

5F
file
c-122 file

Type Test ☒ Initial FOUR POINT ☐ Annual ☐ Special					Test Date RECEIVED 6-29-82		660 FNL		
Company STEVENS OPERATING					Connection AIR NEW WELL		660 FEL		
Tool UNDESIGNATED					Formation ABO		Unit A		
Completion Date 6-28-82		Total Depth 4520		Plug Back TD 4510 4484		ARTESIA, OFFICE 3753		Farm or Lease Name SUN FEDERAL	
Log Size 4.5	Wt. 10.5	d 4.052	Set At 4520	Perforations: From 4460 To 4472		Well No. 4			
Log Size 2.375	Wt. 4.7	d 1.995	Set At 4384	Perforations: From OPEN To ENDED		Unit A		Sec. Twp. Rge. 28 7S 26E	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE					Packer Set At 4384		County CHAVES		
Producing thru TUBING		Reservoir Temp. °F 98 4468		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State NEW MEXICO	
L 4468	H 4468	G _g .6388	% CO ₂ .255	% N ₂ 7.092	% H ₂ S	Prover 2.000	Meter Run	Taps	

FLOW DATA							TUBING DATA		B.H.P. DATA		Duration of Flow
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	CHOKE	
SI							1079				
1	2.00	X	.0625	980	.00	87	1027	96			1 HR
2	2.00	X	.125	620	.00	95	963	97			1 HR
3	2.00	X	.125	825	.00	97	887	99			1 HR
4	2.00	X	.025	260	.00	97	818	100			1 HR
5											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	0.06405	.00	993.2	.9750	1.252	1.070	83
2	.2648	.00	633.2	.9680	1.252	1.041	211
3	.2648	.00	838.2	.9662	1.252	1.055	283
4	1.087	.00	273.2	.9662	1.252	1.018	366
5							

NO	P _h	Temp. °F	T _g	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/Lbl.
1	1.51	547	1.55	.873	A.P.I. Gravity of Liquid Hydrocarbons _____ (Deg.)
2	.96	555	1.58	.922	Specific Gravity Separator Gas _____
3	1.27	557	1.58	.898	Specific Gravity Flowing Fluid _____
4	.41	557	1.58	.965	Critical Pressure _____ P.S.I.A.
5					Critical Temperature _____ °F

NO	P _c	P _w	P _w ²	P _c ² - P _w ²
1	1092.2	1192.9	1082.1	110.8
2			953.6	239.3
3			811.6	381.3
4			693.0	499.9
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.3863$

And $Q = \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 873.4$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.3863$

