

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

SF
File
Form C-122
Revised 9-1-66

RECEIVED

DEC 20 1979

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 12/5/79		SPUD DATE: 7-18-79							
Company Southland Royalty Company		Office ARTESIA, OFFICE									
Pool Angell Ranch morrow		Formation Morrow		Unit							
Completion Date 9-29-79		Total Depth 11136		Flag Back TD 10780							
Casing Size 4 1/2		Set At 10882		Perforations: From 10373 To 10730							
Tubing Size 2 3/8		Set At 10317		Perforations: From To							
Type Well - Single - Bronthead - G.G. or G.O. Multiple Single				Facker Set At 10317							
Producing Thru Tbg.		Reservoir Temp. °F 177 @ 10317		Mean Annual Temp. °F 60							
				Baro. Press. - P _a 13.2							
L 10317		H 10317		G _g .630							
				% CO ₂ .56							
				% N ₂ 4.83							
				% H ₂ S							
				Prover							
				Meter Run 2							
				Flange							
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
51							2692				72 hrs.
1.	2	x	.750	405	4.0	78	2315				1 hr.
2.	2	x	.750	420	8.0	68	1910				1 hr.
3.	2	x	.750	450	12.0	64	1405				1 hr.
4.	2	x	.750	440	16.0	64	625				1 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mhd				
1	2.709	40.90	418.2	.9831	1.260	1.036	142				
2	2.709	58.87	433.2	.9924	1.260	1.041	208				
3	2.709	74.55	463.2	.9962	1.260	1.045	265				
4	2.709	85.15	453.2	.9962	1.260	1.044	302				
5											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio <u>Dry</u> Mcf/bbl.						
1	.62	538	1.46	.931	A.P.L. Gravity of Liquid Hydrocarbons _____ Deg.						
2	.65	528	1.43	.922	Specific Gravity Separator Gas <u>.630</u> X X X X X X X X						
3	.69	524	1.42	.916	Specific Gravity Flowing Fluid X X X X X						
4	.68	524	1.42	.917	Critical Pressure <u>670</u> P.S.I.A. P.S.I.A.						
5					Critical Temperature <u>368</u> °R °R						
P _c 2705.2 P _w 7318.1					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.059$						
					(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.034$						
NO.	P _c	P _w	P _w ²	P _c ² - P _w ²	ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .312$						
1		2328.3	5421.1	1897.0							
2		1923.5	3700.0	3618.1							
3		1419.0	2013.5	5304.6							
4		640.7	410.5	6907.6							
5											
Absolute Open Flow <u>312</u> Mhd @ 15.025					Angle of Slope @ <u>60°</u>		Slope, n <u>.580</u>				
Remarks:											
Approved by Commission:		Conducted by:		Calculated by:		Checked by:					
		Rick Pagan		Rick Pagan		D. CRAIG <i>etc</i>					