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O. C. D.
ARTESIA, OFFICE
Form C-122NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test [x] Initial [] Annual [] Special					Test Date 6/15/90	
Company Yates Petroleum Corporation				Connection Transwestern Pipeline Company		
Pool Pecos Slope				Formation Abo		Unit
Completion Date 2/17/90		Total Depth 4115.0'		Plug Back TD 4026.0'		Elevation 3871.2'
Csg Size 4.500"		Wt. 9.500#	d 4.090"	Set At 4115.0'	Perforations: From 3570.0' To 3882.0'	
Tbg Size 2.375"		Wt. 4.700#	d 1.995"	Set At 3478.0'	Perforations: From 0.0' To 0.0'	
Type Well Single					Packer Set At 3478.0'	
Producing Thru Tubing		Resv. Temp. °F 92 @ 3726'		Mean Temp. °F 62.0		Baro. Press. - Pa 13.2 psia.
L 3478.0'		H 3478.0'	Gg .646	%CO2 .02	%N2 4.89	%H2S 0.00
Prover 0.000"		Meter Run 2.000"		Taps Flange		

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO	Prover Size	Orifice X Size	Press. psig	Diff. hw	Temp. °F	Press. psig	Temp. °F	Press. psig	Temp. °F	
SI	0.000	X 0.000	0	0.0	97	825	0	0	0	0 hrs.
1.	2.067	X 1.000	290	8.0	98	794	62	0	0	24 hrs.
2.	2.067	X 1.000	310	31.8	99	734	62	0	0	24 hrs.
3.	2.067	X 1.000	330	42.0	97	718	62	0	0	24 hrs.
4.	2.067	X 1.000	335	57.0	99	690	62	0	0	24 hrs.
5.	0.000	X 0.000	0	0.0	0	0	0	0	0	0 hrs.

RATE OF FLOW CALCULATIONS

NO	Coefficient (24 HOUR)	$\sqrt{hwPm}$	Pressure Pm	Flow Temp Factor Ft.	Gravity Factor Fg	Super Compress. Fact. Fpv	Rate of Flow Q, Mcfd
1.	4.947	49.25	303.20	.965	1.244	1.020	298
2.	4.947	101.38	323.20	.964	1.244	1.021	614
3.	4.947	120.06	343.20	.966	1.244	1.023	730
4.	4.947	140.88	348.20	.964	1.244	1.023	855
5.	0.000	0.00	0.00	0.000	0.000	0.000	0

NO	Pr	Temp. °R	Tr	Z	Gas Liquid Hydrocarbon Ratio Dry	Mcf/bbl.
1.	.46	558	1.56	.962	A.P.I. Gravity of Liquid Hydrocarbons	0.000 Deg.
2.	.49	559	1.56	.959	Specific Gravity Separator Gas	.646
3.	.52	557	1.56	.956	Specific Gravity Flowing Fluid	xxxxxx
4.	.53	559	1.56	.956	Critical Pressure	662.3 PSIA
5.	0.00	0	0.00	0.000	Critical Temperature	357.5°R

Pc	838.2	Pc ²	702.6	
NO	Pt ²	Pw	Pw ²	Pc ² -Pw ² (1)
1.	651.6	807.8	652.6	50.0
2.	558.3	750.1	562.7	139.9
3.	534.7	735.4	540.9	161.7
4.	494.5	709.3	503.1	199.5
5.	0.0	0.0	0.0	0.0

$$\frac{Pc^2}{Pc^2 - Pw^2} = \frac{3.5252}{\left[\frac{Pc^2}{Pc^2 - Pw^2} \right]^n} = \frac{2.6094}{\left[\frac{Pc^2}{Pc^2 - Pw^2} \right]^n} = 2232 \text{ Mcfd}$$

Absolute Open Flow 2232 Mcfd @ 15.025 Angle of Slope, 0 37 Slope, n .761
Remarks:

Approved By:	Conducted By: David Weaver	Calculated By: Andrea Carpenter	Checked By:
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WORKSHEET FOR CALCULATION OF STATIC COLUMN WELLHEAD PRESSURE (Pw) C-122D

