# **UNITED STATES** DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

**NMOCD** Artesia

FORM APPROVED OMB NO. 1004-0137 Expires: January 31, 2018

# 5. Lease Serial No. NMNM0506A

**SUNDRY NOTICES AND REPORTS ON WELLS** 

 *****	1111000	,0,1	

Do not use this abandoned we	Do not use this form for proposals to drill or to re-enter an abandoned well. Use form 3160-3 (APD) for such proposals.									
SUBMIT IN	TRIPLICATE - Other instr	uctions on	page 2	-,77	-	7. If Unit or CA/Agre	ement	, Name and/or No.		
1. Type of Well						8. Well Name and No POKER LAKE U		TWP 104H		
② Oil Well ☐ Gas Well ☐ Oth  2. Name of Operator.		(5) 1 3/ 1/AD	200							
XTO PERMIAN OPERATING	Contact:     LLC	(ELLY KAR) @xtoenergy.		. *		9. API Well No. 30-015-45054				
3a. Address 6401 HOLIDAY HILL RD BLD MIDLAND, TX 79707	G 5	3b. Phone No Ph: 432-62	o. (include area 20-4374	code)		10. Field and Pool or Exploratory Area PURPLE SAGE; WOLFCAMP				
4. Location of Well (Footage, Sec., T	., R., M., or Survey Description)					11. County or Parish,	State			
Sec 15 T24S R31E Mer NMP	SESW 360FSL 1805FWL					EDDY COUNT	Y, NN	1		
12. CHECK THE A	PPROPRIATE BOX(ES)	TO INDICA	TE NATUR	E OF 1	NOTICE,	REPORT, OR OT	HER	DATA		
TYPE OF SUBMISSION		<i>)</i>	TYP	E OF A	CTION					
Notice of Intent     ■	pen	1	☐ Production	on (Start/Resume)		Water Shut-Off				
☐ Subsequent Report	☐ Alter Casing ☐ Hy				□ Reclama	tion		Well Integrity		
☐ Subsequent Report	☐ Casing Repair ☐ New Construction ☐ Recon				□ Recompl	ete	Ø	Other		
Final Abandonment Notice	inal Abandonment Notice					nporarily Abandon Change to Original A				
	☐ Convert to Injection	☐ Plug	; Back	I	■ Water D	isposal				
Attach the Bond under which the wor following completion of the involved testing has been completed. Final Attached that the site is ready for fixTO Permitting Operating, LL attached drilling program	operations. If the operation resubandonment Notices must be filed inal inspection.	ilts in a multip d only after all	le completion o requirements, i	r recomp including	pletion in a no greclamation	ew interval, a Form 316 have been completed	60-4 m	ust he filed once		
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						NS OF APP	RC	WAI.		
	JUL	2 3 2019	C	UNI	טוווט	N2 OL WIT	ico	, 4 1 1 II		
	DISTRICTI	I-APPTESIA	CD.							
14. I hereby certify that the foregoing is	true and correct. Electronic Submission #4 For XTO PERMIA Committed to AFMSS for p	N OPERATII	IG ĹLC, sen	t to the	Carlsbad	.,				
Name (Printed/Typed) KELLYKA	RDOS / //		Title RE	GULAT	ORY COC	RDINATOR				
Signature (Electronic S	Submission)		Date 03/	12/201		PROVED		6 - 4.		
	THIS SPACE FO	R FEDERA	L OR STA	TE OF	FFICENAS	E1 3 2019				
AMETOVED BY MICH	(1) [[-]	) 	Title	,	-	AND MANAGEME	NT.	Date :		
onditions of approval, if any, are attached ertify that the applicant holds legal or equ which would entitle the applicant to condu	itable litle to those rights in the s	ot warrant or subject lease	Office			ELD MANAGEMEN				
itle 18 U.S.C. Section 1001 and Title 43 States any false, fictitious or fraudulent s	U.S.C. Section 1212, make it a c statements or representations as t	rune for any pe o any matter w	rson knowingl ithin its jurisdi	y and wi	llfully to mal	te to any department or	agenc	y of the United		

\*\* OPERATOR-SUBMITTED \*\* OPERATOR-SUBMITTED \*\* Ruf 10-29-19

#### DRILLING PLAN: BLM COMPLIANCE (Supplement to BLM 3160-3)

XTO Energy Inc. PLU 15 Twin Wells Ranch 104H Projected TD: 25076' MD / 11826' TVD SHL: 360' FSL & 1805' FWL, Section 15, T24S, R31E BHL: 2440' FNL & 2310' FWL, Section 34, T24S, R31E Eddy County, NM

#### 1. Geologic Name of Surface Formation

Quaternary

#### 2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

Formation -	Well Depth (TVD)	Water/Oil/Gas
Rustler	. 719'	. Water
Top of Salt	1077'.	Water
Base of Salt	4263'	Water
Delaware	4486'	Water
Bone Spring	8441'	Water
1st Bone Spring Ss	9407'	Water/Oil/Gas
2nd Bone Spring Ss	9993'	Water/Oil/Gas
3rd Bone Spring Ss	11240'	Water/Oil/Gas
Target/Land Curve	11826'	Water/Oil/Gas

<sup>\*\*\*</sup> Hydrocarbons @ Brushy Canyon

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 18-5/8" inch casing @ 870' (207' above the salt) and circulating cement back to surface. The salt will be isolated by setting 13-3/8" inch casing at 4320' and circulating cement to surface. The second intermediate will isolate from the salt down to the next casing seat by setting 9-5/8" inch casing at 10650' and a DV tool at 4388'. A 8-3/4" inch curve and lateral hole will be drilled to MD/TD and 5-1/2 inch casing will be set at TD and cemented 500' inside the previous shoe.

#### 3. Casing Design

Hole Size	Depth	OD Csg	Weight	Collar	Grade	New/Used	SF Burst	SF Collapse	SF Tension
24"	0' - 870'	18-5/8"	87.5	STC	H-40	New	1.24	1.58	7.34
17-1/2"	0' 4320'	13-3/8" -	68	STC	J-55	New	1.16	1.46	2.44
12-1/4"	0' – 10650'	9-5/8"	40	LTC	P-110	New	2.23	1.15	2.32
8-3/4"	0' – 25076'	5-1/2"	17	втс	P-110	New	1.12	1.22	1.91

- · XTO requests to utilize centralizers only in the curve after the KOP and only a minimum of one every other joint.
- 13-3/8" Collapse analyzed using 50% evacuation based on regional experience.
- 9-5/8" Collapse analyzed using 33% evacuation based on regional experience.
- 5-1/2" Tension calculated using vertical hanging weight plus the lateral weight multiplied by a friction factor of 0.35
- Test on 2M Annular & Casing will be limited to 70% burst of the casing or 1500 psi, whichver is less

#### Wellhead:

Temporary Wellhead

18-5/8" SOW bottom x 21-1/4" 2M top flange.

Permanent Wellhead – GE RSH Multibowl System A. Starting Head: 13-5/8" 5M top flange x 13-3/8" SOW bottom

- B. Tubing Head: 13-5/8" 5M bottom flange x 7-1/16" 10M top flange
  - Wellhead will be installed by manufacturer's representatives.
  - Manufacturer will monitor welding process to ensure appropriate temperature of seal.
  - Operator will test the 9-5/8" casing per BLM Onshore Order 2
  - Wellhead Manufacturer representative will not be present for BOP test plug installation

<sup>\*\*\*</sup> Groundwater depth 40' (per NM State Engineers Office).

#### 4. Cement Program

Surface Casing: 18-5/8", 87.5 New H-40, STC casing to be set at +/- 870'

Lead: 760 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)

Tail: 550 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

1st Intermediate Casing: 13-3/8", 68 New J-55, STC casing to be set at +/- 4320'

Lead: 2980 sxs EconoCem-HLTRRC (mixed at 12.9 ppg, 1.87 ft3/sx, 10.13 gal/sx water)
Tail: 300 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.35 ft3/sx, 6.39 gal/sx water)
Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Intermediate Casing: 9-5/8", 40 New P-110, LTC casing to be set at +/- 10650' ECP/DV Tool to be set at 4388' 1st Stage

Lead: 1910 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)

Tail: 230 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

2nd Stage

Lead: 1290 sxs Halcem-C + 2% CaCl (mixed at 12.9 ppg, 1.88 ft3/sx, 9.61 gal/sx water)

Tail: 230 sxs Halcem-C + 2% CaCl (mixed at 14.8 ppg, 1.33 ft3/sx, 6.39 gal/sx water)

Compressives: 12-hr = 900 psi 24 hr = 1500 psi

Production Casing: 5-1/2", 17 New P-110, BTC casing to be set at +/- 25076'

Lead: 50 sxs NeoCem (mixed at 10.5 ppg, 2.69 ft3/sx, 12.26 gal/sx water)

Tail: 2950 sxs VersaCem (mixed at 13.2 ppg, 1.61 ft3/sx, 8.38 gal/sx water)

Compressives: 12-hr = 1375 psi 24 hr = 2285 psi

#### 5. Pressure Control Equipment

The blow out preventer equipment (BOP) on surface casing temporary wellhead will consist of a 21-1/4" minimum 2M . Hydril. MASP should not exceed 1318 psi.

Once the permanent WH is installed on the 13-3/8" casing, the blow out preventer equipment (BOP) will consist of a 13-5/8" minimum 5M Hydril and a 13-5/8" minimum 5M Double Ram BOP. MASP should not exceed 3548 psi.

All BOP testing will be done by an independent service company. Annular pressure tests will be limited to 50% of the working pressure. When nippling up on the 13-3/8", 5M bradenhead and flange, the BOP test will be limited to 5000 psi. When nippling up on the 9-5/8", the BOP will be tested to a minimum of 5000 psi. All BOP tests will include a low pressure test as per BLM regulations. The 5M BOP diagrams are attached. Blind rams will be functioned tested each trip, pipe rams will be functioned tested each day.

A variance is requested to allow use of a flex hose as the choke line from the BOP to the Choke Manifold. If this hose is used, a copy of the manufacturer's certification and pressure test chart will be kept on the rig. Attached is an example of a certification and pressure test chart. The manufacturer does not require anchors.

#### 6. Proposed Mud Circulation System

INTERVAL	Hole Size	Mud Type	MW (ppg)	Viscosity (sec/qt)	Fluid Loss (cc)
0' - 870'	' - 870' 24"		8.4-8.8	35-40	NC
870' - 4320'	17-1/2" _	Brine	9.8-10.2	30-32	NC .
4320' to 10650'	12-1/4"	FW / Cut Brine	8.7-9.4	30-32	NC
10650' to 25076'	8-3/4"	Cut Brine / Polymer	9.7 - 10	29-32	NC - 20

The necessary mud products for weight addition and fluid loss control will be on location at all times.

Spud with fresh water/native mud. Drill out from under 18-5/8" surface casing with brine solution. A ppg-10.2ppg brine mud will be used while drilling through the salt formation. Use fibrous materials as needed to control seepage and lost circulation. Pump viscous sweeps as needed for hole cleaning. Pump speed will be recorded on a daily drilling report after mudding up. A Pason or Totco will be used to detect changes in loss or gain of mud volume. A mud test will be performed every 24 hours to determine: density, viscosity, strength, filtration and pH as necessary. Use available solids controls equipment to help keep mud weight down after mud up. Rig up solids control equipment to operate as a closed loop system.

#### 7. Auxiliary Well Control and Monitoring Equipment

- A. A Kelly cock will be in the drill string at all times.
- B. A full opening drill pipe stabbing valve having appropriate connections will be on the rig floor at all times.
- C. H2S monitors will be on location when drilling below the 13-3/8" casing.

#### 8. Logging, Coring and Testing Program

Mud Logger: Mud Logging Unit (2 man) below intermediate casing.

Open hole logging will not be done on this well.

#### 9. Abnormal Pressures and Temperatures / Potential Hazards

None Anticipated. BHT of 175 to 195 F is anticipated. No H2S is expected but monitors will be in place to detect any H2S occurrences. Should these circumstances be encountered the operator and drilling contractor are prepared to take all necessary steps to ensure safety of all personnel and environment. Lost circulation could occur but is not expected to be a serious problem in this area and hole seepage will be compensated for by additions of small amounts of LCM in the drilling fluid. The maximum anticipated bottom hole pressure for this well is 6150 psi.

#### 10. Anticipated Starting Date and Duration of Operations

Road and location construction will begin after Santa Fe and BLM have approved the APD. Anticipated spud date will be as soon after Santa Fe and BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 40 days. If production casing is run, an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.

