

UNITED STATES  
DEPARTMENT OF THE INTERIOR  
BUREAU OF LAND MANAGEMENT

APPLICATION FOR PERMIT TO DRILL OR REENTER

OCD - HOBBS  
06/17/2020  
RECEIVED

FORM APPROVED  
OMB No. 1004-0137  
Expires: January 31, 2018

1a. Type of work: <input checked="" type="checkbox"/> DRILL <input type="checkbox"/> REENTER		5. Lease Serial No. NMNM132079
1b. Type of Well: <input checked="" type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other		6. If Indian, Allottee or Tribe Name
1c. Type of Completion: <input type="checkbox"/> Hydraulic Fracturing <input checked="" type="checkbox"/> Single Zone <input type="checkbox"/> Multiple Zone		7. If Unit or CA Agreement, Name and No.
2. Name of Operator MATADOR PRODUCTION COMPANY [228937]		8. Lease Name and Well No. UNCLE CHES 2116 FED COM 232H [326210]
3a. Address 5400 LBJ Freeway, Suite 1500 Dallas TX 75240	3b. Phone No. (include area code) (972)371-5200	9. API Well No. 30-025-47338
4. Location of Well (Report location clearly and in accordance with any State requirements. *) At surface SESW / 260 FSL / 1797 FWL / LAT 32.5521085 / LONG -103.4650448 At proposed prod. zone NENW / 240 FNL / 2310 FWL / LAT 32.5797943 / LONG -103.4633815		10. Field and Pool, or Exploratory JENNINGS; BONE SPRING, WEST / AN1 [98346]
14. Distance in miles and direction from nearest town or post office* 12 miles		12. County or Parish LEA
15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) 260 feet		13. State NM
16. No of acres in lease 160		17. Spacing Unit dedicated to this well 640
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. 30 feet		20. BLM/BIA Bond No. in file FED: NMB001079
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3717 feet		22. Approximate date work will start* 08/01/2019
		23. Estimated duration 30 days
24. Attachments		

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, and the Hydraulic Fracturing rule per 43 CFR 3162.3-3 (as applicable)

- |  |   |
|--|---|
| 1. Well plat certified by a registered surveyor.   | 4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above). |
| 2. A Drilling Plan.  | 5. Operator certification.  |
| 3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office). | 6. Such other site specific information and/or plans as may be requested by the BLM.            |

25. Signature (Electronic Submission)	Name (Printed/Typed) Lara Thompson / Ph: (505)431-2678	Date 02/25/2019
Title Project Manager		
Approved by (Signature) (Electronic Submission)	Name (Printed/Typed) Cody Layton / Ph: (575)234-5959	Date 06/16/2020
Title Assistant Field Manager Lands & Minerals CARLSBAD		

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.  
Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

GCP Rec 06/17/2020

SL

(Continued on page 2)

APPROVED WITH CONDITIONS  
Approval Date: 06/16/2020

KZ  
06/29/2020

\*(Instructions on page 2)



U.S. Department of the Interior  
BUREAU OF LAND MANAGEMENT

# Operator Certification Data Report

06/16/2020

## Operator Certification

*I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.*

**NAME:** Lara Thompson

**Signed on:** 10/04/2018

**Title:** Project Manager

**Street Address:** 5647 Jefferson Street NE

**City:** Albuquerque

**State:** NM

**Zip:** 87109

**Phone:** (505)431-2678

**Email address:** Lara.Thompson@swca.com

## Field Representative

**Representative Name:**

**Street Address:**

**City:**

**State:**

**Zip:**

**Phone:**

**Email address:**



APD ID: 10400034848

Submission Date: 02/25/2019

Highlighted data  
reflects the most  
recent changes

Operator Name: MATADOR PRODUCTION COMPANY

Well Name: UNCLE CHES 2116 FED COM

Well Number: 232H

[Show Final Text](#)

Well Type: OIL WELL

Well Work Type: Drill

## Section 1 - General

APD ID: 10400034848

Tie to previous NOS? N

Submission Date: 02/25/2019

BLM Office: CARLSBAD

User: Lara Thompson

Title: Project Manager

Federal/Indian APD: FED

Is the first lease penetrated for production Federal or Indian? FED

Lease number: NMNM132079

Lease Acres: 160

Surface access agreement in place?

Allotted?

Reservation:

Agreement in place? NO

Federal or Indian agreement:

Agreement number:

Agreement name:

Keep application confidential? YES

Permitting Agent? YES

APD Operator: MATADOR PRODUCTION COMPANY

Operator letter of designation:

## Operator Info

Operator Organization Name: MATADOR PRODUCTION COMPANY

Operator Address: 5400 LBJ Freeway, Suite 1500

Zip: 75240

Operator PO Box:

Operator City: Dallas

State: TX

Operator Phone: (972)371-5200

Operator Internet Address: amonroe@matadorresources.com

## Section 2 - Well Information

Well in Master Development Plan? NO

Master Development Plan name:

Well in Master SUPO? NO

Master SUPO name:

Well in Master Drilling Plan? NO

Master Drilling Plan name:

Well Name: UNCLE CHES 2116 FED COM

Well Number: 232H

Well API Number:

Field/Pool or Exploratory? Field and Pool

Field Name: JENNINGS; BONE  
SPRING, WEST

Pool Name: ANTELOPE  
RIDGE; BONE SPRING

Is the proposed well in an area containing other mineral resources? NATURAL GAS,OIL

Operator Name: MATADOR PRODUCTION COMPANY

Well Name: UNCLE CHES 2116 FED COM

Well Number: 232H

Is the proposed well in an area containing other mineral resources? NATURAL GAS,OIL

Is the proposed well in a Helium production area? N Use Existing Well Pad? NO New surface disturbance?

Type of Well Pad: MULTIPLE WELL

Multiple Well Pad Name: SLOT Number: 2

Well Class: HORIZONTAL

Number of Legs: 1

Well Work Type: Drill

Well Type: OIL WELL

Describe Well Type:

Well sub-Type: INFILL

Describe sub-type:

Distance to town: 12 Miles

Distance to nearest well: 30 FT

Distance to lease line: 260 FT

Reservoir well spacing assigned acres Measurement: 640 Acres

Well plat: Matador\_Uncle\_Ches\_232H\_20181004122735.pdf

Well work start Date: 08/01/2019

Duration: 30 DAYS

### Section 3 - Well Location Table

Survey Type: RECTANGULAR

Describe Survey Type:

Datum: NAD83

Vertical Datum: NAVD88

Survey number:

Reference Datum:

Wellbore	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD	Will this well produce from this lease?
SHL Leg #1	260	FSL	179 7	FW L	20S	35E	21	Aliquot SESW	32.55210 85	- 103.4650 448	LEA	NEW MEXI CO	NEW MEXI CO	F	NMNM 132079	371 7	0	0	
KOP Leg #1	260	FSL	179 7	FW L	20S	35E	21	Aliquot SESW	32.55210 85	- 103.4650 448	LEA	NEW MEXI CO	NEW MEXI CO	F	NMNM 132079	- 797 2	117 10	116 89	
PPP Leg #1-1	330	FSL	231 1	FW L	20S	35E	21	Aliquot SESW	32.55230 22	- 103.4633 761	LEA	NEW MEXI CO	NEW MEXI CO	F	NMNM 132079	- 854 8	126 19	122 65	

**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

Wellbore	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD	Will this well produce from this lease?
PPP Leg #1-2	1286	FSL	2311	FWL	20S	35E	21	Aliquot SESW	32.5549283	- 103.463376	LEA	NEW MEXICO	NEW MEXICO	F	NMNM 137465	- 8548	13575	12265	
EXIT Leg #1	330	FSL	2310	FWL	20S	35E	16	Aliquot NENW	32.5795469	- 103.4633814	LEA	NEW MEXICO	NEW MEXICO	S	STATE	- 8548	22234	12265	
BHL Leg #1	240	FNL	2310	FWL	20S	35E	16	Aliquot NENW	32.5797943	- 103.4633815	LEA	NEW MEXICO	NEW MEXICO	S	STATE	- 8548	22324	12265	



APD ID: 10400034848

Submission Date: 02/25/2019

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reflects the most  
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Operator Name: MATADOR PRODUCTION COMPANY

Well Name: UNCLE CHES 2116 FED COM

Well Number: 232H

[Show Final Text](#)

Well Type: OIL WELL

Well Work Type: Drill

## Section 1 - Geologic Formations

Formation ID	Formation Name	Elevation	True Vertical Depth	Measured Depth	Lithologies	Mineral Resources	Producing Formation
404808	RUSTLER	1774	1964	1964		NONE	N
404809	SALADO	-533	2307	2307		NONE	N
404810	DELAWARE	-4519	6293	6293		NATURAL GAS, OIL	N
404811	BRUSHY CANYON	-5570	7344	7344		NATURAL GAS, OIL	N
404812	BONE SPRING 1ST	-7834	9608	9608		NATURAL GAS, OIL	N
404813	BONE SPRING 2ND	-8297	10071	10071		NATURAL GAS, OIL	N
404814	BONE SPRING 3RD	-9172	10946	10946		NATURAL GAS, OIL	N
404815	WOLFCAMP	-9923	11697	11697		NATURAL GAS, OIL	Y

## Section 2 - Blowout Prevention

Pressure Rating (PSI): 5M

Rating Depth: 12000

**Equipment:** A 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams. An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed.

**Requesting Variance?** YES

**Variance request:** Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used. Matador is requesting a variance to use a speed head for setting the intermediate (9-5/8") casing. In the case of running a speed head with landing mandrel for 9-5/8" casing, BOP test pressures after setting surface casing will be 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. The BOPs will not be tested again until after setting 7-5/8" x 7" casing unless any flanges are separated. A diagram of the speed head is attached.

**Testing Procedure:** Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position. A third party company will test the BOPs. After setting surface casing, and before drilling below the surface casing shoe, BOPE will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high. After setting 9-5/8" casing, pressure tests will be made to 250 psi low

**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. After setting 7-5/8" x 7" Casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 5000 psi high.

**Choke Diagram Attachment:**

BLM\_Choke\_Mod\_20181004125242.pdf

**BOP Diagram Attachment:**

BOP\_809\_001\_20181004125258.pdf

809\_CoFlex\_Certs\_\_\_Uncle\_Ches\_Copy\_20181004125316.pdf

### Section 3 - Casing

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	20	13.375	NEW	API	N	0	1984	0	1984			1984	J-55	54.5	OTHER - BTC	1.125	1.125	DRY	1.8	DRY	1.8
2	INTERMEDIATE	12.25	9.625	NEW	API	N	0	5900	0	5900			5900	J-55	40	OTHER - BTC	1.125	1.125	DRY	1.8	DRY	1.8
3	INTERMEDIATE	8.75	7.625	NEW	API	Y	0	12450	0	12240			12450	P-110	29.7	OTHER - BTC	1.125	1.125	BUOY	1.8	BUOY	1.8
4	PRODUCTION	6.125	5.5	NEW	API	Y	0	22324	0	12265			22324	P-110	20	OTHER - TXP	1.125	1.125	DRY	1.8	DRY	1.8

