

c/SF
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 12-4-82			
Company Mesa Petroleum Co. ✓		Connection Unconnected		DEC 9 1982	
Pool Undesignated ABO		Formation ABO		Unit O. C. D. ARTESIA, OFFICE	
Completion Date 12-4-82		Total Depth 3100'	Plug Back TD 3052'	Elevation 4022'	Farm or Lease Name Haley Com
Ceq. Size 4 1/2	Wt. 10.5#	Set At 3059'	Perforations: From 2775 To 2892		Well No. 1
Thq. Size 2 3/8	Wt. 4.7#	Set At 2842'	Perforations: From open ended To		Unit Sec. Twp. Rge. F 7 7S 23E
Type Well - Single - Brdenhead - G.C. or G.O. Multiple Single			Packer Set At None		County Chaves
Producing Thru Tubing		Reservoir Temp. °F 97 @ 3100'	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2	State New Mexico
L	H	C _g .65	% CO ₂ 1	% N ₂ 1	% H ₂ S 2" Critical Flow Prover

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							800		795		72 hr. SI
1.	2" X 1"			22		36	758	53	763		1 hr.
2.	2" X 1"			51		38	703	57	722		1 hr.
3.	2" X 1"			74		46	590	60	660		1 hr.
4.	2" X 1"			76		52	435	62	550		1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	17.09	Flow Prover	35	1.024	1.24		759
2	17.09	Flow Prover	64	1.022	1.24		1386
3	17.09	Flow Prover	87	1.014	1.24		1869
4	17.09	Flow Prover	89	1.008	1.24		1901
5.							

NO.	R _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/obl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 808	P _c ² 653				
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.9434$
1		776	602	51	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3941$
2		735	540	113	
3		673	452	201	
4		563	317	336	
5					

AOG = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2,700$

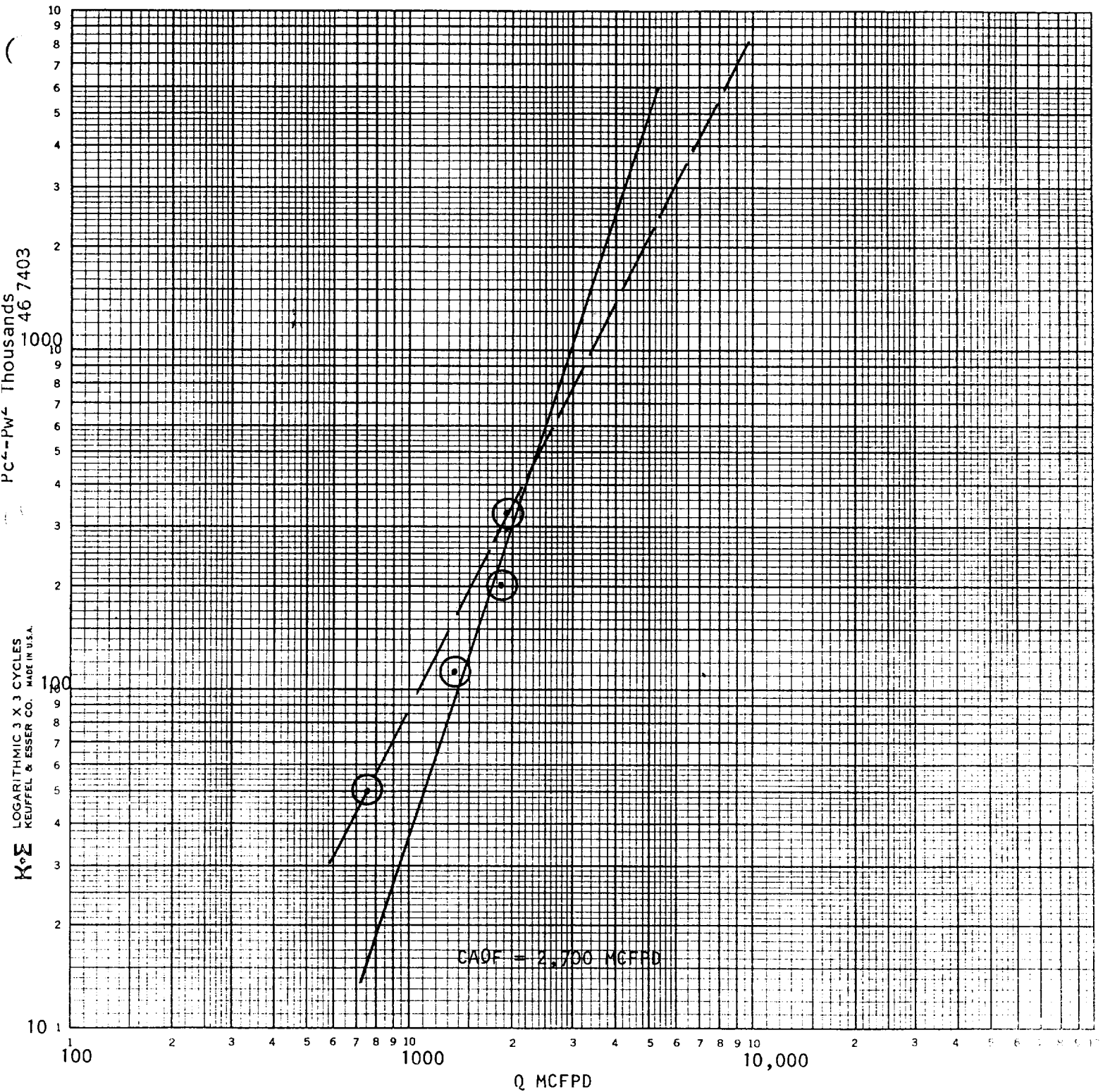
Post ID-2
12-17-82
Camp & BK

Absolute Open Flow 2,700	Mcfd @ 15.025	Angle of Slope θ 63.5°	Slope, n 5
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Remarks: Plot of P_c² - P_w² vs Q yielded a straight line with a θ greater than 63.5°.
Drew 63.5° line through highest point.

Approved By Division	Conducted By: James Craig	Calculated By: E. L. Buttross, Jr.	Checked By:
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Mesa Petroleum Co.
 Haley Com #1
 Chaves Co., NM
 12-4-82



Assumed N = .5 and $\theta = 63.5^\circ$