

V MEXICO OIL CONSERVATION COM' ION
MULTIPOINT AND ONE POINT BACK PRESSURE TEL. FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

C/SF
C-122
4563

Type Test ☒ Initial ☐ FOUR POINT ☐ Annual				☐ Special		Test Date 2-17-82		MAR - 1 1982			
Company VIKING PETROLEUM, INC.				Connection AIR NEW WELL				O. C. D. ARIESA, OFFICE			
Pool Pecos slope 1st gas UNDESIGNATED				Formation ABO				Unit N			
Completion Date 2-10-82		Total Depth 4071		Plug Back TD 4005		Elevation 3981 KB		Farm or Lease Name Grynberg 14 State Conn			
Csg. Size 4.500	Wt. 10.5	Id 4.052	Set At 4005	Perforations: From 3652 To 3919		Well No. 1					
Thq. Size 2.375	Wt. 4.7	Id 1.995	Set At 3602	Perforations: From OPEN To ENDED		Unit N		Sec. 14		Twp. Rge. 55 24E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At NONE		County CHAVES					
Producing Thru TUBING		Reservoir Temp. °F 99 @ 3786		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State NEW MEXICO			
L 3786	H 3786	Gg .695	% CO ₂ 1.43	% N ₂ 11.51	% H ₂ S	Prover 2.000	Meter Run		Taps		

FLOW DATA							TUBING DATA		B.H.P. DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
51							937	64	1034		168 HRS
1.	2.00	X	.500	143	0	39	897	60	997		1
2.	2.00	X	.500	245	0	43	841	60	947		1
3.	2.00	X	.500	337	0	50	774	59	888		1
4.	2.00	X	.500	421	0	53	701	58	826		1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	4.3880	.00	156.2	1.000	1.1995	1.0133	833
2	4.3880	.00	253.2	1.000	1.1995	1.0222	1389
3	4.3880	.00	350.2	1.0020	1.1995	1.0202	1901
4	4.3880	.00	434.2	1.0019	1.1995	1.0375	2376
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.24	520	1.47	.974			.6950	X X X X X X X X	653	353
2	.39	520	1.47	.957			X X X X X			
3	.53	519	1.47	.942						
4	.66	518	1.47	.929						
5										

$P_c = 1047.2$ $P_c^2 = 1096.6$				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.7975$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.9245$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²			
1		101.2	1020.5	76.0			
2		960.2	922.0	175.0			
3		901.2	812.2	284.0			
4		839.2	704.3	392.0			
5							

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4572.6$			
Absolute Open Flow <u>4572.6</u> Mcfd @ 15.025		Angle of Slope θ <u>57.5</u>	
		Slope, n <u>.6364</u>	

Remarks: <u>BOTTOM HOLE PRESSURES MEASURED WITH AMERADA PRESSURE ELEMENTS.</u>			
Approved By Commission:	Conducted By: RICHARD TOWNLEY	Calculated By: BENNETT-CATHEY	Checked By: