m 3160-5 DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT						OMB N	APPROVED O. 1004-0137 anuary 31, 2018
	SUNDRY Do not use the	ŀ	6. If Indian, Allottee of	or Tribe Name			
·		II. Use form 3160-3 (APD) f 	·····			7. If Unit or CA/Agre	ement, Name and/or No.
1. Type of Well						8. Well Name and No.	
	🛾 Gas Well 📋 Otl	her				SND 12 01 FED (
2. Name of Operator CHEVRON US	SA INCORPOR	ATED E-Mail; LBECERRA@				 API Well No. 30-015-45177-0 	00-X1
3a. Address 6301 DEAUVI MIDLAND, TX		Den	Phone No. (includ h: 432-687-766	le area code) 5		10. Field and Pool or PURPLE SAGE	Exploratory Area E-WOLFCAMP (GAS)
		., R., M., or Survey Description	Artesia	² IIIC	3	11. County or Parish,	State
	R31E SESE 367 Lat, 103.724297	7FSL 404FEL				EDDY COUNT	Y, NM
12. C	CHECK THE AI	PPROPRIATE BOX(ES) TO	INDICATE NA	TURE O	F NOTICE, 1	REPORT, OR OTI	HER DATA
TYPE OF SUI	BMISSION			TYPE OF	FACTION		
Notice of Inte	tent	🗋 Acidize	Deepen	<u> </u>	Producti	on (Start/Resume)	□ Water Shut-Off
		Alter Casing	🗖 Hydraulic l	Fracturing	🗖 Reclama	tion	Well Integrity
Subsequent F	Report	Casing Repair	New Const	ruction	🗖 Recompl	ete	Other Drilling Operations
Final Abando	onment Notice	Change Plans	Plug and A	bandon		rily Abandon	Drining Operations
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(Instructions on page 2) ** BLM REVISED **

1. FORMATION TOPS

The estimated tops of important geologic markers are as follows:

 766	
2,990	
4,575	
4,626	
5,480	
6,760	
8,443	
9,380	
10,032	
11,330	
 11,769	
11,984	21,973
12,545	
	4,626 5,480 6,760 8,443 9,380 10,032 11,330 11,769 11,984

2. ESTIMATED DEPTH OF WATER, OIL, GAS & OTHER MINERAL BEARING FORMATIONS

The estimated depths at which the top and bottom of the anticipated water, oil, gas, or other mineral bearing formations are expected to be encountered are as follows:

Substance	Formation	Depth
Deepest Ex	xpected Base of Fresh Water	400
Water	Castile	2,990
Water	Cherry Canyon	5,480
Oil/Gas	Brushy Canyon	6,760
Oil/Gas	Avalon	8,443
Oil/Gas	First Bone Spring	9,380
Oil/Gas	Second Bone Spring	10,032
Oil/Gas	Third Bone Spring	11,330
Oil/Gas	Wolfcamp A	11,769
Oil/Gas	Wolfcamp B	12,545

All shows of fresh water and minerals will be reported and protected.

3. BOP EQUIPMENT

Chevron will have a minimum of a 5,000 psi rig stack (see proposed schematic) for drill out below surface casing. The Wolfcamp is not exposed until drill out of the intermediate casing, and the stack will be tested as specified in the attached testing requirements.Batch drilling of the surface, intermediate, and production will take place. A full BOP test will be performed unless approval from BLM is received otherwise. Flex choke hose will be used for all wells on the pad (see attached specs). BOP test will be conducted by a third party.

Chevron requests a variance to use a FMC Technologies UH-S Multibowl wellhead, which will be run through the rig floor on surface casing. BOPE will be nippled up and tested after cementing surface casing. Subsequent tests will be performed as needed, not to exceed 30 days. The field report from FMC Technologies and BOP test information will be provided in a subsequent report at the end of the well. Please see the attached wellhead schematic. An installation manual has been placed on file with the BLM office and remains unchanged from previous submittal.

