

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 10-15-81		OCT 26 1981	
Company McClellan Oil Corp. /				Connection To Air				O. C. D.	
Pool WILDCAT				Formation ABO				Unit ARTESIA, OFFICE	
Completion Date 10-12-81		Total Length 4603'		Plug Back TD 4345		Elevation 3720 Gl.		Farm or Lease Name PZ Fed.	
Csg. Size 4 1/2	Wt. 10.5 #	d 4.052"	Set At 4602	Perforations: From 4125 To 4292		Well No. 1			
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 4214	Perforations: From OPENENDED To		Unit Soc. Twp. Rge. 0 7 9S 26E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE						Packer Set At NONE		County Chaves	
Producing Thru TUBING		Reservoir Temp. °F @		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 1	H 1	Gg .8701	% CO ₂ 26.16	% N ₂ 4.16	% H ₂ S -0-	Prover 2"		Meter Run	Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							942		940	CHOKE	24 Hrs.
1.	2"	X	.250	340		39	885	56	890	4/64	1 Hr.
2.	2"	X	.250	600		55	727	61	750	10/64	1 Hr.
3.	2"	X	.375	357		63	357	64	357	OPEN	1 Hr.
4.	2"	X	.500	100		64	100	64	110	OPEN	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super. Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	1.087		353.2	1.021	1.072	1.042	438
2	1.087		613.2	1.005	1.072	1.069	768
3	2.378		370.2	.9971	1.072	1.639	978
4	4.279		113.2	.9962	1.072		517
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.46	499	1.28	.921	-0-	-0-	.8701	X X X X X X X X	769	390
2.	.80	515	1.32	.875				X X X X X		
3.	.48	523	1.34	.927						
4.										
5.										

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1		903.2	815.7	93.3
2		763.2	582.5	326.5
3		370.2	137.0	772.
4				
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 9.743$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1367$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.121$$

Posted ID-2 & Comp. Book SI 12-18-81

Absolute Open Flow <u>1.367</u> Mcfd @ 15.025		Angle of Slope θ <u>63.5°</u>	Slope, n <u>.5000</u>
Remarks: <u>Plot too steep use 63.5° thru low rate.</u>			
Approved By Commission:		Conducted By: W.S.	Calculated By: M.K.
		Checked By: M.K.	