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#### 2. Estimated Tops of Geological Markers & Depths of Anticipated Fresh Water, Oil or Gas

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<sup>\*\*\*</sup> Groundwater depth 40' (per NM State Engineers Office

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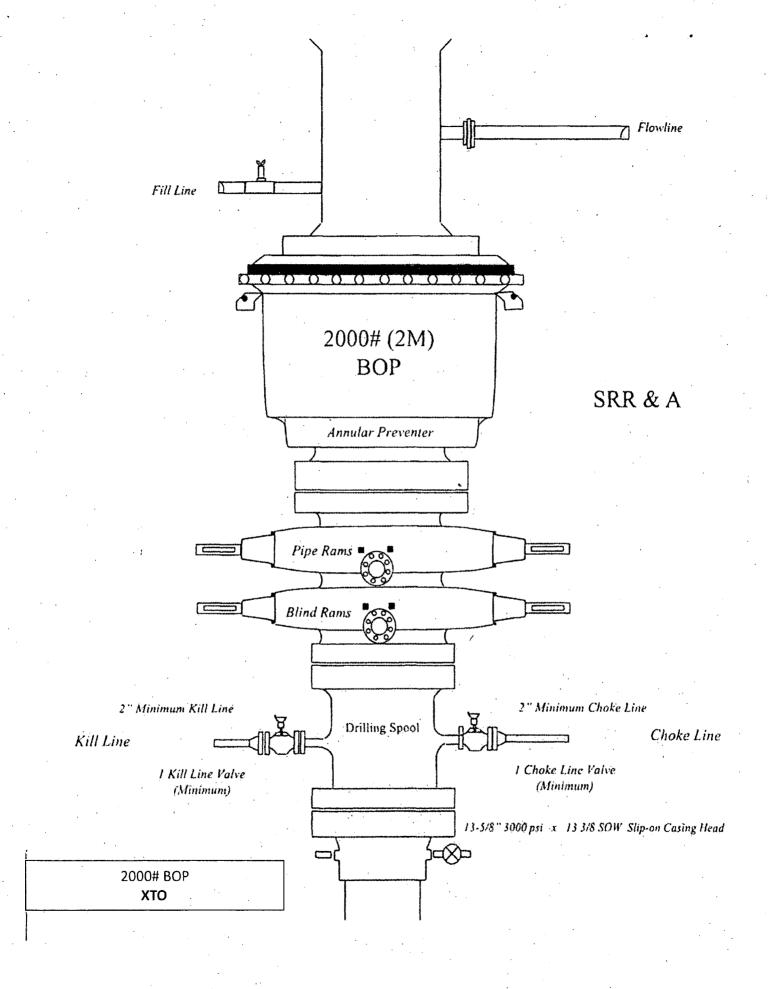
Open hale logging will not be done on this well.

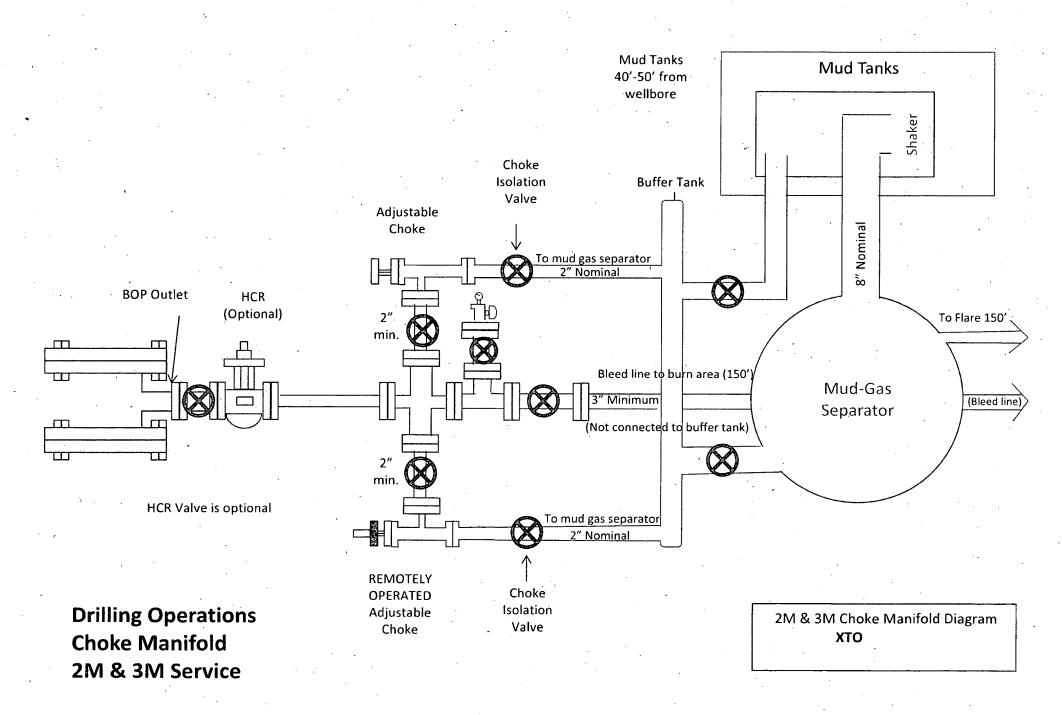
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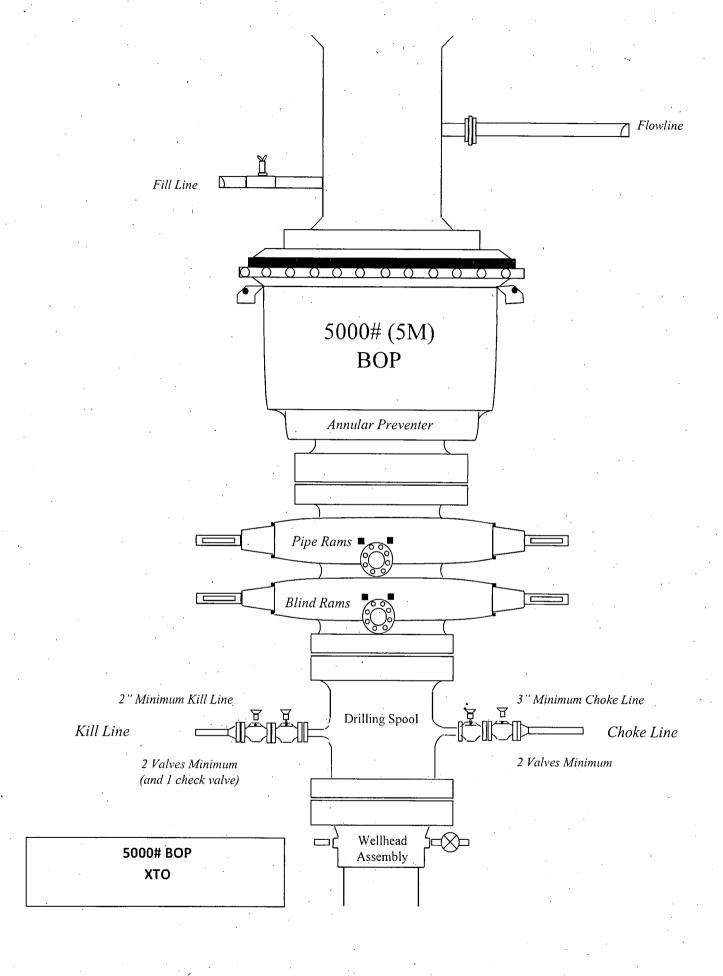
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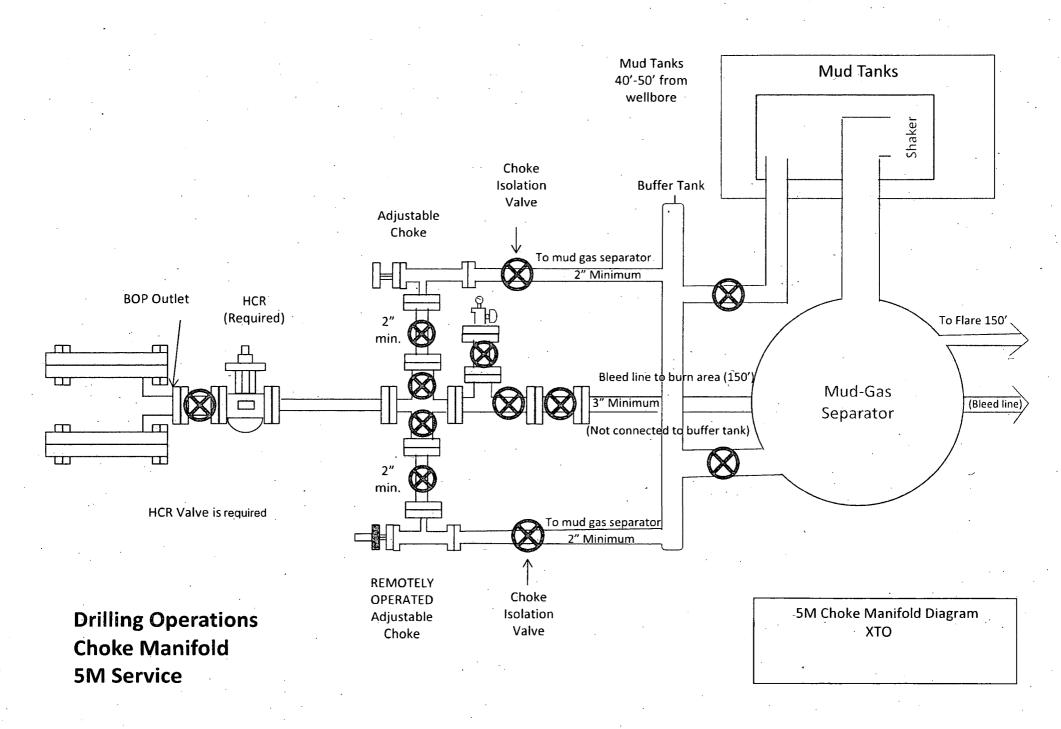
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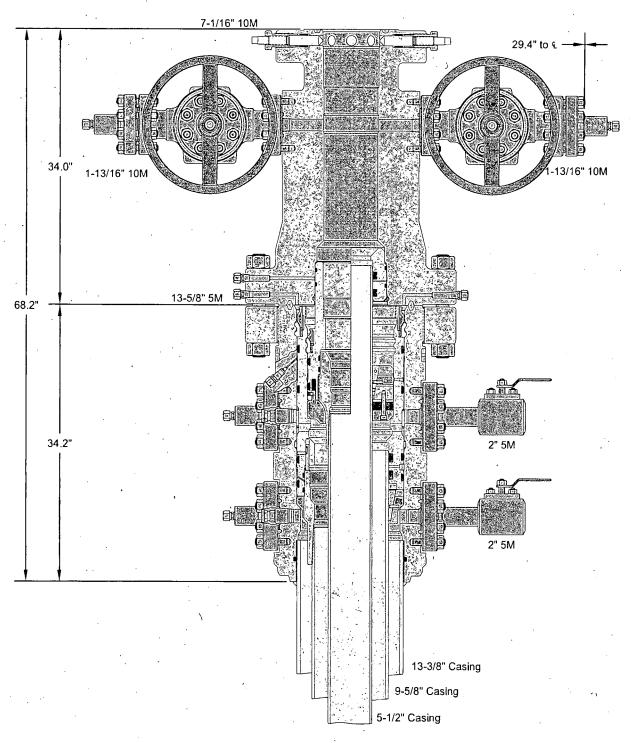












ALL DIMENSIONS ARE APPROXIMATE

This drawing is the property of GE Oil & Gas Pressure Control LP and is considered confidential. Unless otherwise approved in writing, neither it nor its contents may be used, copied, transmitted or reproduced except for the sole purpose of GE Oil & Gas Pressure Control LP.

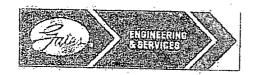
XTO ENERGY, INC.

13-3/8" x 9-5/8" x 5-1/2" 10M RSH-2 Wellhead Assembly, With T-EBS-F Tubing Head

DRAWN	VJK	16FEB17
APPRV	KN	16FEB17

FOR REFERENCE ONLY

DRAWING NO. 10012842



GATES E & S NORTH AMERICA, INC

DU-TEX

134 44TH STREET

CORPUS CHRISTI, TEXAS 78405

PHONE: 361-887-9807

FAX: 361-887-0812

EMAIL: crpe&s@gates.com

WEB: www.gates.com

# GRADE D PRESSURE TEST CERTIFICATE

Customer Ref. :	AUSTIN DISTRIBUTING	Test Date:	6/8/2014	
<del> </del>	PENDING	Hose Serial No.:	D-060814-1	
Invoice No. :	201709	Created By:	NORHA	
Product Description:		FD3.042.0R41/16.5KFLGE/E	Lii .	
End Fitting 1:	4 1/16 m.5K FLG	Foot Faring 5		
Sales Part No. :	4774-6001	End Fitting 2 :	4 1/16 in.5K FLG	
		Assembly Code :	L33090011513D-060814-1	
Verking Pressure :	5,000 PSI	Test Pressure :		

Gates E & S North America, Inc. certifies that the following hose assembly has been tested to the Gates Oilfield Roughneck Agreement/Specification requirements and passed the 15 minute hydrostatic test per API Spec 7K/Q1, Fifth Edition, June 2010, Test pressure 9.6.7 and per Table 9 to 7,500 psi in accordance with this product number. Hose burst pressure 9.6.7.2 exceeds the minimum of 2.5 times the working pressure per Table 9.

