NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT A[illegible] ONE POINT BACK PRESSURE TEST[illegible] OR GAS WELL

Form C-122
Revised 9-1-65

C/SF
C-122

RECEIVED
APR 21 1982
O. C. D.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 4-14-81	
Company: MESA PETROLEUM CO. ✓		Connection: UNCONNECTED			
Pool: ~~Focos Slope~~ UNDESIGNATED ABO		Formation: ABO			Unit:
Completion Date: 4-14-82	Total Depth: 4150'	Plug Back TD: 4062'	Elevation: 3796'	Farm or Lease Name: RIC	
Csg. Size: 4½" / Wt.: 10.5# / d: / Set At: 4129'		Perforations: From 3500' To 3668'		Well No.: 5	
Tbg. Size: 2 3/8" / Wt.: 4.7# / d: / Set At: 3595'		Perforations: From OPEN ENDED To		Unit: M / Sec.: 20 / Twp.: 6S / Rge.: 25E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: NONE		County: CHAVES	
Producing Thru: TUBING	Reservoir Temp. °F: 101 @ 4150'	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2	State: NEW MEXICO	
L:	H:	Gg: .65	% CO_2: 1	% N_2: 1	% H_2S:
Prover: CHOKE	Meter Run:	Taps:			

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						930		925		72 HR SI
1.	CHOKE	15/64"	840		84	840	84	855		1 HR
2.	COEFF.	17/64"	760		87	760	87	785		1 HR
3.		20/64"	625		87	625	87	670		1 HR
4.		23/64"	495		85	495	85	565		1 HR
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.9165	CHOKE	853	.9777	1.240		948
2.	1.187	CHOKE	773	.9750	1.240		1109
3.	1.645	CHOKE	638	.9750	1.240		1269
4.	2.180	CHOKE	508	.9768	1.240		1347
5.							

NO.	P_t	Temp. °R	T_r	Z
1.				
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas _____ XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX _____
Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
Critical Temperature _____ R _____ R

P_c 938 P_c^2 880

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		868	753	127
2		798	637	243
3		683	466	414
4		578	334	546
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.6117$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.2695$

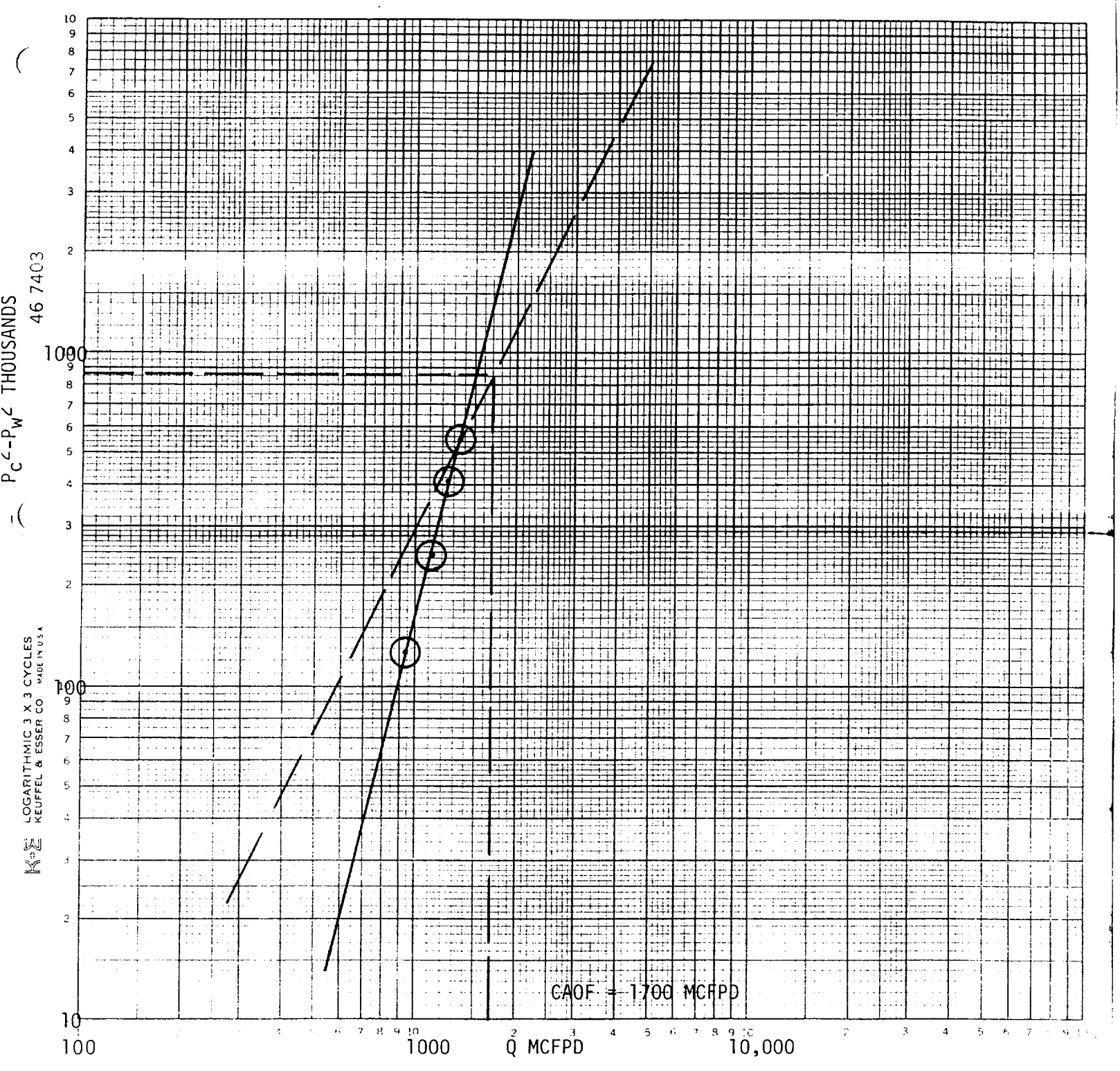
AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1700$

Absolute Open Flow 1700 Mcfd @ 15.025 Angle of Slope θ 63.5° Slope, n .5

Remarks: PLOT OF $P_c^2 - P_w^2$ vs Q YIELDED A STRAIGHT LINE WITH A θ GREATER THAN 63.5°. DREW 63.5° LINE THROUGH HIGHEST POINT.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	JAMES CRAIG	E. L. BUTTROSS, JR. EBB 4-19-82	

M[illegible] PETROLEUM CO.
R[illegible] COM NO. 5
CHAVES CO., NM
4-14-82



ASSUMED N = .5 AND θ = 63.5°