOL 4 :		PSIA 4 :											#DIV/0!			#DIV/0!			
				PCR :	666									n =	1.000				
				TCR :	343														
												Pc2/(Pc2-Pw2) =			1.019				
															#DIV/0!				
															#DIV/0!				
LINE	RATE 1		RATE 2		RATE 3		RATE 4												
	1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND											
1 QM	0.254	0.254	0.000	0.000	0.000	0.000	0.000	0.000											
2 TW	534	534	534	534	534	534	534	534				[Pc2/Pc2-Pw2]n =			1.019				
3 Ts	649.4	649.4	649.4	649.4	649.4	649.4	649.4	649.4							#DIV/0!				
4 T	591.7	591.7	591.7	591.7	591.7	591.7	591.7	591.7							#DIV/0!				
PR (est)	0.79		0.00		0.00		0.00								#DIV/0!				
5 Z(est)	0.929	0.923	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
6 TZ	549.8	546.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					AOF= Q		0.259				
7 GH/TZ	12.633	12.712	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!							#DIV/0!				
8 eS	1.606	1.611	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!							#DIV/0!				
9 l-e-S	0.377	0.379	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!							#DIV/0!				
10 Pt	529.2	529.2	0.0	0.0	0.0	0.0	0.0	0.0											
11 Pt2 /1000	280.1	280.1	0.0	0.0	0.0	0.0	0.0	0.0											
12 Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.0107631											
13 Fc=FrTZ	5.918	5.881	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
14 FcQm	1.50	1.49	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
15 L/H(FcQm)^2	2.3	2.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
16 Fw	0.852487	0.846102	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
17 Pw2	280.9	280.9	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
18 Ps2	451.1	452.5	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
19 Ps	671.7	672.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
20 P	600.4	600.9	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
21 Pr	0.90	0.90	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!											
22 Tr	1.73	1.73	1.73	1.73	1.73	1.73	1.73	1.73											
23 Z	0.923	0.923	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!							FORM C122-D				