NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TES. FOR GAS WELL

Form C-122
Revised 9-1-65

C/SF
C-122

RECEIVED
APR 19 1982
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 4-7-82	
Company: MESA PETROLEUM CO.		Connection: UNCONNECTED			
Pool: PECOS SLOPE ABO		Formation: ABO		Unit: ARTESIA, OFFICE	
Completion Date: 4-7-82	Total Depth: 4100'	Plug Back TD: 4030'	Elevation: 3895'	Farm or Lease Name: CAMACK FED COM	
Csg. Size: 4 1/2" / Wt.: 10.5# / d: / Set At: 4080'		Perforations: From 3640' To 3788'		Well No.: 6	
Tbg. Size: 2 3/8" / Wt.: 4.7# / d: / Set At: 3545'		Perforations: From OPEN ENDED To		Unit: H / Sec.: 12 / Twp.: 5S / Rge.: 24E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: NONE		County: CHAVES	
Producing Thru: TUBING	Reservoir Temp. °F: 101 @ 4100'	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO	
L	H	Gg: .65	% CO_2: 1	% N_2: 1	% H_2S:
Prover: CHOKE	Meter Run:	Taps:			

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						927		802		65 HR SI
1.	CHOKE	13/64	900		61	900	61	785		1 HR
2.	COEFF.	17/64	840		68	840	68	755		1 HR
3.		21/64	775		70	775	70	725		1 HR
4.		25/64	680		72	680	72	685		1 HR
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.6778	CHOKE	913	.9990	1.240		767
2	1.1870	CHOKE	853	.9924	1.240		1246
3	1.8170	CHOKE	788	.9905	1.240		1759
4	2.5870	CHOKE	693	.9887	1.240		2198
5							

NO.	P_t	Temp. °R	T_r	Z
1				
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 815 P_c^2 664

NO	P_t	P_w	P_w^2	$P_c^2 - P_w^2$
1		798	637	27
2		768	590	74
3		738	545	119
4		698	487	177
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 3.7514 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 2.0968

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 4,600

Absolute Open Flow 4600 Mcfd @ 15.025 Angle of Slope θ 60.8° Slope, n .56

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	JAMES CRAIG	E. L. BUTTROSS, JR. 4-13-82	