

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPLE AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-65

|                                                                                                                           |              |                                  |                             |                                    |                           |                                       |           |                                           |  |
|---------------------------------------------------------------------------------------------------------------------------|--------------|----------------------------------|-----------------------------|------------------------------------|---------------------------|---------------------------------------|-----------|-------------------------------------------|--|
| Type Test<br><input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special |              |                                  |                             |                                    |                           | Test Date<br>11-6-81                  |           | <b>RECEIVED</b><br><br><b>DEC 18 1981</b> |  |
| Company<br>IKE LOVELADY, INC. ✓                                                                                           |              |                                  |                             |                                    |                           | Connection<br>TO AIR                  |           |                                           |  |
| Pool<br>WILDCAT, Abo                                                                                                      |              |                                  |                             |                                    |                           | Formation<br>ABO                      |           | Unit<br>O. C. D.                          |  |
| Completion Date<br>10/31/81                                                                                               |              | Total Depth<br>4800              |                             | Peg Back TD<br>4719                |                           | Elevation<br>3765.4 Gl.               |           | Farm or Office<br>ARTESIA, OFFICE         |  |
| Csg. Size<br>4 1/2"                                                                                                       | Wt.<br>10.5# | d<br>4.052"                      | Set At<br>4798              | Perforations:<br>From 4301 To 4702 |                           | Well No.<br>1                         |           |                                           |  |
| Thq. Size<br>2 3/8"                                                                                                       | Wt.<br>4.7#  | d<br>1.995                       | Set At<br>4163              | Perforations:<br>From OPENENDED    |                           | Unit Sec. Twp. Rge.<br>J 16 9S 26E    |           |                                           |  |
| Type Well - Single - Bradenhead - G.C. or G.O. Multiple<br>SINGLE                                                         |              |                                  |                             |                                    |                           | Packer Set At<br>NONE                 |           | County<br>CHAVES                          |  |
| Producing Thru<br>TUBING                                                                                                  |              | Reservoir Temp. °F<br>92° @ 4502 |                             | Mean Annual Temp. °F<br>60°        |                           | Baro. Press. - P <sub>a</sub><br>13.2 |           | State<br>New Mexico                       |  |
| L<br>4502                                                                                                                 | H<br>4502    | G <sub>g</sub><br>.8368          | % CO <sub>2</sub><br>21.616 | % N <sub>2</sub><br>4.601          | % H <sub>2</sub> S<br>-0- | Prover<br>2"                          | Meter Run | Taps                                      |  |

| FLOW DATA |                  |   |              |                 |                      |          | TUBING DATA     |          | CASING DATA     |          | Duration of Flow |
|-----------|------------------|---|--------------|-----------------|----------------------|----------|-----------------|----------|-----------------|----------|------------------|
| NO.       | Prover Line Size | X | Orifice Size | Press. p.s.i.g. | Diff. h <sub>w</sub> | Temp. °F | Press. p.s.i.g. | Temp. °F | Press. p.s.i.g. | Temp. °F |                  |
| 1.        | 2"               | x | 1/16         | 759             |                      | 39°      | 780             | 70       | PKR.            |          | 24 Hr.           |
| 2.        | 2"               | x | 3/16         | 320             |                      | 27°      | 759             | 70       | 759             |          | 1 Hr.            |
| 3.        | 2"               | x | 3/16         | 513             |                      | 47°      | 682             | 70       | 682             |          | 1 Hr.            |
| 4.        | 2"               | x | 7/32         | 350             |                      | 42°      | 513             | 70       | 513             |          | 1 Hr.            |
| 5.        |                  |   |              |                 |                      |          | 350             | 70       | 350             |          | 1 Hr.            |

| RATE OF FLOW CALCULATIONS |                       |                  |                         |                                  |                               |                                         |                      |
|---------------------------|-----------------------|------------------|-------------------------|----------------------------------|-------------------------------|-----------------------------------------|----------------------|
| NO.                       | Coefficient (24 Hour) | $\sqrt{h_w P_m}$ | Pressure P <sub>m</sub> | Flow Temp. Factor F <sub>t</sub> | Gravity Factor F <sub>g</sub> | Super Compress. Factor, F <sub>pv</sub> | Rate of Flow Q, Mcfd |
| 1.                        | .06405                |                  | 772.2                   | 1.021                            | 1.094                         | 1.102                                   | 61                   |
| 2.                        | .6082                 |                  | 333.2                   | 1.033                            | 1.094                         | 1.042                                   | 239                  |
| 3.                        | .6082                 |                  | 526.2                   | 1.013                            | 1.094                         | 1.063                                   | 377                  |
| 4.                        | .8393                 |                  | 363.2                   | 1.018                            | 1.094                         | 1.039                                   | 353                  |
| 5.                        |                       |                  |                         |                                  |                               |                                         |                      |

| NO. | P <sub>t</sub> | Temp. °R | T <sub>r</sub> | Z    | Gas Liquid Hydrocarbon Ratio T.S.T.M. Mcf/bbl. | A.P.I. Gravity of Liquid Hydrocarbons _____ Deg. | Specific Gravity Separator Gas _____ | Specific Gravity Flowing Fluid _____ | Critical Pressure _____ P.S.I.A. | Critical Temperature _____ P.S.I.A. |
|-----|----------------|----------|----------------|------|------------------------------------------------|--------------------------------------------------|--------------------------------------|--------------------------------------|----------------------------------|-------------------------------------|
| 1.  | 1.03           | 499      | 1.28           | .823 |                                                |                                                  |                                      |                                      |                                  |                                     |
| 2.  | .444           | 487      | 1.25           | .921 |                                                |                                                  |                                      |                                      |                                  |                                     |
| 3.  | .702           | 507      | 1.30           | .885 |                                                |                                                  |                                      |                                      |                                  |                                     |
| 4.  | .484           | 502      | 1.29           | .927 |                                                |                                                  |                                      |                                      |                                  |                                     |
| 5.  |                |          |                |      |                                                |                                                  |                                      |                                      |                                  |                                     |

| P <sub>c</sub> 782.12 | P <sub>c</sub> <sup>2</sup> 611.7 | (1) $\frac{P_c^2}{P_c^2 - P_w^2} = 14.80$ | (2) $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.857$ |                                                           |
|-----------------------|-----------------------------------|-------------------------------------------|------------------------------------------------------------|-----------------------------------------------------------|
| NO.                   | P <sub>t</sub> <sup>2</sup>       | P <sub>w</sub>                            | P <sub>w</sub> <sup>2</sup>                                | P <sub>c</sub> <sup>2</sup> - P <sub>w</sub> <sup>2</sup> |
| 1                     |                                   | 755.4                                     | 570.6                                                      | 41.1                                                      |
| 2                     |                                   | 746.8                                     | 557.7                                                      | 54                                                        |
| 3                     |                                   | 544                                       | 311.0                                                      | 300.7                                                     |
| 4                     |                                   | 381.3                                     | 145.4                                                      | 466.3                                                     |
| 5                     |                                   |                                           |                                                            |                                                           |

