NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1

RECEIVED
DEC 01 1983
O. C. D.
ARTESIA, OFFICE

45F File

Type Test: [X] Initial 4 POINT [ ] Annual [ ] Special

Test Date: 11-7-83

Company: H.W. Pace	Connection: AIR NEW WELL	
Pool: PECOS SLOCUM ~~U.D. POOL~~	Formation: ABO	Unit: ~~C~~
Completion Date: ~~12-17-82~~ 2-16-83	Total Depth: ~~6429.~~ 6462	Plug Back T.D.: 5920.
Elevation: ~~3808.~~ 3798	Farm or Lease Name: DEKALB FEDERAL	

Csg. Size	Wt.	d	Set At	Perforations	Well No.
4.5000	9.50		~~6514~~ 5920.	From 4368. To 4503.	1

Tbg. Size	Wt.	d	Set At	Perforations	Unit	Sec.	Twp.	Rge.
2.3750	4.70		~~4546~~ 4411.	From 0. To 0.	C	21	8S	26E

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
SINGLE	0.	CHAVES

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
TUBING	110 @ 4435.	60	13.2 PSIA	NEW MEXICO

L	H	G_g	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
4435.	4435.	0.636	0.08	6.64	0.	2.00	0.	

NO.	FLOW DATA: Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	B.H.P. DATA: Press. p.s.i.g.	CHOKE	Duration of Flow
SI					1120.	60.			96.0
1	2.00 X 0.188	65.	0.	60.	290.	60	0.	12/64	24.0
2	2.00 X 0.203	30.	0.	60.	262	60	0.	13/64	24.0
3	2.00 X 0.219	38.	0.	60.	259.	60	0.	14/64	24.0
4	2.00 X 0.250	28.	0.	60.	242.	60	0.	16/64	24.0
5									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor F_t	Gravity Factor F_g	Super Compress. Factor, F_{pv}	Rate of Flow Q, Mcfd
1	0.61	0.	78.2	1.0000	1.2540	1.0065	60.
2	0.72	0	43.2	1.0000	1.2540	1.0036	39.
3	0.84	0.	51.2	1.0000	1.2540	1.0042	54.
4	1.11	0.	41.2	1.0000	1.2540	1.0034	58.
5							

NO.	P_t	Temp. °R	T_d	Z
1	0.12	520.	1.48	0.987
2	0.07	520.	1.48	0.993
3	0.08	520.	1.48	0.992
4	0.06	520.	1.48	0.993
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.

A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.

Specific Gravity Separator Gas	0.636	XXXXXXXXXX
Specific Gravity Flowing Fluid	XXXXX	0.636
Critical Pressure	660. P.S.I.A.	660. P.S.I.A.
Critical Temperature	352. R	352. R

P_c 1133.2 P_c^2 1284.

NO	P_t^2	P_w	R_w^2	$P_c^2 - R_w^2$
1		303.	92.	1192.
2		275.	76.	1208.
3		272.	74.	1210.
4		255.	65.	1219.
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.0772$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.0381$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 62.$

Absolute Open Flow	Mcfd @ 15.025	Angle of Slope θ	Slope, n
62.		63.3	0.503

Remarks: _____

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
		BENNETT & CATHEY	