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ONSHORE ORDER NO. 1 Chevron SND 12 01 FED 004 3H Eddy County, NM

4. CASING PROGRAM

a. The proposed casing program will be as follows:

Purpose	From	То	Hole Size	Csg Size	Weight	Grade	Thread	Condition
Surface	0'	800'	17-1/2"	13-3/8"	54.5 #	J-55	STC	New
Intermediate	0'	11.250	12-1/4"	9-5/8"	43.5#	L-801C	LTC	New
Production	0'	21,973'	8-1/2"	5-1/2"	20.0 #	P-110 ICY	TXP BTC	New

An alternative casing design with a contingency string is as follows:

Purpose	From	То	Hole Size	Csg Size	Weight	Grade	Thread	Condition
Surface	0'	800'	17-1/2"	13-3/8"	54.5 #	J-55	STC	New
Intermediate Csg	0'	11,260	12-1/4"	9-5/8"	43.5#	L-80IC	LTC	New
Intermediate Liner	10,950	11,900'	8-1/2"	7-5/8"	29.7 #	P-110	Wedge 513	New
Production	0'	11,750'	6-3/4"	5-1/2"	20.0 #	P-110 ICY	TXP BTC	New
Production	11,750	21,973'	0-3/4	5"	18.0 #	P-110 IC	Wedge 521	New

b. Casing design subject to revision based on geologic conditions encountered.

c. ***A "Worst Case" casing design for wells in a particular area is used below to calculate the Casing Safety Factors. If for any reason the casing design for a particular well requires setting casing deeper than the following "worst case" design, then the Casing Safety Factors will be recalculated & sent to the BLM prior to drilling.

SF Calculations based on the following "Worst Case" casing design:

Surface Casing:	800' TVD
Intermediate Casing:	112601 TVD
Intermediate Liner Casing:	11900' TVD
Production Casing:	22,003' MD/11,882' TVD (10,071' VS @ 90 deg inc)

Casing String	Min SF Burst	Min SF Collapse	Min SF Tension	Min SF Tri-Axial
Surface	1.40	2.74	3.55	1.74
Intermediate	1,25	1.92	1.60	1,53
Production	1.11	1.22	2.11	1.31

For alternate casing design with contingency:

Casing String	Min SF Burst	Min SF Collapse	Min SF Tension	Min SF Tri-Axial
Surface	1.40	2.74	3.55	1.7 <u>4</u>
Intermediate Csg	1.26	1,92	1,60	1.53
Intermediate Liner	1.83	2,28	2.49	2.25
Production	1.11	1.64	1.68	1.35

The following worst case load cases were considered for calculation of the above Min. Safety Factors:

Burst Design		Surf	Int	Liner	Prod
Pressure Test- Surfac	e, Int, Prod Csg	Х	X	X	X
P external:	Mud weight above TOC, PP below				
P internal:	Test psi + next section heaviest mud in csg				_
Displace to Gas- Surf	Csg	Х			-
P external:	Mud weight above TOC, PP below				
P internal:	Dry Gas from Next Csg Point				
Gas over mud (60/40)	- Int Csg/Liner		X	X	
P external:	Mud weight above TOC, PP below		1		
P internal:	60% gas over 40% mud from Pilot hole TD PP				
Stimulation (Frac) Pre	ssures- Prod Csg				X
P external:	Mud weight above TOC, PP below		1		
P internal:	Max inj pressure w/ heaviest injected fluid				
Tubing leak- Prod Cs	g (packer at KOP)				X
P external:	Mud weight above TOC, PP below				
P internal:	Leak just below surf, 8.45 ppg packer fluid			_	
Collapse Design		Surf	Int	Liner	Prod
Full Evacuation		Х	X	X	X
P external:	Mud weight gradient				
P internal:	none				
Cementing- Surf, Int,	Prod Csg	X	X	X	X
P external:	Wet cement				
P internal:	displacement fluid - water				
Tension Design		Surf	Int	Liner	Prod
100k lb overpull		Х	X	X	X

d. Chevron will fill casing at a minimum of every 20 jts (840') while running for intermediate and production casing in order to maintain collapse SF.

Slurry	Туре	Тор	Bottom	Weight	Yield	%Excess	Sacks	Water	Volume
Surface				(ppg)	(cu ft/sk)	Open Hole		gal/sk	bbls
Tail	Class C	0'	800'	14.8	1.34	50	686	6.40	184
Intermediate Csg - Star	qe <u>1</u>								
Lead	Class C	4,600'	10,250'	11.9	2.56	35	932	14.66	425
Tail	Class C	10,250	11,250'	14.8	1.33	35	346	6.38	82
Intermediate Csg - Star	ge 2 (DV tool @ 4,60	<u>))</u>							
Lead	Class C	0'	4,100'	11.9	2.56	35	662	14.66	302
Tail	Class C	4,100'	4,600'	14.8	1.33	35	159	6.38	38
Production									
Lead	Class C	10,750'	20,973'	14.5	1.38	35	2269	6.85	55 8
Tail	Class H	20,973'	21,973'	15	2.18	35	147	9.56	57

Cementing Program for alternate casing design with contingency string:

*No change to surface and intermediate cement design with implementation of contingency liner.