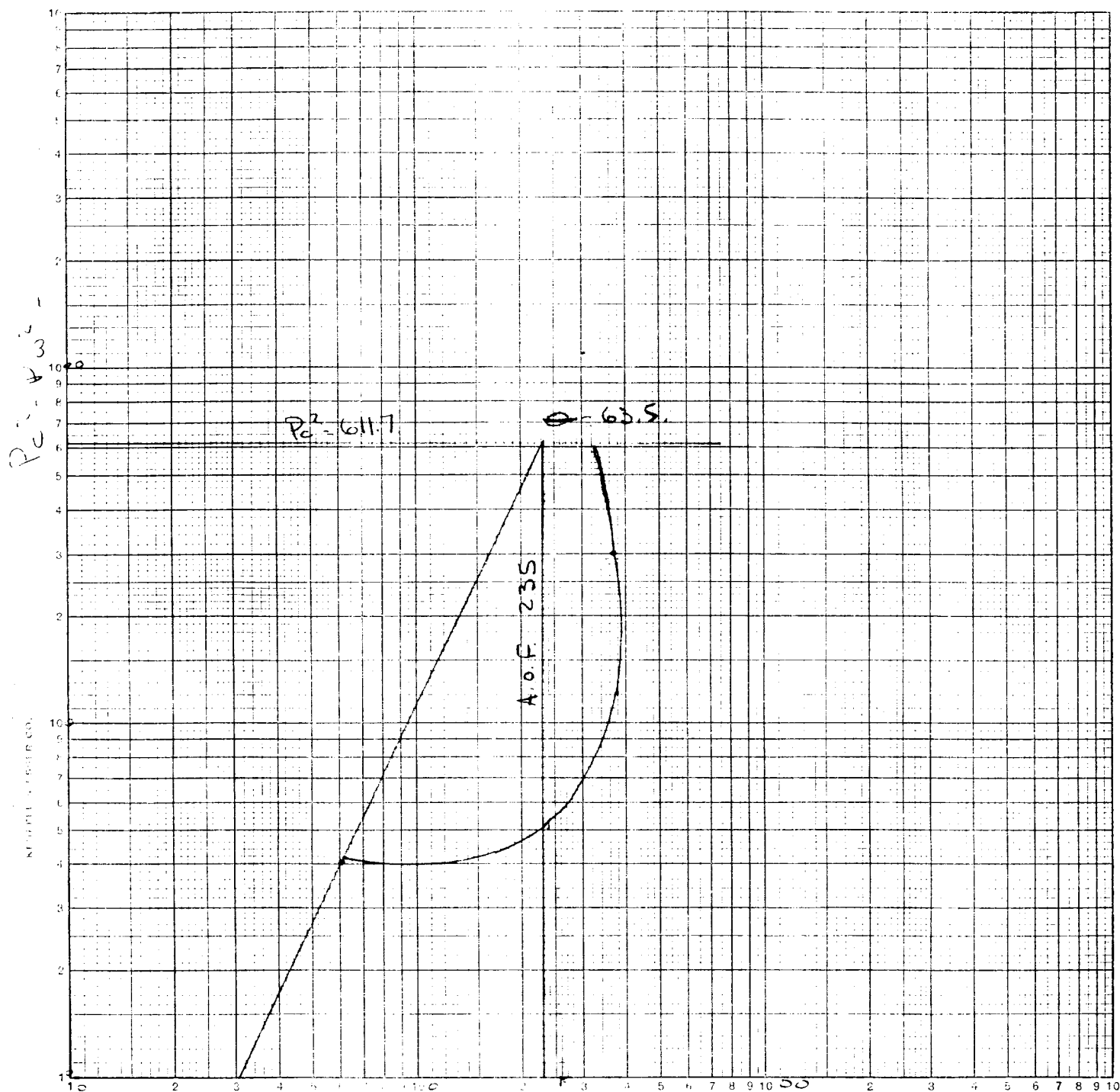
AGF = 2     $\left[ \frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 235$

|                    |     |                |                  |      |          |      |
|--------------------|-----|----------------|------------------|------|----------|------|
| Absolute Open Flow | 235 | Mcf/d @ 15.025 | Angle of Slope @ | 63.5 | Slope, n | .500 |
|--------------------|-----|----------------|------------------|------|----------|------|

Remarks: Plot too steep use 63.5 thru low rate.

|                         |                       |                        |                     |
|-------------------------|-----------------------|------------------------|---------------------|
| Approved By Commission: | Conducted By:<br>W.S. | Calculated By:<br>M.K. | Checked By:<br>M.K. |
|-------------------------|-----------------------|------------------------|---------------------|

$$61 \left( \frac{611.7}{41.1} \right)^{1.5} = 235$$



MC 107 - 10005

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURES ( $P_c$  or  $P_s$ )  
FROM KNOWN BOTTOM HOLE PRESSURE ( $P_f$  or  $P_s$ )

Adopted 8-1-55

COMPANY THE LONGHARDY LEASE Penitentiary ST "A" WELL NO. 1 DATE 11-6-81

LOCATION: Unit I Section 16 Township 9 South Range 26 East

L H 4502 L/H G 8368 %CO<sub>2</sub> 21.616 %N<sub>2</sub> 4.601 %H<sub>2</sub>S -0-

