

W MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 6/26/77		JUL 14 1977	
Company Southern Union Supply Co.				Connection None			
Pool Undesignated				Formation Morrow		Unit O. C. C. ARTEZIA, OFFICE	
Completion Date 6/26/77		Total Depth 10450'		Plug Back TD 10345		Elevation 3780' KB	
Csg. Size 4 1/2"		WT. 11.6		Set At 10450'		Perforations: From 10046' To 10110'	
Tbg. Size 2 3/8"		WT. 4.6		Set At 10020		Perforations: Open Ended	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10023'		Farm or Lease Name Exxon Federal	
Producing Thru Tubing		Reservoir Temp. °F 168 @ 10021		Mean Annual Temp. °F 60		Baro. Press. - P _g 13.2	
L 10078'		H -		G _g 0.6010		% CO ₂ 0.971	
				% N ₂ 0.385		% H ₂ S -	
				Prover X		Meter Run F	
FLOW DATA							
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Duration of Flow
1.	4 18/64	1.250	500	80	60	3097	87.0
2.	4 11/64	1.250	500	58	60	2059	4.25
3.	4 10/64	1.250	500	38	62	2332	2.00
4.	4 8/64	1.250	720	20	64	2497	1.75
5.						2607	4.00
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mcfd
1.	7.469	202.62	513.2	1.0000	1.290	1.043	2036.20
2.	7.469	172.53	513.2	1.0000	1.290	1.043	1733.81
3.	7.469	139.64	513.2	0.9981	1.290	1.043	1400.62
4.	7.469	121.09	733.2	0.9962	1.290	1.061	1233.16
5.							
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 33.92 Mcf/bbl.		
1.	0.76	520	1.47	0.919	A.P.I. Gravity of Liquid Hydrocarbons - Deg.		
2.	0.76	520	1.47	0.919	Specific Gravity Separator Gas 0.6010 XXXXXX		
3.	0.76	522	1.47	0.919	Specific Gravity Flowing Fluid XXXXX		
4.	1.09	524	1.48	0.889	Critical Pressure 674 P.S.I.A.		
5.					Critical Temperature 354 R		
P _c 3978.2 P _c ² 15826.1							
NO.	P _t ²	P _w ²	P _w ² - P _t ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.854$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.608$			
1.	2700.2	7291.1	8335.0	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3274$			
2.	2979.2	8875.6	6950.5				
3.	3235.2	10466.5	5359.6				
4.	3372.2	11371.7	4454.4				
5.							
Absolute Open Flow 3274 Mcfd @ 15.625					Angle of Slope 51° 27'		Slope, n 0.769
Remarks: * BHP @ (-6288) 10078' Used for Pressure Calculations							
Approved By Commission:		Conducted By: Jarrel Services, Inc		Calculated By: Joe A. Coleman		Checked By: Joe A. Coleman	