Slurry	Туре	Тор	Bottom	Weight	Yield	%Excess	Sacks	Water	Volume
				(ppg)	(cu ft/sk)	Open Hole		gal/sk	bbls
Intermediate Liner									
Tail	Class C	10,950'	11,900'	14.5	1.4	35	70	6.77	17
Production									
Lead	Class C	10,750	20,973'	14.5	1.4	35	1323	6.77	330
Tail	Class H	20,973	21,973'	15	2.19	35	73	9.54	29

1. Final cement volumes will be determined by caliper.

2. Surface casing shall have at least one centralizer installed on each of the bottom three joints starting with the shoe joint.

3. Production casing will have one horizontal type centralizer on every joint for the first 1000' from TD, then every other joint to EOB, and then every third joint to KOP. Bowspring type centralizers will be run from KOP to intermediate

4. Intermediate casing cement job will be a 2 stage job with DV tool set at the base of Lamar.

5. Chevron requests a variance to qualify the additional 300' of cement above the liner top as the required cement tieback interval with >0.422" clearance for the production csg cmt job in the four string design.

4.966 psi

6. MUD PROGRAM

From	То	Туре	Weight	Viscosity	Filtrate
0'	800'	Spud Mud	8.3 - 8.9	28-30	N/C
800'	11,250'	OBM	8.7 - 9.6	10-20	10-12
11.250	21,973	OBM	8.8 - 11.9	10-15	15-25

A closed system will be used consisting of above ground steel tanks. All wastes accumulated during drilling operations will be contained in a portable trash cage and removed from location and deposited in an approved sanitary landfill. Sanitary wastes will be contained in a chemical porta-toilet and then hauled to an approved sanitary landfill.

All fluids and cuttings will be disposed of in accordance with New Mexico Oil Conservation Division rules and regulations.

A mud test shall be performed every 24 hours after mudding up to determine, as applicable: density, viscosity, gel strength, filtration, and pH.

Visual mud monitoring equipment shall be in place to detect volume changes indicating loss or gain of circulating fluid volume. When abnormal pressures are anticipated -- a pit volume totalizer (PVT), stroke

A weighting agent and lost circulating material (LCM) will be onsite to mitigate pressure or lost circulation as

7. TESTING, LOGGING, AND CORING

The anticipated type and amount of testing, logging, and coring are as follows:

a. Drill stem tests are not planned.

	b. The logging program will be as follows:		
Mudlogs	2 man mudlog	Int Csg to TD	Drillout of Int Csg
LWD	MWD Gamma	Int. and Prod. Hole	While Drilling

c. Conventional whole core samples are not planned.

d. A directional survey will be run.

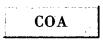
8. ABNORMAL PRESSURES AND HYDROGEN SULFIDE

a. No abnormal pressure or temperatures are expected. Estimated BHP is:

b. Hydrogen sulfide gas is not anticipated. An H2S Contingency plan is attached with this APD in the event that H2S is encountered

PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

OPERATOR'S NAME:	CHEVRON USA INC.
LEASE NO.:	NMNM120901
WELL NAME & NO.:	SND 12 01 FED 004 – 3H
SURFACE HOLE FOOTAGE:	367'/S & 404'/E
BOTTOM HOLE FOOTAGE	100'/N & 1254'/E
LOCATION:	SECTION 12, T24S, R31E, NMPM
COUNTY:	EDDY, NEW MEXICO



H2S	r Yes	r No	
Potash		• Secretary	C R-111-P
Cave/Karst Potential	C Low		
Variance	None	Flex Hose	• Other
Wellhead	Conventional	Multibowl	C Both
Other	☐ 4 String Area	Capitan Reef	F WIPP

A. Hydrogen Sulfide

Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.