Quality

Obto :

Signature:

QUALITY

6/8/2014

Technical Supervisor:

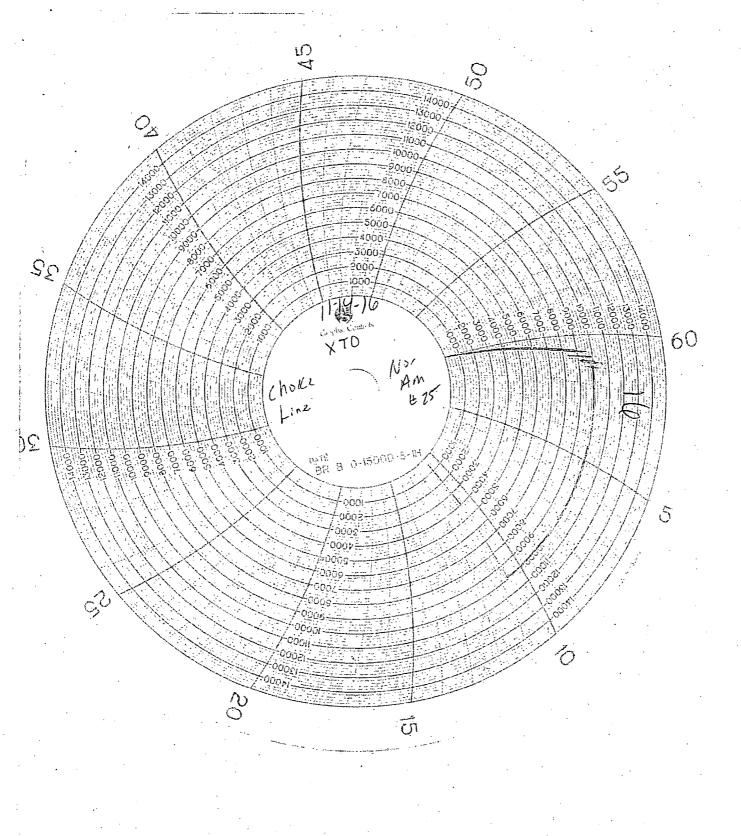
Date:

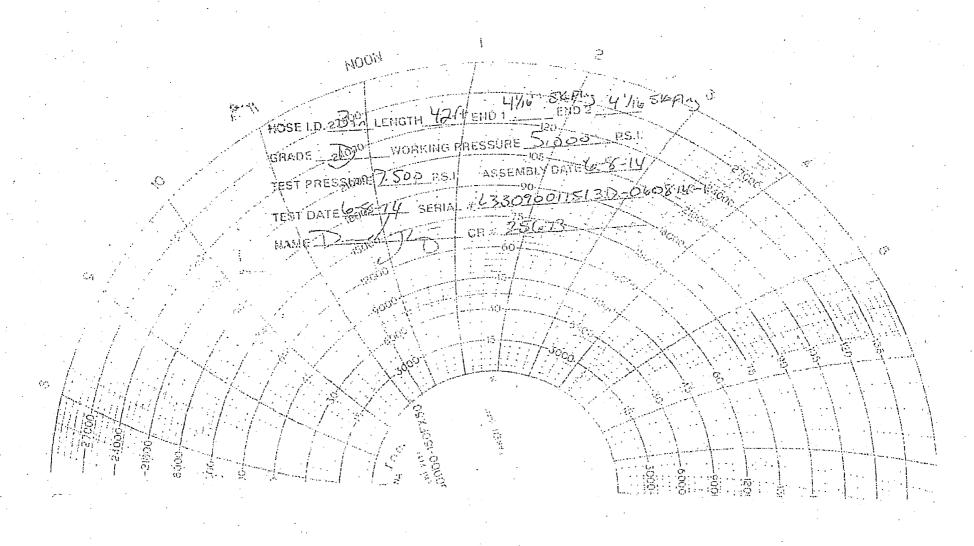
Signature:

....

PRODUCTION -56/8/2014

Forni PTC - 01 Rev.0.2





W1.05 5 501 W 101.05 30 610 W 6674.5. The Visit American 64 1 Section of Trust 110 143 100 G SHE CONTROLLY AMERICAL TO 110 143 100 G SHE CONTROLLY AMERICAL TO 141 133 1 D S. SHE CONTROLLY AMERICAL TO EASING LANGE (LANGE) (1255 H 11 CT546 S 12 TF 12 23 55 H 11 CT546 S 12 TF 12 25 55 H 11 CT546 H 11 374 Laidhuda 32' 12' 39.467 N 1200 \$222E Northing 640923.50 Hame PLU IS TWR STORE - LTP PLU IS TWR STORE - PEP \*\*\*\* \*\*\*\*





EDM 5000.1 Single User Db Database XTO ENERGY, INC. Company:

Eddy County, NM Sec 15, T24S; R31E

Well: PLU 15 Twin Wells Ranch #104H

Wellbore #1 Wellbore: Désign #1

TVD Reference: MD Reference: North Reference

System Datum:

Survey Calculation Method:

Well PLU 15 Twin Wells Ranch #104H

KB=22 @ 3561.0usft (Akita #22) KB=22 @ 3561.0usft (Akita #22)

Grid.

Minimum Curvature

Eddy County, NM

Map System: Geo Datum:

Map Zone:

US State Plane 1927 (Exact solution)

NAD 1927 (NADCON CONUS)

New Mexico East 3001

Mean Sea Level

Sec 15, T24S, R31E

Site Position:

From:

Easting:

440,929.80 usft 674,875.90 usft

Longitude:

103° 46' 4.488 W

Position Uncertainty:

0.0 usft Slot Radius:

Grid Convergence:

13-3/16 "

0.30

PLU 15 Twin Wells Ranch #104H Well

Well Position

+N/-S +E/-W 0.0 usft 0.0 usft

Easting:

674,875.90 usft

**Position Uncertainty** 

0.0 usft

Wellhead Elevation:

Longitude: Ground Level: 103° 46' 4.488 W 3,539,0 usft

Wellbore

Magnetics\*

Model Name

(nT)

IGRF2015

3/21/2019

60.00

47,728.19082882

Design

Audit Notes:

Version:

**PLAN** 

Tie On Depth:

0.0

Vertical Section:

Depth From (TVD) (usft)

+N/-S 0.0

+E/-W (usft) 0.0

Direction

177.46

Plan Sections

Measured Depth (usft)	nclination (°)	Azimuth (°)	Vertical Depth (usft)	+Ñ/-S (üsft)	÷E/-W (usft)	Dogleg Rate (*/100usff)	Build: Rate (*/100usft) (*	Turn Rate /100usft)	(F)	Target
0.0	. 0.00	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.00	
11,091.1	0.00	0.00	11,091.1	0.0	0.0	0.00	0.00	0.00	0.00	
11,591.1	50.00	110.00	11,530.0	-70.0	192.3	10.00	10.00	0.00	110.00	
. 12,335.0	89.80	179.62	11,811.0	-618.8	508.2	10.00	5.35	9.36	76.72 PL	J 15 TWR #104H -
25,076.4	89.80	179.62	11,855.5	-13,359.8	593.4	0.00	0.00	0.00	0.00 PL	U 15 TWR #104H -





EDM 5000.1 Single User Db. XTO ENERGY, INC.

Database Company: Project: Site: Well: Eddy County, NM Sec 15, T24S, R31E

PLU 15 Twin Wells Ranch #104H

Local Co-ordinate Reference : EXTYPE Reference : MD Reference : North Reference : Survey Calculation Method:

Well PLU 15 Twin Wells Ranch #104H KB=22 @ 3561 Ousft (Akita #22)

KB=22 @ 3561.0usft (Akita #22) Grid

Minimum Curvature

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Design: Des	sign #1	nesacatani Sunten Standarda	anana mananana ama			e de la companya de	describer propor describerá	manus Manus recorded and action of the	de de samme de men di man di man di managan managan mangan di saminan sami di
Planned Survey	egetiletin bezan	NACONT LAND	ALECTINA DESCRIP	ನ್ನಡ-ಕ್ರಾಪ್ತ್ ಆ " ಒಂದಾವಿಚಿತ" ಶೆ.	on at the training	ka i Impurati 37	e po especiales	WINDSTEIN W	en komi samér ve mesenden.
	图 孫政	<b>经验</b> 证据的			A STATE	KITTAN			
Measured 3			Vertical .		V. Line	ertical	Dogleg	Build	Turn
Depth Incl	ination	Azimuth 4	Depth	+N/-S	+E/-W\$	ection	- Rate ∵	Rate	Rate
a : (usft).	(°):	(3)	(usft)	(usft)	(usft)	(ustt) 🛴 (	°/100usft) (	°/100usft)%	(°/100usft)
0.0	0.00	0.00	0.0	0.0	0.0	0.0	0.00	0.00	0.00
100.0	0.00	0.00	100.0	0.0	0.0	0.0	0.00	0.00	0.00
200.0	0.00	0.00	200.0	0.0	0.0	. 0.0	0.00	0.00	0.00
300.0	0.00	0.00	300.0	0.0	0.0	. 0.0	0.00	0.00	0.00
400.0	0.00	0.00	400.0	0.0	0.0	0.0	,0.00	0.00	0.00
500.0	0.00	0.00	500.0	0.0	0.0	0.0	0.00	0.00	0.00
600.0	0.00	0.00	600.0	0.0	,0.0	0.0	0.00	0.00	0.00
Rustler									
699.0 700.0	0.00 0.00	0.00 0.00	699.0 700.0	0.0 0.0	0.0 0.0	0.0 0 <u>.</u> 0 ·	0.00	0.00 0.00	0.00
Magenta Dolomite		, 0.00	700.0	0.0	0.0	0,0	0.00	0.00	0.00
780.0	0.00	0.00	780.0	0.0	0.0	0.0	0.00	0.00	0.00
	0.00								
800.0 900.0	0.00	0.00 0.00	800.0 900.0	0.0	0.0 0.0	0.0 0.0	0.00 0.00	0.00 0.00	0.00 0.00
1,000.0	0.00	0.00	1,000.0	0.0	0.0	0.0	0.00	0.00	0.00
Top Salt*		*	, . = = • =						5
1,057.0	0.00	0.00	1,057.0	0.0	0.0	0.0	0.00	0.00	0.00
1,100.0	0.00	0.00	1,100.0	0.0	0.0	0.0	0.00	0.00	0.00
1,200.0	0.00	0.00	1,200.0	0.0	0.0	0.0	0.00	0.00	0.00
1,300.0	0.00	0.00	1,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1,400.0	0.00	0.00	1,400.0	0.0	0.0	0.0	0.00	0.00	0.00
1,500.0	0.00	0.00	1,500.0	0.0	0.0	0.0	0.00	0.00	0.00
1,600.0	0.00	0.00	1,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1,700.0	0.00	0.00	1,700.0	0.0	0.0	0.0	0.00	0.00	0.00
1,800.0	0.00	0.00	1,800.0	0.0	0.0	0.0	0.00	0.00	0.00
1,900.0 2,000.0	0.00 0.00	0.00 0.00	1,900.0 2,000.0	. 0.0 0.0	· 0.0 0.0	0.0 0.0	0.00 0.00	0.00 0.00	0.00 0.00
2,100.0	0.00	0.00	2,100.0	0.0	0.0	0.0	0.00	0.00	0.00
2,200.0 2,300.0	0.00 0.00	· 0.00 0.00	2,200.0 2,300.0	0.0 0.0	0.0 0.0	0.0 0.0	0.00 0.00	0.00	0.00 0.00
2,400.0	0.00	0.00	2,400.0	0.0	0.0	0.0	0.00	0.00	0.00
2,500.0	0.00	0.00	2,500.0	0.0	0.0	0.0	0.00	0.00	0,00
2,600.0	0.00	0.00	2,600.0	0.0	0.0	0.0	0.00	0.00	. 0.00
2,700.0	0.00	0.00	2,700.0	0.0	0.0	0.0	0.00	0.00	0.00
2,800.0	0.00	0.00	2,800.0	0.0	0.0	0.0	0.00	0.00	0.00
2,900.0	0.00	0.00	2,900.0	0.0	0.0	0.0	0.00	0.00	0.00
3,000.0	0,00 0,00	0.00	3,000.0	0,0 0,0	0.0 0.0	0.0 0.0	. 0.00 0.00	0.00	0.00
3,100.0		0.00	3,100.0					0,00	0.00
3,200.0	0.00	0.00	3,200.0	0.0	0.0	0.0	0.00	0.00	0.00
3,300.0 3,400.0	0.00 0.00	0.00	3,300.0 3,400.0	0.0 0.0	0.0 0.0	0.0 0.0	0.00 0.00	0.00 0.00	0.00 0.00
3,500.0	0.00	0.00	3,500.0	0.0	0.0	0.0	0.00	0.00	0:00
3,600.0	0.00	0.00	3,600.0	0.0	0.0	0.0	0.00	0.00	0.00
3,700.0	0.00	0.00	3,700.0	0.0	0.0	0.0	0.00	0.00	0.00
3,800.0	0.00	0.00	3,800.0	0.0	0.0	0.0	0.00	0.00	0.00
3,900.0	0.00	0.00	3,900.0	0.0	0.0	0.0	0.00	0.00	0.00
4,000.0	0.00	0.00	4,000.0	0.0	0.0	0.0	0.00	0.00	0.00
4,100.0	0.00	. 0.00	4,100.0	0.0	0.0	0.0	0.00	0.00	0.00
4,200.0	0.00	0.00	4,200.0	0.0	0.0	0.0	0.00	0.00	0.00
Base of Salt (Anh	ydrite)					1. 1			
4,243.0	0.00	0.00	4,243.0	0.0	0.0	0.0	0.00	0.00	0.00
4,300.0	0.00	0.00	4,300.0	0.0	0.0	0.0	0.00	0.00	0.00
4,400.0	0.00	0.00	4,400.0	0.0	0.0	0.0	0.00	0.00	0.00
Bell Canyon Ss./ [	Jelaware			<u> </u>	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	<u></u>	<u>, , , , , , , , , , , , , , , , , , , </u>	<u> </u>	<u> </u>





Database: Company: Project: Site: Well Wellbore: Design: EDM:5000.1 Single User, Db XTO ENERGY, INC Eddy County, NM Sec 15, T24S, R31E

PLU 15 Twin Wells Ranch #104H

Wellbore #1 Design #1

Local Co-ordinate Reference TVD Reference: MD Reference North Reference: Survey Calculation Method

Well PLU 15 Twin Wells Ranch #104H KB≣22 @ 3561.0usft (Akita #22) KB=22 @ 3561 Ousft (Akita #22) Grid Minimum Curvature

Design: Desig	N #1 ri sissiferskenistske	on Santakon Orios kontra ranta en en en en	والما والمناول والمناول والمناول والمناول المناول المناول		MIL WHILE		de en out comment occur.	era latera e transferencia de la compansa en esta de la compansa en esta de la compansa en esta de la compansa	
WORKS WATER TO STREET	e, ditum, dans	include Carrier of the Land	SIMBERGUARA (	OF BELLEVILLERSCON, NUMBER	LATTER ASSESSED ASSESSED	The Later Company	general constru	months of the west of	CATTO WAS CARRIED IN
Planned Survey	en in dispression on	increased regarded and the time of	Service and services services	e -vantarianianianianianiani, sociali ii	en ten ten ten en e	tions against an arms of the control of the		د الرساط د مهر جوه ميها ويوسيد و يميد مرد	man of the state of the state of the state of
	4 4	4年,第24年,大学		1.5					
Measured		1. 24 May 1. 14	Vertical				第688章:"A.S.		
[1] [1] [1] [2] [2] [2] [2] [2] [2] [2] [2] [2] [2	is in the		the sale of the sale of the	10 mm	1 C. C. S. M. P. C. S.	Vertical .	Dogleg "	Build	Turn
Depth	ation .	Azimuth	Depth	+N/-S	+E/-W	Section 🦠 🦿	Rate	Rate	, Rate → ( )
(usft) (°	150 2000	(°)	(usft)	(usft)	(usft)	(usft) ີ ເ	°/100usft) (	°/100usft) (°	/100usft)
	KART		过海路的人				METALLS SE	LANGE TO BE	A BOOK POOL OF SERVICE
4,466.0	0.00	0.00	4,466.0	0.0	0.0	0.0	0.00	0.00	0.00
			.,				0.00	0.00	0.00
4,500.0	0.00	0.00	4,500.0	0.0	0.0	0.0	0.00	0.00	0.00
4,600.0	0.00	0.00	4,600.0	0.0	0.0	0.0	0.00	0:00	0.00
4,700.0	0.00	0.00	4,700.0	0.0	0.0	0.0	0.00	0.00	0.00
4,800.0	0.00		4.800.0						
		0.00	• •	0.0	0.0	0.0	0.00	0.00	0.00
4,900.0	0.00	0.00	4,900.0	0.0	0.0	0.0	0.00	0.00	0.00
5,000.0	0.00	0.00	5,000.0	0.0	0.0	0.0	0.00	0.00	. 0.00
						0.0	0.00	0.00	0.00
5,100.0	0.00	0.00	5,100.0	0.0	0.0	0.0	0.00	0.00	0.00
5,200.0	0.00	0.00	5,200.0	0.0	0.0	0.0	- 0.00	0.00	0.00
5,300.0	0.00	0.00	5,300.0	0.0	0.0	0.0	0.00	0.00	0.00
1			·						
Cherry Canyon Ss.	0.00								·
5,378.0	0.00	0.00	5,378.0	0.0	0.0	. 0.0	0.00	0.00	0.00
E 400.0	0.00	0.00	E 400.0	0.0	٠		0.00	0.00	0.00
5,400.0	0.00	0.00	5,400.0	0.0	0.0	0.0	0.00	0.00	0.00
5,500.0	0.00	0.00	5,500.0	0.0	0.0	0.0	0.00	0.00	0.00
5,600.0	0.00	0.00	5,600.0	0.0	0.0	0.0	0.00	0.00	0.00
5,700.0	0.00	. 0.00	5,700.0	0.0	0.0	0.0	0.00	0.00	0.00
5,800.0	0.00	. 0.00	5,800.0	0.0	0.0	0.0	0.00	0.00	0.00
5,000.0	0.00	. 0.00	0,000.0	0.0	0.0	0.0	0.00	0,00	0.00
5,900.0	0.00	0.00	5,900.0	0.0	. 0.0	0.0	0.00	0.00	0.00
6,000.0	0.00	0.00	6,000.0	0.0	0.0	0.0	0.00	0.00	0.00
6,100.0		0.00	6,100.0						
	0.00			0.0	0.0	0.0	0.00	0.00	0.00
6,200.0	0.00	0.00	6,200.0	0.0	0.0	0.0	0.00	0.00	0.00
6,300.0	0.00	0.00	6,300.0	0.0	0.0	0.0	0.00	0.00	0.00
0.400.0	0.00	0.00	0.400.0	0.0		• •			
6,400.0	0.00	0.00	6,400.0	0.0	0.0	0.0	0.00	0.00	0.00
6,500.0	0.00	0.00	6,500.0	0.0	0.0	0.0	0.00	0,00	0.00
6,600.0	0.00	0.00	6,600.0	0.0	0.0	0.0	0.00	0.00	0.00
6,700.0	0.00	0.00	6,700.0	0.0	0.0	0.0	0.00	0.00	0.00
6,800.0	0.00	0.00	6,800.0	0.0	0.0	0.0	0.00	0.00	0.00
0,000.0	0.00	. 0.00	0,000.0	9.0	0.0	0.0	0.00	0.00	0.00
6,900.0	0.00	0.00	6,900.0	0.0	0.0	0.0	0.00	0.00	0.00
7,000.0	0.00	0.00	7,000.0	0.0	0.0	0.0	0.00	0.00	0.00
'			.,				****		, ,,,,,
Brushy Canyon Ss.								<b>A</b> 12.22	
7,002.0	0.00	0.00	7,002.0	0.0	0.0	0.0	0.00	0.00	0.00
7,100.0	0.00	0.00	7,100.0	0.0	0.0	0.0	0.00	. 0.00	0.00
7,200.0	0.00	0.00	7,200.0	0.0	0.0	0.0	0.00	0.00	0.00
7,300.0	0.00	0.00	7,300.0	0.0	0.0	0.0	0.00	0.00	0.00
7,400.0	0.00	. 0.00	7,400.0	0.0	0.0	0.0	. 0.00	0.00	0.00
7,500.0	0.00	0.00	7,500.0	0.0	0.0	0.0	0.00	0.00	0.00
7,600.0	0.00	0.00	7,600.0	0.0	0.0	0.0	0.00	0.00	0.00
7,700.0	0.00	0.00	7,700.0	0.0	. 0.0	0.0	0.00	0.00	0.00
7,700.0	0.00	0.00	1,100.0	0.0	. 0.0	0.0	0.00	00,0	0.00
7,800.0	0.00	0.00	7.800.0	0.0	0.0	0.0	0.00	0.00	0.00
7,900.0									1
	0.00	0.00	7,900.0	0.0	, 0.0	0.0	0.00	0.00	0.00
8,000.0	0.00	0.00	8,000.0	0.0	0.0.	0.0	0.00	0.00	0.00
8,100.0	0.00	0.00	8,100.0	0.0	0.0	0.0	0.00	0.00	0.00
8,200.0	0.00	0.00	8,200.0	0.0	0.0	0.0	0.00	0.00	0.00
		•							
8,300.0	0.00	0.00	8,300.0	0.0	0.0	0.0	0.00	0.00	0.00
Bone Spring Lm.					5	, -		Agricultural Company	
8,319.0	0.00	0.00	8,319.0	0.0	0.0	0.0	0.00	. 0.00	0.00
	11	3,00	0,010.0		0.0	0.0	1. 1.		1,00
Avalon Ss.					South And Se	红色 化双氯酚	4.1.	والوالمي يأورون فالمالي	
8,400.0	0.00	0.00	8,400.0	0.0	0.0	0.0	0.00	0.00	′ 0.00
Bone Spg. Upper Av	alon Shale					* 3757			
8,421.0	0.00	0.00	8,421.0	0.0	0.0	0.0	0.00	0.00	0.00
8,500.0	0.00	0.00	8,500.0	0.0	0.0	0.0	0.00	0.00	0.00
8,600.0	0.00	0.00	8,600.0	0.0	0.0	0.0	0.00	0.00	0.00
8,700.0	0.00	0.00	8,700.0	0.0	0.0	0.0	0.00	0.00	0.00



EDM 5000.1 Single User Db XTO ENERGY, INC. Company: Eddy County, NM Project:

Sec 15, T24S, R31E PLU 15 Twin Wells Ranch #104H

 
 Site
 Sec. 15, T24

 Well
 PLU 15 Twir

 Wellbore:
 Wellbore #1

 Design:
 Design #1
 Wellbore #1 Local Co-ordinate Reference TVD Reference MD Reference:

North Reference: Survey Calculation Method:

Well PLU 15 Twin Wells Ranch #104H KB=22 @ 3561 0usft (Akita #22) KB=22 @ 3561 Ousft (Akita #22)