### Casing Attachments

**Casing ID:** 1      **String Type:** SURFACE

**Inspection Document:**

**Spec Document:**

**Tapered String Spec:**

**Casing Design Assumptions and Worksheet(s):**

BLM\_Casing\_Design\_Assumptions\_4\_string\_Wolfcamp\_20181004133215.docx



**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

#### Casing Attachments

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**Casing ID:** 2      **String Type:** INTERMEDIATE

**Inspection Document:**

**Spec Document:**

**Tapered String Spec:**

**Casing Design Assumptions and Worksheet(s):**

BLM\_Casing\_Design\_Assumptions\_4\_string\_Wolfcamp\_20181004133257.docx

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**Casing ID:** 3      **String Type:** INTERMEDIATE

**Inspection Document:**

**Spec Document:**

**Tapered String Spec:**

7.625in\_29.7\_\_P110HC\_BTC\_20190222111326.PDF

**Casing Design Assumptions and Worksheet(s):**

BLM\_Casing\_Design\_Assumptions\_4\_string\_Wolfcamp\_20181009123840.docx

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**Casing ID:** 4      **String Type:** PRODUCTION

**Inspection Document:**

**Spec Document:**

**Tapered String Spec:**

5.5in\_20\_\_P110IC\_TXP\_20190222111428.pdf

**Casing Design Assumptions and Worksheet(s):**

BLM\_Casing\_Design\_Assumptions\_4\_string\_Wolfcamp\_20181009123832.docx

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#### Section 4 - Cement



**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1984	2188	1.75	13.5	3829	100	C	3% NaCl + LCM
SURFACE	Tail		0	1984	694	1.38	14.8	958	100	C	5% NaCl + LCM
INTERMEDIATE	Lead		0	5900	1344	1.81	13.5	2433	100	C	Bentonite + 1% CaCL2 + 8% NaCl + LCM
INTERMEDIATE	Tail		0	5900	536	1.38	14.8	740	100	C	5% NaCl + LCM
INTERMEDIATE	Lead		4900	12450	946	2.36	11.5	2233	35	TXI	Fluid Loss + Dispersant + Retarder + LCM
INTERMEDIATE	Tail		11559	22324	105	1.38	13.2	228	35	TXI	Fluid Loss + Dispersant + Retarder + LCM
PRODUCTION	Lead		11450	22324	816	1.38	15.8	1126	35	H	Fluid Loss + Dispersant + Retarder + LCM
PRODUCTION	Tail										none

### Section 5 - Circulating Medium

**Mud System Type:** Closed

**Will an air or gas system be Used?** NO

**Description of the equipment for the circulating system in accordance with Onshore Order #2:**

**Diagram of the equipment for the circulating system in accordance with Onshore Order #2:**

**Describe what will be on location to control well or mitigate other conditions:** All necessary mud products for weight addition and fluid loss control will be on location at all times. Mud program subject to change due to hole conditions.

**Describe the mud monitoring system utilized:** The Mud Monitoring System is an electronic Pason system satisfying requirements of Onshore Order 1.

### Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	PH	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	22324	OIL-BASED MUD	12	12							

**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	PH	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	1245 0	OTHER : FW/Cut Brine	9	9							
0	1984	SPUD MUD	8.4	8.4							
0	5900	SALT SATURATED	10	10							

## Section 6 - Test, Logging, Coring

**List of production tests including testing procedures, equipment and safety measures:**

- Mud Logging Program: 2 man unit from 1984 – TD
- Electric Logging Program: No electric logs are planned at this time. GR will be collected through the MWD tools from Inter. Csg to TD
- No DSTs or cores are planned at this time
- CBL w/ CCL from as far as gravity will let it fall to TOC