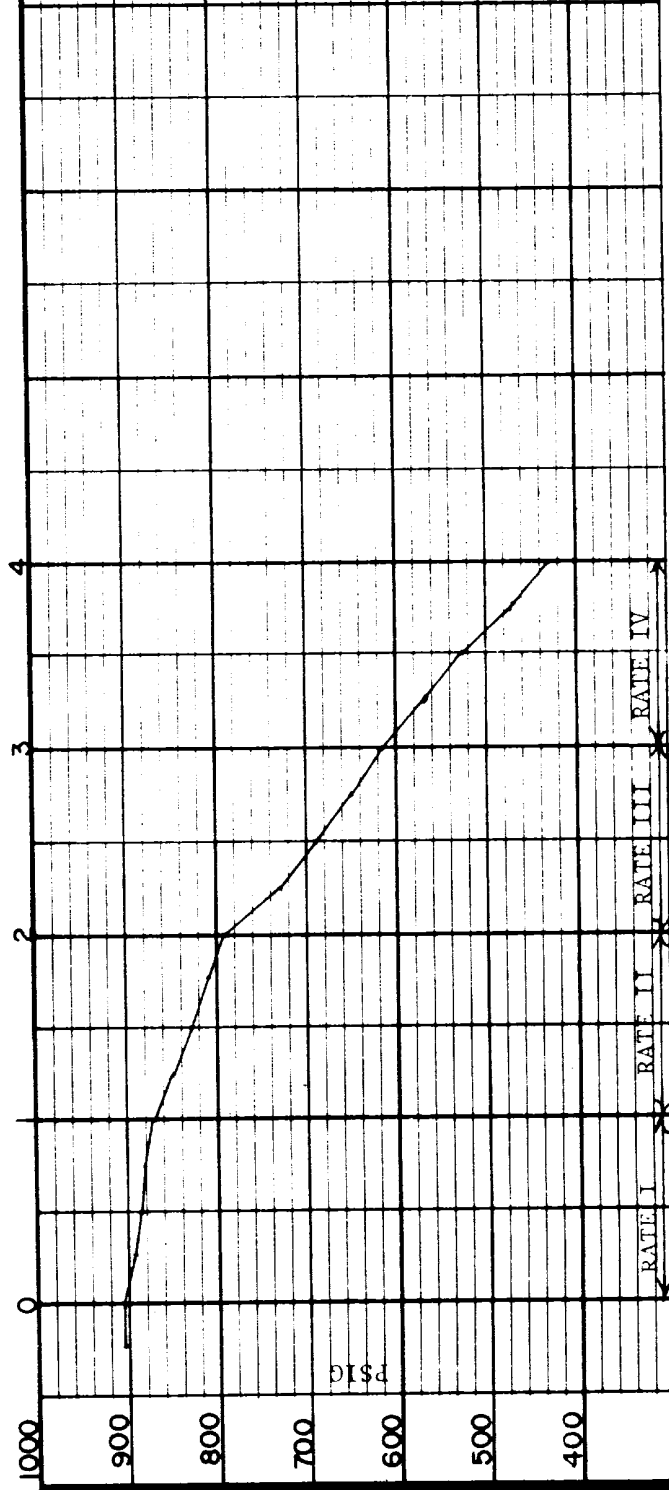
gh GH Pa 150 Ta 389 SH 552  
TABLE I & II TABLE I & II TABLE I & II  
S.I. RATE I RATE II RATE III RATE IV

