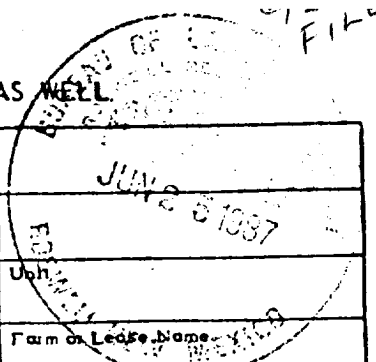


MULTIPOINT AND ONE POINT PRESSURE TEST FOR GAS WELL



Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		Test Date 5/29/87	
Company MCKAY OIL CORPORATION		Connection Air	
Pool West Pecos Slope		Formation Abo	
Completion Date 5/29/87		Total Depth 3400	
Plug Back TD 3138		Elevation 4258	
Casing Size 4-1/2"		Well No. #13	
Tubing Size 2-3/8"		Unit Sec. Twp. Rge. I 27 6S 22E	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single		County Chaves	
Producing Thru Tubing 2911.75		State N.M.	
Reservoir Temp. °F 92		Mean Annual Temp. °F 60	
Baro. Press. - P ₀ 13.2		Prover 2.00	
G _g 0.628		% CO ₂ 0.215	
% N ₂ 5.487		% H ₂ S 0	
Meter Run --		Taps --	

NO.	FLOW DATA				TUBING DATA		CASING DATA		Duration of Flow
	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							976	978	SI 72 HRS
1.	2.000	.250	118	--	86	954	86	958	60 MIN
2.	2.000	.375	113	--	68	923	68	927	60 MIN
3.	2.000	.625	55	--	61	867	61	874	60 MIN
4.	2.000	.750	47	--	54	800	54	814	60 MIN
5.									

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{spv}	Rate of Flow
							O. Mcid
1	1.087	--	131.2	.9759	1.262	1.009	177
2	2.378	--	126.2	.9924	1.262	1.011	380
3	6.473	--	68.2	.9990	1.262	1.006	560
4	9.453	--	60.2	1.0058	1.262	1.005	726
5.							

NO.	R	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio		Mcf/bbl.
					A.P.I. Gravity of Liquid Hydrocarbons	0	
1	0.20	546	1.56	.982	0	0	0
2	0.19	528	1.50	.979	.628	.628	XXXXXX
3	0.10	521	1.48	.989			XXXXXX
4	0.09	514	1.46	.990			
5							

NO.	P _c 991.2 P _c ² 982.5		P _w ²	P _c ² - P _w ²
	P _w	P _w ²		
1	971.2	943.2	943.2	39.3
2	940.2	884.0	884.0	98.5
3	887.2	787.1	787.1	195.4
4	827.2	684.3	684.3	298.2
5				

