

SEP 18 '89

clsr
File

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 9-11-89				
Company McCLELLAN OIL CORP. ✓					Connection AIR				
Pool S, Pecos Slope <i>H/S</i>					Formation ABO				
Completion Date 9-12-89		Total Depth 4740		Plug Back TD 4687		Elevation 3755		Farm or Lease Name PENJACK <i>Fed.</i>	
Coq. Size 4-1/2	Wt. d	Set At TD	Perforations: From 4187 To 4529			Well No. 8			
Thq. Size 2-3/8	Wt. 4.7	Set At 4160	Perforations: From OPEN To ENDED			Unit Sec. Twp. Rge. <i>FD</i> 6 10S 26E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE					Packer Set At NONE				
Producing Thru TUBING		Reservoir Temp. °F 8		Mean Annual Temp. °F		Baro. Press. - P _a		State NEW MEXICO	
L	H	G _g .648	% CO ₂	% N ₂	% H ₂ S	Prover 2"		Meter Run	Taps

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI				930			930		926		
1.	2	x	3/32	890		60	890		890		1 hr.
2.	2	x	1/8	845		60	845		843		"
3.	2	x	7/32	640		60	640		645		"
4.	2	x	1/4	490		60	490		490		"
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	.141		903.2	1.000	1.2423	1.0965	173
2.	.2648		858.2	1.000	1.2423	1.0912	308
3.	.8393		653.2	1.000	1.2423	1.0677	723
4.	1.087		503.2	1.000	1.2423	1.0510	725
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ XXXXXXXXXX
3.					Specific Gravity Flowing Fluid _____ XXXXX
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c 1036	P _c ² 1073		
NO.	P _t ²	P _w	P _w ²
1		991	982
2		941	885
3		716	513
4		550	303
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.91$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1102$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.52$$

Post ID-2
9-29-89
comp + BK

Absolute Open Flow	1102	Mcf/d @ 15.025	Angle of Slope @	57°	Slope, n	.65
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Remarks: ALL BOTTOM HOLE PRESSURES DONE WITH AMERADA TYPE GAUGE.

Approved By Division	Conducted By:	Calculated By:	Checked By:
	KELTIC SERVICES	MIKE KELLY	