**List of open and cased hole logs run in the well:**

CBL,GR,MWD,MUDLOG

**Coring operation description for the well:**

NA

## Section 7 - Pressure

**Anticipated Bottom Hole Pressure:** 6132

**Anticipated Surface Pressure:** 3433.7

**Anticipated Bottom Hole Temperature(F):** 170

**Anticipated abnormal pressures, temperatures, or potential geologic hazards?** NO

**Describe:**

**Contingency Plans geohazards description:**

**Contingency Plans geohazards attachment:**

**Hydrogen Sulfide drilling operations plan required?** YES

**Hydrogen sulfide drilling operations plan:**

H2S\_Emergency\_Contacts\_20181004131244.docx

Matador\_Hydrogen\_Sulfide\_Drilling\_Uncle\_Ches\_20181004131245.docx

**Operator Name:** MATADOR PRODUCTION COMPANY

**Well Name:** UNCLE CHES 2116 FED COM

**Well Number:** 232H

MRC\_Energy\_Co\_\_Drilling\_Contingency\_plan\_20181004131245.doc

## Section 8 - Other Information

### **Proposed horizontal/directional/multi-lateral plan submission:**

Matador\_UncleChesFed\_232H\_PrelimA\_WPReport\_20181004130811.pdf

Matador\_UncleChesFed\_232H\_PrelimA\_20181004131111.PDF

Matador\_UncleChesFed\_232H\_PrelimA\_ACReport\_20181009124151.pdf

### **Other proposed operations facets description:**

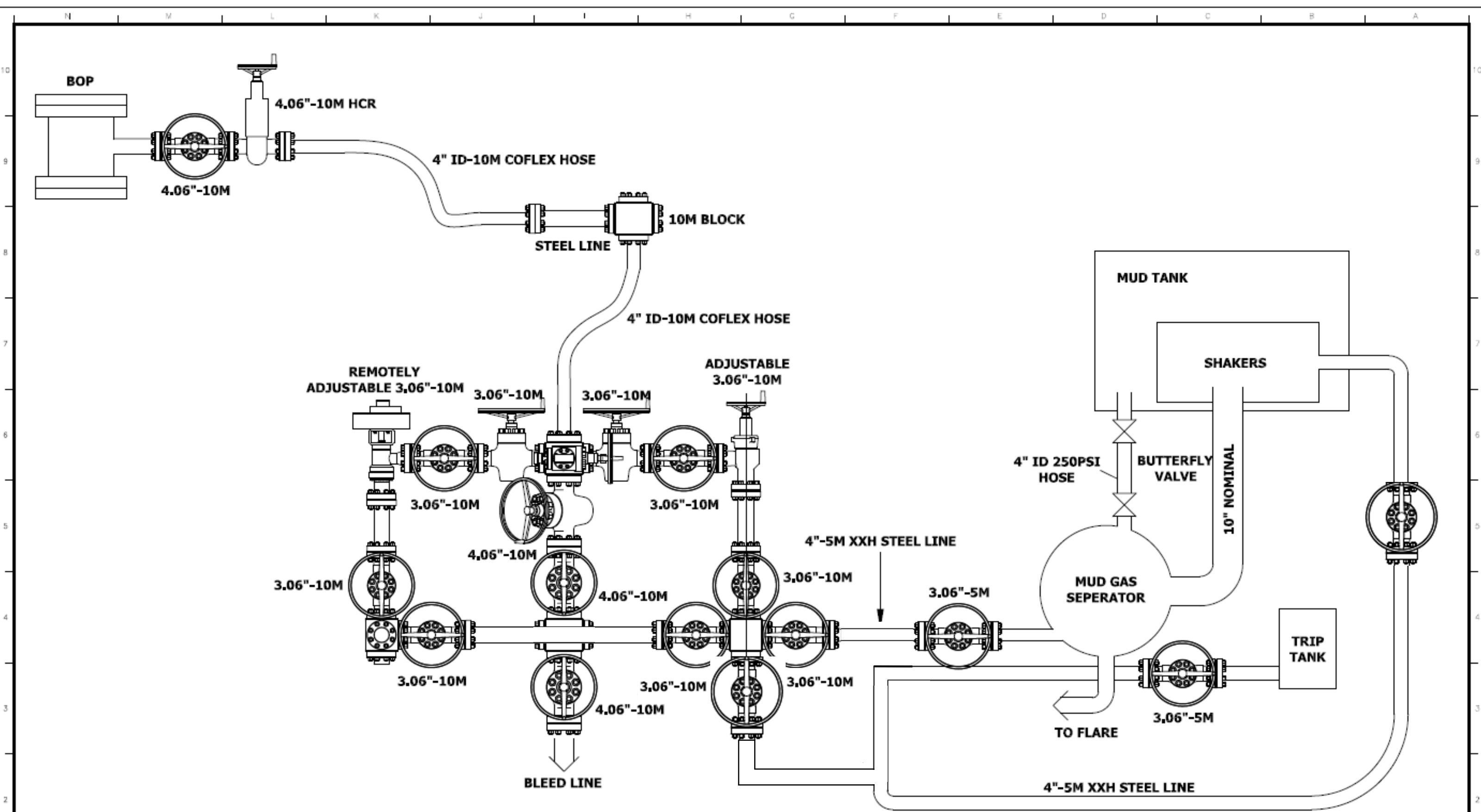
### **Other proposed operations facets attachment:**

### **Other Variance attachment:**

Close\_Loop\_System\_20181004130901.docx

4\_String\_Wellhead\_Diagram\_20181004131055.pdf

Uncle\_Ches\_Fed\_\_232H\_MTDR\_Drill\_Plan\_4.13.20\_20200413165605.pdf



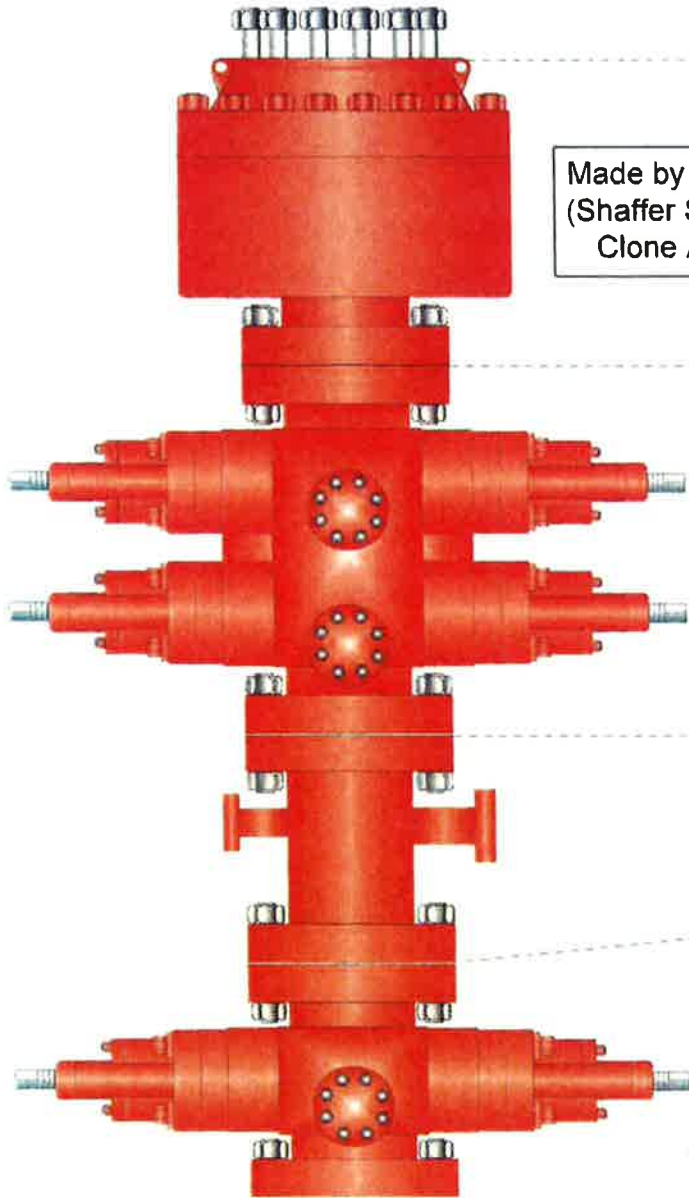
WELDING NOTE & TOLERANCES UNLESS OTHERWISE SPECIFIED.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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**PATTERSON-UTI**  
*Well Control*

Exhibit E-1: BOP  
Uncle Ches Fed Com #232H  
Matador Resources Company

**RIG:** **809**



Made by Cameron  
(Shaffer Spherical)  
Clone Annular

PATTERSON-UTI # PS2-628  
STYLE: New Shaffer Spherical  
BORE 13 5/8" PRESSURE 5,000  
HEIGHT: 48 1/2" WEIGHT: 13,800 lbs

PATTERSON-UTI # PC2-128  
STYLE: New Cameron Type U  
BORE 13 5/8" PRESSURE 10,000  
RAMS: TOP 5" Pipe BTM Blinds  
HEIGHT: 66 5/8" WEIGHT: 24,000 lbs

Length 40" Outlets 4" 10M  
DSA 4" 10M x 2" 10M

PATTERSON-UTI # PC2-228  
STYLE: New Cameron Type U  
BORE 13 5/8" PRESSURE 10,000  
RAMS: 5" Pipe  
HEIGHT: 41 5/8" WEIGHT: 13,000 lbs

2" Minimum Kill Line

**WING VALVES**

3" Minimum Choke Line



2" Check Valve



2" Manual Valve



2" Manual Valve



4" Manual Valve



4" Hydraulic Valve

## **Casing Design Criteria and Load Case Assumptions**

### **Surface Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

### **Intermediate #1 Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Intermediate #2 Casing**

Collapse:  $DF_c=1.125$

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## Production Casing

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).



## **Casing Design Criteria and Load Case Assumptions**

### **Surface Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

### **Intermediate #1 Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Production Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered.

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## **Casing Design Criteria and Load Case Assumptions**

### **Surface Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

### **Intermediate #1 Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Intermediate #2 Casing**

Collapse:  $DF_c=1.125$

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## Production Casing

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

## **Casing Design Criteria and Load Case Assumptions**

### **Surface Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

### **Intermediate #1 Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Intermediate #2 Casing**

Collapse:  $DF_c=1.125$

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## Production Casing

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

## **Casing Design Criteria and Load Case Assumptions**

### **Surface Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

### **Intermediate #1 Casing**

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

### **Intermediate #2 Casing**

Collapse:  $DF_c=1.125$

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).



- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

## Production Casing

Collapse:  $DF_c=1.125$

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst:  $DF_b=1.125$

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile:  $DF_t=1.8$

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Exhibit E-6: H2S Contingency Plan Emergency Contacts  
 Uncle Ches Fed Com #232H  
 Matador Resources Company  
 UL: N, Sec. 21, 20S, 35E  
 Lea Co, NM

Company Office			
Matador Resources Company		(972)-371-5200	
Key Personnel			
Name	Title	Office	Mobile
Billy Goodwin	Vice President Drilling	972-371-5210	817-522-2928
Dee Smith	Drilling Superintendent	972-371-5447	972-822-1010
Toby Solis	Drilling Superintendent		817-372-7817
Patrick Walsh	Drilling Engineer	972-371-5291	626-318-5808
	Construction		
Jimmy Benefield	Superintendent		318-548-6659
Artesia			
Ambulance		911	
State Police		575-746-2703	
City Police		575-746-2703	
Sheriff's Office		575-746-9888	
Fire Department		575-746-2701	
Local Emergency Planning Committee		575-746-2122	
New Mexico Oil Conservation Division		575-748-1283	
Carlsbad			
Ambulance		911	
State Police		575-885-3137	
City Police		575-885-2111	
Sheriff's Office		575-887-7551	
Fire Department		575-887-3798	
Local Emergency Planning Committee		575-887-6544	
New Mexico Oil Conservation Division		575-887-6544	
Santa Fe			
New Mexico Emergency Response Comission (Santa Fe)		505-476-9600	
New Mexico Emergency Response Comission (Santa Fe) 24 hrs		505-827-9126	
New Mexico State Emergency Operations Center		505-476-9635	
National			
National Emegency Response Center (Washington, D.C.)		800-424-8802	
Medical			
Flight for Life- 4000 24th St.; Lubbock, TX		806-743-9911	
Aerocare- R3, Box 49F; Lubbock, TX		806-747-8923	
Med Flight Air Amb- 2301 Yale Blvd S.E., D3; Albuquerque, NM		505-842-4433	
SB Air Med Service- 2505 Clark Carr Loop S.E.; Albuquerque, NM		505-842-4949	
Other			
Boots & Coots IWC	800-256-9688	or 281-931-8884	
Cudd Pressure Control	432-699-0139	or 432-563-3356	
Haliburton	575-746-2757		



