

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST OR GAS WELL

Form C-122
Revised 9-1-65

C/SF
C-122

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2-25-82		APR 19 1982	
Company Yates Petroleum Corporation					Connection Transwestern Pipeline Co.			
Well Pecos Slope Abo					Formation Abo		Unit O. C. D. ARTESIA, OFFICE	
Completion Date 1-7-82		Total Length 4250		Plug Back TD 4070		Elevation 3988.4 GL		Form or Lease Name Everette "00" Fed.
Casing Size 4-1/2"	Wt. 9.5#	Id 4.090	Set At 4250	Perforations: From 3699 To 3869		Well No. 3		
Tubing Size 2-3/8"	Wt. 4.7#	Id 1.995	Set At 3786	Perforations: From To		Unit Sec. Twp. Rge. C 26 5S 24E		
Type Well - Single - Production - G.G. or G.O. Multiple Single					Packer Set At -		County Chaves	
Producing thru tubing		Reservoir Temp. °F 100° 3784		Mech Annual Temp. °F 62°		Baro. Press. - P _a 13.2		State New Mexico
L 3786	H 3786	G _g .690	% CO ₂ 5.21	% N ₂ 8.30	% H ₂ S 0	Previor -	Meter Run 2	Temp Flanged

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Previor Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1000				days
1.	2.067 x 1.125			250	3.0	58	839	62			24 hrs
2.	2.067 x 1.125			250	4.7	50	808	62			24 hrs
3.	2.067 x 1.125			230	8.2	60	683	62			24 hrs
4.	2.067 x 1.125			250	13.1	62	460	62			24 hrs
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	6.393	28.0	263.2	1.002	1.204	1.024	221
2	6.393	35.1	263.2	1.010	1.204	1.025	280
3	6.393	44.7	243.2	1.000	1.204	1.021	351
4	6.393	58.7	263.2	.9981	1.204	1.025	462
5.							

NO.	P _r °C	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Dry _____ Mcf/Lbl.	A.P.I. Gravity of Liquid Hydrocarbons _____ Dry _____ Deg.
1	.39	518	1.45	.954	Specific Gravity Separator Gas .690 X X X X X X X X	.690
2	.39	510	1.43	.952	Specific Gravity Flowing Fluid X X X X X	.690
3	.36	520	1.46	.959	Critical Pressure 676 P.S.I.A.	676 P.S.I.A.
4	.39	522	1.46	.951	Critical Temperature 357 R	357 R
5.						

NO.	P _r °C	P _w °C	P _r °C	P _w °C	P _r °C	P _w °C
1	726.2		726.9		299.7	
2	674.4		675.5		351.1	
3	484.7		486.5		540.1	
4	223.9		227.1		799.5	
5						

(1) $\frac{P_r^2}{P_c^2 - P_w^2} = 1.284$

ADP = Q $\left[\frac{P_r^2}{P_c^2 - P_w^2} \right]^n = 559 \text{ mcfpd}$

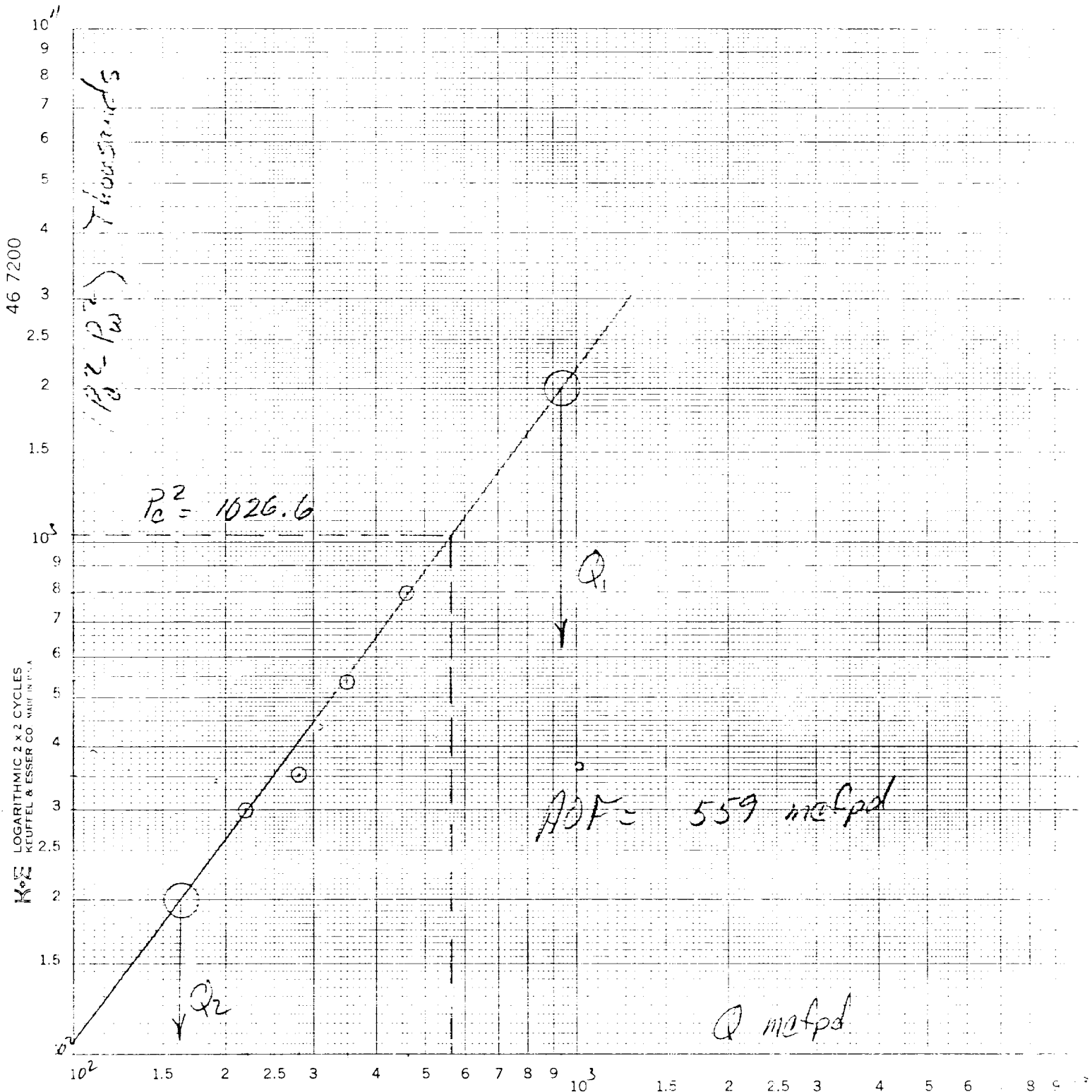
(2) $\left[\frac{P_r^2}{P_c^2 - P_w^2} \right]^n = 1.210$

Absolute Open Flow	559	Mcf/d @ 15.025	Angle of Slope °	Slope, n .761
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Remarks:

Approved By: _____	Conducted By: David Weaver	Calculated By: Al Springer	Checked By:
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Notes: 12/1/1961
 Everett '00' - cal. # 3
 C, SEC 26-55-21E
 Chaves, NM



$$(P_0^2 - P_w^2)_1 = 2,000$$

$$(P_0^2 - P_w^2)_2 = 200$$

$$Q_1 = 935'$$

$$Q_2 = 162$$

$$\log Q_1 = 2.97081$$

$$\log Q_2 = 2.20952$$

$$n = .76130 = .761$$

28/11

100

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TABLE

[illegible]