

26. Perforation record (interval, size, and number)

4" Casing gun

6/28/95	7048 - 7052	13 Holes
7/3/95	7008 - 7015	22 Holes
7/24/95	6938 - 6946	16 Holes
	6954 - 6956	4 Holes
	6959 - 6964	10 Holes
	6983 - 6991	16 Holes
	6996 - 7000	8 Holes
	Total 6938 - 7000	54 Holes

27. ACID, SHOT, FRACTURE, CEMENT, SQUEEZE, ETC.

Depth Interval	Amount and Kind of Material Used
7048 - 7052	Acid w/250 gal 20% NEFE w/Inh
7048 - 7052	Sqz 50 Sx Cl "C" w/4% Halad 50 Sx Cl "C" neat Rev. out 25 Sx
7008 - 7015	Acid 500 gal 15% NEFE W/Inh
6938 - 7000	Acid 1500 gal 15% NEFE W/Inh

28. PRODUCTION

Add pressure test: (see attached results)
 Pressure Bomb
 07/07 - 07/14/95 ext res pres = 2518 psi
 perm = 1.3 md

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132225

PAGE NO. 1

TEST DATE:
07-JUL-1995

STAR

Schlumberger Transient Analysis Report Based on Model Verified Interpretation

Schlumberger

COMPANY: THORNTON OPERATING CORP.		WELL: NORTHERN LIGHTS #1	
TEST IDENTIFICATION		WELL LOCATION	
Test Type	Slickline BU	Field	Wildcat
Test No.	two	County	Chaves
Formation	Fusselman	State	NM
Test Interval (ft)	7008 to 7015	Sec/Twn/Rng	S7-TS8-R29E
COMPLETION CONFIGURATION		TEST STRING CONFIGURATION	
Total Depth (MD/TVD) (ft)		Tubing Length (ft)/I.D. (in) ..	
Casing/Liner I.D. (in)	5.500 / 4.767	Tubing Length (ft)/I.D. (in) ..	
Hole Size (in)	7.875	Packer Depth (ft)	
Perforated Interval (ft)	7008 to 7015	Gauge Depth (ft)/Type	6921/NG-00019
Shot Density (shots/ft)	3	Downhole Valve (Y/N)/Type	
Perforation Diameter (in)	.46	TEST CONDITIONS	
Net Pay (ft)	7	Tbg/Wellhead Pressure (psi) ..	
		Separator Pressure (psi)	
INTERPRETATION RESULTS		ROCK/FLUID/WELLBORE PROPERTIES	
Model of Behavior	Homogeneous	Oil Density (deg. API)	49.5
Fluid Type Used for Analysis ..	Oil	Basic Solids (%)	
Reservoir Pressure (psi)	2518 @ 6921'	Gas Gravity	0.65
Transmissibility (md.ft/cp) ..	10.97	GOR (scf/STB)	950 (est.)
Effective Permeability (md) ..	1.30	Water Cut (%)	0
Skin Factor	-1.5	Viscosity (cp)	0.823
Radius of Investigation (ft) ..	98	Total Compressibility (1/psi) ..	2.75e-4
		Porosity (%)	10
		Reservoir Temperature (F)	137
		Form.Vol.Factor (bbl/STB)	1.078

LAST RATE DURING TEST: 60 bopd

COMMENTS:

This is Model Verified interpretation of a 160 hour buildup on the well, Northern Lights #1. The test followed an acid job of 500 gallons. The test is a short flow period of 20.5 hours followed by swabbing for 6 hours. The swabbing crew reported a last rate of 2.5 bbls of oil per hour. The GOR is estimated at 950 scf/stb.

The data is modeled a homogeneous infinite system with decreasing wellbore storage and skin. The tested interval is indicated to have fair permeability to the produced oil for the reported 7 feet of net pay. There wellbore is stimulated at a -1.5 skin. The reservoir pressure is 2518 psia at 6921 feet. See page three for a rate prediction if the well skin is improved to a -4. Thank you for using Schlumberger Companies. For questions about this report Gil Hilsman (915) 684-0700.

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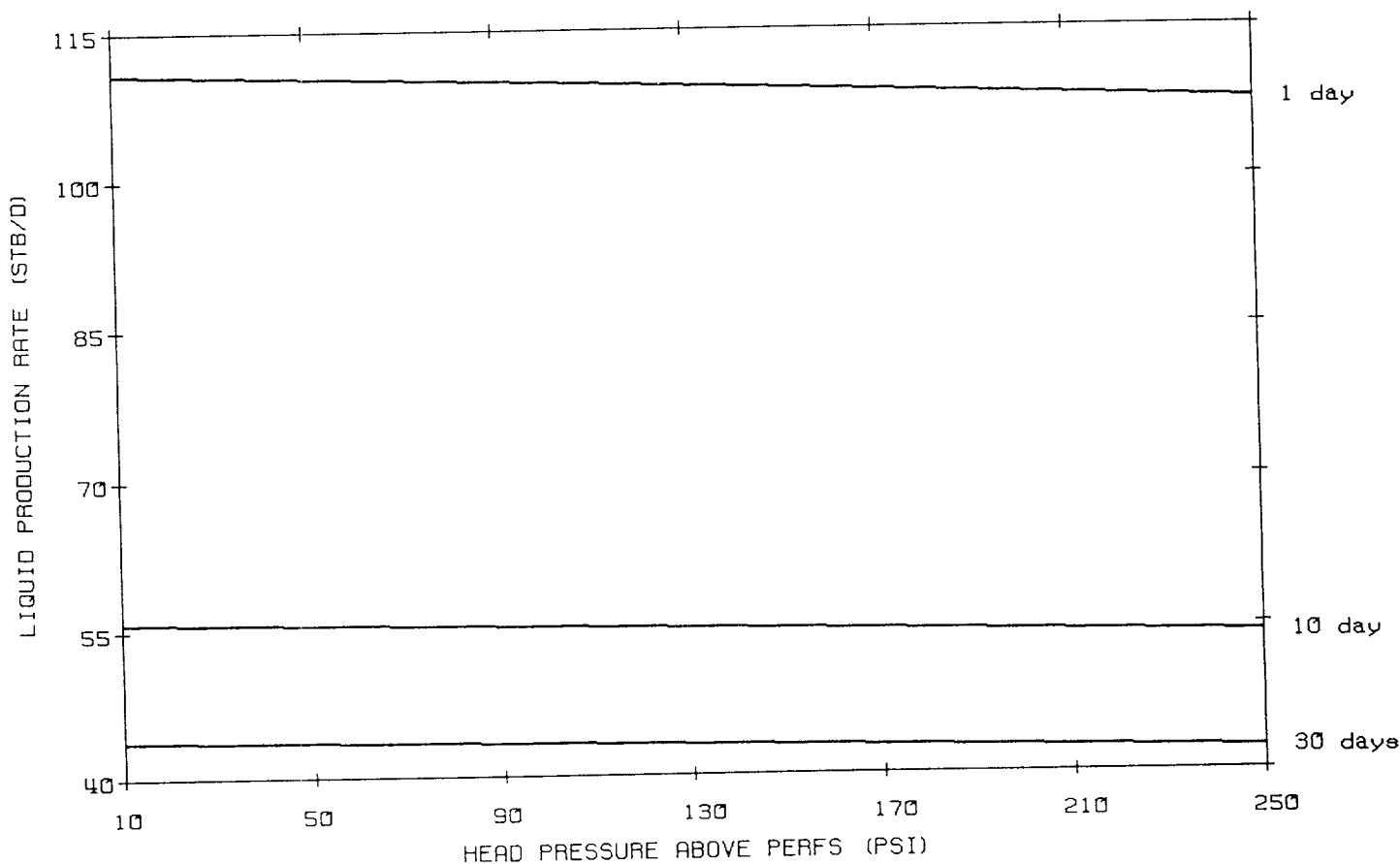
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Rate Prediction

Skin Improved to -4

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Below is a plot of the possible production from the tested interval if all the conditions of this projection are met. The plot is based on the model from this interpretation. Some of the conditions are as follows: pumping oil well; skin improved to -4.0; the formation continues to produce the same fluid at the same GLR; the formation remains homogeneous, infinite and constant for the drainage area of this prediction.



PRODUCTION RATE VS. HEAD PRESSURE ABOVE PERFS, TRANSIENT COND.
1 TO 30 DAYS

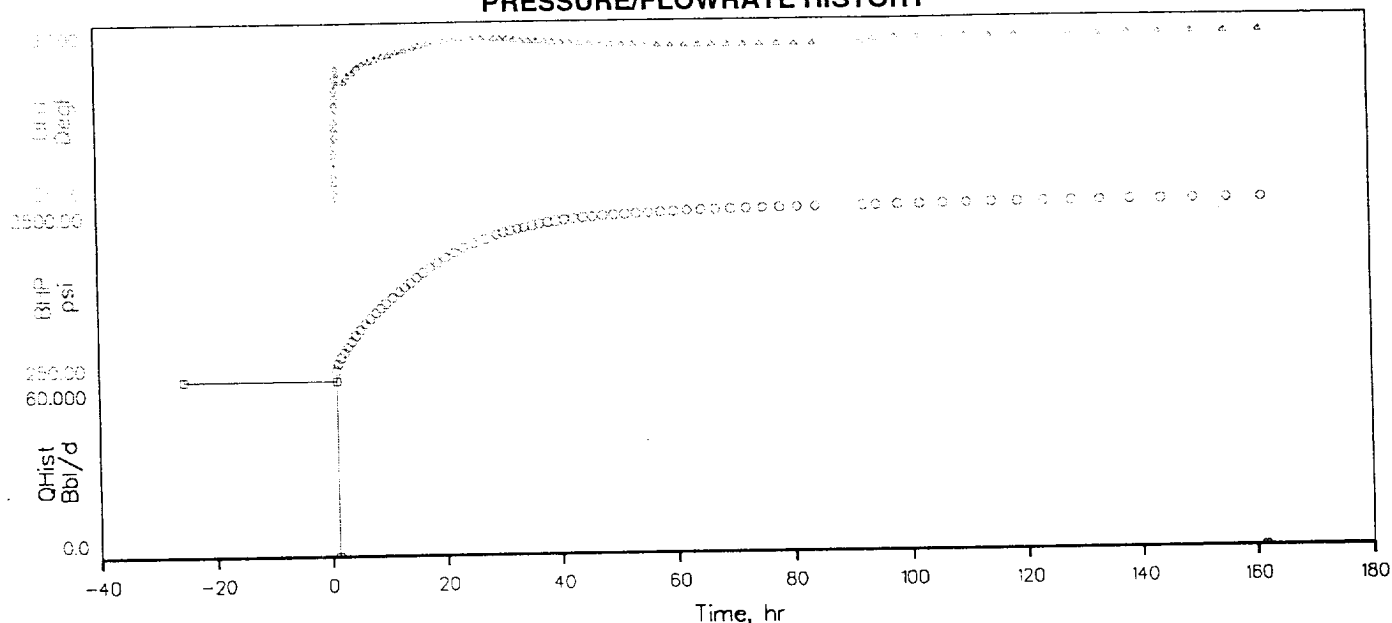
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DATA SUMMARY

