

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

C/SF

C-122

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2/18/82		FEB 24 1982			
Company McClellan Oil Corporation						Connection Air		O. C. D.			
Pool Undesignated Pecos Slope Abo						Formation Abo		Unit ARTESIA, OFFICE			
Completion Date 2/15/82			Total Depth 4200'		Plug Back TD 4177'		Elevation 3832' G.L.		Farm or Lease Name McClellan		
Coq. Size 4-1/2"	Wt. 10.5	d 4"	Set At 4177'	Perforations: From 3669' To 4016'		Well No. 1					
Tiq. Size 2-3/8"	Wt. 4.7	d 2"	Set At 3831'	Perforations: From To		Unit N 30 5-S 25-E					
Type Well - Single - Bronthead - G.G. or G.O. Multiple Single						Packer Set At NA		County Chaves			
Producing Thru Tubing		Reservoir Temp. °F 112 @ 3800'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.7		State New Mexico			
L 3800	H 3800	Gg .826	% CO ₂ 17.4	% N ₂ 8.087	% H ₂ S	Prover 2"	Meter Run	Taps			

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	2		1.25		7.37		950	61			1 hour
2.	2		1.25		17.68		920	64			1 hour
3.	2		1.25		19.65		900	63			1 hour
4.	2		1.25		25.54		870	65			1 hour
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mscf/d
1.	73.70			.999	1.211	1.16	764
2.	73.70			.996	1.211	1.15	1812
3.	73.70			.997	1.211	1.155	2017
4.	73.70			.995	1.211	1.147	2606
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	1.46	456	1.27	.739	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	1.43	457	1.28	.746	Specific Gravity Separator Gas _____ X X X X X X X X
3.	1.41	456	1.27	.75	Specific Gravity Flowing Fluid _____ X X X X X
4.	1.36	457	1.28	.76	Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

NO.	P _t	P _w	P _w ²	P _t ² - P _w ²
1		1103	1218	38
2		1086	1180	76
3		1069	1142	112
4		1053	1108	146
5				

(1) $\frac{P_t^2}{P_t^2 - P_w^2} = 8.58$

(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 3.26$

ACF = Q $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 8500$

*Posted ID-2
& Comp. Book
SI
3-5-82*

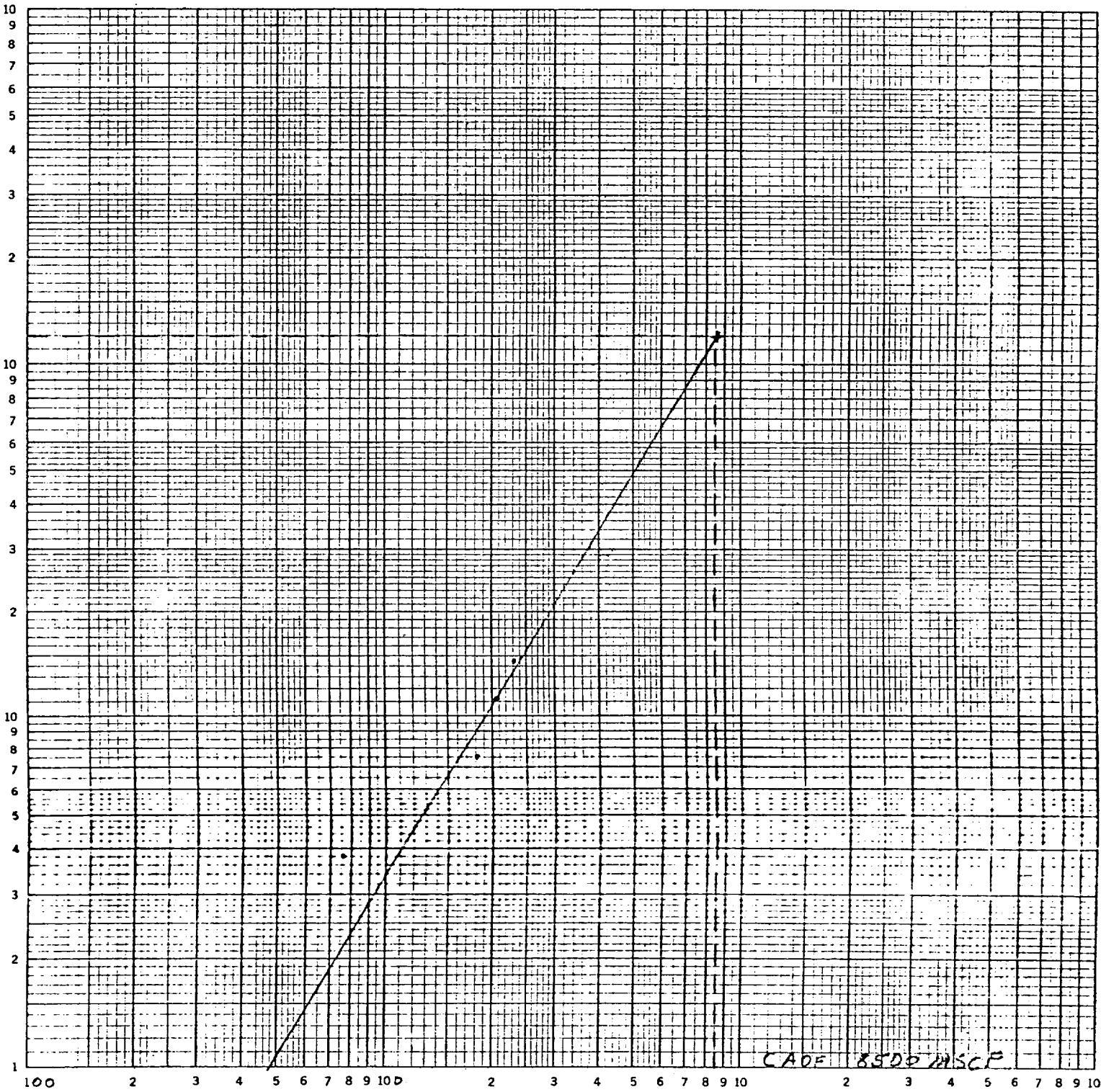
Absolute Open Flow	8500	Mscf/d P.S.I.A.	Angle of Slope θ	Slope, n	.55
Remarks:					
Approved By: _____		Conducted By: M. Kelly		Checked By:	

McClellan Oil Corp

MOC

$P = P^s(1000)$
467400

K₀Σ LOGARITHMIC 3 X 3 CYCLES
HEUVEL & ESSER CO. MADE IN U.S.A.



Q MSCF

CAOF 8500 MSCF