| LINE |                                          | 1       | 2       | 3       | 4        | 5       | 6 | 7 | 8 |
|------|------------------------------------------|---------|---------|---------|----------|---------|---|---|---|
| 1    | $T_w(W.H. \cdot R)$                      | 499     | 499     | 487     | 507      | 502     |   |   |   |
| 2    | $T_s(B.H. \cdot R)$                      | 552     | 552     | 552     | 552      | 552     |   |   |   |
| 3    | $T_c(T_w + T_s)$                         | 525.5   | 525.5   | 519.5   | 529.5    | 527     |   |   |   |
| 4    | $Z(EST.)$                                | 838     | 842     | 852     | 898      | 919     |   |   |   |
| 5    | $TZ$                                     | 440.369 | 442.47  | 442.61  | 475.491  | 484.313 |   |   |   |
| 6    | $GH/TZ$                                  | 8.5548  | 8.51417 | 8.51141 | 7.92291  | 7.7785  |   |   |   |
| 7    | $e^S$ (Table XIV)                        | 1.3782  | 1.37613 | 1.37599 | 1.345962 | 1.33869 |   |   |   |
| 8    | $P_f$ or $P_s$                           | 918.2   | 886.2   | 806.2   | 631.2    | 441.2   |   |   |   |
| 9    | $P_f^2$ or $P_s^2$                       | 843.09  | 785.35  | 649.95  | 398.41   | 194.657 |   |   |   |
| 10   | $P_c^2 - P_f^2/es$ or $P_w^2 = P_s^2/es$ | 611.717 | 570.69  | 472.35  | 296.00   | 145.40  |   |   |   |
| 11   | $P_c$ or $P_w$                           | 782.12  | 755.4   | 687.3   | 544      | 381.3   |   |   |   |
| 12   | $P_c \cdot (F_w + P_s)$ or $(P_c + P_s)$ | 850.16  | 820.8   | 746.75  | 587.6    | 411.25  |   |   |   |
| 13   | $P_c = (P/P_c)$                          | 1.13    | 1.10    | 1.00    | .78      | .55     |   |   |   |
| 14   | $T_c(T/T_c)$                             | 1.35    | 1.35    | 1.34    | 1.36     | 1.35    |   |   |   |
| 15   | $Z$ (Table XI)                           | .838    | .847    | .852    | .898     | .919    |   |   |   |

TEST DATE: NOVEMBER 6, 1981  
TEST DEPTH: 4502 FEET  
ELEMENT NO: 17772  
RANGE: 0-3850 psi  
CLOCK NO: E/6532  
RANGE: 0-72 Hours

NOTE: See tabulation of Times and Pressures on attached sheet.

TIME IN HOURS



IKE LOVELADY, INC.

PENNZOIL STATE "A" NO. 1

PRESSURES TO USE FOR CALCULATING 4-POINT BACK PRESSURE TEST.

JOHN W. WEST ENGINEERING CO. HOBBS, NEW MEXICO

Date: 11-9-81 Drawn by: bsm Scale: as shown

IKE LOVELADY, INC.  
PENNZOIL STATE "A" NO. 1

TEST CONDUCTED BY:  
JOHN WEST ENGINEERING COMPANY

PRESSURES TO USE FOR CALCULATING 4-POINT  
BACK PRESSURE TEST.

TABULATION OF TIMES AND PRESSURES.

TEST DATE: NOVEMBER 6, 1981  
TEST DEPTH: 4502 FEET  
ELEMENT NO: 17772 (0-3850 psi)  
OPERATOR: W.S.

| <u>DATE</u> | <u>TIME</u> | <u>CUM HRS. / MIN.</u> | <u>PSIG @ 4502 FEET</u>                  |
|-------------|-------------|------------------------|------------------------------------------|
| 11-6-81     | 11:15 A.M.  |                        | 905 Gauge reached 4502 Feet              |
|             | 11:30 A.M.  | 00 Hrs. 00 Min.        | 905 Begin Test.                          |
|             | 11:45 A.M.  | 00 15                  | 898                                      |
|             | 12:00 Noon  | 00 30                  | 886                                      |
|             | 12:15 P.M.  | 00 45                  | 880                                      |
|             | 12:30 P.M.  | 01 00                  | 873 End Rate I                           |
|             | 12:45 P.M.  | 01 15                  | 847                                      |
|             | 1:00 P.M.   | 01 30                  | 826                                      |
|             | 1:15 P.M.   | 01 45                  | 809                                      |
|             | 1:30 P.M.   | 02 00                  | 793 End Rate II                          |
|             | 1:45 P.M.   | 02 15                  | 728                                      |
|             | 2:00 P.M.   | 02 30                  | 687                                      |
|             | 2:15 P.M.   | 02 45                  | 651                                      |
|             | 2:30 P.M.   | 03 00                  | 618 End Rate III                         |
|             | 2:45 P.M.   | 03 15                  | 570                                      |
|             | 3:00 P.M.   | 03 30                  | 523                                      |
|             | 3:15 P.M.   | 03 45                  | 471                                      |
| 11-6-81     | 3:30 P.M.   | 04 00                  | 428 End Rate IV, Gauge out,<br>End Test. |