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PRESSURE/FLOWRATE HISTORY



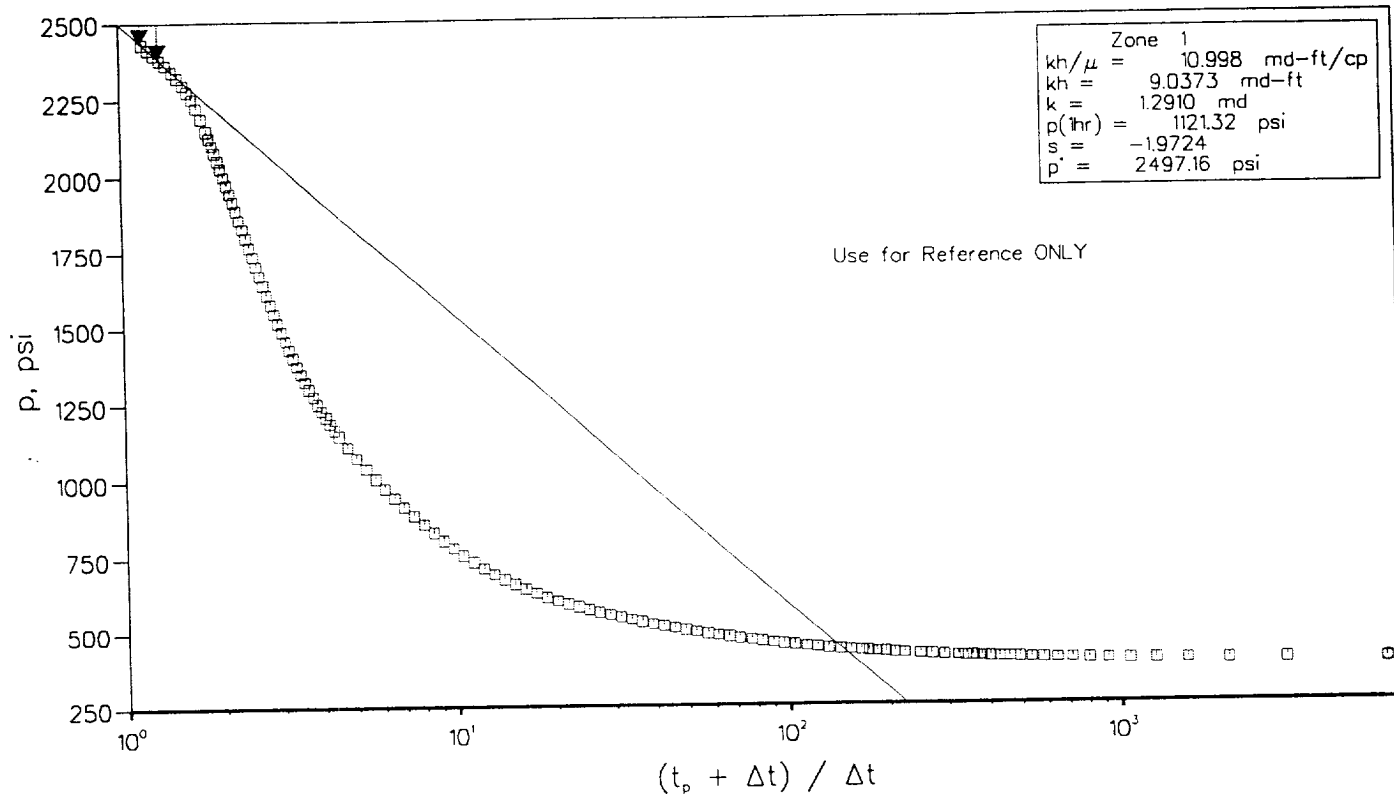
SEQUENCE OF EVENTS

EVENT NO.	DATE	TIME (HR:MIN)	DESCRIPTION	ELAPSED TIME (HR:MIN)	BHP
1	07-JUL	17:50	START FLOW	0:27	353.58
2	07-JUL	18:31	END FLOW & START SHUT-IN	1:08	386.87
3	14-JUL	10:50	END SHUT-IN	161:27	2434.04

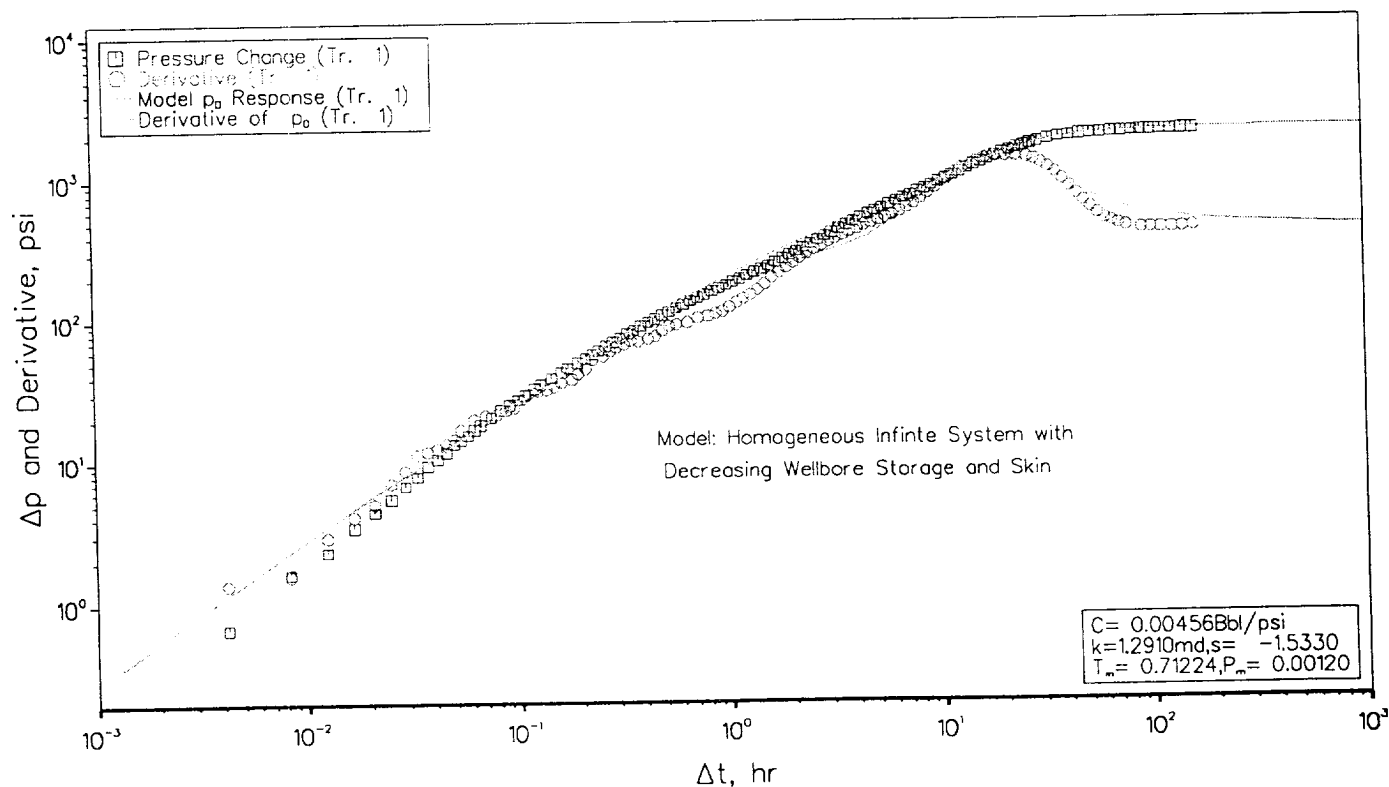
SUMMARY OF FLOW PERIODS

PERIOD	DURATION (HR:MIN)	PRESSURE		OIL FLOWRATE Bbl/D
		START	STOP	
# 1, DD	26:30	0.0	0.0	60.000
# 2, BU	160:19	386.87	2433.70	0.0