B. CASING

Option 1

- 1. The 13-3/8 inch surface casing shall be set at approximately 836 feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface.
 - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
 - b. Wait on cement (WOC) time for a primary cement job will be a minimum of <u>24 hours in the Potash Area</u> or 500 pounds compressive strength, whichever is greater. (This is to include the lead cement)

- c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
- d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Operator shall filled 50% of casing with fluid while running intermediate casing to maintain collapse safety factor.

2. The minimum required fill of cement behind the 9-5/8 inch intermediate casing is: Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to cave/karst or potash.

Operator has proposed a DV tool, the depth may be adjusted as long as the cement is changed proportionally. The DV tool may be cancelled if cement circulates to surface on the first stage.

- a. First stage to DV tool: Cement to circulate. If cement does not circulate off the DV tool, contact the appropriate BLM office before proceeding with second stage cement job.
- b. Second stage above DV tool:Cement to surface. If cement does not circulate, contact the appropriate BLM office.
- 3. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 500 feet into previous casing string. Operator shall provide method of verification.

OPTION 2

Operator shall contact BLM 4hrs before proceeding with Option 2(contingency plan) in Drilling Plan.

Operator shall filled 1/3rd of casing with fluid while running intermediate casing to maintain collapse safety factor.

4. The minimum required fill of cement behind the 7-5/8 inch production liner is:

• Cement should tie-back 100' into the previous casing. Operator shall provide method of verification.

Variance was approved for an annular spacing between the 7.625" x 5.5" casing.

- 5. The minimum required fill of cement behind the 5-1/2 inch production casing is:
 - Cement should tie-back at least 500 feet into previous casing string. Operator shall provide method of verification.

C. PRESSURE CONTROL

- 1. Variance approved to use flex line from BOP to choke manifold. Manufacturer's specification to be readily available. No external damage to flex line. Flex line to be installed as straight as possible (no hard bends).
- 2. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be **5000 (5M)** psi.

GENERAL REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

- a. Spudding well (minimum of 24 hours)
- b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
- c. BOPE tests (minimum of 4 hours)
 - Chaves and Roosevelt Counties Call the Roswell Field Office, 2909 West Second St., Roswell NM 88201. During office hours call (575) 627-0272. After office hours call (575)
 - Eddy County

Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822

- Lea County Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240, (575) 393-3612
- 1. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval.
 - a. In the event the operator has proposed to drill multiple wells utilizing a skid/walking rig. Operator shall secure the wellbore on the current well, after installing and testing the wellhead, by installing a blind flange of like pressure rating to the wellhead and a pressure gauge that can be monitored while drilling is performed on the other well(s).
 - b. When the operator proposes to set surface casing with Spudder Rig
 - Notify the BLM when moving in and removing the Spudder Rig.
 - Notify the BLM when moving in the 2nd Rig. Rig to be moved in within 90 days of notification that Spudder Rig has left the location.
 - BOP/BOPE test to be conducted per Onshore Oil and Gas Order No. 2 as soon as 2nd Rig is rigged up on well.

- 2. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works are located, this does not include the dog house or stairway area.
- 3. The record of the drilling rate along with the GR/N well log (one log per well pad is acceptable) run from TD to surface (horizontal well vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

A. CASING

- 1. Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.
- <u>Wait on cement (WOC) for Potash Areas:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least <u>24</u> <u>hours</u>. WOC time will be recorded in the driller's log. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 3. <u>Wait on cement (WOC) for Water Basin:</u> After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least <u>8 hours</u>. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements. The casing intergrity test can be done (prior to the cement setting up) immediately after bumping the plug.
- 4. Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.
- 5. No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

- 6. On that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Formation at the shoe shall be tested to a minimum of the mud weight equivalent anticipated to control the formation pressure to the next casing depth or at total depth of the well. This test shall be performed before drilling more than 20 feet of new hole.
- 7. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.
- 8. Whenever a casing string is cemented in the R-111-P potash area, the NMOCD requirements shall be followed.
- **B. PRESSURE CONTROL**
- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API RP 53 Sec. 17.
- 2. If a variance is approved for a flexible hose to be installed from the BOP to the choke manifold, the following requirements apply: The flex line must meet the requirements of API 16C. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.
- 3. 5M or higher system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.
- 4. If the operator has proposed a multi-bowl wellhead assembly in the APD. The following requirements must be met:
 - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
 - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
 - c. Manufacturer representative shall install the test plug for the initial BOP test.