Grid. Minimum Curvature

Design: 5/2. D	esign #1	transmission is vantured and security in	and the consistency of the constant of		التحديد والما		r Kanadamakan ana shina asac sa	naturánia acom naturoperaturbat	معاريات براعه والعارد والعالم
DESCRIPTION OF THE PARTY OF THE	The or a ready	BY P. SPATE STREET	न्द्रक्रमा स्टार स्ट्रीनी का प्रकृत	CYNTUST AFTERN	लाम् प्राची संस्था	antibut nabersi	AND PARTY OF	referenci militale	STATE LEGISTAN
Planned Survey	fij Meson ree presidence	and seeming the seeming of the section		a market and the state of the s	: No description of the second	wife angular parameters and state point	allegation of seasons assume these	nia making namatan mana di Manasana	not object this was made to their description of
PARTY OF THE STATE		A to the first			reko walenda	dian's wife		and many production	
Measured		3-15 X 14	Vertical :		學表示(學是	ertical	Dogleg	Build .	Turn
The state of the s			STORY OF THE STORY		AND THE RESERVE	the state of the state of	200 - 1 market	· · · · · · · · · · · · · · · · · · ·	Standard Co., William Supplied to
「中国20年」とが発展したされては、新知され、大学、大学の多数なです。	iclination 🐫	Azimuth	Depth	: <sub>-4</sub> +N/-S: '``````.	+E/-W	ection	Rate	Rate	Rate:
(usft)	(2)"	j. (°)	ر (usft) و الم	(usft)	"(usft) 🏎 🗟 🥶	(usft) 🚅 🦭 (	/100usft) (	°/100usft) 🧎 🖟 (%	100usft)
			Here's Comment						ar and the same
8,800.0	0.00	0.00 •	8,800.0	0,0	0.0	0.0	0.00	0.00	0.00
Bone Spg. Lowe	er Avalon Shale	e .		1.4					State of the state of
8,856.0	0.00	0.00	8,856.0	0.0	0.0	0.0	0.00	0.00	0.00
8,900.0	0.00	0.00	8,900.0	0.0 .	0.0	0.0	0.00	0.00	0.00
8,900.0	0.00	0.00	0,900.0	0,0 .	0.0	0.0	0.00	0.00	0.00
9,000.0	0.00	0.00	9.000.0	0.0	0.0	0.0	0.00	0.00	0.00
9,100.0	0.00	0.00	9,100.0	0.0	0.0	0.0	0.00	0.00	0.00
		9.00	0,100.0		• • • • • • • • • • • • • • • • • • • •			0.00	
1st Bone Spring	<u>-</u>								
. 9,196.0	0.00	0.00	9,196.0	0.0	0.0	0.0	0.00	0.00	0.00
9,200.0	0.00	0.00	9,200.0	0.0	0.0	0.0	0.00	0.00	0.00
9,300.0	0.00	0.00	9,300.0	0.0	0.0	0.0	0.00	0.00	0.00
_	•				•		•	• .	
1st Bone Spring	Ss.							1	
9,387.0	0.00	0.00	9,387.0	0.0	0.0	0.0	0.00	0.00	0.00
9,400.0	0.00	. 0.00	9,400.0	0.0	0.0	0.0	0.00	0.00	0.00
9,500.0	0.00	0.00	9,500.0	0.0	0.0	0.0	0.00	0.00	0.00
9,600.0	0.00	0.00	9,600.0	0.0	0.0	0.0	0.00	0.00	0.00
1									
9,700.0	0.00	0.00	9,700.0	0.0	0.0	0.0	0.00	0.00	0.00
2nd Bone Spring	a Carb								
, ,	• .	0.00	0.770.0	0.0	0.0			0.00	
9,776.0	0.00	0.00	9,776.0	0.0	0.0	0.0	0.00	0.00	0.00
9,800.0	0.00	0.00	9,800.0	0.0	0.0	0.0	0.00 .	0.00	0.00
9,900.0	0.00	. 0.00	9,900.0	0.0	0.0	0.0	0.00	0.00	0.00
2nd Bone Spring	q Ss.					•			
9,973.0	0.00	0.00	9,973.0	0.0	0.0	0.0	0.00	0.00	0.00
10,000.0	0.00	0.00	10,000.0	0.0	0.0	0.0	0.00	0.00	0.00
10,000.0	0.00	0.00	10,000.0	0.0	0.0	0.0	0.00	, 0.00	0.00
10,100.0	0.00	0.00	10,100.0	0.0	0.0	0.0	0.00	0.00	0.00
10,200.0	0.00	0.00	10,200.0	0.0	0.0	0,0	0.00	0.00	0.00
10,300.0	0.00	0.00	10,300.0	0.0	0.0	0.0	0.00	0.00	0.00
10,400.0	0.00	0.00	10,400.0	0.0	0.0			0.00	,
· · · · · · · · · · · · · · · · · · ·		0.00	10,400.0	. 0.0	0.0	0.0	0.00	0.00	0.00
3rd Bone Spring	g Carb.	-							
10,482.0	0.00	0.00	10,482.0	0.0	0.0	0.0	0.00	0.00	0.00
10,500.0	0.00	0.00	10,500.0	0.0	0.0	0.0	0.00	0.00	0.00
10,600.0	0.00	0.00	10,600.0	0.0	0.0	0.0	0.00	0.00	0.00
10,700.0	0.00	0.00	10,700.0	0.0	• 0.0	0.0	0.00	0.00	0.00
10,800.0	0.00	0.00	10,800.0	0.0	0.0	0.0	0.00	0.00	0.00
10,900.0	0.00	0.00	10,900.0	. 0.0	0.0	0.0	0.00	0.00	0.00
								1	
11,000.0	0.00	0.00	11,000.0	0.0	0.0	0.0	0.00	0.00	0.00
Build 10°/100'		Same of the							
11,091.1	0.00	0.00	11,091.1	0.0	0.0	0.0	0.00	0.00	0.00
11,100.0	0.89	110.00	11,100.0	0.0	0.1	0.0	10.00	10.00	0.00
11,150.0	5,89	110.00	11,149.9	-1.0	2.8	1.2	10.00	10.00	0.00
									•
11,200.0	10.89	110.00	11,199.3	· <b>-3</b> .5	9.7	4.0	10.00	10.00	0.00
3rd Bone Spring	. Se	and the second	, 4				1.50		
		110.00	11 220 0	5.0	42.0		10.00	10.00	
11,221.1	- 13.00	110.00	11,220.0	<b>-</b> 5.0	13.8	5.6	10.00	10.00	0.00
11,250.0	15.89	110.00	11,248.0	-7.5	20.6	8.4	10.00	10.00	0.00
11,300.0	20.89	110.00	11,295.4	<i>-</i> 12.9	35.4	14.4	10.00	10.00	0.00
11,350.0	25.89	110.00	11,341.3	-19.7	54.0	22.0	10.00	10.00	0.00
11,400.0	30.89	110.00	11,385.3	-27.8	76.4	31.2	10.00	10.00	0.00
								•	
11,450.0	35.89	110.00	11,427.0	· -37.2	102.2	41.7	10.00	10.00	0.00
War Wink Ss.			1	18 18 18 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Carrier Garage	er e e e e e e e e e e e	at an extra	
11,476.4	38.53	110.00	11,448.0	-42.7	117.2	47.8	10.00	10.00	0.00
1 .									
11,500.0	40.89	110.00	11,466.2	-47.8 50.0	131.4	53.6	10.00	10.00	0.00
11,550.0	45.89	110.00	11,502.5	-59.6	163.7	66.8	, 10.00	10.00	0.00
ÉOB @ 50:00° Ir	nc / 110.00° Azı	m - Build 10°/10	00' 🖈	ويجيؤها بولوج الأقال			18 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
11,591.1	50.00	110.00	11,530.0	-70.0	192.3	78.5	10.00	10.00	0.00



Database: Company: EDM 5000.1 Single User Db

XTO ENERGY, INC. Eddy County, NM Sec 15, T24S, R31E

PLU 15 Twin Wells Ranch #104H

Well: Wellbore #1

Local Co-ordinate Reference TVD Reference MD Reference North Reference: Survey Calculation Method:

Well PLU 15 Twin Wells Ranch #104H KB=22 @ 3561.0usft (Akita #22).

