

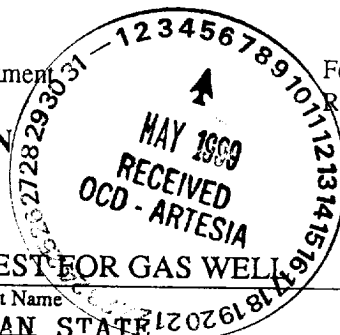
Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

Form C-122
Revised 4-1-91



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator ELK OIL COMPANY				Lease or Unit Name JAN STATE 12026181			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4-1-1999		Well No. #3	
Completion Date 4-1-1999		Total Depth		Plug Back TD 6335		Elevation	
Csg. Size 4 1/2	Wt. 17	d 4.892	Set At 6335	Perforations: From: 6246 To: 6289		Unit Ltr. - Sec. - TWP - Rge. B 36 2S 26E	
Tbg. Size 2 3/8	Wt. 4.85	d 1.995	Set At 6224	Perforations: From: To: Foot Ranch		County CHAVES	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 6224		Formation PRE PERMIAN	
Producing Thru TUBING		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press - P _a 13.2	
Connection PIPELINE		Meter Run 2.0		Taps			
L 6268	H 6268	Gg 0.612	% CO ₂ 0.201	% N ₂ 3.032	% H ₂ S 0	Prover	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	2 x 1	250				1900		PACKER		
1.	2 x 1	250	116	17	73	1650				1 hr
2.	2 x 1	250	127	45	78	1250				1 hr
3.	2 x 1	250	133	53	83	950				1 hr
4.	2 x 1	250	140	32	86	750				1 hr
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	10 310	46.87	129.2	0.9877	1.2783	1.0102	616
2.	10 310	79.43	140.2	0.9831	1.2783	1.0108	1040
3.	10 310	88.03	146.2	0.9786	1.2783	1.0109	1148
4.	10 310	70.02	153.2	0.9759	1.2783	1.0112	911
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A.P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas	XXXXXXXXXX
3.					Specific Gravity Flowing Fluid	XXXXXX
4.					Critical Pressure	P.S.I.A.
5.					Critical Temperature	R

P_c **2059.1** P_w **4239.8**

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.		1730.0	2992.9	1246.9
2.		1295.8	1679.1	2560.7
3.		978.2	956.9	3282.9
4.		768.7	590.9	3648.8
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{2059.1}{P_c^2 - P_w^2}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4239.8$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1384$

Absolute Open Flow **1384** Mcfd @ 15.025 Angle of Slope θ **54** Slope, n **.73**

Remarks: **CHOKE SETTINGS: 1st rate 8/64 2nd rate 12/64 3rd rate 16/64 4th rate 18/64**

Approved By Division	Conducted By: KELTIC SERVICES	Calculated By: MIKE KELLY	Checked By:
----------------------	---	-------------------------------------	-------------