- d. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.
- e. Whenever any seal subject to test pressure is broken, all the tests in OOGO2.III.A.2.i must be followed.
- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
 - a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).
 - b. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time, except the casing pressure test can be initiated immediately after bumping the plug (only applies to single stage cement jobs).
 - c. The tests shall be done by an independent service company utilizing a test plug. The results of the test shall be reported to the appropriate BLM office.
 - d. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
 - e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
 - f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes. This test shall be performed prior to the test at full stack pressure.
 - g. BOP/BOPE must be tested by an independent service company within 500

feet of the top of the Wolfcamp formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

C. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the Wolfcamp formation, and shall be used until production casing is run and cemented.

D. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

Waste Minimization Plan (WMP)

In the interest of resource development, submission of additional well gas capture development plan information is deferred but may be required by the BLM Authorized Officer at a later date.

ZS 080218

243112P APD18-1340 SND 12 01 FED 004 3H 30025 NMNM120901 CHEVRON 12-55 08022018 ZS

Sec P KFC

13 3/8	surface	csg in a	17 1/2	inch hole.		<u>Design I</u>	actors	SUR	FACE
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	Weight
"A"	54.50	J	55	ST&C	11.28	2.92	0.5	836	45,562
"B"								0	0
w/8.4#/g	mud, 30min Sfo	: Csg Test psig	: 1,500	Tail Cmt	does	circ to sfc.	Totals:	836	45,562
Comparison of	of Proposed t	<u>o Minimum</u>	Required C	ement Volume	S				
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cplg
17 1/2	0.6946	821	1100	635	73	8.90	3069	5M	1.56
						FRAC GRAD. :	2730/800=3	4	

Burst Frac Gradient(s) for Segment(s) A, B = , b All > 0.70, OK.

the second se

.

95/8	casing in	side the	13 3/8	<u>A Buc</u>	oyant	<u>Design</u>	Factors	INTERI	MEDIATE
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	Weight
"A"	43.50	L	. 80	LT&C	1.95	0.69	0.85	11,010	478,935
"B"								0	0
w/8.4#/g	mud, 30min Sf	c Csg Test psig	:				Totals:	11,010	478,935
The c	ement volun	ne(s) are inte	ended to ach	ieve a top of	0	ft from s	urface or a	836	overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cplg
12 1/4	0.3132	look 🖌	0	3508		9.60	4772	5M	0.81
· D V Tool(s):			4600				sum of sx	<u>Σ CuFt</u>	Σ%excess
t by stage % :		29	29				2006	4514	29
Class 'H' tail cm	it yld > 1.20						MASP is with	n 10% of 50	00psig, need

Burst Frac Gradient(s) for Segment(s): A, B, C, D = 0.57, b, c, d <0.70 a Problem!!

ALT. COLLAPSE SF: 0.69*2=1.38

5 1/2	casing ins	ide the	9 5/8		_	Design Fa	ctors	PROD	UCTION
Segment	#/ft	Grade		Coupling	Joint	Collapse	Burst	Length	Weight
"A"	20.00	Р	110	TXP	2.67	1.57	1.7	11,450	229,000
"B"	20.00	Р	110	ТХР	8.01	1.39	1.7	10,523	210,460
w/8.4#/g	g mud, 30min Sfc	Csg Test psig:	2,519				Totals:	21,973	439,460
В	would be:				60.02	1.50	if it were a	vertical we	ellbore.
	lot Hole Plan	nod	MTD	Max VTD	Csg VD	Curve KOP	Dogleg ^e	Severity®	MEOC
NO PI		neu	21973	11984	11984	11450	90	10	12350
The c	cement volume	e(s) are inte	nded to ach	ieve a top of	10510	ft from s	urface or a	500	overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Req'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cplg
8 1/2	0.2291	2563	3655	2643	38	11.90			1.20
Class 'H' tail or	mt uld > 1.20								