## Hydrogen Sulfide Drilling

### Operations Plan

#### Matador Resources

##### 1 H2S safety instructions to the following:

- Characteristics of H2S
- Physical effects and hazards
- Principal and operation of H2S detectors, warning system and briefing areas
- Evacuation procedures, routes and first aid
- Proper use of safety equipment & life support systems
- Essential personnel meeting medical evaluation criteria will receive additional training on the proper use of 30min pressure demand air packs

##### 2 H2S Detection and Alarm Systems:

- H2S sensor/detectors to be located on the drilling rig floor, in the base of the sub structure / cellar area, on the mud pits in the shale shaker area. Additional H2S detectors may be placed as deemed necessary
- An audio alarm system will be installed on the derrick floor and in the doghouse

##### 3 Windsocks and / Wind Streamers:

- Windsocks at mud pit area should be high enough to be visible
- Windsock on the rig floor and / top of doghouse should be high enough to be visible

##### 4 Condition Flags and Signs:

- Warning sign on access road to location
- Flags to be displayed on sign at entrance to location
  - o Green Flag – Normal Safe Operation Condition
  - o Yellow Flag – Potential Pressure and Danger
  - o Red Flag – Danger (H2S present in dangerous concentrations) Only H2S trained personnel admitted on location

##### 5 Well Control Equipment:

- See Exhibit E-1

##### 6 Communication:

- While working under masks chalkboards will be used for communications

- Hand signals will be used where chalk board is inappropriate
- Two way radio will be used to communicate off location in case of emergency help is required. In most cases cellular telephones will be available at most drilling foreman's trailer or living quarters.

#### 7 Drilling Stem Testing:

- No DST cores are planned at this time

8 Drilling contractor supervisor will be required to be familiar with the effects H<sub>2</sub>S has on tubulars good and other mechanical equipment

9 If H<sub>2</sub>S is encountered, mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H<sub>2</sub>S scavengers if necessary

#### 11 Emergency Contacts

- See exhibit E-6

**HYDROGEN SULFIDE CONTINGENCY PLAN**  
**Drilling, Testing, & Completion**

**MRC ENERGY CO.**

**Uncle Ches Fed Com #232H**

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**Reviewers**

----- Operations Manager  
----- Operations Supt.  
----- Staff RES  
----- Field Supv.  
----- Engineering

**Latitude: 32.5519" N**  
**Longitude: 103.4646" W**

**(Surface Location)**

**H2S Contingency Plan # 0165      Revision# 0**

**This H2S Contingency Plan is subject to updating**

Effective date: July 8, 2015

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## **INTRODUCTION**

**The H<sub>2</sub>S equipment will be rigged up 2 days prior to reaching a potential H<sub>2</sub>S containing zone. Drilling into any potential H<sub>2</sub>S zone shall not commence until the on-site MRC Drilling Supervisor has confirmed this plan in place.**

**The onsite Drilling Foreman will give Total Safety one week (7 days) notice to prepare for rig up of H<sub>2</sub>S equipment)**

To be effective, the plan requires the cooperation and effort of each person participating in the drilling of an H<sub>2</sub>S well. Each person must know his/her responsibilities and all emergency and safety procedures. He/she should thoroughly understand and be able to use with accuracy, all safety equipment while performing his/her normal duties, if the circumstance should arise. He/she should therefore familiarize himself/herself with the location of all safety equipment and check to see that it is properly stored, easily accessible at all times, and routinely maintained.

It is the intention of MRC ENERGY CO. and the Drilling Contractor to make every effort to provide adequate safeguards against harm to persons on the rig and in the immediate vicinity from the effects of hydrogen sulfide, which may be released into the atmosphere under emergency conditions. However, the initiative rests with the individual in utilizing the safeguards provided. The ideas and suggestions of the individuals involved in the drilling of this well are highly welcomed and act as a fundamental tool for providing the safest working conditions possible.

The drilling representative is required to enforce these procedures. They are set up for your safety and the safety of all others.

## **II. PURPOSE**

It is MRC Energy Co.'s intent to provide a safe working place, not only for its employees, but also for other contractors who are aiding in the drilling of this well. The safety of the general public is of utmost concern. All precautions will be taken to keep a safe working environment and protect the public.

There is a possibility of encountering toxic hydrogen sulfide gas. Safety procedures must be adhered to in order to protect all personnel connected with the operations as well as people living within the area.

The MRC Energy Co. representative will enforce all aspects of the H<sub>2</sub>S Contingency Plan. This job will become easier by a careful study of the following pages and training and informing all personnel that will be working on the well, their duties and responsibilities.

## **A. OPERATING PROCEDURES**

### **DEFINITIONS:**

**For purpose of this plan, on-site personnel shall be referred to as “In Scope Personnel” or “Out of Scope Personnel”, per the following definitions:**

**In Scope Personnel** – Personnel who will be working or otherwise present in potential H<sub>2</sub>S release areas, including the rig floor, cellar, pits, and shaker areas.

**Out of Scope Personnel** – Personnel who will not be working or Otherwise present in potential H<sub>2</sub>S areas. Such personnel include rig Site visitor, delivery and camp services personnel.

### **GENERAL:**

Before this H<sub>2</sub>S contingency plan becomes operational, all regularly assigned In Scope Personnel (primarily the MRC, drilling contractor, and certain service personnel,) shall be thoroughly trained in the use of breathing equipment, emergency procedures, and responsibilities. Total Safety Technician or a designee assigned by the MRC Drilling Foreman shall keep a list of all personnel who have been through the on-site H<sub>2</sub>S training program at the drill site.