KB=22 @ 3561.0usft (Akita #22) Grid

Minimum Curvature

Section   Sect	Design: 🎉 👢 🕒 .	Design #1	and the second second	an in the Association in the American Institution in the				ang adam taka dagan daga kanan panggan	Bitalytine Automotivasya no systematy nei region y su party.	State Commission of the commis	
	Planned Survey	aran da est. M	THE PROPERTY OF THE	Andreas and the second	THE STATE OF STREET	eron constins	er ann mae'r daig y ar goll	WARRING THE BUILDING	Peneral Personal Appropria	eosgerikiikiik	
Popt   Spring   Company	R. W. Walter State				A STATE OF THE STA	建设有管理			inerte		
Popt   Spring   Company	Measured			Vertical			Vertical	Dogleg	Build	Turn	
11,600	18 年 - 大学 - 大学   大学 大学   大学   大学   大学   大学	nclination	Azimuth	2. 質量がどものにつている	+N/-S	FF/-W	The state of the s		THE PERSON OF TH	State of the state	
11,000,0   50,1   11,13   11,5357   7.24   18,67   198,7   81,1   10,00   2.75   12.39	EREST 1 4: 20 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(2)	(8)	· 1000年11月1日 11月1日 11月1	THE PARTY OF THE PARTY OF	BANGAL CALLSON	CONTRACTOR OF THE PROPERTY OF	是是"其他"的文化,在"是"在"是"是	THE PARTY OF THE P	TO THE PERSON OF	
11,650.0   51,59   117.32   11,867.3   -88.3   234.1   98.8   10.00   2.75   12.39									The Call	THE STATE OF THE	THE
11,680.0   51,59   117.32   11,687.3   -88.3   234.1   98.6   10,00   2.75   12.39	11,600.0	50.21	111,13	11,535.7	-72.4	198.7	81. <b>1</b>	10.00	2.36	12.67	
11,660.9 51.93 118.64 11,574.0 92.3 241.6 103.0 10.00 3.14 12.08 11,700.0 53.28 123.26 11,597.8 1083.3 268.2 120.1 10.00 3.44 118.2 11,700.0 55.25 128.93 11,827.0 -132.2 301.0 145.5 10.00 3.44 11.33 11.800.0 57.4 134.31 11.854.7 -158.9 332.1 174.5 10.00 4.44 10.77 Wolfcamp Sh 11.855.1 57.5 134.95 11.858.0 -163.5 335.8 178.3 10.00 4.69 10.46 Wolfcamp X 5d 11.858.0 -163.5 335.8 178.3 10.00 4.69 10.46 Wolfcamp X 5d 11.858.0 -163.5 335.8 178.3 10.00 4.69 10.46 Wolfcamp X 5d 11.859.0 58.0 18.0 18.0 18.0 18.0 18.0 18.0 18.0 1	11,650.0	51.59	117.32	11,567.3	-88.3	234.1	98.6				1
11,700.0 \$52.8 123.26 11,597.8 -106.3 288.2 120.1 10.00 3.44 11.82 11,760.0 \$5.25 128.93 11.827.0 -132.2 30.10 145.5 10.00 3.94 11.33 11.80.0 \$7.47 134.31 11,654.7 -159.9 332.1 174.5 10.00 4.44 10.77 Worksamp Sh 11.800.1 \$7.75 134.95 11,658.0 -163.5 335.8 178.3 10.00 4.69 10.46 Worksamp X Sd 11.84.0 \$1.33 11.82.0 1 \$7.75 134.95 11,658.0 -163.5 335.8 178.3 10.00 4.69 10.46 Worksamp X Sd 11.84.6 \$1.38.8 11.678.0 -163.5 335.8 178.3 10.00 4.69 10.46 Worksamp X Sd 11.84.6 \$1.38.8 11.678.0 -187.5 388.2 203.2 10.00 4.88 10.22 11.890.0 6.5.3 144.27 11,704.8 -225.5 388.3 242.5 10.00 5.25 9.71 11.900.0 6.5.3 144.27 11,704.8 -225.5 388.3 242.5 10.00 5.25 9.71 11.900.0 6.5.2 148.90 11,726.8 -263.0 413.0 281.0 10.00 5.57 9.25 12.000.0 68.24 153.31 17,746.5 -303.2 435.2 322.2 10.00 5.84 8.83 Worksamp Y Sd 12.026.6 69.84 155.59 11,756.0 -325.6 445.9 345.0 10.00 5.87 8.83 12.100.0 74.49 156.8 11,778.0 -325.6 445.9 345.0 10.00 6.02 8.55 12.100.0 74.49 156.8 11,778.0 -325.6 445.9 345.0 10.00 6.02 8.55 12.100.0 74.49 156.8 11,778.0 -325.6 445.9 345.0 10.00 6.22 8.39 12.100.0 77.60 165.60 11,778.0 -325.6 445.9 345.0 10.00 6.22 8.17 12.250.0 8.85 159.46 11,778.0 -380.6 411.3 411.1 10.00 6.25 8.17 12.250.0 8.85 159.46 11,806.0 5.29.0 502.4 455.0 458.2 10.00 6.60 6.51 7.73 Worksamp A Sh. 12.244.8 8.3.60 172.86 11,806.0 5.29.0 502.4 455.0 10.00 6.52 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 507.2 605.7 10.00 6.62 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 507.2 605.7 10.00 6.62 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 508.2 50.7 10.00 6.62 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 508.2 50.7 10.00 6.62 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 508.2 50.7 10.00 6.62 7.54 12.250.0 8.80 179.62 11,811.0 -618.8 508.2 50.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Red Hills Ss.	F	1 7 %	677							
11,750.0 55.25 128,93 11,627.0 -132.2 301.0 145.5 10.00 3,94 11,33 11,800.0 57.47 134.31 11,654.7 -159.9 332.1 174.5 10.00 4.44 10,77	11,660.9	51.93	118.64	11,574.0	-92.3	241.6	103.0	10.00	3.14	12.09	,
### 11,880.0	11,700.0	53.28	123.26	11,597.8	-108.3	268.2	120.1	10.00	3.44		
Workcamp SN   11,806.1   57.75   134.95   11,658.0   -163.5   335.8   178.3   10.00   4.69   10.46   Workcamp X Sct   11,880.0   59.63   138.88   11,678.0   -157.5   358.2   203.2   10.00   4.88   10.02   11,880.0   59.63   139.42   11,880.7   -191.0   361.3   206.9   10.00   5.05   9.99   37.1   11,990.0   62.53   144.27   11,704.8   -263.0   413.0   221.0   10.00   5.57   9.25   37.1   11,990.0   63.24   143.01   11,746.5   -303.2   435.2   322.2   10.00   5.57   9.25   12,000.0   68.24   153.31   11,746.5   -303.2   435.2   322.2   10.00   5.84   8.83   Workcamp X Sct   12,000.0   71.27   157.55   11,766.0   -325.6   445.9   345.0   10.00   6.02   8.55   12,000.0   71.27   157.55   11,766.0   -325.6   445.9   345.0   10.00   6.02   8.55   12,000.0   74.40   151.64   11,778.6   -306.6   471.3   411.1   10.00   6.25   8.17   12,150.0   77.60   165.66   11,790.7   437.2   485.0   459.2   10.00   6.25   8.17   12,200.0   80.85   169.46   11,800.0   485.1   495.5   506.6   10.00   6.51   7.73   12,200.0   80.85   169.46   11,800.0   485.1   495.5   506.6   10.00   6.51   7.73   12,200.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   500.7   500.0   0.00   0.00   0.00   0.00   0.	. 11,750.0	55.25	128.93	11,627.0	-132.2	301.0	145.5	10.00	3.94	11.33	
Workcamp SN   11,806.1   57.75   134.95   11,658.0   -163.5   335.8   178.3   10.00   4.69   10.46   Workcamp X Sct   11,880.0   59.63   138.88   11,678.0   -157.5   358.2   203.2   10.00   4.88   10.02   11,880.0   59.63   139.42   11,880.7   -191.0   361.3   206.9   10.00   5.05   9.99   37.1   11,990.0   62.53   144.27   11,704.8   -263.0   413.0   221.0   10.00   5.57   9.25   37.1   11,990.0   63.24   143.01   11,746.5   -303.2   435.2   322.2   10.00   5.57   9.25   12,000.0   68.24   153.31   11,746.5   -303.2   435.2   322.2   10.00   5.84   8.83   Workcamp X Sct   12,000.0   71.27   157.55   11,766.0   -325.6   445.9   345.0   10.00   6.02   8.55   12,000.0   71.27   157.55   11,766.0   -325.6   445.9   345.0   10.00   6.02   8.55   12,000.0   74.40   151.64   11,778.6   -306.6   471.3   411.1   10.00   6.25   8.17   12,150.0   77.60   165.66   11,790.7   437.2   485.0   459.2   10.00   6.25   8.17   12,200.0   80.85   169.46   11,800.0   485.1   495.5   506.6   10.00   6.51   7.73   12,200.0   80.85   169.46   11,800.0   485.1   495.5   506.6   10.00   6.51   7.73   12,200.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   87.47   177.00   11,810.2   583.8   507.2   605.7   10.00   6.64   7.50   12,300.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   705.6   0.00   0.00   0.00   0.00   12,800.0   89.80   179.62   11,811.3   463.7   500.7   500.7   500.0   0.00   0.00   0.00   0.00   0.	11.800.0	57.47	134.31	11.654.7	-159.9	332 1	174 5	10.00	4 44	10.77	1
11,806.1   57,75   134.95   11,658.0   -163.5   335.8   178.3   10,00   4,69   10,46	Wolfcamp Sh								,		į
Wolfcamp X St  11,844.6	,	57.75	134.95	11.658.0	-163.5	335.8	178.3	10.00	4.69	10.46	.
11,844.6	i .			•						10,10	
11,850.0 59,90 139,42 11,860,7 - 191.0 361.3 206.9 10.00 5.05 9.99 11,900.0 62.53 144.27 11,704.8 -225.5 388.3 242.5 10.00 5.25 9.71 11,950.0 62.53 144.890 11,726.8 -263.0 413.0 281.0 10.00 5.57 9.25 12,000.0 68.24 153.31 11,746.5 -303.2 435.2 322.2 10.00 5.84 8.83 Wolfcamp Y Sd			138,88	11,678.0	-187.5	358.2	203.2	10.00	4.88	10 22	İ
11,900.0 62.53 144.27 11,704.8 225.5 388.3 242.5 10.00 5.25 9.71 11,950.0 65.32 148.90 11,768.8 -263.0 413.0 281.0 10.00 5.67 9.25 12,000.0 68.24 153.31 11,746.5 -303.2 435.2 322.2 10.00 5.84 8.83 Wolfcamp Y Sd 12,026.6 69.84 155.59 11,756.0 -325.6 445.9 345.0 10.00 6.02 8.55 12,050.0 71.27 157.55 11,763.8 -345.9 454.6 365.7 10.00 6.12 8.39 12,100.0 74.40 161.64 11,776.6 -390.6 471.3 411.1 10.00 6.25 8.17 12,150.0 77.60 165.60 11,790.7 437.2 485.0 458.2 10.00 6.40 7.92 12,200.0 80.85 169.46 11,800.0 -485.1 495.5 506.6 10.00 6.51 7.73 Wolfcamp A Sh. 12,244.8 83.80 172.86 11,800.0 5.290.0 502.4 550.7 10.00 6.62 7.54 12,300.0 87.47 177.00 11,810.2 583.8 507.2 605.7 10.00 6.62 7.54 12,300.0 87.47 177.00 11,810.2 583.8 507.2 605.7 10.00 6.62 7.54 12,400.0 89.80 179.62 11,811.0 618.8 508.2 640.7 10.00 6.66 7.46 12,400.0 89.80 179.62 11,811.3 683.7 508.7 508.7 10.00 6.66 7.46 12,400.0 89.80 179.62 11,811.3 883.7 508.7 508.7 508.0 0.00 0.00 0.00 12,500.0 89.80 179.62 11,811.3 883.7 508.3 805.5 0.00 0.00 0.00 0.00 12,500.0 89.80 179.62 11,811.3 883.7 508.3 805.6 0.00 0.00 0.00 0.00 12,500.0 89.80 179.62 11,811.3 883.7 508.3 805.6 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,811.3 883.7 510.0 905.5 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,813.3 893.7 510.7 1,005.4 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,813.7 1.837.7 512.7 1,005.2 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,813.7 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,813.7 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,813.7 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,814.1 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,814.1 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,814.1 1.183.7 510.0 1,505.1 0.00 0.00 0.00 0.00 0.00 13,000.0 89.80 179.62 11,814.5 1.183.7 510.7 1,505.1 0.00 0.00 0.00 0.00 0.00 0.00 0.00	-										
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12,000.0   68.24   153.31   11,746.5   -303.2   435.2   322.2   10.00   5.84   8.83	11,950.0	65.32	148 90	11 726 R	-263 O	413.0	281 N	10.00	5 57		
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12,800.0       89.80       179.62       11,812.7       -1,083.7       511.4       1,105.3       0.00       0.00       0.00         12,900.0       89.80       179.62       11,813.0       -1,183.7       512.0       1,205.3       0.00       0.00       0.00         13,000.0       89.80       179.62       11,813.4       -1,283.7       512.7       1,305.2       0.00       0.00       0.00         13,100.0       89.80       179.62       11,813.7       -1,383.7       513.4       1,405.1       0.00       0.00       0.00         13,200.0       89.80       179.62       11,814.4       -1,583.7       514.0       1,505.1       0.00       0.00       0.00         13,300.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.5       -1,783.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.5       -1,833.7			,								Ì
12,900.0       89.80       179.62       11,813.0       -1,183.7       512.0       1,205.3       0.00       0.00       0.00         13,000.0       89.80       179.62       11,813.4       -1,283.7       512.7       1,305.2       0.00       0.00       0.00         13,100.0       89.80       179.62       11,813.7       -1,383.7       513.4       1,405.1       0.00       0.00       0.00         13,200.0       89.80       179.62       11,814.1       -1,483.7       514.0       1,505.1       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.8       -1,683.7       515.4       1,704.9       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.5       -1,833.7       516.0       1,804.8       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.5       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.5       -2,183.7			•								
13,000.0       89.80       179.62       11,813.4       -1,283.7       512.7       1,305.2       0.00       0.00       0.00         13,100.0       89.80       179.62       11,813.7       -1,383.7       513.4       1,405.1       0.00       0.00       0.00         13,200.0       89.80       179.62       11,814.4       -1,583.7       514.0       1,505.1       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,400.0       89.80       179.62       11,815.1       -1,783.7       516.0       1,804.8       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.5       -1,883.7       516.7       1,904.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.5       -2,183.7											
13,100.0       89.80       179.62       11,813.7       -1,383.7       513.4       1,405.1       0.00       0.00       0.00         13,200.0       89.80       179.62       11,814.1       -1,483.7       514.0       1,505.1       0.00       0.00       0.00         13,300.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,500.0       89.80       179.62       11,814.8       -1,683.7       515.4       1,704.9       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.5       -1,883.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.8       -1,983.7       516.7       1,904.8       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.5       -2,183.7				,							
13,200.0       89.80       179.62       11,814.1       -1,483.7       514.0       1,505.1       0.00       0.00       0.00         13,300.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.8       -1,683.7       515.4       1,704.9       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.1       -1,783.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.8       -1,983.7       516.7       1,904.8       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       518.7       2,204.6       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.9       -2,383.7	l -						•				.
13,300.0       89.80       179.62       11,814.4       -1,583.7       514.7       1,605.0       0.00       0.00       0.00         13,400.0       89.80       179.62       11,814.8       -1,683.7       515.4       1,704.9       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.5       -1,883.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.5       -1,883.7       516.7       1,904.8       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,817.2       -2,383.7       519.4       2,304.5       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7	i										
13,400.0       89.80       179.62       11,814.8       -1,683.7       515.4       1,704.9       0.00       0.00       0.00         13,500.0       89.80       179.62       11,815.1       -1,783.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.8       -1,983.7       516.7       1,904.8       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.5       -2,183.7       518.0       2,104.6       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.8       -2,283.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7	13 300 0	89.80	179.62	11 814 4	-1 583 7	514.7	1 605 0	0.00			İ
13,500.0       89.80       179.62       11,815.1       -1,783.7       516.0       1,804.8       0.00       0.00       0.00         13,600.0       89.80       179.62       11,815.5       -1,883.7       516.7       1,904.8       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.6       -2,783.7											
13,600.0       89.80       179.62       11,815.5       -1,883.7       516.7       1,904.8       0.00       0.00       0.00       0.00         13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.9       -2,583.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,818.2       -2,683.7       521.4       2,604.3       0.00       0.00       0.00         14,600.0       89.80       179.62       11,818.6											
13,700.0       89.80       179.62       11,815.8       -1,983.7       517.4       2,004.7       0.00       0.00       0.00         13,800.0       89.80       179.62       11,816.2       -2,083.7       518.0       2,104.6       0.00       0.00       0.00         13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.2       -2,683.7       522.0       2,704.2       0.00       0.00       0.00         14,500.0       89.80       179.62       11,818.6       -2,783.7											1
13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.2       -2,683.7       522.0       2,704.2       0.00       0.00       0.00         14,500.0       89.80       179.62       11,818.6       -2,783.7       522.7       2,804.1       0.00       0.00       0.00         14,600.0       89.80       179.62       11,818.9       -2,883.7       523.4       2,904.1       0.00       0.00       0.00         14,700.0       89.80       179.62       11,819.3       -2,983.7	13,700.0	89.80	179.62	11,815.8		517.4					1
13,900.0       89.80       179.62       11,816.5       -2,183.7       518.7       2,204.6       0.00       0.00       0.00         14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.2       -2,683.7       522.0       2,704.2       0.00       0.00       0.00         14,500.0       89.80       179.62       11,818.6       -2,783.7       522.7       2,804.1       0.00       0.00       0.00         14,600.0       89.80       179.62       11,818.9       -2,883.7       523.4       2,904.1       0.00       0.00       0.00         14,700.0       89.80       179.62       11,819.3       -2,983.7	13 800.0	89 80	179 62	11.816.2	-2.083 7	518.0	2.104.6	, 0.00	0.00	0.00	
14,000.0       89.80       179.62       11,816.8       -2,283.7       519.4       2,304.5       0.00       0.00       0.00         14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.2       -2,683.7       522.0       2,704.2       0.00       0.00       0.00         14,500.0       89.80       179.62       11,818.6       -2,783.7       522.7       2,804.1       0.00       0.00       0.00         14,600.0       89.80       179.62       11,818.9       -2,883.7       523.4       2,904.1       0.00       0.00       0.00         14,700.0       89.80       179.62       11,819.3       -2,983.7       524.1       3,004.0       0.00       0.00       0.00         14,800.0       89.80       179.62       11,819.6       -3,083.7	•	The second second									
14,100.0       89.80       179.62       11,817.2       -2,383.7       520.0       2,404.4       0.00       0.00       0.00       0.00         14,200.0       89.80       179.62       11,817.5       -2,483.7       520.7       2,504.3       0.00       0.00       0.00         14,300.0       89.80       179.62       11,817.9       -2,583.7       521.4       2,604.3       0.00       0.00       0.00         14,400.0       89.80       179.62       11,818.2       -2,683.7       522.0       2,704.2       0.00       0.00       0.00         14,500.0       89.80       179.62       11,818.6       -2,783.7       522.7       2,804.1       0.00       0.00       0.00         14,600.0       89.80       179.62       11,818.9       -2,883.7       523.4       2,904.1       0.00       0.00       0.00         14,700.0       89.80       179.62       11,819.3       -2,983.7       524.1       3,004.0       0.00       0.00       0.00         14,800.0       89.80       179.62       11,819.6       -3,083.7       524.7       3,103.9       0.00       0.00       0.00	1										
14,300.0     89.80     179.62     11,817.9     -2,583.7     521.4     2,604.3     0.00     0.00     0.00       14,400.0     89.80     179.62     11,818.2     -2,683.7     522.0     2,704.2     0.00     0.00     0.00       14,500.0     89.80     179.62     11,818.6     -2,783.7     522.7     2,804.1     0.00     0.00     0.00       14,600.0     89.80     179.62     11,818.9     -2,883.7     523.4     2,904.1     0.00     0.00     0.00       14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00	1 .	89.80	179.62	11,817.2							-
14,400.0     89.80     179.62     11,818.2     -2,683.7     522.0     2,704.2     0.00     0.00     0.00       14,500.0     89.80     179.62     11,818.6     -2,783.7     522.7     2,804.1     0.00     0.00     0.00       14,600.0     89.80     179.62     11,818.9     -2,883.7     523.4     2,904.1     0.00     0.00     0.00       14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00	14,200.0	89.80	179.62	11,817.5	-2,483.7	520.7	2,504.3	0.00	0.00	0.00	İ
14,400.0     89.80     179.62     11,818.2     -2,683.7     522.0     2,704.2     0.00     0.00     0.00       14,500.0     89.80     179.62     11,818.6     -2,783.7     522.7     2,804.1     0.00     0.00     0.00       14,600.0     89.80     179.62     11,818.9     -2,883.7     523.4     2,904.1     0.00     0.00     0.00       14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00	14 300 0	89.80	179.62	11 817 0	-2 583 7	521 A	2 604 3	. 0.00	0.00	0.00	
14,500.0     89.80     179.62     11,818.6     -2,783.7     522.7     2,804.1     0.00     0.00     0.00       14,600.0     89.80     179.62     11,818.9     -2,883.7     523.4     2,904.1     0.00     0.00     0.00       14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00							•	•			
14,600.0     89.80     179.62     11,818.9     -2,883.7     523.4     2,904.1     0.00     0.00     0.00       14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00											
14,700.0     89.80     179.62     11,819.3     -2,983.7     524.1     3,004.0     0.00     0.00     0.00       14,800.0     89.80     179.62     11,819.6     -3,083.7     524.7     3,103.9     0.00     0.00     0.00											. 1
				•							.
	14 800 0	20 20	179.62		-3 083 7						
	14,900.0		179.62	11,820.0	-3,183.7	525.4	3,203.8	0.00	0.00	0.00	