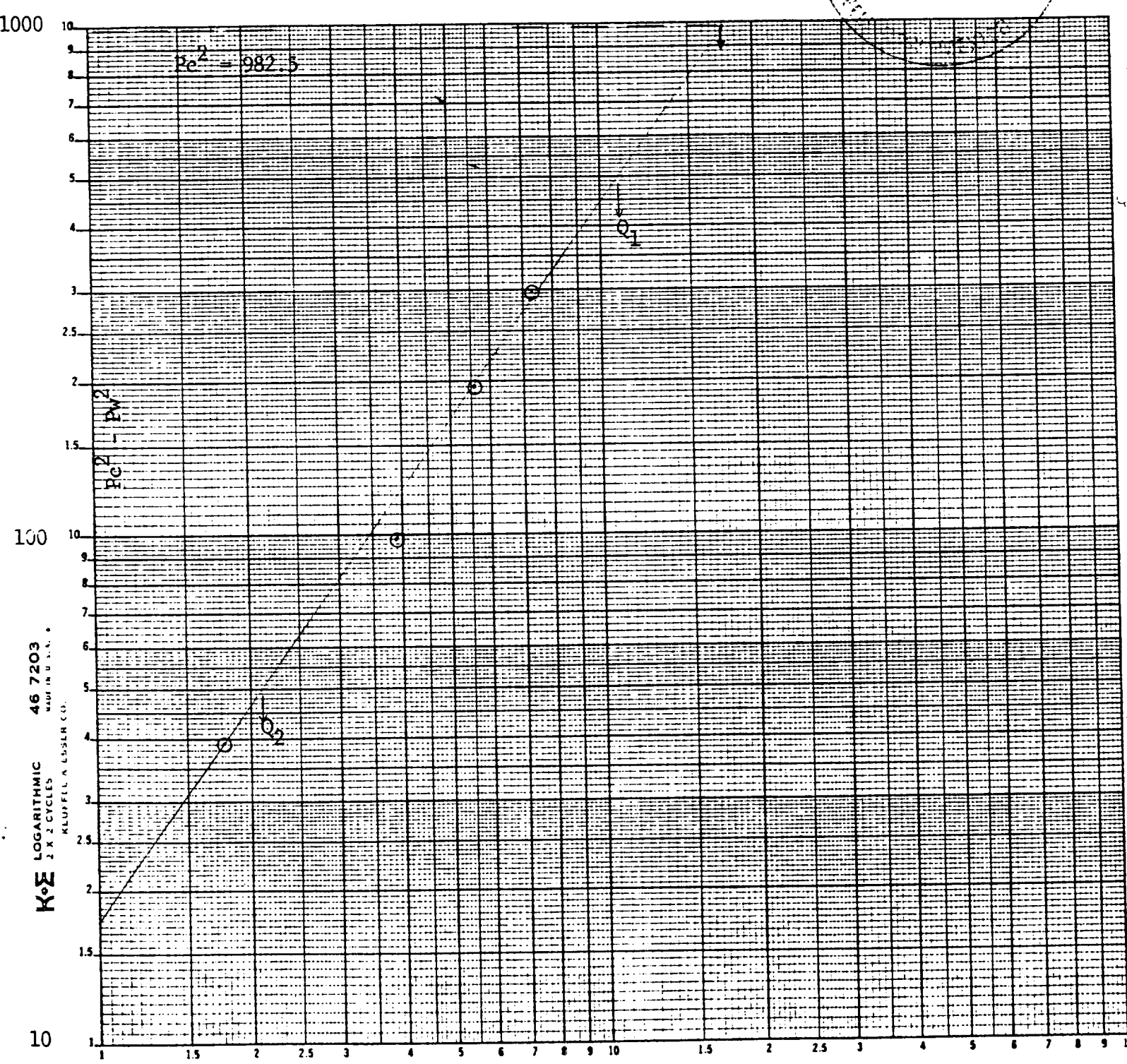
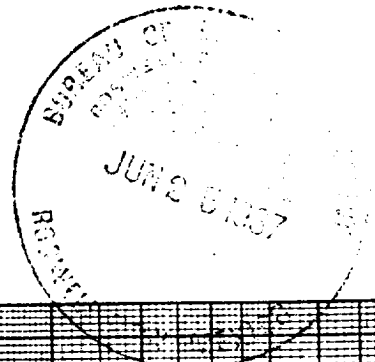
(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{25.0}{P_c^2 - P_w^2}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{9.830}{P_c^2 - P_w^2}$

AOF = 0 $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1740}{P_c^2 - P_w^2}$

Absolute Open Flow 1740 Mcid @ 15.025		Angle of Slope @ 54.625		Slope, n 0.71	
Remarks:					
Approved By Division		Conducted By: R. Snyder		Checked By: P. Stewart	
		Calculated By: C. Sanders			

MCKAY OIL CORPORATION
 Remmele Federal Comm. #13
 Sec. 27, T6S R22E
 05/29/87



K₀E LOGARITHMIC
 46 7203
 MADE IN U.S.A.
 KLUPFEL & ESSER CO.

1000
 Q, MCFPD
 Q₁ = 1080 MCFPD; log = 3.03342
 Q₂ = 211 MCFPD; log = 2.32428
 n = 0.70914
 n = 0.71
 AOF = 1740 MCFPD