HORNER PLOT



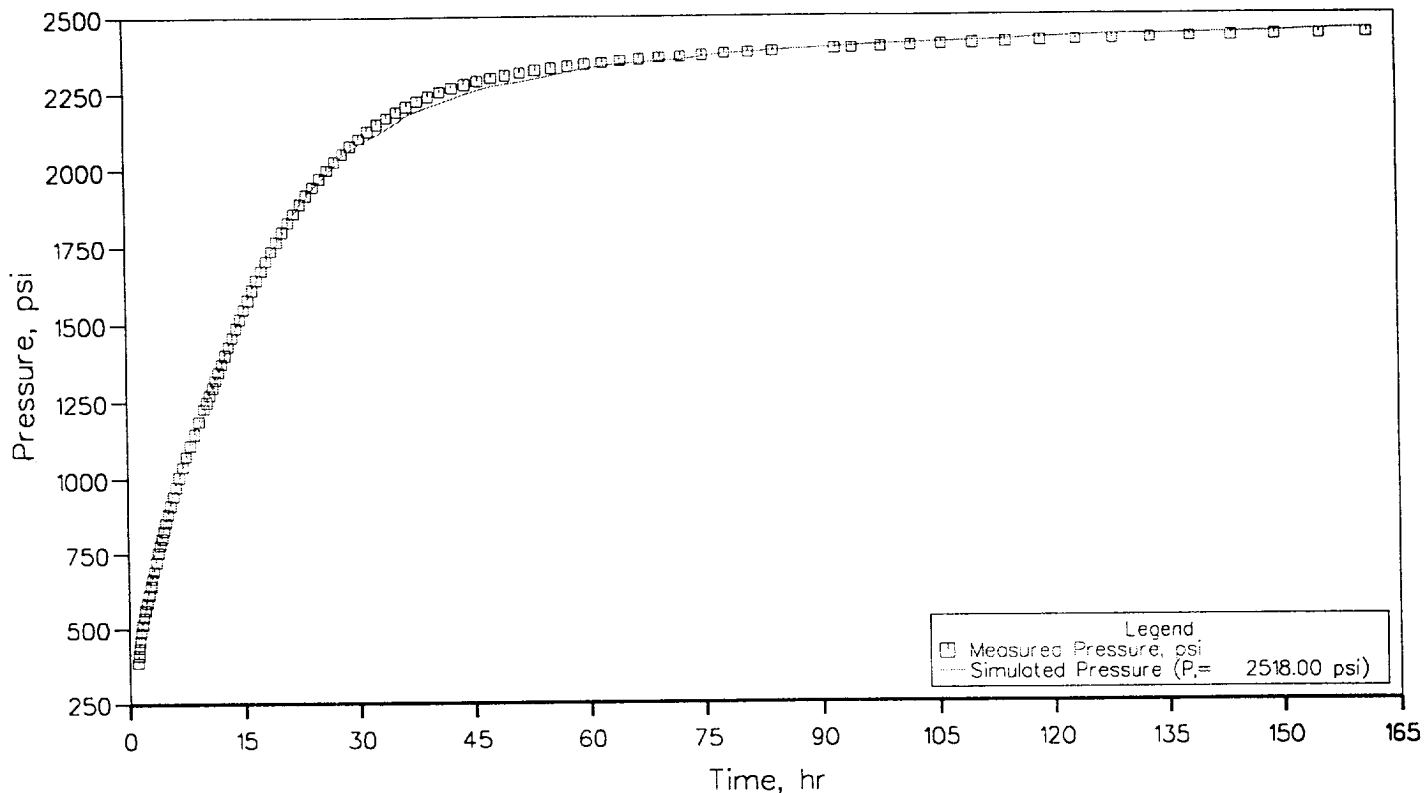
MULTI-RATE TYPE-CURVE MATCH



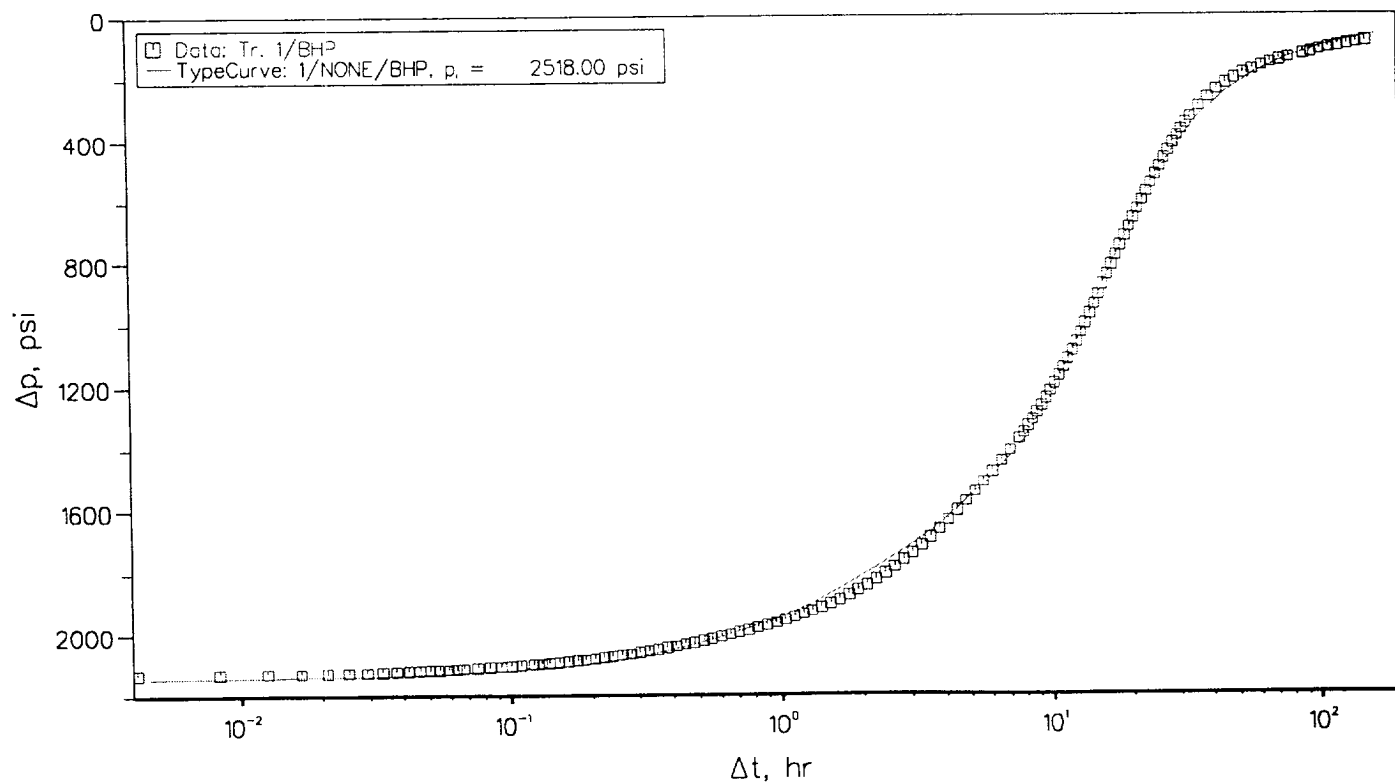
VERIFICATION PLOTS
Transient 1

Schlumberger

PRESSURE HISTORY SIMULATION

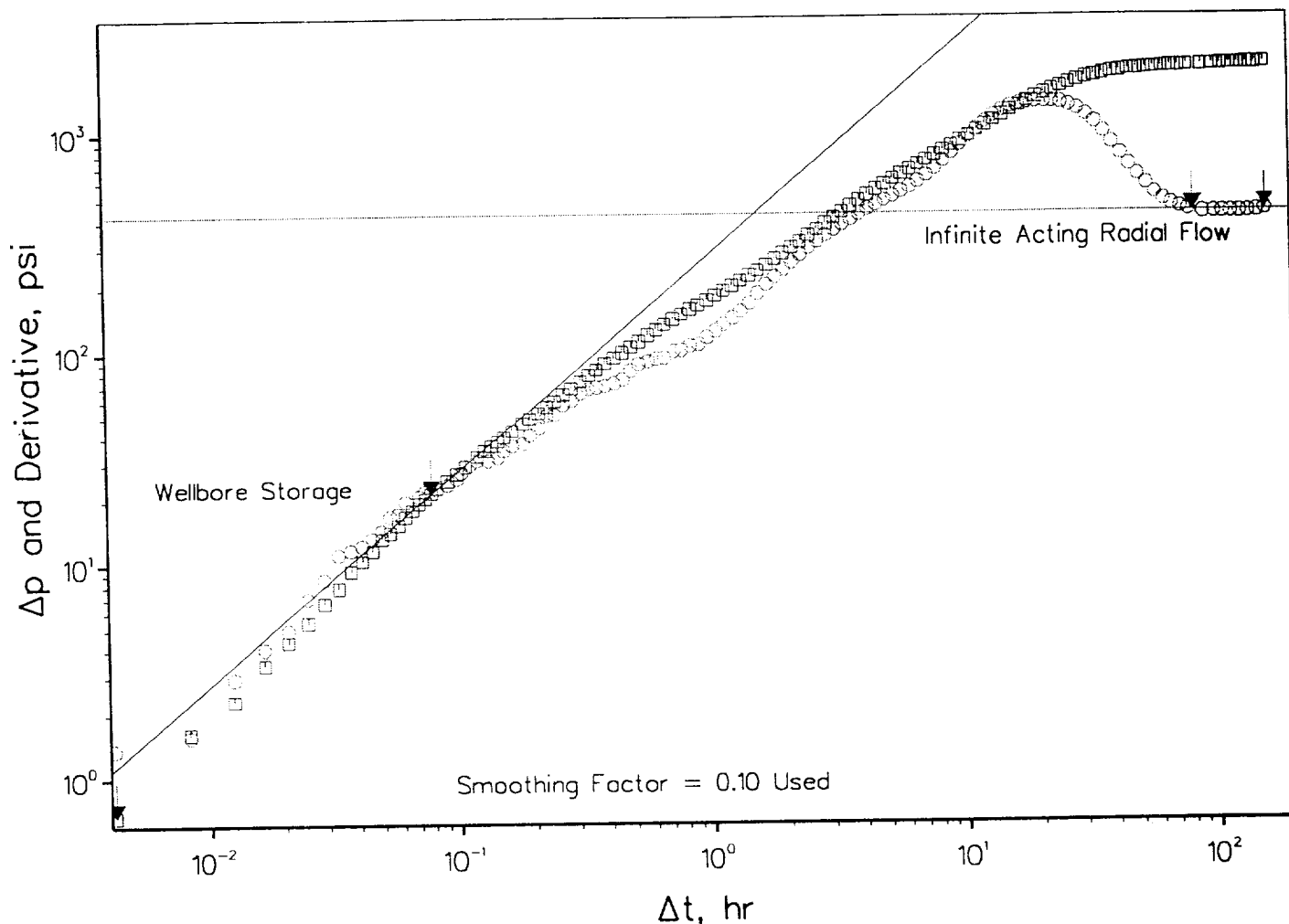


DIMENSIONLESS SUPERPOSITION PLOT



FLOW REGIME IDENTIFICATION
Transient 1

Schlumberger



Flow Regime Identification:

From the above plot, flow regimes influenced by inner boundary, reservoir and/or outer boundary conditions are identified if encountered during the test. From this a reservoir model can be generated that would attempt to describe all flow regimes, and matched to the test data.