Database Company: Project: Site Well: EDM 5000.1 Single User Db XTO ENERGY, INC. Eddy County, NM

Sec 15, T24S; R31E

PLU 15 Twin Wells Ranch #104H Wellbore #1 Local Co-ordinate Reference:

TVD Reference: MD Reference: North Reference:

Survey Calculation Method

Well PLU 15 Twin Wells Ranch #104H

KB=22 @ 3561 Ousft (Akita #22) KB=22 @ 3561 Ousft (Akita #22)

Grid Minimum Curvature

Wellbore Wellbore #1
Design Design #1

Planned S		gerimaninesia A	PROPERTIES LA LINGUE	ining manager		electrician and an electrician	months and a series	PARTICIPATE PORTAR PROPERTY.	NAMES OF THE PARTY	en derrett inder betreit bestimmt.
			数例的基							在7分配套10
1 - 1 - 2 - 2 - 2 - 20 LEG	leasured -			Vertical			Vertical,	Dogleg 👍 🖟	Build	Turn
14453	the state of the s	clination, 😘 🔏		Depth: 📏	+N/-S	+E/-W	Section	Rate	Rate	Rate
	(usft)	$(\hat{\mathfrak{q}})$ is $\hat{\mathfrak{q}}$	(°)	(usft)	(usft) 🕮 🚁	∵√(usft)≽√ ;	ૂ (usft) ૄ	(°/100usft)⊊ .≦(	'/100usft) (°	/100usft)
* ***	15,000.0	89.80	179.62	11,820.3	-3,283.7	526.1	3,303.8	0.00	0.00	0.00
	15,100.0	89.80	179.62	11,820.7	-3,383.7	526.7	3,403.7	0.00	0.00	0.00
	15,200.0	89.80	179.62	11,821.0	-3,483.7	527.4	3,503.6	0.00	0.00	0.00
	15,300.0	89.80	179.62	11,821.4	-3,583.6	528.1	3,603.5	0.00	0.00	0.00
İ	15,400.0	89.80	179.62	11,821.7	-3,683.6	528.7		0.00	0.00	0.00
	15,500.0	89.80	179.62	11,822.1	-3,783.6	529.4	3,803.4	0.00	0.00	0.00
	15,600.0	89.80	179.62	11,822.4	-3,883.6	530.1	3,903.3	0.00	0.00	0.00
	15,700.0	89.80	179.62	11,822.8	-3,983.6	530.7	4,003.3	0.00	0.00	0.00
	15,800.0	89.80	179.62	11,823.1	-4,083.6	531.4	4,103.2	0.00	0.00	0.00
Ì	15,900.0	89.80	179.62	11,823.5	-4,183.6	532.1	4,203.1	0.00	0.00	0.00
	16,000.0	89.80	179.62	11,823.8	•	532.7	4,303.0	. 0.00	0.00	0.00
	16,100.0 16,200.0	89.80 89.80	179.62 179.62	11,824.2 11,824.5	-4,383.6 -4,483.6	533.4 534.1	4,403.0 4,502.9	0.00 0.00	0.00 0.00	0.00 0.00
						•				
	16,300.0	89,80	179.62	11,824.9	-4,583.6 4,683.6	534.7	4,602.8	0.00	0.00	0.00
	16,400.0 16,500.0	89.80 89.80	179.62 179.62	11,825.2 11,825.6	-4,683.6 -4.783.6	535.4 536.1	4,702.8	0.00	0.00	0.00
	16,600.0	89.80 89.80	179.62	11,825.6	-4,783.6 -4,883.6	536,1 536,8	4,802.7 4,902.6	0.00 0.00	0,00 0,00	0.00 0.00
	16,700.0	89.80	179.62	11,826.3	-4,983.6	537.4	5,002.5	0.00	0.00	0.00
		89.80								
1	16,800.0 16,900.0	89.80	179.62 179.62	11,826.6 11,827.0	-5,083.6 -5,183.6	538.1 538.8	5,102.5 * 5,202.4	0.00	0.00 0.00	0.00 0.00
	17,000.0	89.80	179.62	11,827.3	-5,283.6	539.4	5,302.3	0.00	0.00	0.00
Ì	17,100.0	89.80	179.62	11,827.7	-5,383.6	540.1	5,402.3	0.00	.0.00	0.00
	17,200.0	89.80	179.62	11,828.0	-5,483.6	540.8	,	0.00	0.00	0.00
	17,300.0	89.80	179.62	11,828.4	-5,583.6	541.4	5,602.1	0.00	0.00 <b>n</b>	0.00
	17,400.0	89.80	179.62	11,828.7	-5,683.6	542.1	5,702.0	0.00	0.00 <b>g</b> 0.00	0.00
ł	17,500.0	89.80	179.62	11,829.1	-5,783.6	542.8	5,802.0	0.00	0.00	0.00
	17,600.0	89.80	179.62	11,829.4	-5,883.6	543.4	5,901.9	0.00	0.00	0.00
	17,700.0	89.80	179.62	11,829.8	-5,983.6	544.1	6,001.8	0.00	0.00	0.00
	17,800.0	89.80	179.62	11,830.1	-6,083.6	544.8	6,101.8	0.00	0.00	0.00
	17,900.0	89.80	179.62	11,830.5	-6,183.6	545.4	6,201.7	0.00	0.00	0.00
	18,000.0	89.80	179.62	11,830.8	-6,283.6	546.1	6,301.6	0.00	0.00	0.00
	18,100.0	89.80	179.62	11,831.2	-6,383.6	- 546.8	6,401.5	0.00	0.00	0.00
	18,200.0	89.80	179.62	11,831.5	-6,483.6	547.4	6,501.5	0.00	0.00	0.00
,	18,300.0	89.80	179.62	11,831.9	-6,583.6	548.1	6,601.4	0.00	0.00	0.00
	18,400.0	89.80	179.62	11,832.2	-6,683.6	548.8	6,701.3	0.00	0.00	0.00
	18,500.0	89.80	179.62	11,832.6	-6,783.6	549.4	6,801.3	0.00	0.00	0.00
	18,600.0 18;700.0	89.80 89.80	179.62 179.62	11,832.9 11,833.3	-6,883.6 <del>-</del> 6,983.6	550.1 550.8	6,901.2	0.00	0.00	0.00 0.00
							7,001.1		0.00	
	18,800.0	89.80	179.62	11,833.6	-7,083.5	551.5	7,101.0	0.00	0.00	0.00
	18,900.0 19,000.0	89.80	179.62 179.62	. 11,834.0	-7,183.5 -7,283.5	552.1 552.8	7,201.0 7,300.9	0.00 0.00	0.00	0.00
	19,000.0	89.80 89.80	179.62	11,834,3 11,834.7	-7,283.5 -7,383.5	552,8 553.5	7,300.9 7,400.8	0.00	0.00 0.00	0,00 0.00
,	19,200.0	89.80	179.62	11,835.0	-7,483.5	554.1	7,500.8	0.00	0.00	0.00
1							* *			
	19,300.0 19,400.0	89.80 89.80	179.62 179.62	11,835.3 11,835.7	-7,583.5 -7,683.5	554.8 555.5	7,600.7 7,700.6	0.00 0.00	0.00 0.00	0.00
	19,400.0	89.80	179.62	11,836.0	-7,063.5 -7,783.5	556.1	7,700.6	0.00	0.00	0.00
	19,600.0	89.80	179.62	11,836.4	-7,883.5	556.8	7,900.5	0.00	0.00	0.00
	19,700.0	89.80	179.62	11,836.7	-7,983.5	557.5	8,000.4	0.00	0.00	0.00
	19,800.0	89.80	179.62	11,837.1	-8,083.5	558.1	8,100.3	0.00	0.00	0.00
	19,800.0	89.80	179.62	11,837.1	-6,063.5 -8,183.5	558.8	8,200.3	0.00	0.00	0.00
	20,000.0	. 89.80	179.62	11,837.8	-8,283.5	559.5	8,300.2	0.00	0.00	0.00
	20,100.0	89.80	179.62	11,838.1	-8,383.5	560.1	8,400.1	0.00	0.00	0.00
	20,200.0	89.80	179.62	11,838.5	-8,483.5	560.8	8,500.0	0.00	0.00	0.00
	20,300.0	89.80	179.62	11,838.8	-8,583.5	561.5	8,600.0	0.00	0.00	0.00
L	£0,000.0	55.00	110.02	11,000.0	5,505.5	301.5	0,000.0	3.00	0.00	0.00





EDM 5000.1 Single User Db XTO ENERGY, INC. Database: Company: Project:
Site
Well:
Wellbore
Design

Eddy County, NM Sec 15, T24S, R31E

PLU 15 Twin Wells Ranch #104H

Wellbore #1 Design #1

Local Co-ordinate Reference : TVD Reference: MD Reference: North Reference:

Survey Calculation Method:

Well PLU 15 Twin Wells Ranch #104H

KB=22 @ 3561 0 usft (Akita #22) KB=22 @ 3561.0usft (Akita #22).

