

NEW MEXICO OIL CONSERVATION COMMISSION  
MULTIPOINT AND ONE RECEIVED PRESSURE TEST FOR GAS WELL

Form C-122  
Revised 9-1-80

C.S.F

MAY - 7 1980

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special		O.C.D.		Start Date 4-18-80		SPUD DATE: 3-10-80				
Company C & K Petroleum, Inc.				Office ARTESIA, OFFICE						
Pool Undesignated				Formation Delaware		Unit J				
Completion Date 4-18-80		Total Depth 3000'		Plug back To 2957'		Elevation N/A				
Csg. Size 5 1/2		Set At 3000'		Perforations: From 2619 To 2870		Well No. 2-Z				
Tub. Size 2 3/8		Set At 2536		Perforations: From open To ended		Unit Sec. Twp. Rge. J 08 24 26				
Type well - Single - Bradenhead - G.O. or G.O. Multiple Single				Factor Set At None		County Eddy				
Producing thru Tbg.		Reservoir Temp. °F 101 @ 2744		Mean Annual Temp. °F 60		State New Mexico				
L 2536		H 2536		Gg .723		% CO <sub>2</sub> .38				
				% N <sub>2</sub> 21.97		% H <sub>2</sub> S 0				
				Prover OCT Positive Chokes		Meter Run Pages				
FLOW DATA				TUBING DATA		CASING DATA				
NO.	Positive Chokes	Orifice Size	Press. p.s.i.g.	Diff. h <sub>w</sub>	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI						1129		1129		48 hrs.
1.	8/64		1119	----	54	1119	54	1119		30 Min.
2.	12/64		1065	----	56	1065	56	1065		60 Min.
3.	14/64		998	----	56	998	56	998		60 Min.
4.	16/64		775	----	64	775	64	938		60 Min.
5.										
RATE OF FLOW CALCULATIONS										
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P <sub>m</sub>	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow O, Mcfd			
1	.2618	-----	1132.2	1.006	1.176	1.092	383			
2	.6101	-----	1078.2	1.004	1.176	1.090	847			
3	.8419	-----	1011.2	1.004	1.176	1.084	1090			
4	1.112	-----	788.2	.9962	1.176	1.066	1095			
5										
NO.	R <sub>1</sub>	Temp. °R	T <sub>1</sub>	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.79	514	1.52	.838	None		.723	X X X X X X X X X	631	338
2	1.71	516	1.53	.842				X X X X X		
3	1.60	516	1.53	.851						
4	1.25	524	1.55	.880						
5										
$r_e = 1142.2$ $r_w = 1304.6$										
NO.	$r_e^2$	$r_w^2$	$P_e^2$	$P_w^2$	$P_e^2 - P_w^2$	(1) $\frac{P_e^2}{P_e^2 - P_w^2} =$	(2) $\left[ \frac{P_e^2}{P_e^2 - P_w^2} \right]^n =$			
1		1132.2	1281.9	22.7		57.471	7.581			
2		1078.2	1162.5	142.1						
3		1011.2	1022.5	282.1						
4		951.2	904.8	399.8						
5										
$ADP = 0$ $\left[ \frac{P_e^2}{P_e^2 - P_w^2} \right]^n = 2.904$										
Absolute Open Flow				2,904 Mcfd @ 15.025		Angle of Slope $\theta = 63.5$		Slope, n = 500		
Remarks: Made two barrels water with trace of oil during test.										
Approved by Concession:			Conducted By:			Calculated By:			Checked By:	
			Bob McMurray			Bob McMurray				