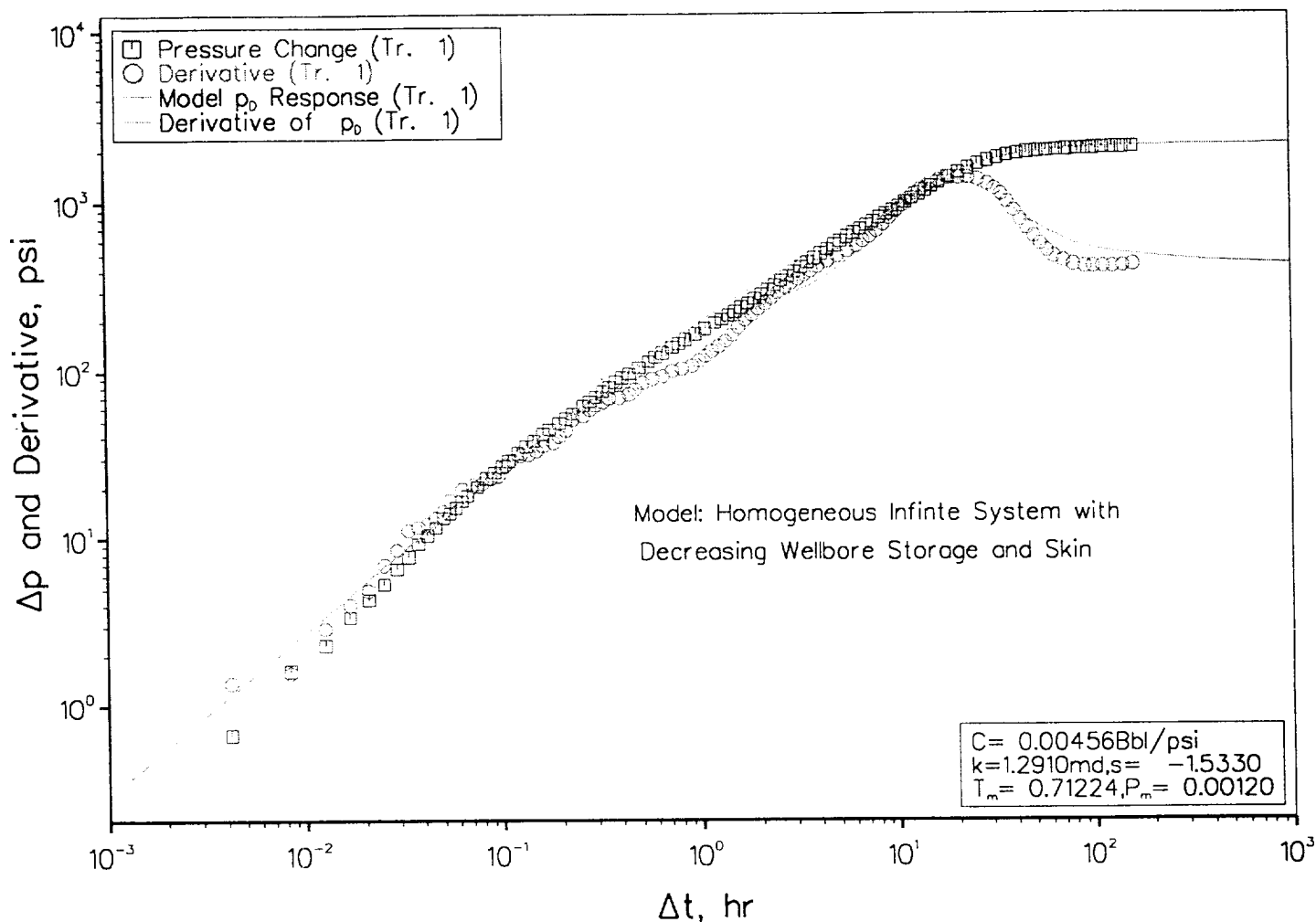
Some of the more common flow regimes are shown below. For a more detailed explanation of flow regime identification see SPE 18594, "Use of the Pressure Derivative for Diagnosing Pressure Transient Behavior"

..Note: All flow regimes listed below may not be observed during the test

Flow Regime	Log-Log Characteristic
Bilinear Flow	1/4 slope early time
Linear Flow	1/2 slope early time
Wellbore Storage	Unit slope early time
Double Porosity	Dip below IARF in middle time
Infinite Acting Radial Flow	Constant Plateau middle time
Single Sealing Fault	Constant Plateau (2 X IARF Plateau)
Two Faults at right angle to well	Constant Plateau (4 X IARF Plateau)

MULTI-RATE TYPE CURVE MATCH
Transient 1

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Middle-Time Flow Regime Analysis:

Log-log (Model Verified) Analysis:

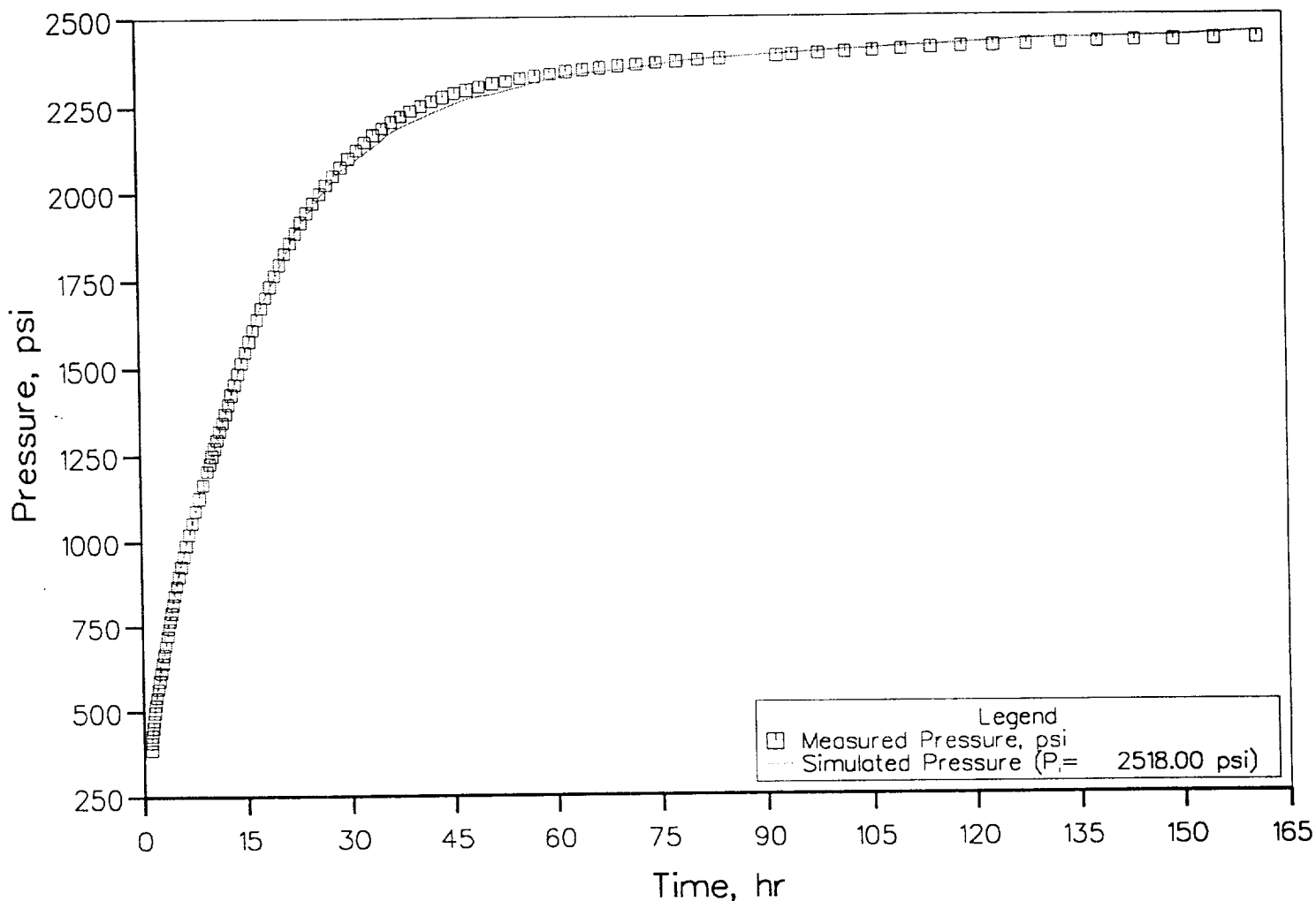
The above plot shows the Model-Verified, Multi-Rate Type Curve analysis match obtained for the test data. The type-curve generated represents the the total reservoir system. Using the match parameters and the equations listed below, the desired IARF reservoir parameters were obtained.

$$Kh = 141.2 * Dq * \mu * B * P_m$$

$$C = (kh / 3389 * \mu) * 1/T_m$$

$$CD = (0.8936 * C) / (\phi * Ct * h * rw^{**2})$$

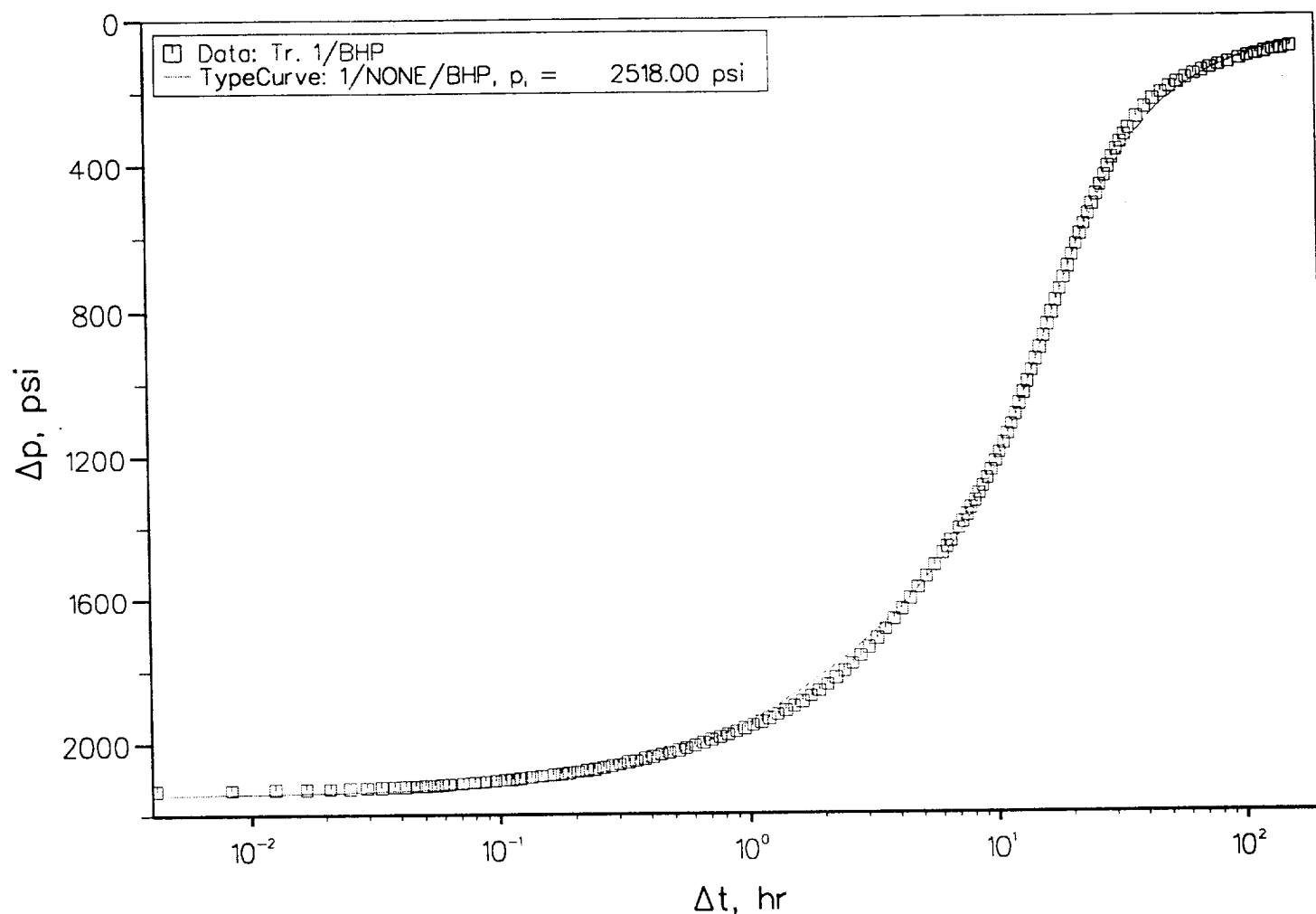
$$S = 0.5 * \ln (CDE2S / CD)$$



Checking Procedure (Pressure History Match)

The above plot is used as a check of the interpretation procedures.

