

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

C/SF
C-122

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 4-23-82		APR 30 1982	
Company McCLELLAN OIL CORP /				Connection Air			O. C. D.	
Pool Undesignated <i>also</i>				Formation Abo			Unit ARTESIA, OFFICE	
Completion Date 4-18-82		Total Depth 4300		Plug Back TD 4067		Elevation 3545 Gr		Form or Lease Name Dana Fed
Csg. Size 4 1/2	Wt. 10.5	d 4.052	Set At 4222	Perforations: From 4006 To 4011			Well No. 3	
Tub. Size 2 3/8	Wt. 4.7	d 1.995	Set At 3942	Perforations: From To			Unit Sec. Twp. Rge. G 3 9S 25E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At None		County Chaves	
Producing Thru Tubing		Reservoir Temp. °F 99 @ 4000		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico
L	H	Gg .626	% CO ₂	% N ₂	% H ₂ S	Prover 2"	Meter Run	Temp

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1022	53			
1.	2	X	1.25		8		986	52			1 hr
2.	2	X	1.25		21		922	51			"
3.	2	X	1.25		42		867	52			"
4.	2	X	1.25		47		855	51			"
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	593			1.008	.979	1.108	648
2	838			1.008	.979	1.101	910
3	1240			1.008	.979	1.098	1343
4	1369			1.005	.979	1.094	1474
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/Sbl.
1.	1.55	528	1.42	.800	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	1.49	528	1.42	.815	Specific Gravity Separator Gas _____ X X X X X X X X
3.	1.42	528	1.42	.825	Specific Gravity Flowing Fluid _____ X X X X X
4.	1.34	528	1.42	.830	Critical Pressure _____ 671 _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ 373 _____ R _____ R

P _c 1161 P _c ² 1347		(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.463$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.01$	
NO.	P _w	P _w ²	P _c ² - P _w ²	$AOI^* = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2700$	
1	1119	1253	94		
2	1034	1069	277		
3	979	958	389		
4	872	761	586		
5					

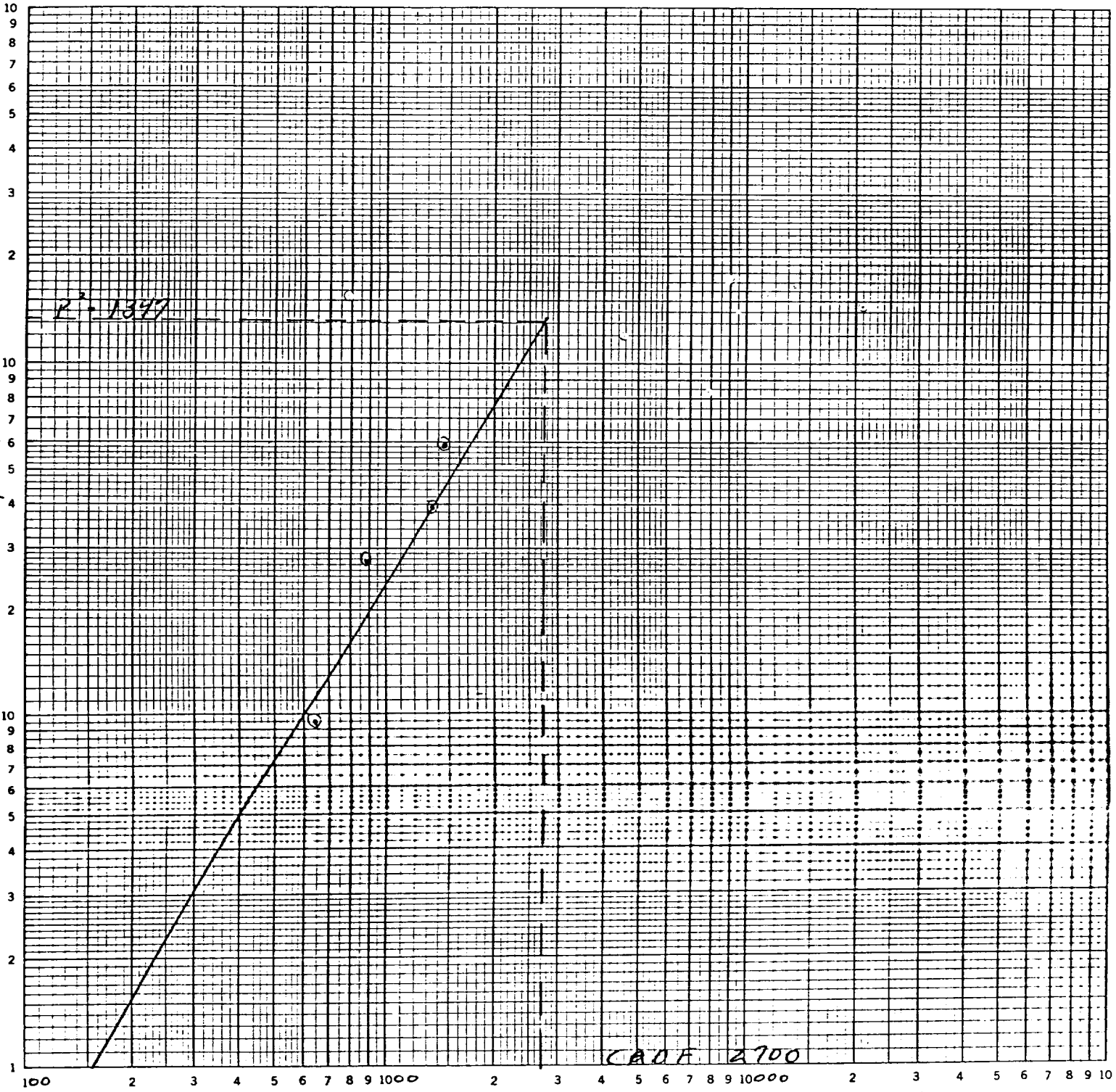
Absolute Open Flow _____ 2700 _____ Mcfd @ 15.025		Angle of Slope α _____ 30	Slope, n _____ .58
Remarks: Bottom hole pressures taken with Amerada type gauge			
Approved By Commission:		Conducted By: KELTIC SERVICE	Calculated By: M. Kelly
		Checked By:	

Posted I-D-2
 5-7-82
 Comp. - SF

46 7400

$P^2 - P^2$

K.E. LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.



Q
MSCFPD