Class 'H' tail cmt yld > 1.20

243112P APD18-1340 SND 12 01 FED 004 3H 30025 NMNM120901 CHEVRON 12-55 08022018 ZS CONTINGENCY PLAN

13 3/	8 surface	csg in a	17 1/2	inch hole.	रत्नकार (° 45. °° 47 € न्हरू	Design	actors	SUR	FACE
Segmen		Grade		Coupling	Joint	Collapse	Burst	Length	Welgh
"A"	54.50		55	ST&C	11.28	2.92	0.5	836	45,562
"B"	•			-,				0	0
	#/g mud, 30min Sfe	c Csg Test psig:	1.500	Tail Cmt	does	circ to sfc.	Totals:	836	45,562
•	n of Proposed t		•				rouis.		
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling)	Calc	Req'd	Min Dist
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cpl
17 1/2	0.6946	821	1100	635	73	8.90	3069	5M	1.56
	0.00 10					FRAC GRAD. :			
lurst Frac G	Gradient(s) for Se	gment(s) A, B	=,b Ail>0	.70, OK.		ar 2017 a' 104 a - 1 and 2		(* 42.) + 654 (* 4	ile a azi e anit
- 95/	8 casing in	side the	13 3/8	A Buc		Design I	actore		NEDIATE
Segmen		Grade	13 3/8	Coupling	Joint	Collapse			Weigh
"A"	43.50	· · · ·	80	LT&C	1.95	0.69	.0.86	Length	-
"B"	43.50	··· · .	00	LIQU	1.80	0.09	.0.00	11,010 ••• 0	478,93 0
	#/g mud, 30min Sf	r fog Taet neie					Totals:	11,010	478,93
	The cement vol		itended to ac	hieve a ton of	0	ft from su		836	overlap.
Hole	Annular	1 Stage	1 Stage	Min	1 Stage	Drilling	Calc	Rea'd	Min Dis
Size	Volume	Cmt Sx	CuFt Cmt	Cu Ft	% Excess	Mud Wt	MASP	BOPE	Hole-Cp
12 1/4	0.3132	look 🖌	0	3508	,0 Ex0633	9.60	4738	5M	0.81
۲ <u>۳،</u> ۲۷ V Tool(s)		I NUCI	4600	5500		3.00	4730 <u>sum of sx</u>	Σ CuFt	Σ%exces
by stage %		29	4600 29				2006	4514	2 //erces 29
	i cmt yld > 1.20	43	23			1	2000 MASP is withi		
Problem!! Tail crr 7 5/8		· · · · · · · · · · · · · · · · · · ·	10710		ALT. CULLAP 65= 2:445:0 4:45 4 1:4 4:5 4:45	SE SF: 0.69*2=		анда жаларан жаларан аларан 111	NER
, sys Segmen		Grade	10/10	Coupling	Joint	Collapse	Burst	Length	Weigh
"A"	29.70		110	NEDGE 51:	18.97	0.97	1.28	1,190	35,343
"B" -	29.70	F	110	NEDGE 51	10.97	. 0.57	1.20	0	0
_	#/g mud, 30min Sfe	Con Tost print	1 426	ALDOL 31			Totals:	1,190	35,343
w/8.4	would be:		1,430		15.96	0.97	if it were a		
			MTD	Max VTD	Csg VD	Curve KOP	Dogteg ^o	Severity ^o	MEOC
No	Pilot Hole Pla	nned	11900	11900	11900	11450	45	0	0
		lume(s) are ir			10910	ft from su		100.0	overlap.
	The cement vol		tended to do			11 11 0111 014			overlap.
	The cement vol		1 Stane			Drilling	Calc	Roa'd	Min Dis
Hole	Annular	1 Stage	1 Stage CuFt Cmt	Min	1 Stage	Drilling Mud Wr	Caic MASP	Req'd BOPE	Min Dis
Hole Size	Annular Volume	1 Stage Cmt Sx	CuFt Cmt	Min Cu Ft	1 Stage % Excess	Mud Wt	MASP	BOPE	Hole-Cp
Hole Size 8 1/2	Annular Volume 0.0770	1 Stage Cmt Sx 88	CuFt Cmt 123	Min Cu Ft 90	1 Stage % Excess 37	Mud Wt 11.90		•	
Hole Size 8 1/2	Annular Volume	1 Stage Cmt Sx 88	CuFt Cmt 123	Min Cu Ft	1 Stage % Excess 37 sig, need exr	Mud Wt 11.90 ta equip?	MASP	BOPE	Hole-Cp
Hole Size 8 1/2 lass 'H' tail	Annular Volume 0.0770 I cmt yld > 1.20 casing in	1 Stage Cmt Sx 88 side the	CuFt Cmt 123	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI	1 Stage % Excess 37 sig, need exr	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u>	MASP 4772	BOPE 5M	Hole-Cp
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segmen	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft	1 Stage Cmt Sx 88 Iside the Grade	CuFt Cmt 123 MASP is withi 7 5/8	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1 Joint	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse	MASP 4772 <u>actors</u> Burst	BOPE 5M PROD Length	Hole-Cp 0.44 • UCTION Weigh
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segment "A"	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00	1 Stage Cmt Sx 88 iside the Grade P	CuFt Cmt 123 MASP is withi 75/8 110	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP	1 Stage % Excess 37 sig, need exr 5 F: 0.95*1 Joint 3.05	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71	MASP 4772 Factors Burst 1.94	BOPE 5M PROD	Hole-Cp 0.44 • UCTION Weigh 229,00