Partial ID 7-16-82

Calculate open flow	873.4	Mcf/d @ 15.025	Angle of Slope @	45°	Slope, n	1.000
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Remarks:	
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Approved By Commission:	Conducted By: DON BENNETT	Calculated By: BENNETT - CATHEY	Checked By:
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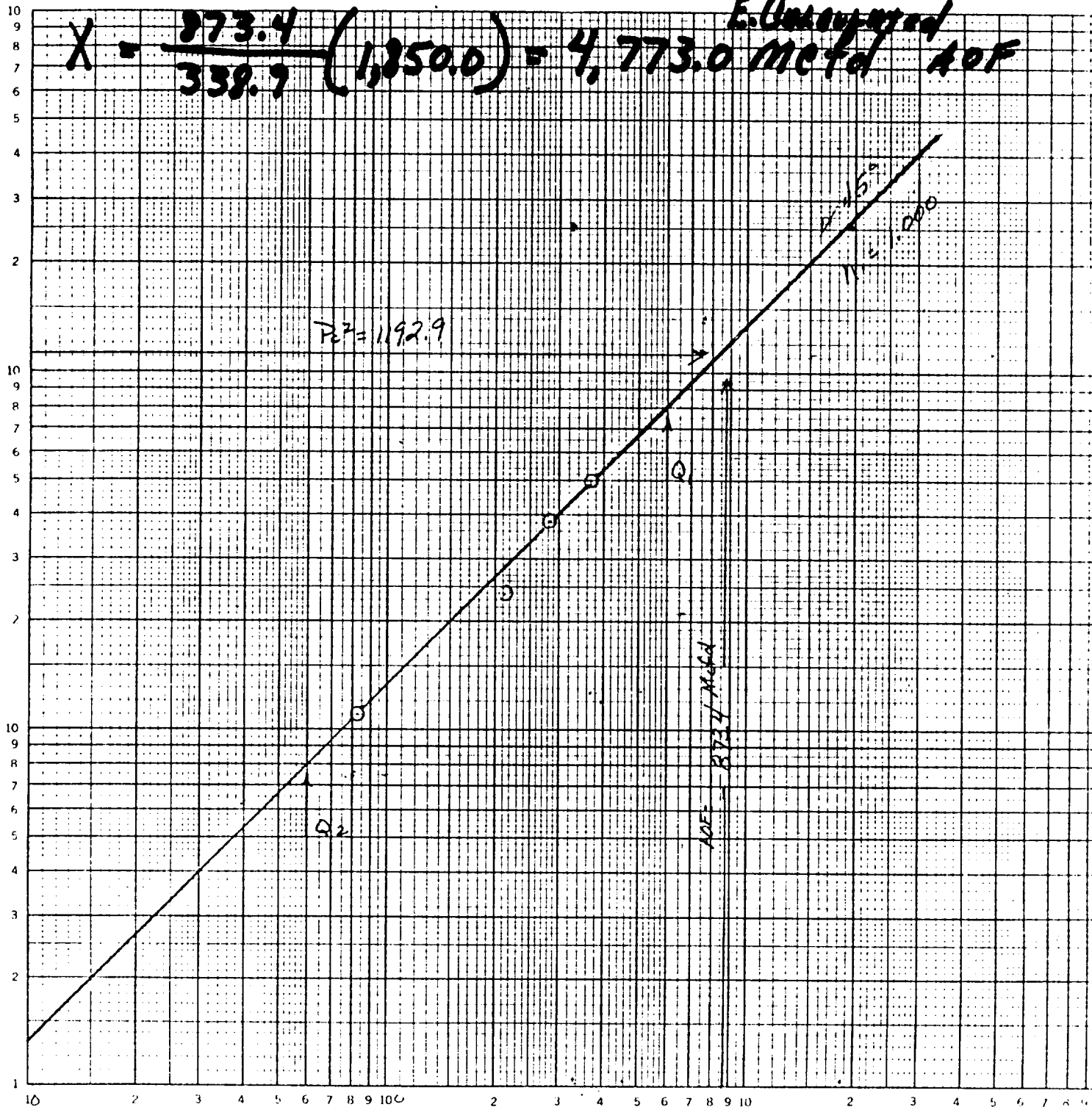
SUN FEDERAL #4
A 528 T 75 R26E
CHAYFS COUNTY
6-29-82

$$X = \frac{873.4}{338.9} (1,350.0) = 4,773.0 \text{ Mcfd AOF}$$

E. Outcropping

46 7400

K_oΣ LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.



