

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT ID ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 3-26-71	
Company Twinlakes Oil Co.				Connection None	
Pool Twin Lakes				Formation San Andres	
Completion Date		Total Depth 2617		Plug Back TD 2600	
				Elevation 3947	
Farm or Lease Name State CH Com.				Unit O.C.C. ARTESIA, B-1 FILE	
Csg. Size 4 1/2	Wt. 9.5	d 4.000	Set At 2617	Perforations: From 2576 To 2581	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 2584	Perforations: From 2550 To 2556	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2550	
Producing Thru Tbg		Reservoir Temp. °F 88 @		Mean Annual Temp. °F 60	
				Baro. Press. - P _a 13.2	
L		H	Gg	% CO ₂	% N ₂
				% H ₂ S	Prover
				Meter Run	Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
Sl	Orifice Well Tester						485	66			72
1.	2 X 1.250			17" Hg		60	445	71			1
2.	2 X 1.250			22" Hg		60	415	73	Packer		1
3.	2 X 1.250			28" Hg		60	375	72			1
4.	2 X 1.250			36" Hg		60	320	71			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcid
1	721				.8305		599
2	838				.8305		696
3	969				.8305		805
4	1133				.8305		941
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
					Dry	
1.	.726	520	1.207	.846	A.P.I. Gravity of Liquid Hydrocarbons Dry	Deq.
2.	.679	520	1.209	.857	Specific Gravity Separator Gas 0.870	XXXXXXXXXX
3.	.618	520	1.208	.870	Specific Gravity Flowing Fluid XXXXX	
4.	.535	520	1.207	.837	Critical Pressure 633 P.S.I.A.	P.S.I.A.
5.					Critical Temperature 447 R	R

NO.	P _t ²	P _w ²	P _c ²	P _c ² - P _w ²
1	209.8		212.7	35.25
2	183.2		187.5	60.52
3	150.5		156.7	91.32
4	110.9		120.0	128.02
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 5.952$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.976$

AGF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.780$

Absolute Open Flow 1,780 Mcid @ 15.025 Angle of Slope θ 63.5° Slope, n 0.500

Remarks: _____

Approved By Commission:	Conducted By: <i>E. Ringer</i>	Calculated By: <i>Cities Service</i>	Checked By: <i>V. K. ...</i>
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