

clsf
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 3-10-89	
Company STEVENS OPERATING		Connection AIR	
Pool PECOS Slope ABO		Formation ABO	
Completion Date 3-9-89		Total Depth 4122	
Ceq. Size 5 1/2		Plug Back TD -	
Wt. -		Elevation 3597' GL	
Thg. Size 2-3/8		Set At 3859	
Type Well - Single - Dradhead - G.C. or G.O. Multiple SINGLE		Perforations: From 3683 To 3857	
Producing Thru TUBING		Perforations: From OPEN To ENDED	
Reservoir Temp. °F 60		Baro. Press. - P _g 13.2	
Mean Annual Temp. °F 60		Packer Set At NONE	
L -		H -	
G _g .62		% CO ₂ -	
% N ₂ -		% H ₂ S -	
Prover 2"		Meter Run -	
Taps -		Unit H 32 6S 26E	
Farm or Lease Name GESSERT		Well No. COM #1	
County CHAVES		State NEW MEXICO	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI											
1.	3/32	x	2	838		62	865		880		
2.	1/8	x	2	810		62	838		845		1 hr.
3.	3/16	x	2	728		62	810		815		"
4.	1/4	x	2	612		62	728		741		"
5.						62	612		630		"

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1.	.1410		851.2	.9981	1.27	1.0788	164
2.	.2648		823.2	.9981	1.27	1.0760	297
3.	.6082		741.2	.9981	1.27	1.0678	910
4.	1.0870		625.2	.9981	1.27	1.0564	910
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.										
2.										
3.										
4.										
5.										

P _c 965.2		P _c 931.61	
NO	P ₁ ²	P _w	P _w ²
1		937.2	878.3
2		906.2	821.2
3		826.2	682.6
4		691.2	477.8
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.05$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1596$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.75$

Post ID-2
4-28-89
comp & BK

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.05$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.75$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1596$

Post ID-2
4-28-89
comp + BK

Absolute Open Flow 1596 Mcfd @ 15.025 Angle of Slope 52° Slope, n .78

Remarks: ALL BOTTOMHOLE PRESSURES DONE WITH AMERADA TYPE GAUGE.

Approved By Division Conducted By: KELTIC SERVICES Calculated By: MIKE KELLY Checked By:

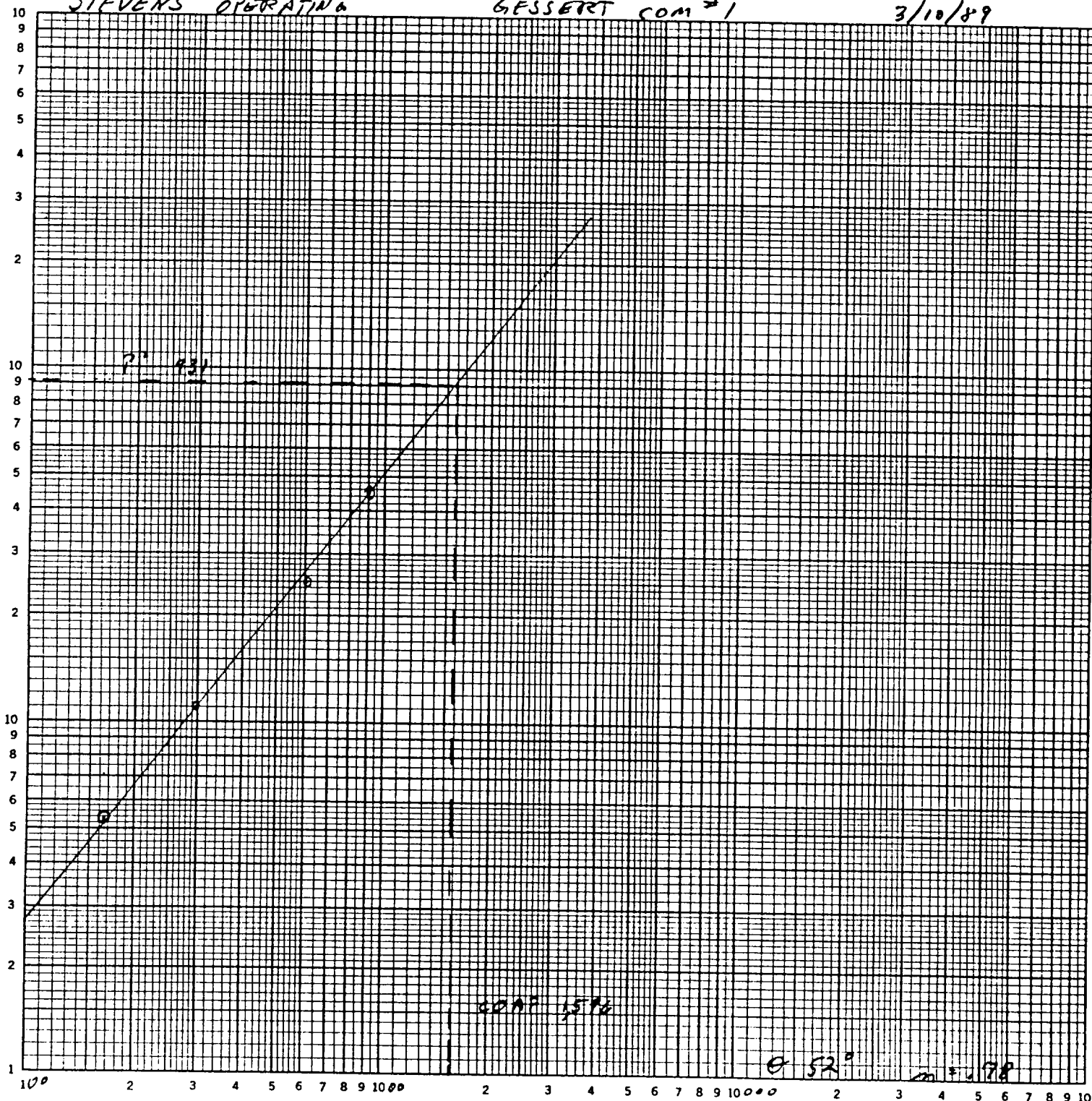
46 7400
P-T (000 J)

K.E. LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.

STEVENS OPERATING

GESSERT COM #1

3/10/89



Qent

Q
MSCPPD

KELTIC SERVICES

COMPANY	STEVENS	OPERATING	DATE	MAR 10-13, 89
LEASE	CESSERT	COM	WELL #	1
DEPTH	3850	SITP	890	PSIG
		SICP	910	PSIG

TIME HOURS	PRESSURE PSIG
0.00	678
0.25	734
0.50	770
0.75	792
1.00	815
1.25	830
1.50	843
1.75	853
2.00	861
2.50	878
3.00	891
3.50	899
4.00	909
4.50	916
5.00	919
6.00	927
7.00	934
8.00	939
9.00	944
10.00	947
15.00	959
20.00	967
30.00	980
40.00	987
50.00	989
60.00	992
70.00	993

KELTIC SERVICES

COMPANY	STEVENS OPERATING	DATE	MAR 10-13, 89
LEASE	CESSERT COM	WELL #	1
DEPTH	3850	SITP	865 PSIG
		SICP	880 PSIG

MULTI-FLOW TEST DATA.