$$\Delta \bar{P}^2 P_e^2 - P_w^2 = 800$$

$$\Delta \bar{P}^2 P_e^2 - P_w^2 = 80$$

$$Q_1 = 873.4$$

$$Q_2 = 60$$

$Q, \text{ Mcfd}$

$$\log Q_1 = 2.7781$$

$$\log Q_2 = 1.7781$$

$$\lambda = 1.000$$

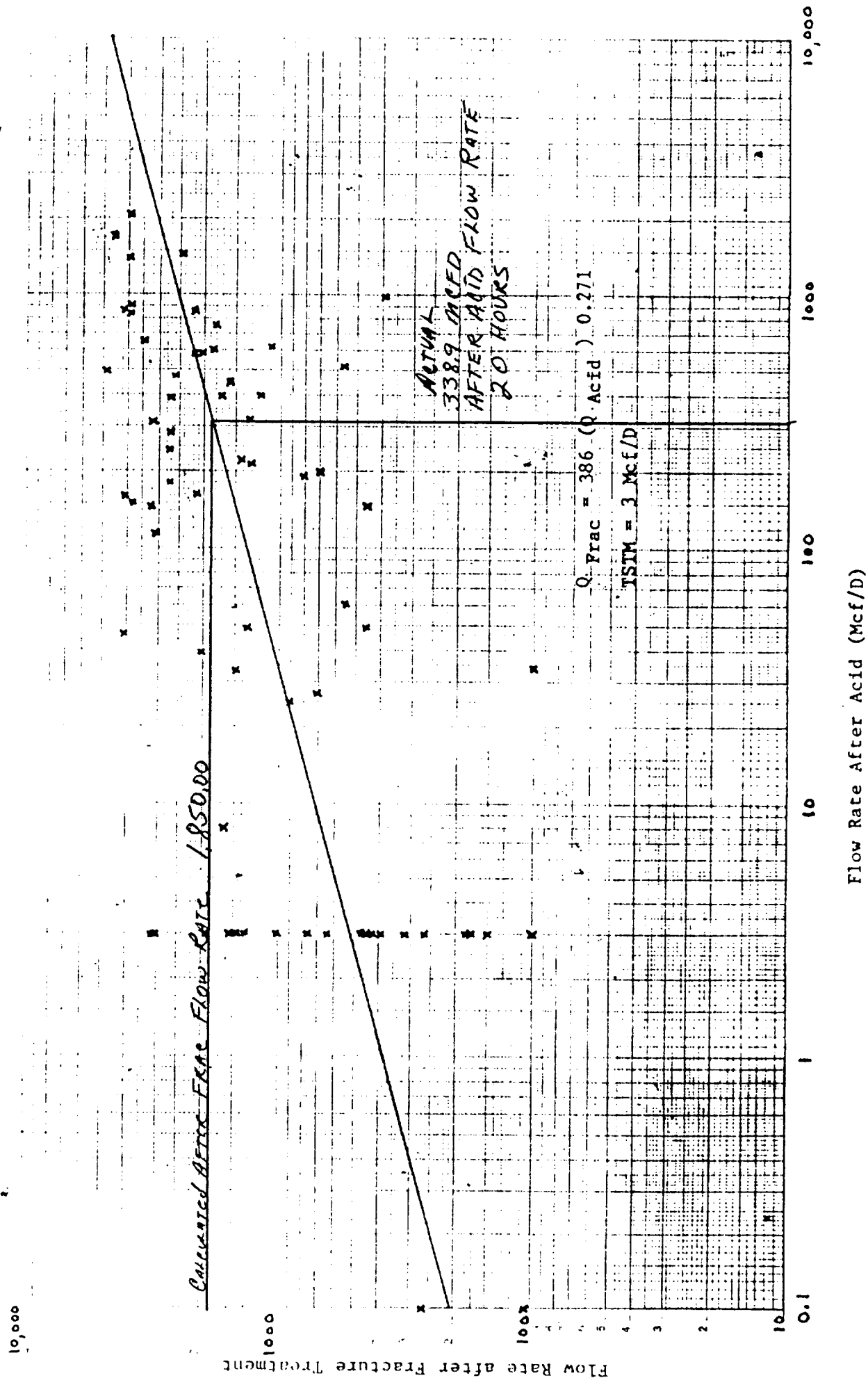
RECEIVED

