

Submit in duplicate to appropriate district office See Rule 401 & Rule 1122

OIL CONSERVATION DIVISION

P.O. Box 2088 Santa Fe, New Mexico 87504-2088

C/SF

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator <i>Penwell Energy</i>				Lease or Unit Name <i>Filaree 24 Fed Com</i>			
Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date <i>7-3-97</i>		Well No. <i>1</i>	
Completion Date <i>5-13-97</i>		Total Depth <i>11557</i>		Plug Back TD <i>11510</i>		Elevation <i>3380 GR</i>	
Csg. Size <i>5 1/2</i>		Wt. d <i>17 4.87</i>		Set At <i>11557</i>		Perforations: From: <i>10,144</i> To: <i>11557</i>	
Tbg. Size <i>2 3/8</i>		Wt. d <i>4.7 1.995</i>		Set At <i>10,141</i>		Perforations: From: <i>10,141</i> To: <i>10,141</i>	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple <i>Single</i>				Packer Set At <i>10,141</i>		Formation <i>Atoka</i>	
Producing Thru <i>TBG</i>		Reservoir Temp. °F <i>175°</i>		Mean Annual Temp. °F <i>60°</i>		Baro. Press - P _a <i>13.2</i>	
L <i>10,144</i>		H <i>10,144</i>		G _g <i>.594</i>		% CO ₂ <i>.44%</i>	
				% N ₂ <i>.75</i>		% H ₂ S <i>0</i>	
				Prover <i>0</i>		Meter Run <i>3.068</i>	
						Taps <i>F/G</i>	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						<i>1270</i>		<i>PKR</i>	
1.	<i>3.068 X 1.500</i>	<i>410</i>	<i>2.3</i>	<i>118°</i>	<i>1125</i>	<i>91°</i>			<i>60 min</i>
2.	<i>3.068 X 1.500</i>	<i>397</i>	<i>7.7</i>	<i>114°</i>	<i>980</i>	<i>92°</i>			<i>60 min</i>
3.	<i>3.068 X 1.500</i>	<i>397</i>	<i>16.0</i>	<i>111°</i>	<i>805</i>	<i>92°</i>			<i>60 min</i>
4.	<i>3.068 X 1.500</i>	<i>384</i>	<i>25.0</i>	<i>103°</i>	<i>570</i>	<i>92°</i>			<i>60 min</i>
5.									

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$h_w P_m$	Pressure P _m	Flow Temp. Factor FL	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	<i>11.13</i>	<i>31.2</i>	<i>423.2</i>	<i>.9485</i>	<i>1.298</i>	<i>1.030</i>	<i>440</i>
2.	<i>11.13</i>	<i>56.2</i>	<i>410.2</i>	<i>.9518</i>	<i>1.298</i>	<i>1.031</i>	<i>796</i>
3.	<i>11.13</i>	<i>81.0</i>	<i>410.2</i>	<i>.9543</i>	<i>1.298</i>	<i>1.031</i>	<i>1148</i>
4.	<i>11.13</i>	<i>99.6</i>	<i>397.2</i>	<i>.9610</i>	<i>1.298</i>	<i>1.034</i>	<i>1429</i>
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl
1.	<i>.85</i>	<i>578</i>	<i>1.65</i>	<i>.942</i>	<i>N/A</i>	<i>N/A</i>
2.	<i>.85</i>	<i>574</i>	<i>1.64</i>	<i>.947</i>	<i>N/A</i>	<i>N/A</i>
3.	<i>.84</i>	<i>571</i>	<i>1.63</i>	<i>.940</i>	<i>.594</i>	<i>XXXXXXXXXX</i>
4.	<i>.83</i>	<i>563</i>	<i>1.60</i>	<i>.936</i>	<i>N/A</i>	<i>N/A</i>
5.					<i>N/A</i>	<i>N/A</i>

P _c <i>1223.2</i> P _w <i>1496.2</i>				1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{1.373}{}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.245}{}$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.779}{}$		
1.	<i>1295.5</i>	<i>1140.8</i>	<i>1301.4</i>	<i>194.8</i>			
2.	<i>986.4</i>	<i>1003.1</i>	<i>1006.2</i>	<i>490.1</i>			
3.	<i>669.5</i>	<i>843.3</i>	<i>711.2</i>	<i>785.0</i>			
4.	<i>340.1</i>	<i>637.7</i>	<i>406.6</i>	<i>1089.6</i>			
5.							

Absolute Open Flow *1.779* Mcfd @ 15.025 Angle of Slope Θ *55.39* Slope, n *.6899*

Remarks:

Approved By Division _____ Conducted By: *Pro Well Tester's* Calculated By: *MB* Checked By: *BM*