The plot presents on cartesian coordinates, for the given transient, the data generated using the interpretation parameters, plotted against the actual test data. The match takes into account the total system, therefore, it provides a look at quality of the match.



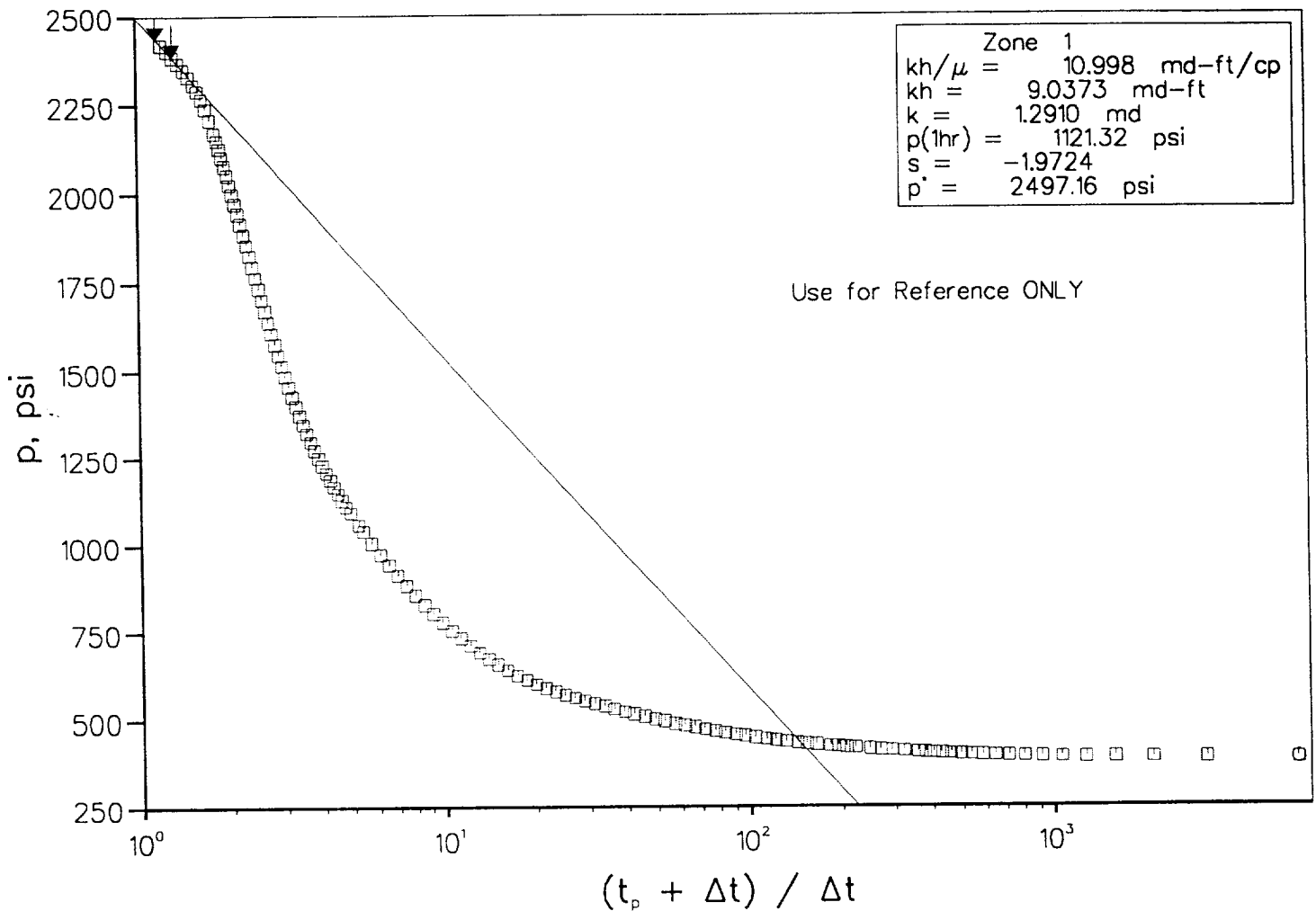
Checking Procedure (Dimensionless Superposition):

The above plot is used as a check of the interpretation procedures.

The plot presents on semi-log coordinates, for the given transient the data generated using the interpretation parameters, plotted against the actual test data. As with the pressure history match, the dimensionless superposition type-curve takes into account the total system. The dimensionless superposition type-curve highlights different time ranges from the pressure history simulation, therefore, it provides a different look at quality of the match.

SEMI-LOG ANALYSIS
Transient 1

Schlumberger



Semi-log (Superposition) Analysis:

Due to the fact that there were rate changes prior to the well test the semi-log analysis was conducted using the Superposition time function. above plot contains the values obtained from the straight line drawn through the IARF period. The equations listed below were used to determine the desired reservoir parameters

$$Kh = (162.6 * \mu * B) / m'$$

$$S = 1.151 * \left[\frac{(P_{1hr} - P_0)}{m''(Q_n - 1 - Q_n)} - \log \left(\frac{K}{\phi * \mu * C_t * r_w^{**2}} \right) + 3.2275 \right]$$

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FLOW RATE HISTORY

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FLOW HISTORY

Reference Date: 07-JUL-1995 17:23:00

Date	Time of Day	Elapsed Time	Flowrate	
DD-MMM-YYYY	HH:MM:SS	HR	Bbl/d	
06-JUL-1995	16:01:38	-25.3560	60.0000	
07-JUL-1995	18:31:30	1.1417	0.0000	

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FIELD SEQUENCE OF EVENTS

Schlumberger

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DD-MON	HR-MN	DESCRIPTION	DEPTH or PRESSURE
07-JUL	16:30	AOL, rig up; swabbing well	
	17:30	Tandem inst' in lube.	TSTM
	17:50	Inst' @ 6921'KB.	
	17:50	START FLOW	
	18:32	END FLOW & START SHUT-IN	
14-JUL	10:50	END SHUT-IN	

This is Schlumberger-Geoquest's Model-Verified(tm) interpretation report. With Model-Verified(tm) interpretation, the goal of the Geoquest analyst is to construct a total system reservoir model that matches all of your well test data. This provides you with reliable answers that you can have confidence in.

From the diagnostic log-log plot of pressure and pressure derivative, the Geoquest analyst identifies the flow regimes governed by the inner boundary conditions, basic reservoir behavior, and outer boundary conditions. A reservoir model is then constructed and the test data are matched to it. In order to verify the quality of the match, the theoretical model response (type curve) and the test data are plotted together. The presentation of the match can be shown in any of three different forms.

- 1) Log-log plot (delta pressure and derivative vs. delta time)
- 2) Semi-log plot (pressure vs. superposition time)
- 3) Cartesian plot (pressure vs. time)

Geoquest uses superposition techniques (multi-rate analysis) to account for the well's prior production history. Especially in cases where the prior production is erratic or unusual, superposition is the only means of providing an accurate type curve match of the well test data. For gas wells, the pseudo-pressure technique is used to account for the change in gas properties with changing pressure.

In some instances, the well test data will not be unique, i.e., more than one reservoir model will match the test data. The most appropriate model can be determined as we work with you and discuss the area lithology and geology.

The reservoir answers derived from Model-Verified(tm) interpretation can include; effective permeability (k), skin damage (s), reservoir pressure (p^*), fracture half-length (x_f), fracture capacity (kfw), boundary conditions and distance to boundaries, as well as the model of basic reservoir behavior.

Using the reservoir model determined by Model-Verified(tm) interpretation, flowrate predictions can be made for the well. Additionally, we can help you optimize well performance by using Geoquest's nodal analysis software to examine the well's sensitivity to different completion designs (e.g., fracture half-length, tubing size, wellhead pressure, skin value, shot density). This affords you the opportunity to forecast production potential for the well before making final completion/recompletion decisions.

The Schlumberger-Geoquest analyst constructs the total system reservoir model that best matches your test data by choosing the inner boundary condition(s), a basic reservoir model, and the outer boundary condition(s). These components are put together into one reservoir model and the test data is matched by adjusting the model parameters (e.g., permeability and skin) to obtain the best fit. The following is a partial list of the model components available to the Schlumberger-Geoquest analyst for matching your well test data.

Inner Boundary Condition

- No wellbore storage
- Constant wellbore storage
- Variable wellbore storage
- Finite conductivity vertical fracture
- Infinite conductivity vertical fracture
- Uniform flux vertical fracture
- Horizontal fracture
- Partial penetration

Basic Reservoir Model

- Homogeneous
- Dual porosity, pseudo steady state interporosity flow
- Dual porosity, transient interporosity flow
- Triple porosity
- Dual permeability
- Radial composite

Outer Boundary Condition

- Infinite system
- Single sealing no flow boundary
- Partially sealing boundary
- Single constant pressure boundary
- Two intersecting no flow boundaries (wedge geometry)
- Parallel no flow boundaries (channel)
- Gas cap/bottom water drive
- Closed (no flow) circle
- Constant pressure circle
- Closed (no flow) rectangle
- Constant pressure rectangle
- Mixed boundary rectangle

For some applications, such as horizontal and layered reservoir tests, all of the possible combinations are not available. References on most model components can be found in SPE papers.

