

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT A ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122 C-122
Revised 9-1-65

RECEIVED

JAN 9 1974

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date <u>1-4-74</u>				
Company Yates Petroleum Corp.				Connection				D. C. C. ARTESIA, OFFICE	
Pool Riverside				Formation Morrow				Unit	
Completion Date 1-4-74		Total Depth 8746'		Plug Back TD 8450'		Elevation 3309 KB		Farm or Lease Name Holden DE Com	
Csg. Size 4 1/2"	Wt. 11.6	d 4.000	Set At 8734	Perforations: From 8354 To 8376			Well No. 1		
Tbg. Size 2-3/8"	Wt. 4.7	d 1.995	Set At 8207	Perforations: From To			Unit Sec. Twp. Rge. J 12 17S 26E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 8207		County Eddy		
Producing Thru Tbg		Reservoir Temp. °F 131		Mean Annual Temp. °F 62		Baro. Press. - P _a 13.2		State New Mexico	
L	H 8365	Gg 0.641	% CO ₂ 2.54	% N ₂ 0.27	% H ₂ S Nil	Prover	Meter Run X	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2668				Days
1.	3		1.000	405	27	98	2387	54			1
2.	3		1.000	407	44	91	2220	55			1
3.	3		1.000	407	64	88	2033	56			1
4.	3		1.000	407	87	83	1822	54			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	4.801	106.24	418	.9653	1.249	1.031	631
2	4.801	135.94	420	.9715	1.249	1.033	814
3	4.801	163.95	420	.9741	1.249	1.034	985
4	4.801	191.15	420	.9786	1.249	1.035	1155
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
					180					
1.	.613	558	1.512	.940		55	0.641	XXXXXX		
2.	.616	551	1.493	.937				XXXXXX		
3.	.616	548	1.485	.935				XXXXXX		
4.	.616	543	1.472	.933				XXXXXX		
5.								XXXXXX		

NO.	P _c	P _w	P _r	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
	3473				4.834	2765
1		3093	9567	2495		
2		2885	8323	3739		
3		2661	7081	4981		
4		2405	5484	6278		
5						

Absolute Open Flow 1745 Mcfd @ 15.025				Angle of Slope θ		Slope, n 0.6466	
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Remarks: Witnessed by Jack Moore & Bob Alston of Transwestern Pipeline Co.			
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Approved By Commission:	Conducted By: Don Weaver	Calculated By: Eddie Mahfood	Checked By:
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