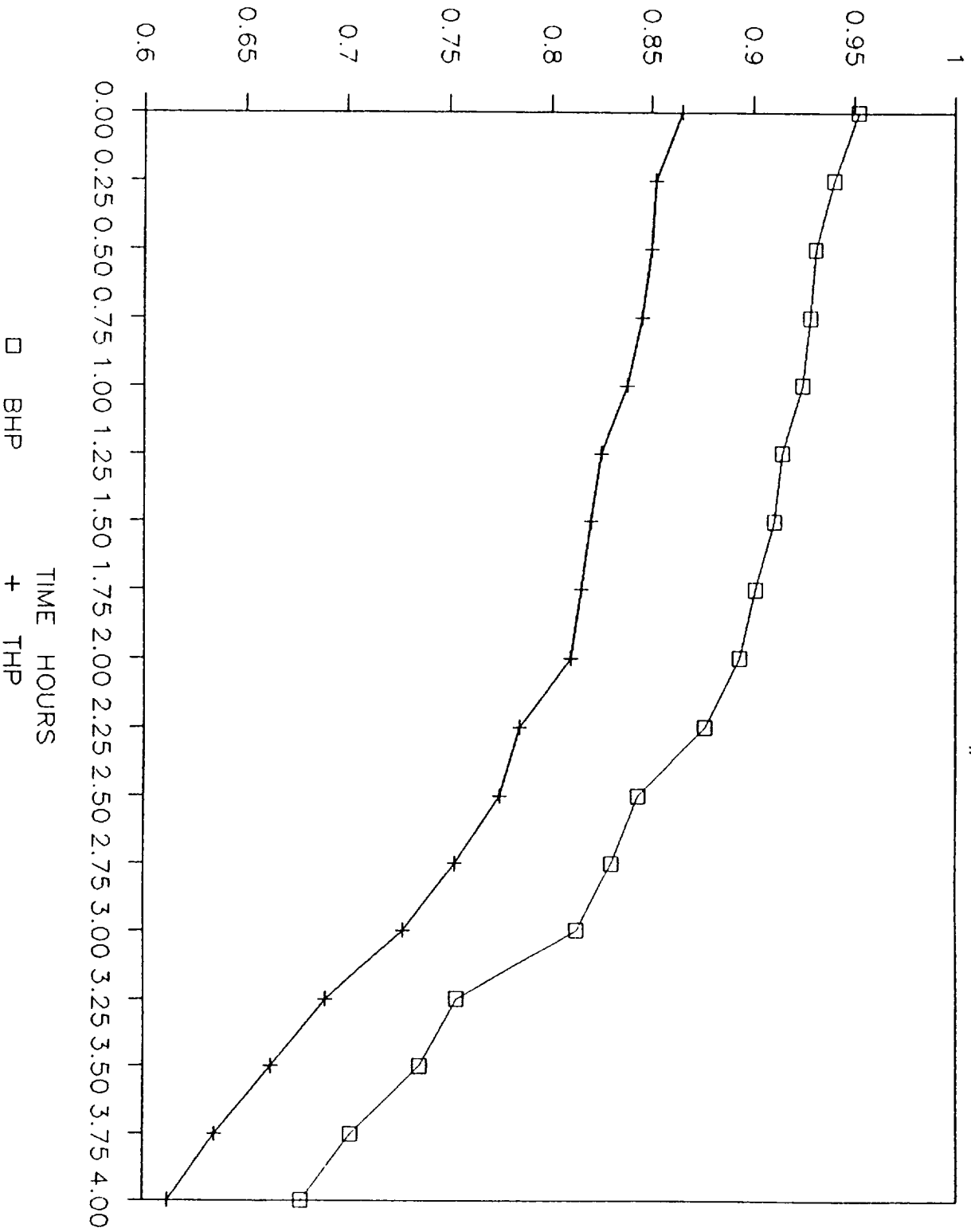
TIME HOURS	BHP PSIG	THP PSIG
0.00	952	865
0.25	940	852
0.50	931	850
0.75	928	845
1.00	924	838
1.25	914	825
1.50	910	820
1.75	901	815
2.00	893	810
2.25	876	785
2.50	843	775
2.75	830	753
3.00	813	728
3.25	754	690
3.50	736	663
3.75	702	635
4.00	678	612

Coeff.	Pres.	Temp	Grav.	Compres.	Flow Rate
0.1410	851.2	0.9981	1.2700	1.0788	164.1
0.2648	823.2	0.9981	1.2700	1.0760	297.3
0.6082	741.2	0.9981	1.2700	1.0678	610.2
1.0870	625.2	0.9981	1.2700	1.0564	910.0

STEVENS OPERATING

CESSERT COM #1

(Thousands)



PRESSURE PSIG

STEVENS OPERATING

CESSERT COM #1