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REPORT DISTRIBUTION

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PAGE NO. 16

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NC = Number of Copies

NAME	ADDRESS	ADDRESS	CITY	ST	ZIP	ATTENTION	NC
THORNTON OPERATING CORP.	Bakersman Hand Carry		Midland	TX		Robert Thornton	3

The following pages contain plots and printouts of the gauge data obtained during the test. Plots of bottomhole pressure vs. time are presented along with bottomhole temperature vs. time if a temperature channel was recorded. If gradient stops were recorded either running into, or pulling out of the well, then plots and printouts of these stops will be included.

Any interpretations or recommendations are opinions and necessarily based on inferences and empirical factors and assumptions which are not infallible. Accordingly, Schlumberger-Geoquest cannot and does not warrant the accuracy or correctness of any interpretation or measurement. Under no circumstances should any interpretation or measurement be relied upon as the sole basis for any drilling, completion, well treatment or production decision or any procedure involving risk to the safety of any drilling venture, drilling rig or its crew or any other individual. The Customer has full responsibility for all drilling, completion, well treatment and production procedure, and all other activities relating to the drilling or production operation.

BOTTOMHOLE PRESSURE LOG

FIELD REPORT NO. 132225

COMPANY : THORNTON OPERATING CORP.

INSTRUMENT NO. NG-00018

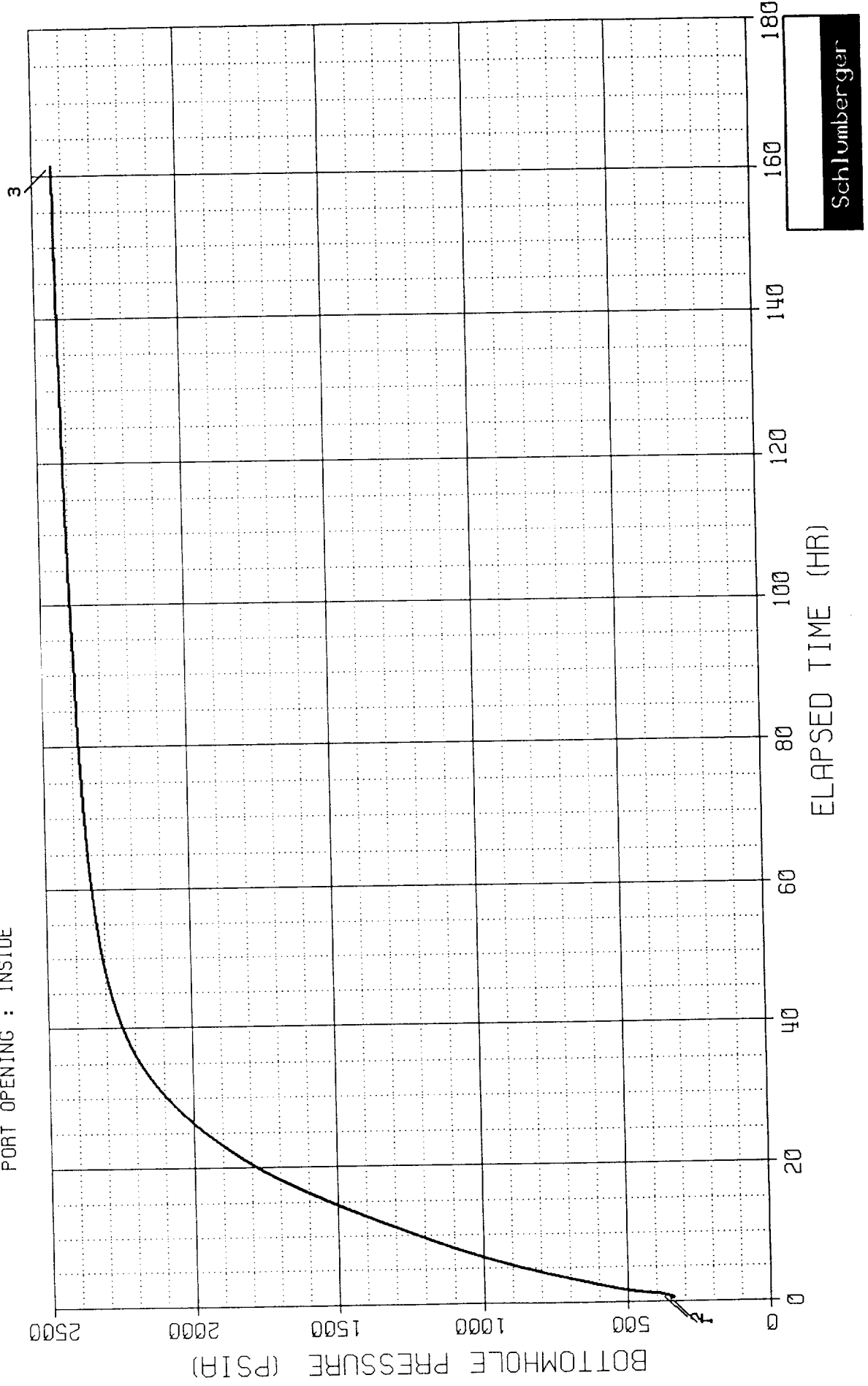
WELL : NORTHERN LIGHTS #1

DEPTH : 6921 FT

CAPACITY : 10000 PSI

PORT OPENING : INSIDE

Electronic Pressure Data



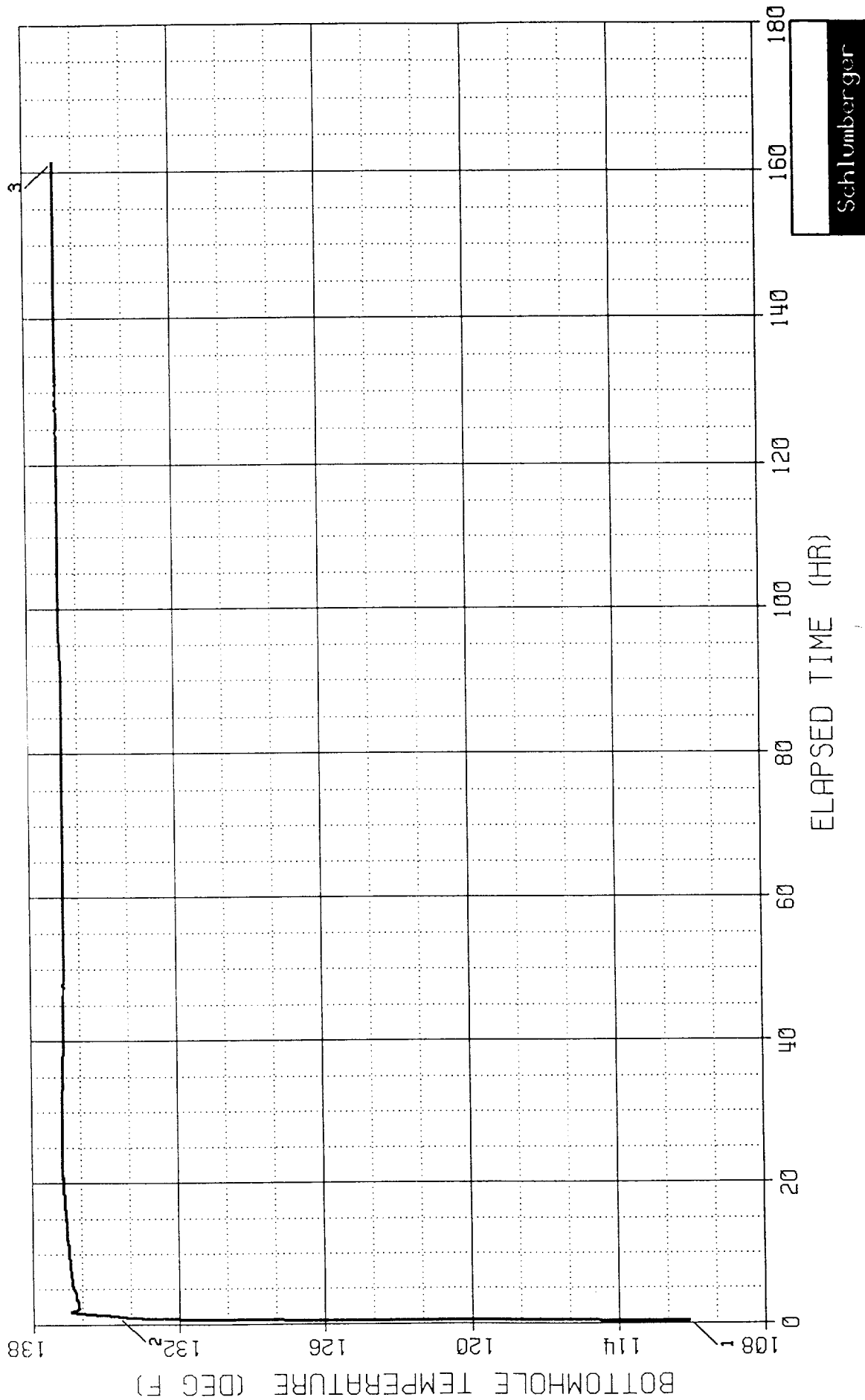
BOTTOMHOLE TEMPERATURE LOG

FIELD REPORT NO. 132225 COMPANY : THORNTON OPERATING CORP.