CORRELATION OF FLOW RATES FOR ABO WELLS

JUL 12 1982

O. C. D.

ARTESIA, OFFICE



LOCATION: Unit _____ Section _____ Township _____ Range _____

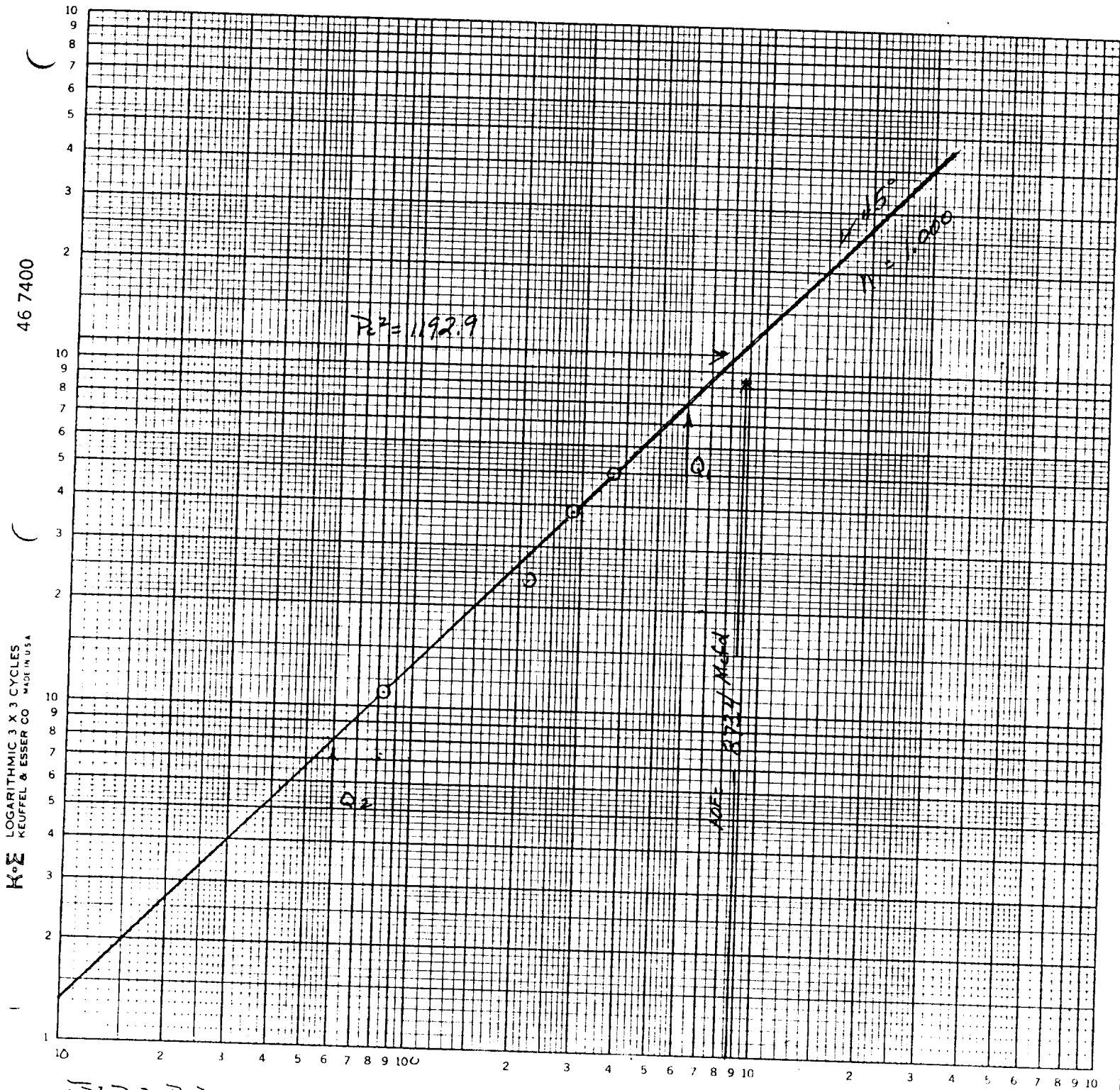
L 4468 H 4468 L/H 1.00 C .639 % CO₂ .25 % N₂ 7.09 % H₂S _____

