

Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator CONOCO, INC.						Lease or Unit Name ANDERSON RANCH					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8-26-94		Well No. 1			
Completion Date		Total Depth 12356		Plug Back TD		Elevation		Unit Lr. - Sec. - TWP - Rge. 11-16S-32E			
Csg. Size 4 1/2	Wt. 11.5	d 4.00	Set At 12356	Perforations: From: 12168 To: 12194				County LEA			
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 12103	Perforations: From: To:				Pool			
Type Well - Single - Bradenhead - G.G. or H.O. Multiple SINGLE		Packer Set At 12103		Formation MARROW				Connection AIR			
Producing Thru TBG.		Reservoir Temp. °F 170		Mean Annual Temp. °F 60°		Baro. Press - P _a 13.2		Meter Run 3.068			
L *12170	H 12170	Gg .722	% CO ₂ .53	% N ₂ 1.17	% H ₂ S	Prover		Taps FLG.			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						710				
1.	3.068 X 1.000		120	2	73	690		pkx		1 hr.
2.	3.068 X 1.000		120	12	72	670		"		1 hr.
3.	3.068 X 1.000		120	52	62	655		"		1 hr.
4.	3.068 X 1.500		110	30	61	430		"		1 hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	4.789	16.32	133.2	.9877	1.177	1.015	92
2.	4.789	39.98	133.2	.9887	1.177	1.015	226
3.	4.789	83.23	133.2	.9981	1.177	1.015	475
4.	11.13	60.79	123.2	.9990	1.177	1.015	808
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcft/bbl.
1.	.20	533	1.35	.971	A.P. I. Gravity of Liquid Hydrocarbons	DRY	Deg.
2.	.20	532	1.35	.971	Specific Gravity Separator Gas	.722	XXXXXXXXXX
3.	.20	522	1.32	.971	Specific Gravity Flowing Fluid	DRY	XXXXXX
4.	.19	521	1.32	.971	Critical Pressure	667	P.S.I.A. P.S.I.A.
5.					Critical Temperature	395	R R

P _c 686.1 P _c ² 470.73					$1) \frac{P_c^2}{P_c^2 - P_w^2} = \underline{2.27802}$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1.90400}$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{1,538}$	
1.		663.0	439.57	31.16		
2.		656.2	430.60	40.13		
3.		631.7	399.04	71.69		
4.		513.9	264.09	206.64		
5.						

Absolute Open Flow 1,538 Mcfd @ 15.025	Angle of Slope Θ 52	Slope, n .78216
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Remarks: _____

* BHP INST. SET HERE FOR 4 PT. TEST

Approved By Division	Conducted By: PRO WELL TESTER	Calculated By: KS	Checked By: BM
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