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segment "A" "B"	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00	1 Stage Cmt Sx 88 iside the Grade P P	CuFt Cmt 123 MASP is withi 75/8 110 110	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1 Joint	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54	MASP 4772 	BOPE 5M PROD Length 11,450 300	Hole-Cp 0.44 • UCTION Weigh 229,00 6,000
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segment "A" "B" "C"	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00	1 Stage Cmt Sx 88 iside the Grade P P	CuFt Cmt 123 MASP is withi 75/8 110	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP	1 Stage % Excess 37 sig, need exr 5 F: 0.95*1 Joint 3.05	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71	MASP 4772 Factors Burst 1.94	BOPE 5M PROD Length 11,450	Hole-Cp 0.44 • UCTION Weigh 229,000 6,000 184,01
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segment "A" "B"	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00	1 Stage Cmt Sx 88 iside the Grade P P	CuFt Cmt 123 MASP is withi 75/8 110 110	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1 Joint 3.05 2.81	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54	MASP 4772 	BOPE 5M PROD Length 11,450 300 10,223 0	Hole-Cp 0.44 • UCTION Weigh 229,00 6,000
Hole Size 8 1/2 lass 'H' tail 5 1/2 Segment "A" "B" "C" "D"	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00	1 Stage Cmt Sx 88 side the Grade P P	CuFt Cmt 123 MASP is withi 75/8 110 110 110	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1 Joint 3.05 2.81	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54	MASP 4772 	BOPE 5M PROD Length 11,450 300 10,223	Hole-Cp 0.44 • UCTION Weigh 229,00 6,000 184,01
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segment "A" "B" "C" "D" w/8.44	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00 18.00	1 Stage Cmt Sx 88 side the Grade P P c Csg Test psig:	CuFt Cmt 123 MASP is withi 75/8 110 110 2,519	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP VEDGE 52	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1 Joint 3.05 2.81	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54 2	MASP 4772 Factors Burst 1.94 1.88	BOPE 5M PROD Length 11,450 300 10,223 0 21,973	Hole-Cp 0.44 • UCTION Weigh 229,00 6,000 184,01 0 419,01
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segmen "A" "B" "C" "D" w/8.44	Annular Volume 0.0770 I cmt yld > 1.20 I cmt yld > 1.20 Casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfa 3 Segment Di	1 Stage Cmt Sx 88 side the Grade P P P c Csg Test psig: esign Factor	CuFt Cmt 123 MASP is withi 75/8 110 110 2,519	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP VEDGE 52	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1. 5 SF: 0.95*1. 101.61	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54 2	MASP 4772 <u>actors</u> Burst 1.94 1.94 1.88 Totals:	BOPE 5M PROD Length 11,450 300 10,223 0 21,973	Hole-Cp 0.44 • UCTION Weigh 229,00 6,000 184,01 0 419,01
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segmen "A" "B" "C" "D" w/8.44	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfo	1 Stage Cmt Sx 88 side the Grade P P P c Csg Test psig: esign Factor	CuFt Cmt 123 MASP is withi 75/8 110 110 2,519 s would be:	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP WEDGE 52	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1. 5 SF: 0.95*1. 3.05 2.81 101.61 71.39	Mud Wt 11.90 ta equip? 5=1.42 Design I Collapse 1.71 1.54 2 1.67	MASP 4772 Factors Burst 1.94 1.94 1.88 Totals: f it were a v	BOPE 5M PROD Length 11,450 300 10,223 0 21,973 ertical wellt	Hole-Cp 0.44 • • • • • • • • • • • • • • • • • •