INSTRUMENT NO. NG-00018 WELL : NORTHERN LIGHTS #1

DEPTH : 6921 FT

Electronic Temperature Data



 ** WELL TEST DATA PRINTOUT **

COMPANY: THORNTON OPERATING CORP.
 WELL: NORTHERN LIGHTS #1

FIELD REPORT NO. 132225
 INSTRUMENT NO. NG-00018

RECORDER CAPACITY: 10000 PSI PORT OPENING: INSIDE DEPTH: 6921 FT

LABEL POINT INFORMATION

#	TIME OF DAY HH:MM:SS	DATE DD-MMM	EXPLANATION	ELAPSED TIME, HR	BOT HOLE PRESSURE PSIA	BOT HOLE TEMP. DEG F
1	17:50:00	7-JUL	START FLOW	0.450	353.58	111.13
2	18:31:30	7-JUL	END FLOW & START SHUT-IN	1.142	386.87	134.53
3	10:50:00	14-JUL	END SHUT-IN	161.450	2434.04	136.76

SUMMARY OF FLOW PERIODS

PERIOD	START ELAPSED TIME, HR	END ELAPSED TIME, HR	DURATION HR	START PRESSURE PSIA	END PRESSURE PSIA	INITIAL PRESSURE PSIA
1	0.450	1.142	0.692	353.58	386.87	353.58

SUMMARY OF SHUTIN PERIODS

PERIOD	START ELAPSED TIME, HR	END ELAPSED TIME, HR	DURATION HR	START PRESSURE PSIA	END PRESSURE PSIA	FINAL FLOW PRESSURE PSIA	PRODUCING TIME, HR
1	1.142	161.450	160.308	386.87	2434.04	386.87	26.500

TEST PHASE: FLOW PERIOD # 1

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME, HR	DELTA TIME, HR	BOT HOLE TEMP. DEG F	BOT HOLE PRESSURE PSIA
17:50:00	7-JUL	0.450	0.000	111.13	353.58
17:55:00	7-JUL	0.533	0.083	123.13	343.86
18:00:00	7-JUL	0.617	0.167	128.59	338.48
18:05:00	7-JUL	0.700	0.250	131.32	343.65
18:10:00	7-JUL	0.783	0.333	132.78	350.66
18:15:00	7-JUL	0.867	0.417	133.57	359.00
18:20:00	7-JUL	0.950	0.500	134.04	366.95
18:25:00	7-JUL	1.033	0.583	134.31	375.06
18:30:00	7-JUL	1.117	0.667	134.49	384.06
18:31:30	7-JUL	1.142	0.692	134.53	386.87

TEST PHASE: SHUTIN PERIOD # 1

FINAL FLOW PRESSURE = 386.87 PSIA
PRODUCING TIME = 26.500 HR

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME, HR	DELTA TIME, HR	BOT HOLE TEMP. DEG F	BOT HOLE PRESSURE PSIA	DELTA P PSI	LOG HORN TIME
18:31:30	7-JUL	1.142	0.000	134.53	386.87	0.00	
18:32:15	7-JUL	1.154	0.013	134.56	389.17	2.30	3.3265
18:33:00	7-JUL	1.167	0.025	134.58	392.20	5.33	3.0257
18:33:45	7-JUL	1.179	0.038	134.62	396.18	9.31	2.8498
18:34:30	7-JUL	1.192	0.050	134.64	400.08	13.21	2.7251
18:35:15	7-JUL	1.204	0.062	134.67	403.55	16.68	2.6284
18:36:00	7-JUL	1.217	0.075	134.71	407.18	20.31	2.5494
18:36:45	7-JUL	1.229	0.087	134.74	410.59	23.72	2.4827
18:37:30	7-JUL	1.242	0.100	134.80	413.67	26.80	2.4249
18:38:45	7-JUL	1.263	0.121	134.87	419.23	32.36	2.3430
18:40:00	7-JUL	1.283	0.142	134.96	424.08	37.21	2.2743
18:41:15	7-JUL	1.304	0.162	135.05	428.49	41.62	2.2150
18:42:30	7-JUL	1.325	0.183	135.14	433.05	46.18	2.1630
18:43:45	7-JUL	1.346	0.204	135.21	437.02	50.15	2.1166
18:45:00	7-JUL	1.367	0.225	135.30	441.72	54.85	2.0747
18:46:15	7-JUL	1.388	0.246	135.37	445.92	59.05	2.0366
18:47:30	7-JUL	1.408	0.267	135.45	450.44	63.57	2.0016
18:48:45	7-JUL	1.429	0.287	135.52	454.55	67.68	1.9693
18:50:00	7-JUL	1.450	0.308	135.61	458.92	72.05	1.9392
18:51:15	7-JUL	1.471	0.329	135.66	463.47	76.60	1.9112
18:52:30	7-JUL	1.492	0.350	135.73	467.36	80.49	1.8849
18:53:45	7-JUL	1.513	0.371	135.81	471.02	84.15	1.8601
18:55:00	7-JUL	1.533	0.392	135.86	475.24	88.37	1.8367
18:56:15	7-JUL	1.554	0.412	135.93	478.69	91.82	1.8145
18:57:30	7-JUL	1.575	0.433	136.00	482.05	95.18	1.7935
18:58:45	7-JUL	1.596	0.454	136.06	485.19	98.32	1.7734
19:00:00	7-JUL	1.617	0.475	136.13	488.66	101.79	1.7543
19:01:15	7-JUL	1.638	0.496	136.17	492.00	105.13	1.7360
19:02:30	7-JUL	1.658	0.517	136.22	495.47	108.60	1.7184
19:08:30	7-JUL	1.758	0.617	136.40	511.05	124.18	1.6432
19:14:30	7-JUL	1.858	0.717	136.45	524.71	137.84	1.5795
19:20:30	7-JUL	1.958	0.817	136.33	537.91	151.04	1.5244
19:26:30	7-JUL	2.058	0.917	136.22	549.40	162.53	1.4758

TEST PHASE: SHUTIN PERIOD # 1

FINAL FLOW PRESSURE = 386.87 PSIA
PRODUCING TIME = 26.500 HR

TIME OF DAY HH:MM:SS	DATE DD-MMM	ELAPSED TIME, HR	DELTA TIME, HR	BOT HOLE TEMP. DEG F	BOT HOLE PRESSURE PSIA	DELTA P PSI	LOG HORNER TIME
19:32:30	7-JUL	2.158	1.017	136.17	560.40	173.53	1.4324
19:38:30	7-JUL	2.258	1.117	136.15	571.51	184.64	1.3932
19:44:30	7-JUL	2.358	1.217	136.13	582.58	195.71	1.3576
19:50:30	7-JUL	2.458	1.317	136.15	593.40	206.53	1.3248
19:56:30	7-JUL	2.558	1.417	136.15	603.84	216.97	1.2946
20:02:30	7-JUL	2.658	1.517	136.15	614.36	227.49	1.2665
20:08:30	7-JUL	2.758	1.617	136.15	625.53	238.66	1.2403
20:14:30	7-JUL	2.858	1.717	136.15	636.61	249.74	1.2158
20:20:30	7-JUL	2.958	1.817	136.15	647.81	260.94	1.1928
20:26:30	7-JUL	3.058	1.917	136.15	658.91	272.04	1.1710
20:32:30	7-JUL	3.158	2.017	136.17	669.76	282.89	1.1505
20:38:30	7-JUL	3.258	2.117	136.17	680.83	293.96	1.1310
20:44:30	7-JUL	3.358	2.217	136.18	691.50	304.63	1.1124
20:50:30	7-JUL	3.458	2.317	136.20	702.75	315.88	1.0948
20:56:30	7-JUL	3.558	2.417	136.22	713.74	326.87	1.0779
21:02:30	7-JUL	3.658	2.517	136.24	724.39	337.52	1.0618
21:08:30	7-JUL	3.758	2.617	136.24	735.08	348.21	1.0464
21:14:30	7-JUL	3.858	2.717	136.26	745.81	358.94	1.0316
21:20:30	7-JUL	3.958	2.817	136.26	756.40	369.53	1.0174
21:26:30	7-JUL	4.058	2.917	136.27	766.86	379.99	1.0037
21:32:30	7-JUL	4.158	3.017	136.26	777.39	390.52	0.9905
22:32:30	7-JUL	5.158	4.017	136.35	874.01	487.14	0.8807
23:32:30	7-JUL	6.158	5.017	136.42	959.80	572.93	0.7981
0:32:30	8-JUL	7.158	6.017	136.45	1036.24	649.37	0.7328
1:32:30	8-JUL	8.158	7.017	136.47	1106.13	719.26	0.6791
2:32:30	8-JUL	9.158	8.017	136.49	1171.50	784.63	0.6340
3:32:30	8-JUL	10.158	9.017	136.53	1235.35	848.48	0.5954
4:32:30	8-JUL	11.158	10.017	136.54	1298.42	911.55	0.5618
5:32:30	8-JUL	12.158	11.017	136.58	1360.82	973.95	0.5322
6:32:30	8-JUL	13.158	12.017	136.58	1422.17	1035.30	0.5059
7:32:30	8-JUL	14.158	13.017	136.62	1482.18	1095.31	0.4823
8:32:30	8-JUL	15.158	14.017	136.63	1539.91	1153.04	0.4610
9:32:30	8-JUL	16.158	15.017	136.65	1595.39	1208.52	0.4416
10:32:30	8-JUL	17.158	16.017	136.69	1648.30	1261.43	0.4240
11:32:30	8-JUL	18.158	17.017	136.69	1698.22	1311.35	0.4078
12:32:30	8-JUL	19.158	18.017	136.71	1745.21	1358.34	0.3928
13:32:30	8-JUL	20.158	19.017	136.72	1788.98	1402.11	0.3790
14:32:30	8-JUL	21.158	20.017	136.74	1829.70	1442.83	0.3662
15:32:30	8-JUL	22.158	21.017	136.74	1867.64	1480.77	0.3543
16:32:30	8-JUL	23.158	22.017	136.74	1902.87	1516.00	0.3431
17:33:00	8-JUL	24.167	23.025	136.76	1935.87	1549.00	0.3326
18:33:00	8-JUL	25.167	24.025	136.76	1966.27	1579.40	0.3228
19:33:00	8-JUL	26.167	25.025	136.76	1994.98	1608.11	0.3136
20:33:00	8-JUL	27.167	26.025	136.74	2022.20	1635.33	0.3050
21:33:00	8-JUL	28.167	27.025	136.74	2047.98	1661.11	0.2968
22:33:00	8-JUL	29.167	28.025	136.74	2072.02	1685.15	0.2891
23:33:00	8-JUL	30.167	29.025	136.74	2095.04	1708.17	0.2817
0:33:00	9-JUL	31.167	30.025	136.74	2116.32	1729.45	0.2748
1:33:00	9-JUL	32.167	31.025	136.74	2135.85	1748.98	0.2681
2:33:00	9-JUL	33.167	32.025	136.74	2154.04	1767.17	0.2619