Adopted 9-1-65

DATE 5/6/90

COMPANY Yates Petroleum Corporation LEASE Geneva UI WELL NO. 2

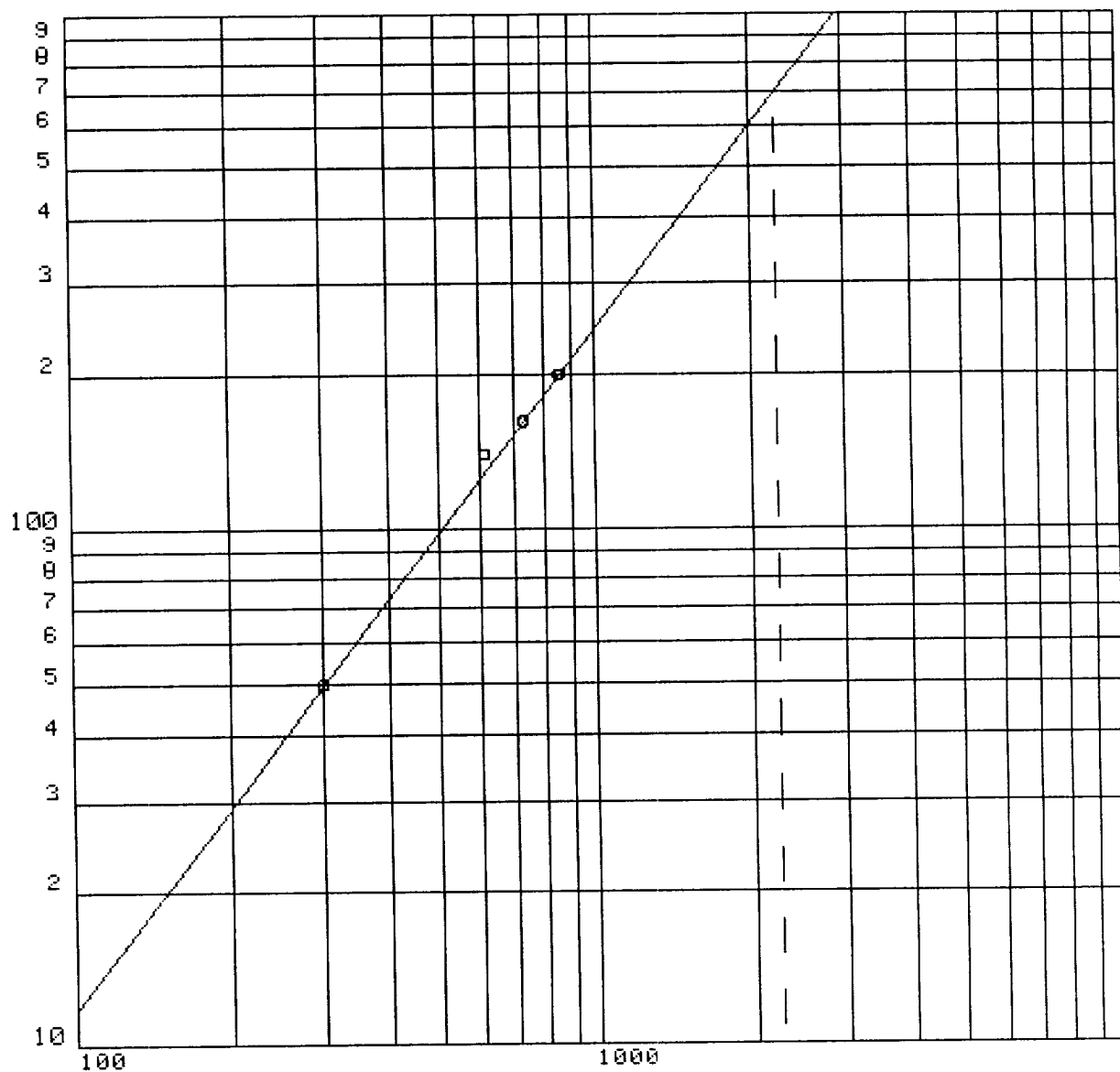
LOCATION: Unit B Section 20 Township 6S Range 25E

L 3478.0 H 3478.0 L/H 1.000 G .646 %CO₂ .02 %N₂ 4.89 %H₂S 0.00

d 1.995 Fr .017777 GH 2246.8 Pcr 662.3 Tcr 357.5

LINE	1st Rate	2nd Rate	3rd Rate	4th Rate	5th Rate
1 Qm	.298	.614	.730	.855	0.000
2 Tw(W.H.°R)	522.0	522.0	522.0	522.0	0.0
3 Ts(B.H.°R)	552.0	552.0	552.0	552.0	0.0
4 T=(Tw+Ts)/2	537.0	537.0	537.0	537.0	0.0
5 Z(Est.)	.879	.887	.890	.894	0.000
6 TZ	472.1	476.6	477.7	479.8	0.0
7 GH/TZ	4.759	4.715	4.703	4.683	0.000
8 e ^s (Table XIV)	1.195	1.193	1.193	1.192	0.000
9 1-e ^{-s} (Table XIV)	.163	.162	.162	.161	0.000
10 Pt	807.2	747.2	731.2	703.2	0.0
11 Pt ² /1000	651.6	558.3	534.7	494.5	0.0
12 Fr(Table XV)	.017777	.017777	.017777	.017777	0.000000
13 Fc=FrTZ	8.393	8.472	8.497	8.534	0.000
14 FcQm	2.505	5.206	6.205	7.299	0.000
15 L/H(FcQm) ²	6.273	27.100	38.500	53.283	0.000
16 Fw=L/H(FcQm) ² (1-e ^{-s})	1.025	4.392	6.222	8.577	0.000
17 Pw ² =Pt ² +Fw	652.6	562.7	540.9	503.1	0.0
18 Ps ² =e ^s Pw ²	780.1	671.5	645.1	599.6	0.0
19 Ps	883.2	819.5	803.2	774.3	0.0
20 P=(Pt+Ps)/2	845.2	783.3	767.2	738.8	0.0
21 Pr=(P/Pcr)	1.28	1.18	1.16	1.12	0.00
22 Tr=(T/Tcr)	1.50	1.50	1.50	1.50	0.00
23 Z(Table XI)	.879	.887	.890	.894	0.000

Company	Yates Petroleum Corporation
Well	Geneva UI No. 2
Location	B, 20-6S-25E
County	Chaves
Date	5/6/90



ROF= 2232

Q, Mcfd