All In Scope Personnel shall be given H<sub>2</sub>S training and the steps to be taken during H<sub>2</sub>S conditions under which the well may be drilled. General information will be explained about toxic gases, as well as the physiological effects of H<sub>2</sub>S and the various classified operating conditions. In addition, the reader will be informed his/her general responsibility concerning safety equipment and emergency procedures.

The Total Safety H<sub>2</sub>S Safety Technician or MRC on-site RSE Technician shall make available the H<sub>2</sub>S Contingency Plan for all personnel to review.

Without exception, all personnel that arrive on location must proceed directly to and sign-in with the on-site MRC RSE Technician. In Scope Personnel will be required to complete an on-site H<sub>2</sub>S training and respirator fit testing before starting work, or produce evidence that they have received equivalent training. Out of Scope Personnel will be required to complete a site H<sub>2</sub>S awareness and general safety briefing. This

briefing will consist of a H<sub>2</sub>S hazard overview, alarm review and required response to alarms.

**B. PROCEDURES TO BE INITIATED PRIOR TO H<sub>2</sub>S CONTINGENCY PLAN COMPLIANCE:**

A list of emergency phone numbers and contacts will be on location and posted at the following locations:

1. MRC ENERGY CO.'S Representative's Office
2. Drilling Contractor's, Toolpusher Office
3. Living Quarters Area

All safety equipment and H<sub>2</sub>S related hardware must be set up as required by MRC Energy Co. with regard to location of briefing areas, breathing equipment, etc. All safety equipment must be inspected periodically (at least weekly) with particular attention to resuscitators and breathing equipment.

In Scope Personnel working in the well site area will be assigned breathing apparatus. Operator and drilling contractor personnel required to work in the following areas will be provided with Self Contained Breathing Apparatus:

1. Rig Floor
2. Mud Pits
3. Derrick
4. Shale Shaker
5. Cellar

The Total Safety H<sub>2</sub>S Safety Technician will be responsible for rigging up all H<sub>2</sub>S continuous monitoring-type detectors. The Total Safety Technician will monitor and bump test the detector units periodically (at least at least once a week to test alarm function during drilling conditions. In the event H<sub>2</sub>S is detected, or when drilling in a zone confirmed to contain H<sub>2</sub>S, the units shall be bump tested at least once every 24 hours. A bump test/calibration log will be kept on location. All results will be reported to the MRC on-site Drilling Foreman.

All Total Safety H<sub>2</sub>S equipment will be maintained and inspected by a Total Safety Technician on at least a Weekly basis.

### **C. DRILLING BELOW CONTINGENCY PLAN DEPTH**

H<sub>2</sub>S response drills will be held at least once per week if possible or as often as necessary to acquaint the crews and service company personnel of their responsibilities and the proper procedures to shut-in a well. Initial drills will be performed until crews demonstrate competency donning and working under mask. After the MRC Energy Co.'s representative is satisfied with initial blowout drill procedures, a drill will be conducted weekly with each crew, as necessary. The H<sub>2</sub>S Safety Technician or designee will conduct safety talks and maintain the safety equipment, consult and carry out the instructions of the drilling supervisor. All personnel allowed in the well work area during drilling or testing operations will be instructed in the use of breathing equipment until supervisory personnel are satisfied that they are capable of using it.

After familiarization, each person must perform a drill with breathing equipment. The drill should include getting the breathing equipment, donning the breathing apparatus, and performing expected duties for a short period. A record shall be kept of all personnel drilled and the date of the drill. H<sub>2</sub>S training records will be kept on location for all personnel.

Rig crews and service company personnel shall be made aware of the location of spare air bottles, resuscitation equipment, portable fire extinguishers, H<sub>2</sub>S monitors and detectors. Knowledge of the location of the H<sub>2</sub>S monitors and detectors are vital in determining as our gas location and the severity of the emergency conditions.

After any device has initially detected H<sub>2</sub>S, all areas of poor ventilation shall be inspected periodically by means of a portable H<sub>2</sub>S detector instrument. The buddy system will be utilized. (When an alarm sounds, personnel will don an SCBA, shut the well in, and proceed to SBA for roll call. The H<sub>2</sub>S Technician or designee will mask up, with a buddy and will verify source of H<sub>2</sub>S and report back to the on-site MRC Foreman.)

### **D. PROCEDURES PROGRAM**

1. Drill Site

- a. The drilling rig will be located to allow prevailing winds to blow across the reserve pit.
- b. A Safe Briefing Area will be provided with a breathing air cascade trailer and or 30-minute SCBA's at the Primary Area. Personnel will assemble at the most up-wind station under alarm conditions, or when so ordered by the MRC Energy Co. representative, the Contractor representative, or the Total Safety H<sub>2</sub>S Safety Technician. Windsocks or streamers will be anchored to various strategic places on a pole about 10 feet high, so it is in easy view from the rig floor at all times.
- c. Warning signs will be posted on the perimeters. "No Smoking" signs will be posted by MRC Energy Co.as well.
- d. One multi-channel automatic H<sub>2</sub>S monitor will be provided by Total Safety and the detector heads will be at the shale shaker, bell nipple, mud pits, rig floor, and quarter's area. The monitor will be located inside HSE or Company man trailer. Should the alarm be shut off to silence the sirens, the blinker light must continue to warn of H<sub>2</sub>S presence. The Total Safety H<sub>2</sub>S Safety Technician or designee will continuously monitor the detectors and will reactivate the alarm if H<sub>2</sub>S concentrations increase to a dangerous level.
- e. A method of escape will be open at all times.
- f. If available, land line telephone service will be provided or cell phones provided. (Primary communications provided)
- g. A rig communication system will be provided, as needed.
- h. A gas trap, choke manifold, and degasser will be installed.
- i. A kill line, securely anchored and of ample strength, will be laid to the well-head from a safe location. This line is to be used only in an emergency.