JOHN W. WEST ENGINEERING COMPANY  
412 NORTH DAL PASO, HOBBS, NEW MEXICO

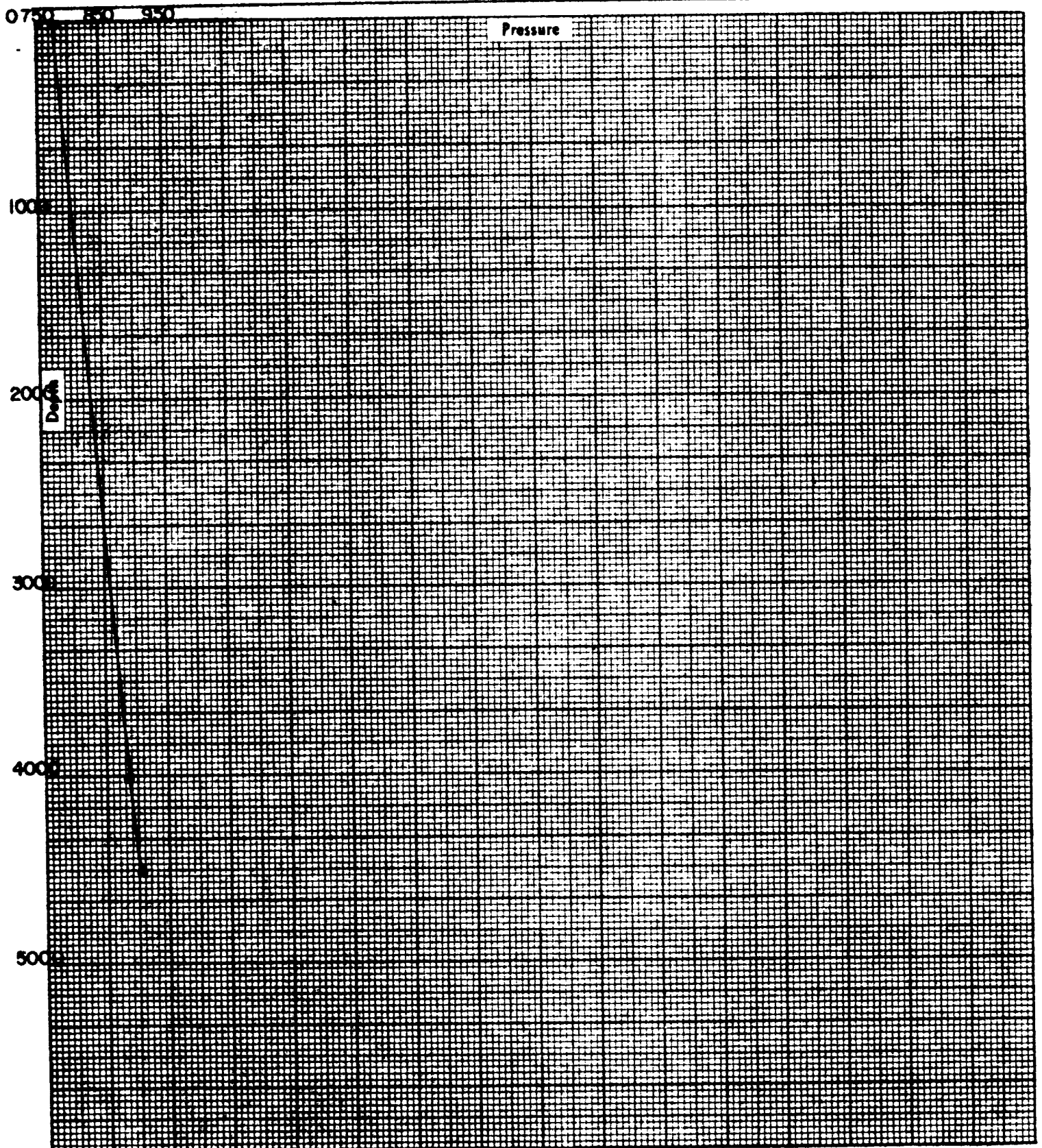
TELEPHONES 393-3942  
393-3117

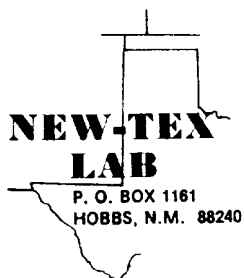
## BOTTOM HOLE PRESSURE SURVEY REPORT

OPERATOR IKE LOVELADY, INC.  
LEASE PENNZOIL STATE "A"  
WELL NO. 1  
FIELD \_\_\_\_\_  
DATE 11-6-81 TIME 11:15 A.M.

| DEPTH | PRESSURE | GRADIENT |
|-------|----------|----------|
| 000   | 780      |          |
| 4002  | 888      | .027     |
| 4502  | 905      | .034     |

STATUS Shut-In TEST DEPTH 4502'  
TIME S.I. 24 Hrs. LAST TEST DATE \_\_\_\_\_  
CAS. PRES. \_\_\_\_\_ BHP LAST TEST \_\_\_\_\_  
TUB. PRES. 780 psi BHP CHANGE \_\_\_\_\_  
ELEV. \_\_\_\_\_ FLUID TOP \_\_\_\_\_  
DATUM \_\_\_\_\_ WATER TOP \_\_\_\_\_  
TEMP \_\_\_\_\_ RUN BY W.S.  
CLOCK NO. E-6532 GAUGE NO. 19389  
ELEMENT NO. 17772 (0-3850 psi)





No. 5988  
Run No.  
Date of Run 11-7-81  
Date Secured 11-6-81

### CERTIFICATE OF ANALYSIS

Sample of Ike Lovelady Pennzoil State "A" #1  
Secured from John West Engineering  
At 412 N Dal Paso Secured by  
Hobbs, NM 88240 Time Date  
Sampling conditions Press  
Temp.  
Station No.

### FRACTIONAL ANALYSIS

#### Percentage Composition

|                  | MOL %   | LIQ. % | G.P.M. |
|------------------|---------|--------|--------|
| Carbon Dioxide   | 21.616  |        |        |
| Air              | 4.601   |        |        |