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3:33:00	9-JUL	34.167	33.025	136.72	2170.82	1783.95	0.2559
4:33:00	9-JUL	35.167	34.025	136.72	2185.75	1798.88	0.2501
5:33:00	9-JUL	36.167	35.025	136.71	2199.65	1812.78	0.2447
6:33:00	9-JUL	37.167	36.025	136.71	2212.48	1825.61	0.2394
7:33:00	9-JUL	38.167	37.025	136.69	2224.30	1837.43	0.2344
8:33:00	9-JUL	39.167	38.025	136.69	2234.94	1848.07	0.2297
9:33:00	9-JUL	40.167	39.025	136.69	2244.77	1857.90	0.2251
10:33:00	9-JUL	41.167	40.025	136.69	2253.73	1866.86	0.2207
11:33:00	9-JUL	42.167	41.025	136.69	2262.04	1875.17	0.2164
12:33:00	9-JUL	43.167	42.025	136.67	2269.60	1882.73	0.2123
13:33:00	9-JUL	44.167	43.025	136.67	2276.75	1889.88	0.2084
14:33:00	9-JUL	45.167	44.025	136.67	2283.39	1896.52	0.2046
15:33:00	9-JUL	46.167	45.025	136.67	2289.39	1902.52	0.2010
16:33:00	9-JUL	47.167	46.025	136.65	2295.02	1908.15	0.1975
17:33:00	9-JUL	48.167	47.025	136.65	2300.23	1913.36	0.1941
18:33:00	9-JUL	49.167	48.025	136.65	2305.17	1918.30	0.1908
19:33:00	9-JUL	50.167	49.025	136.65	2309.41	1922.54	0.1877
20:33:00	9-JUL	51.167	50.025	136.65	2313.49	1926.62	0.1846
21:33:00	9-JUL	52.167	51.025	136.65	2317.49	1930.62	0.1817
22:33:00	9-JUL	53.167	52.025	136.63	2321.20	1934.33	0.1788
23:33:00	9-JUL	54.167	53.025	136.63	2324.64	1937.77	0.1760
0:33:00	10-JUL	55.167	54.025	136.65	2328.06	1941.19	0.1733
1:33:00	10-JUL	56.167	55.025	136.65	2331.28	1944.41	0.1707
2:33:00	10-JUL	57.167	56.025	136.63	2334.33	1947.46	0.1682
3:33:00	10-JUL	58.167	57.025	136.63	2337.10	1950.23	0.1658
4:33:00	10-JUL	59.167	58.025	136.63	2339.92	1953.05	0.1634
5:33:00	10-JUL	60.167	59.025	136.63	2342.58	1955.71	0.1611
6:33:00	10-JUL	61.167	60.025	136.63	2345.16	1958.29	0.1588
7:33:00	10-JUL	62.167	61.025	136.63	2347.77	1960.90	0.1566
8:33:00	10-JUL	63.167	62.025	136.63	2350.02	1963.15	0.1545
9:33:00	10-JUL	64.167	63.025	136.63	2352.29	1965.42	0.1524
10:33:00	10-JUL	65.167	64.025	136.63	2354.42	1967.55	0.1504
11:33:00	10-JUL	66.167	65.025	136.63	2356.25	1969.38	0.1485
12:33:00	10-JUL	67.167	66.025	136.63	2358.16	1971.29	0.1466
13:33:00	10-JUL	68.167	67.025	136.63	2360.07	1973.20	0.1447
14:33:00	10-JUL	69.167	68.025	136.63	2362.02	1975.15	0.1429
15:33:00	10-JUL	70.167	69.025	136.63	2363.71	1976.84	0.1411
16:33:00	10-JUL	71.167	70.025	136.63	2365.46	1978.59	0.1394
17:33:00	10-JUL	72.167	71.025	136.63	2366.94	1980.07	0.1377
18:33:00	10-JUL	73.167	72.025	136.63	2368.73	1981.86	0.1361
19:33:00	10-JUL	74.167	73.025	136.63	2369.86	1982.99	0.1345
20:33:00	10-JUL	75.167	74.025	136.63	2371.35	1984.48	0.1329
21:33:00	10-JUL	76.167	75.025	136.63	2372.86	1985.99	0.1314
22:33:00	10-JUL	77.167	76.025	136.63	2374.22	1987.35	0.1299
23:33:00	10-JUL	78.167	77.025	136.65	2375.76	1988.89	0.1284
0:33:00	11-JUL	79.167	78.025	136.63	2377.02	1990.15	0.1270
1:33:00	11-JUL	80.167	79.025	136.65	2378.43	1991.56	0.1256
2:33:00	11-JUL	81.167	80.025	136.65	2379.66	1992.79	0.1242
3:33:00	11-JUL	82.167	81.025	136.63	2380.97	1994.10	0.1229
4:33:00	11-JUL	83.167	82.025	136.65	2381.82	1994.95	0.1216

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5:33:00	11-JUL	84.167	83.025	136.63	2382.65	1995.78	0.1203
13:48:00	11-JUL	92.417	91.275	136.63	2390.05	2003.18	0.1107
14:48:00	11-JUL	93.417	92.275	136.69	2391.56	2004.69	0.1096
15:48:00	11-JUL	94.417	93.275	136.69	2392.91	2006.04	0.1086
16:48:00	11-JUL	95.417	94.275	136.71	2394.22	2007.35	0.1076
17:48:00	11-JUL	96.417	95.275	136.71	2395.26	2008.39	0.1066
18:48:00	11-JUL	97.417	96.275	136.71	2396.23	2009.36	0.1056
19:48:00	11-JUL	98.417	97.275	136.71	2397.16	2010.29	0.1046
20:48:00	11-JUL	99.417	98.275	136.71	2398.03	2011.16	0.1037
21:48:00	11-JUL	100.417	99.275	136.71	2399.14	2012.27	0.1028
22:48:00	11-JUL	101.417	100.275	136.72	2399.94	2013.07	0.1018
23:48:00	11-JUL	102.417	101.275	136.71	2400.89	2014.02	0.1009
0:48:00	12-JUL	103.417	102.275	136.71	2401.66	2014.79	0.1001
1:48:00	12-JUL	104.417	103.275	136.72	2402.55	2015.68	0.0992
2:48:00	12-JUL	105.417	104.275	136.72	2403.45	2016.58	0.0983
3:48:00	12-JUL	106.417	105.275	136.72	2404.18	2017.31	0.0975
4:48:00	12-JUL	107.417	106.275	136.72	2405.24	2018.37	0.0967
5:48:00	12-JUL	108.417	107.275	136.72	2405.74	2018.87	0.0959
6:48:00	12-JUL	109.417	108.275	136.72	2406.79	2019.92	0.0951
7:48:00	12-JUL	110.417	109.275	136.72	2407.65	2020.78	0.0943
8:48:00	12-JUL	111.417	110.275	136.72	2408.33	2021.46	0.0935
9:48:00	12-JUL	112.417	111.275	136.72	2408.89	2022.02	0.0928
10:48:00	12-JUL	113.417	112.275	136.72	2409.60	2022.73	0.0920
11:48:00	12-JUL	114.417	113.275	136.72	2410.19	2023.32	0.0913
12:48:00	12-JUL	115.417	114.275	136.72	2410.80	2023.93	0.0906
13:48:00	12-JUL	116.417	115.275	136.72	2411.60	2024.73	0.0899
14:48:00	12-JUL	117.417	116.275	136.72	2412.25	2025.38	0.0892
15:48:00	12-JUL	118.417	117.275	136.72	2412.71	2025.84	0.0885
16:48:00	12-JUL	119.417	118.275	136.72	2413.38	2026.51	0.0878
17:48:00	12-JUL	120.417	119.275	136.72	2414.06	2027.19	0.0871
18:48:00	12-JUL	121.417	120.275	136.72	2414.70	2027.83	0.0865
19:48:00	12-JUL	122.417	121.275	136.72	2415.04	2028.17	0.0858
20:48:00	12-JUL	123.417	122.275	136.72	2415.64	2028.77	0.0852
21:48:00	12-JUL	124.417	123.275	136.72	2416.25	2029.38	0.0846
22:48:00	12-JUL	125.417	124.275	136.74	2416.95	2030.08	0.0839
23:48:00	12-JUL	126.417	125.275	136.74	2417.41	2030.54	0.0833
0:48:00	13-JUL	127.417	126.275	136.74	2418.12	2031.25	0.0827
1:48:00	13-JUL	128.417	127.275	136.72	2418.57	2031.70	0.0821
2:48:00	13-JUL	129.417	128.275	136.72	2419.22	2032.35	0.0816
3:48:00	13-JUL	130.417	129.275	136.74	2419.68	2032.81	0.0810
4:48:00	13-JUL	131.417	130.275	136.72	2420.19	2033.32	0.0804
5:48:00	13-JUL	132.417	131.275	136.74	2420.80	2033.93	0.0799
6:48:00	13-JUL	133.417	132.275	136.74	2421.65	2034.78	0.0793
7:48:00	13-JUL	134.417	133.275	136.74	2422.21	2035.34	0.0788
8:48:00	13-JUL	135.417	134.275	136.74	2422.73	2035.86	0.0782
9:48:00	13-JUL	136.417	135.275	136.74	2423.23	2036.36	0.0777
10:48:00	13-JUL	137.417	136.275	136.74	2423.65	2036.78	0.0772
11:48:00	13-JUL	138.417	137.275	136.74	2423.99	2037.12	0.0767
12:48:00	13-JUL	139.417	138.275	136.74	2424.42	2037.55	0.0761
13:48:00	13-JUL	140.417	139.275	136.74	2424.96	2038.09	0.0756

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14:48:00	13-JUL	141.417	140.275	136.74	2425.52	2038.65	0.0752
15:48:00	13-JUL	142.417	141.275	136.74	2425.93	2039.06	0.0747
16:48:00	13-JUL	143.417	142.275	136.74	2426.36	2039.49	0.0742
17:48:00	13-JUL	144.417	143.275	136.74	2426.87	2040.00	0.0737
18:48:00	13-JUL	145.417	144.275	136.74	2427.11	2040.24	0.0732
19:48:00	13-JUL	146.417	145.275	136.74	2427.59	2040.72	0.0728
20:48:00	13-JUL	147.417	146.275	136.74	2427.88	2041.01	0.0723
21:48:00	13-JUL	148.417	147.275	136.74	2428.35	2041.48	0.0719
22:48:00	13-JUL	149.417	148.275	136.74	2428.81	2041.94	0.0714
23:48:00	13-JUL	150.417	149.275	136.74	2429.28	2042.41	0.0710
0:48:00	14-JUL	151.417	150.275	136.76	2429.75	2042.88	0.0705
1:48:00	14-JUL	152.417	151.275	136.74	2430.14	2043.27	0.0701
2:48:00	14-JUL	153.417	152.275	136.74	2430.09	2043.22	0.0697
3:48:00	14-JUL	154.417	153.275	136.74	2430.15	2043.28	0.0693
4:48:00	14-JUL	155.417	154.275	136.74	2430.35	2043.48	0.0688
5:48:00	14-JUL	156.417	155.275	136.74	2430.51	2043.64	0.0684
6:48:00	14-JUL	157.417	156.275	136.74	2431.40	2044.53	0.0680
7:48:00	14-JUL	158.417	157.275	136.76	2432.31	2045.44	0.0676
8:48:00	14-JUL	159.417	158.275	136.76	2432.92	2046.05	0.0672
9:48:00	14-JUL	160.417	159.275	136.76	2433.41	2046.54	0.0668
10:48:00	14-JUL	161.417	160.275	136.76	2433.73	2046.86	0.0665
10:50:00	14-JUL	161.450	160.308	136.76	2434.04	2047.17	0.0664