Grid ·

Minimum Curvature

Design:	Design #1		and the state of t	- man seemed to be her			orta a morama terresimana maistra	iona birrooma war nalanarraanianian	To commission where it is a summarished with the
	THE PRESENCE	nine leweståeniu	CANTERNATION NAMED IN	TO CONTRACTOR TO THE	RIF DOWN WY. I'V	and with the second	TARREST THE THE	BY CONTROL TREESE	DEFENSE OF THE DATE
Planned Survey	vitalin gradens non	n entreprint of		N DANSE STREET	Y 一颗磷酸 下面 to	AND THE PROPERTY	Cantalygias mail a	and the state of t	สะบางจะหมรมตัดของไ
	51.746.94.9				<b>邓</b> ·蓬···································				
Measured			· Vertical · .			Vertical	Dogleg 🗼 🕌	Build 📖 🤲	Turn
/ Depth	Inclination	Azimuth, '	≥ Depth :	+N/-S	+E/-W	Section	Rate	Rate	Rate. 🔭 🚈
(usft)	(0)	) - (°) (°)	ં (usft)ત્≟ે વ	(usft)	(usft)	(usft)	(°/100usft),- ' (°	/100usft) 🤻 🎉 (	/100usft) 🗸 📆 👢 🐷
	a ta iban natif kandabibbilan lan	فمستفلأفكادات			I to the second	Charles Car			
20,400.0	89.80	179.62	11,839.2	-8,683.5	562.1	8,699.9	0.00	0.00	0.00
20,500.0	89.80	179.62	11,839.5	-8,783.5	562.8	8,799.8	0.00	0.00	0.00
20,600.0	89.80	179.62	11,839.9	-8,883.5	563.5	8,899.8	0.00	0.00	0.00
. 20,700.0	89.80	179.62	11,840.2	-8,983.5	564.2	8,999.7	0.00	0.00	0.00
20,800.0	89.80	179.62	11,840.6	-9,083.5	564.8	9,099.6	0.00	0.00	0.00
20,900.0	89.80	179.62	11,840.9	-9,183.5	565.5	9,199.5	0.00	0.00	0.00
21,000.0	89.80	179.62	11,841.3	-9,283.5	566.2	9,299.5	0.00	0.00	0.00
21,100.0	89.80	179.62	11,841.6	-9,383.5	566.8	9,399.4	0.00	0.00	0.00
21,200.0	89.80	179.62	11,842.0	-9,483.5	567.5	9,499.3	0.00	0.00	0.00
21,200.0	03.00	173.02	11,042.0	-9,403.3	307.3	3,433.3	0.00	0.00	0.00
21,300.0	89.80	179.62	11,842.3	-9,583.5	568.2	9,599.2	0.00	0.00	0.00
21,400.0	89.80	179.62	11,842.7	-9,683.5	568.8	9,699.2	0.00	0.00	0.00
21,500.0	89.80	179.62	11,843.0	-9,783.5	569.5	9,799.1	0.00	0.00	0.00
21,600.0	89.80	179.62	11,843.4	-9,883.5	570.2	9,899.0	0.00	0.00	0.00
21,700.0	89.80	179.62	11,843.7	-9,983.5	570.8	9,999.0	0.00	0.00	0.00
21,800.0	89.80	179.62	11.844.1	-10,083.5	571.5	10,098.9	0.00	0.00	0.00
21,900.0	89.80	179.62	11,844.4	-10,083.5	571.3 572.2				
22,000.0	89.80	179.62				10,198.8	0.00	0.00	0.00
1			11,844.8	-10,283.5	572.8	10,298.7	0.00	0.00	0.00
22,100.0	89.80	179.62	11,845.1	-10;383.5	573.5	10,398.7	0.00	. 0.00	0.00
22,200.0	89.80	179.62	11,845.5	-10,483.5	574.2	10,498.6	0.00	0.00	0.00
22,300.0	89.80	179.62	11,845.8	-10,583.4	574.8	10,598.5	0.00	0.00	0.00
22,400.0	89.80	179.62	11,846.2	-10,683.4	575.5	10,698.5	0.00	0.00	0.00
22,500.0	89.80	179.62	11,846.5	-10,783.4	576.2	10,798.4	0.00	0.00	0.00
22,600.0	89.80	179.62	11,846.9	-10,883.4	576.8	10,898.3	0.00	0.00	0.00
22,700.0	89.80	179.62	11,847.2	-10,983.4	577.5	10,998.2	0.00	0.00	0.00
00.000.0		470.00	44.047.0	44,000.4	570.0				
22,800.0	`89.80	179.62	11,847.6	-11,083.4	578.2	11,098.2	0.00	0.00	0.00
22,900.0	89.80	179.62	11,847.9	-11,183.4	578.9	11,198.1	0.00	0.00	0.00
23,000.0	89.80	179.62	11,848.3	-11,283.4	579.5	11,298.0	, 0.00	0.00	0.00
23,100.0	89.80	.179.62	11,848.6	-11,383.4	580.2	11,398.0	0.00	0.00	0.00
23,200.0	89.80	179.62	11,849.0	-11,483.4	580.9	11,497.9	0.00	0.00	0.00
23,300.0	89.80	179.62	11,849.3	-11,583.4	581.5	11,597.8	. 0.00	0.00	0.00
23,400.0	89.80	179.62	11,849.7	-11,683.4	582.2	11,697.7	0.00	0.00	0.00
23,500.0	89.80	179.62	11,850.0	-11,783.4	582.9 -	11,797.7	0.00	0.00	0.00
23,600.0	89.80	179.62	11,850.4	-11,883.4	583.5	11,897.6	0.00	0.00	0.00
23,700.0	89.80	179.62	11,850.7	-11,983.4	584.2	11,997.5	0.00	0.00	0.00
		,	· ·				-	•	
23,800.0	89.80	179.62	11,851.1	-12,083.4	584.9	12,097.5	. 0.00	0.00	0.00
23,900.0	89.80	179.62	11,851.4	-12,183.4	585.5	12,197.4	0.00	0.00	0.00
24,000.0	89.80	179.62	11,851.8	-12;283,4	· 586.2	12,297.3	0.00	0.00	0.00
24,100.0	89.80	179.62	11,852.1	-12,383.4	586.9	12,397.2	0.00	0.00	0.00
24,200.0	89.80	17.9.62	11,852.5	-12,483.4	587.5	12,497.2	0.00	0.00	0.00
24,300.0	89.80	179.62	11,852.8	-12,583.4	588.2	12,597.1	0.00	0.00	0.00
24,400.0	89.80	179.62	11,853.2	-12,683.4	588.9	12,697.0	0.00	. 0.00	0.00′
24,500.0	89.80	179.62	11,853.5	-12,783.4	589.5	12,797.0	0.00	0.00	0.00
24,600.0	89.80	179.62	11,853.8	-12,883.4	590.2	12,896.9	. 0.00	0.00	0.00
24,700.0	89.80	179.62	11,854.2	-12,983.4	590.9	12,996.8	0.00	0.00	0.00
1	•								•
24,800.0	89.80	179.62	11,854.5	-13,083.4	591.6	13,096.7	0.00	0.00	0.00
24,900.0	89.80	179.62	11,854.9	-13,183.4	592.2	13,196.7	0.00	0.00	0.00
25,000.0	89.80	179.62	11,855.2	-13,283.4	592.9	13,296.6	0.00	0.00	0.00
TD @ 25076.4			the street of	7.5.	West, Garage				and the state of t
25,076.4	89.80	179.62	11,855.5	-13,359.8	593.4	13,373.0	0.00	0.00	0.00





EDM 5000.1 Single User Db Company Project: Site: Well XTO ENERGY, INC.

Eddy County, NM Sec 15, T24S, R31E 3 2 3

PLU 15 Twin Wells Ranch #104H Wellbore #1.

Wellbore: Design: 💯 Design #1 Local Co-ordinate Reference

TVD Reference:
MD Reference:
North Reference:

Survey Calculation Method

Well PLU 15 Twin Wells Ranch #104H

KB=22 @ 3561.0usft (Akita #22) KB=22 @ 3561.0usft (Akita #22)

Grid,

Minimum Curvature

Design Targets  Target Name - hit/miss target Dip - Shape	Angle: D			+N/-S (usft)	TE/W (usft)	Northing (usft)	Easting (usft)	Latitude	L'ongitude
PLU 15 TWR #104H - L1 - plan misses target cente - Point	0.00 er by 11855.	0.00 Ousft at 24	0.0 4905,0usft M	-13,229.8 ID (11854.9 T	592.6 FVD, -13188.4 I	427,700.00 N, 592.3 E)	675,468.50	32° 10' 28.535 N	103° 45′ 58.403 W
PLU 15 TWR #104H - F - plan misses target cente - Point	0.00 er by 0.3usft	0.00 at 12402	11,811.0 .8usft MD (1	-686.5 1811.3 TVD,	508.7 -686.5 N, 508.7	440,243.30 7 E)	675,384.60	32° 12′ 32.667 N	103° 45′ 58.610 W
PLU 15 TWR #104H - P. - plan hits target center - Point	0.00	0.00	11,855.5	-13,359.8	593.4	427,570.00	675,469.30	32° 10' 27.249 N	103° 45′ 58 402 W

Formations	and the common of the production of the second seco
Measured	
Measured Vertical Depth Depth	Dip. Direction
(usft) (usft)	Dip Direction Name Lithology (*) (*)
13 करों की केंग्रेग के 14 कि 15 की कि 15 कि 15 की का 14 को 15 की 15 की 15 की 15 की 15 की 15 की 15 की 15 की 15 699.0 699.0	的数据,这个时间,这是我们会会,但是是最终的特别,但是不是一个,我们的这些数据的。这个时间就是有一个人的,我们就是这个人的重要的,这是我们的,这是一个是一个人,
780.0 780.0	
1,057.0 1,057.0	
4,243.0 4,243.0	
4,466.0 4,466.0	
5,378.0 5,378.0	
7,002.0 7,002.0	
8,319.0 8,319.0	
8,400.0 8,400.0	,
8,421.0 8,421.0	Bone Spg. Upper Avalon Shale
8,856.0 8,856.0	Bone Spg. Lower Avalon Shale
9,196.0 9,196.0	1st Bone Spring Lime.
9,387.0 9,387.0	1st Bone Spring Ss.
9,776.0 9,776.0	2nd Bone Spring Carb.
9,973.0 9,973.0	2nd Bone Spring Ss.
10,482.0 10,482.0	3rd Bone Spring Carb.
11,221.1 11,220.0	3rd Bone Spring Ss.
11,476.4 11,448.0	War Wink Ss.
11,660.9 11,574.0	Red Hills Ss.
11,806.1 11,658.0	Wolfcamp Sh
11,844.6 11,678.0	Wolfcamp X Sd
12,026.6 11,756.0	Wolfcamp Y Sd
12,244.8 11,806.0	Wolfcamp A Sh.

Plan Annotations  Measured  Depth  (us(t))	Vertical Depth (usft)	Local Coord +N/S (usft)	inates +E/-W (usft)	Comment
11,091.1	11,091.1	0.0	0.0	Build 10°/100'
11,591.1	11,530.0	<b>-7</b> 0.0	192.3	EOB @ 50.00° Inc / 110.00° Azm - Build 10°/100'
12,335.0	11,811.0	-618.8	508.2	EOC @ 89.80° Inc / 179.62° Azm / 11811.0' TVD
25,076.4	11,855.5	-13,359.8	593.4	TD @ 25076.4' MD / 11855.5' TVD

# PECOS DISTRICT DRILLING CONDITIONS OF APPROVAL

**OPERATOR'S NAME: | XTO Permian Operating, LLC** 

LEASE NO.: | NMNM-0506A

WELL NAME & NO.: Poker Lake Unit 15 TWR 104H

SURFACE HOLE FOOTAGE: | 0360' FSL & 1805' FWL

BOTTOM HOLE FOOTAGE | 2440' FNL & 2310' FWL Sec. 34, T. 24 S., R 31 E.

LOCATION: | Section 15, T. 24 S., R 31 E., NMPM

**COUNTY:** | Eddy County, New Mexico

# The original COAs still stand with the following drilling modifications:

# A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

a. Spudding well (minimum of 24 hours)

b. Setting and/or Cementing of all casing strings (minimum of 4 hours)

c. BOPE tests (minimum of 4 hours)

# **Eddy County**

Call the Carlsbad Field Office, 620 East Greene St., Carlsbad, NM 88220, (575) 361-2822

- 1. Hydrogen Sulfide (H2S) monitors shall be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the Hydrogen Sulfide area shall meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, provide measured values and formations to the BLM.
- 2. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. If the drilling rig is removed without approval an Incident of Non-Compliance will be written and will be a "Major" violation.
- 3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.

4. The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.

#### B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

## Wait on cement (WOC) for Potash Areas:

After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi for all cement blends, 2) until cement has been in place at least 24 hours. WOC time will be recorded in the driller's log.

Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Possibility of water flows in the Salado and Castile.

Possibility of lost circulation in the Red Beds, Rustler, and Delaware.

Abnormal pressure may be encountered in the 3rd Bone Spring and all subsequent formations.

- 1. The 18-5/8 inch surface casing shall be set at approximately 870 feet (in a competent bed below the Magenta Dolomite, which is a Member of the Rustler, and if salt is encountered, set casing at least 25 feet above the salt and cemented to the surface.
  - a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.
  - b. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.
  - c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.
  - d. If cement falls back, remedial cementing will be done prior to drilling out that string.

13-3/8 inch 1st Intermediate casing shall be kept fluid filled while running into hole to meet BLM minimum collapse requirements.

- 2. The minimum required fill of cement behind the 13-3/8 inch 1<sup>st</sup> intermediate casing is:
  - □ Cement to surface. If cement does not circulate see B.1.a, c-d above. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to potash.

Formation below the 13-3/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe (not the mud weight required to prevent dissolving the salt formation) and the mud weight for the bottom of the hole. Report results to BLM office.

9-5/8 inch 2<sup>nd</sup> Intermediate casing shall be kept fluid filled while running into hole to meet BLM minimum collapse requirements.

3. The minimum required fill of cement behind the 9-5/8 inch 2<sup>nd</sup> intermediate casing is:

Operator has proposed DV tool at depth of 4388', but will adjust cement proportionately if moved. DV tool shall be set a minimum of 50' below previous shoe and a minimum of 200' above current shoe. Operator shall submit sundry if DV tool depth cannot be set in this range. If an ECP is used, it is to be set a minimum of 50' below the shoe to provide cement across the shoe. If it cannot be set below the shoe, a CBL shall be run to verify cement coverage.

- a. First stage to DV tool:
- Ement to circulate. If cement does not circulate, contact the appropriate BLM office before proceeding with second stage cement job. Operator should have plans as to how they will achieve circulation on the next stage.
- b. Second stage above DV tool:
- Cement to surface. If cement does not circulate, contact the appropriate BLM office. Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry due to potash.

Formation below the 9-5/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe and the mud weight for the bottom of the hole. Report results to BLM office.

Centralizers required on horizontal leg, must be type for horizontal service and a minimum of one every other joint.

Production casing shall be kept fluid filled while running into hole to meet BLM minimum collapse requirements.

- 4. The minimum required fill of cement behind the 5-1/2 inch production casing is:
  - Cement should tie-back at least 500 feet into previous casing string. Operator shall provide method of verification.
- 5. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

#### C. PRESSURE CONTROL

- 1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API 53.
- 2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor. If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).
- 3. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 2000 (2M) psi.
- 4. Operator has proposed a multi-bowl wellhead assembly. This assembly will only be tested when installed on the 13-3/8 inch 1<sup>st</sup> intermediate casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the 13-3/8 inch 1<sup>st</sup> intermediate casing shoe shall be 5000 (5M) psi.
  - a. Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.
  - b. If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.
  - c. Manufacturer representative shall install the test plug for the initial BOP test.
  - d. Operator shall perform the 9-5/8 inch 2<sup>nd</sup> intermediate casing integrity test to 70% of the casing burst. This will test the multi-bowl seals.
  - e. If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.

5M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

- 5. The appropriate BLM office shall be notified a minimum of 4 hours in advance for a representative to witness the tests.
  - a. In potash areas, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. For all casing strings, casing cut-off and BOP installation can be initiated at twelve hours after bumping the plug. However, **no tests** shall commence until the cement has had a minimum of 24 hours setup time.
  - b. The tests shall be done by an independent service company utilizing a test plug **not** a **cup** or **J-packer**.
  - c. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.
  - d. The results of the test shall be reported to the appropriate BLM office.
  - e. All tests are required to be recorded on a calibrated test chart. A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.
  - f. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.
  - g. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the **Wolfcamp** formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

#### D. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the **Wolfcamp** formation, and shall be used until production casing is run and cemented.

## E. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

# F. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

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