d 1.995 F_r .018231 GH 2855. P_{cr} 658 T_{cr} 352

RATE 1 RATE 2 RATE 3 RATE 4

LINE	1	2	3	4	5	6	7	8		
1 Q _m	.83	.83	.211	.211	.283	.283	.366	.366		
2 T _w (W.H. °R)	534	534	534	534	534	534	534	534		
3 T _s (B.H. °R)	558	558	558	558	558	558	558	558		
4 T = ($\frac{1}{w} + 1$) S	546	546	546	546	546	546	546	546		
5 (Est.)	.870	.862	.875	.868	.883	.879	.891	.886		
6 T _z	475.0	470.7	477.8	473.9	482.1	479.9	486.5	483.8		
7 G _H /T _z	6.0102	6.0661	5.9759	6.0241	5.9218	5.9487	5.8686	5.9017		
8 e ^s (Table XV)	1.2528	1.2554	1.2512	1.2535	1.2486	1.2499	1.2462	1.2477		
9 1 - e ^s (Table XV)	.2017	.2035	.2008	.2022	.1991	.1999	.1975	.1985		
10 F ₁	1040.2	1040.2	976.2	976.2	900.2	900.2	831.2	831.2		
11 P ₁ 2/1000	1082.	1082.0	953.0	953.0	810.4	810.4	690.9	690.9		
12 F ₁ (Table XV)	.018231	.018231	.018231	.018231	.018231	.018231	.018231	.018231		
13 F ₂ = F ₁ T _z	8.6600	8.5805	8.7099	8.6402	8.7895	8.7497	8.8691	8.8194		
14 F ₃ = F ₂	.7187	.7122	1.8378	1.8231	2.4874	2.4761	3.2461	3.2279		
15 L/H (F _c Q _m) ²	.5166	.5072	3.3774	3.3236	6.1873	6.1314	10.5372	10.4192		
16 F _w = L/H (F _c Q _m) ² (1 - e ^s)	.1042	.1032	.6781	.6721	1.2321	1.2259	2.0815	2.0686		
17 P _w ² = P ₁ ² + F _w	1082.1	1082.1	953.6	953.6	811.6	811.6	693.0	693.0		
18 P _s ² = e ^s P _w ²	1355.6	1358.5	1193.2	1195.3	1013.4	1014.4	863.6	864.6		
19 F _s	1164.3	1165.6	1092.3	1093.3	1006.7	1007.2	929.3	929.8		
20 F = ($\frac{P_1}{P_s} + \frac{P_s}{P_1}$)	1102.2	1102.9	1034.3	1034.8	953.4	953.7	880.2	880.5		
21 P ₁ = (P/P _g)	1.6751	1.676	1.5718	1.5725	1.4489	1.4494	1.3378	1.338		
22 T ₁ = (T/T _{cr})	1.55	1.55	1.55	1.55	1.55	1.55	1.55	1.55		
23 Z (Table XI)	.862		.868		.879		.886			

SUN FEDERAL #4
 A 528 T 75 R 26E
 CHAVES COUNTY
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$$\Delta P^2 P_c^2 - P_w^2 = 800$$

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$$Q_1 = 800$$

$$Q_2 = 60$$

Q, Mcfd

$$\text{LOG } Q_1 = 2.7781$$

$$\text{LOG } Q_2 = 1.7781$$

$$h = 1,000$$



NEW-TEX LAB

PHONE 505/393-3561

P. O. BOX 1161

811 W. SNYDER

HOBBS, NEW MEXICO 88240

ANALYSIS CERTIFICATE

CLIENT: BENNETT & CATHEY INC.
ADDRESS: BOX 787
CITY, STATE: ARTESIA NM 88210

ANALYSIS NUMBER : 7737
DATE OF RUN : 6 30 82
DATE SECURED : 6 29 82

SAMPLE IDENT: STEVENS OPERATING - SUN FEDERAL #4
SAMPLING PRESS: SAMPLING TEMP:

***** GAS ANALYSIS *****

	MOLE PERCENT	GAL/ MCF
NITROGEN	7.093	
CARBON DIOXIDE	0.255	
METHANE	86.368	
ETHANE	3.828	1.021
PROPANE	1.177	0.323
ISO-BUTANE	0.232	0.076
NORMAL BUTANE	0.425	0.134
ISO-PENTANE	0.165	0.060
NORMAL PENTANE	0.182	0.066
HEXANES	0.125	0.051
HEPTANES PLUS	0.150	0.069
TOTAL	100.000	1.800

PROPANE GPM:	0.32	BUTANES GPM:	0.21
ETHANE GPM:	1.02	PENTANES PLUS GPM:	0.25

SPECIFIC GRAV (CALC): 0.6388
MOLE WEIGHT: 18.52

HHV-BTU/CU FT	PRESSURE (PSIA)	WET	DRY
14.696	1002		1019
14.650	998		1016
14.730	1004		1022
14.735	1004		1022

ANALYZED BY: DEANE SIMPSON

APPROVED BY