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segment "A" "B" "C" "D" w/8.44 E No I	Annular Volume 0.0770 I cmt yld > 1.20 I cmt yld > 1.20 Casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfa 3 Segment Di	1 Stage Cmt Sx 88 Iside the Grade P P c Csg Test psig: esign Factor nned	CuFt Cmt 123 MASP is withi 75/8 110 110 110 2,519 's would be: MTD 21973	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP WEDGE 52 Max VTD 11984	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1.: Joint 3.05 2.81 101.61 71.39 Csg VD	Mud Wt 11.90 ta equip? 5=1.42 Design I Collapse 1.71 1.54 2 1.67 Curve KOP	MASP 4772 Factors Burst 1.94 1.94 1.88 Totals: f it were a v Dogleg ^o 90	BOPE 5M PROD Length 11,450 300 10,223 0 21,973 ertical wellt Severity ^o	Hole-Cp 0.44 • • • • • • • • • • • • • • • • • •
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segment "A" "B" "C" "D" w/8.44 E No I	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfd 3 Segment Do Pilot Hole Plan	1 Stage Cmt Sx 88 Iside the Grade P P c Csg Test psig: esign Factor nned	CuFt Cmt 123 MASP is withi 75/8 110 110 110 2,519 's would be: MTD 21973	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP WEDGE 52 Max VTD 11984	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1.: Joint 3.05 2.81 101.61 71.39 Csg VD 11984	Mud Wt 11.90 ta equip? 5=1.42 Design I Collapse 1.71 1.54 2 1.67 Curve KOP 11450	MASP 4772 Factors Burst 1.94 1.94 1.88 Totals: f it were a v Dogleg ^o 90	BOPE 5M PROD Length 11,450 300 10,223 0 21,973 ertical wellt Severity ^o 10	Hole-Cp 0.44 • • • • • • • • • • • • • • • • • •
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segment "A" "B" "C" "D" w/8.44 E No I	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfd 3 Segment Do Pilot Hole Plan The cement vol	1 Stage Cmt Sx 88 Iside the Grade P P c Csg Test psig: esign Factor nned Iume(s) are in	CuFt Cmt 123 MASP is withi 75/8 110 110 2,519 10 2,519 10 21973 tended to act	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSE Coupling TXP TXP WEDGE 52 Max VTD 11984 hieve a top of	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1.: Joint 3.05 2.81 101.61 71.39 Csg VD 11984 11400	Mud Wt 11.90 ta equip? 5=1.42 <u>Design I</u> Collapse 1.71 1.54 2 1.67 Curve KOP 11450 ft from su	MASP 4772 actors Burst 1.94 1.94 1.88 Totals: f it were a v Dogleg° 90 rface or a	BOPE 5M PROD Length 11,450 300 10,223 0 21,973 ertical wellt Severity ^o 10 500	Hole-Cp 0.44 • • • • • • • • • • • • • • • • • •
Hole Size 8 1/2 ass 'H' tail 5 1/2 Segment "A" "B" "C" "D" w/8.44 E No I Hole	Annular Volume 0.0770 I cmt yld > 1.20 casing in t #/ft 20.00 20.00 18.00 #/g mud, 30min Sfd 3 Segment Do Pilot Hole Plan The cement vol Annular	1 Stage Cmt Sx 88 Iside the Grade P P c Csg Test psig: esign Factor nned Iume(s) are in 1 Stage	CuFt Cmt 123 MASP is withi 75/8 110 110 2,519 10 2,519 10 21973 tended to act 1 Stage	Min Cu Ft 90 n 10% of 5000p ATL COLLAPSI Coupling TXP TXP WEDGE 52 Max VTD 11984 hieve a top of Min	1 Stage % Excess 37 sig, need exr 5 SF: 0.95*1.: Joint 3.05 2.81 101.61 71.39 Csg VD 11984 11400 1 Stage	Mud Wt 11.90 ta equip? 5=1.42 Design I Collapse 1.71 1.54 2 1.67 Curve KOP 11450 ft from su Drilling	MASP 4772 actors Burst 1.94 1.94 1.88 Totals: f it were a v Dogleg ^o 90 rface or a Calc	BOPE 5M PROD Length 11,450 300 10,223 0 21,973 ertical wellt Severity ^o 10 500 Reg'd	Hole-Cp 0.44 • • • • • • • • • • • • • • • • • •

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