| Nitrogen         |         |        |        |
| Oxygen           |         |        |        |
| Hydrogen sulfide |         |        |        |
| Hydrogen         |         |        |        |
| Methane          | 67.755  |        |        |
| Ethane           | 3.394   |        | .905   |
| Propane          | 1.287   |        | .353   |
| Butanes          |         |        |        |
| Iso-Butane       | .186    |        | .061   |
| N-Butane         | .420    |        | .132   |
| Pentanes         |         |        |        |
| Iso-Pentane      | .118    |        | .043   |
| N-Pentane        | .127    |        | .046   |
| Hexanes          | .108    |        | .044   |
| Heptanes         | .388    |        | .179   |
| Octanes          |         |        |        |
| TOTAL            | 100.000 |        | 1.763  |

Calc. Sp. Gr. 0.8368  
Calc. A.P.I.  
Calc. Vapor Press. PSIA  
Sp. Gr.  
Mol. Wt. 24.27

#### LIQUID CONTENT (GAL., MCF)

Propane Calc. G.P.M. .353  
Butanes Calc. G.P.M. .193  
Pentanes Plus. G.P.M. .312  
Ethane Calc. G.P.M. .905  
RVP Gasoline G.P.M.  
B.T.U./Cu. Ft. @ 14.696 P.S.I.A.  
Dry Basis 833  
Wet Basis 818  
Sulfur Analysis by Titration  
Gr./100 Cu. Ft.  
Hydrogen Sulfide  
Mercaptans  
Sulfides  
Residual Sulfur  
Total Sulfur

Run by Deane Simpson Checked by Approved by Deane Simpson

Additional Data and Remarks