#### General

- a. The MRC Energy Co. representative and/or the Contractor's Toolpusher will be available at all times. The drilling supervisor, while on duty, will have complete charge of the rig and location operations and will take whatever action is deemed necessary to insure personnel safety, to protect the well, and to prevent damage.
- b. b. A Mud Engineer will be on location at all times when  
c drilling takes place at the depth H<sub>2</sub>S may be expected. The mud engineer will be able to verify the presence or absence of H<sub>2</sub>S.



### III. CONDITIONS AND EMERGENCY PROCEDURES

#### A. DEFINITION OF OPERATIONAL “CONDITIONS”

<b>CONDITION I</b>	<b>“POSSIBLE DANGER”</b>
Warning Flags	Green
Alarms	No Alarm. Less than 10 ppm
Characterized By:	Drilling operations in zones that may contain hydrogen sulfide. This condition remains in effect unless H <sub>2</sub> S is detected and it becomes necessary to go to Condition II.
General Action:	<ol style="list-style-type: none"> <li>Be alert for a condition change</li> <li>Check all safety equipment for availability and proper functioning.</li> <li>Perform all drills for familiarization and proficiency.</li> </ol>
<b>CONDITION II</b>	<b>“MODERATE DANGER”</b>
Warning Flags	Yellow
Alarms:	Actuates at 10 ppm. Continuous flashing light.
Characterized By:	Drilling operations in zones containing hydrogen sulfide. This condition will remain in effect until adding chemicals to the mud system neutralizes the hydrogen sulfide or it becomes necessary to go to Condition III.
General Action:	<ol style="list-style-type: none"> <li>Be alert for a condition change</li> <li> <p>WHEN DRILLING AHEAD - Driller and designated crewmember will don 30 min SCBA, shut-in the well and immediately proceed to the Safe Briefing Area.</p> <p>WHEN TRIPPING – Driller and two designated crewmembers will don 30 min SCBA, shut in the well and</p> </li> </ol>

immediately proceed to the Safe Briefing Area. The Derrickman will don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

- c. All In Scope Personnel will proceed directly to the appropriate Safe Briefing Area.
- d. Remain in safe briefing area, take roll call and wait for instructions
- e. Contact the Total H<sub>2</sub>S Technician if not on location.
- f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H<sub>2</sub>S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases.
- g. All Out of Scope Personnel will report to the appropriate Safe Briefing Area.

### **CONDITION III “EXTREME DANGER”**

Warning Flags

Red

Alarms

Actuate at 15 ppm. Continuous Sirens and Flashing Lights

Characterized by:

Critical well operations which pose an immediate threat of H<sub>2</sub>S exposure to on-site personnel and a potential threat to the public.

General Action:

- a. WHEN DRILLING AHEAD - Driller and designated crewmember will don 30 min SCBA, shut-in the

well and immediately proceed to the Safe Briefing Area.

WHEN TRIPPING – Driller and two designated crewmembers will don 30 min SCBA, shut in the well and immediately proceed to the Safe Briefing Area. The Derrickman will don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

- b. All In Scope Personnel should don SCBA if nearby and immediately proceed to Safe Briefing Area. If SCBA is not nearby at time of alarm, **DO NOT GO TOWARDS RIG AREA**, but proceed directly to the Safe Briefing Area
- c. All out of Scope Personnel shall evacuate the location.
- d. Remain in the Safe Briefing Area, take roll call and wait for instructions.
- e. Contact the Total H<sub>2</sub>S Technician if not on location.
- f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H<sub>2</sub>S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases. Use the buddy system.
- g. Remain in safe briefing area, take roll call and wait for instructions.
- h. A cascade breathing air system shall be mobilized and utilized to conduct

any additional on rig work required to correct the H<sub>2</sub>S release condition.

- i. If well is ignited do not assume area is safe. SO<sub>2</sub> is hazardous and not all H<sub>2</sub>S will burn.

## **H<sub>2</sub>S EMERGENCY PROCEDURES; IN SCOPE PERSONNEL**

### **A. Day To Day Drilling Operations**

1. Upon discovering a release of H<sub>2</sub>S gas in the ambient air by warning alarms or in any other way **Do Not Panic**.
2. Hold your breath donning the nearest Self Contained Breathing Apparatus and rapidly move up or across-wind away from the areas where H<sub>2</sub>S sensing devices are in place, to the closest available safe briefing area. Continue to use breathing apparatus until it has been determined that the exposure of H<sub>2</sub>S gas in the ambient air no longer exists. **Do Not Panic!**
3. Utilize the “Buddy System”, i.e.; select and pair up each person participating in the drilling of an H<sub>2</sub>S well prior to an emergency situation.
4. Help anyone who is overcome or affected by the H<sub>2</sub>S gas by taking him/her up-wind out of the contaminated area. (This should be done utilizing an SCBA and with a buddy.)
5. Take necessary steps to confirm the release of the H<sub>2</sub>S gas into the ambient air.
  - When an H<sub>2</sub>S alarm activates, two designated personnel using the buddy system, while wearing their self contained breathing apparatus, will determine by the read-out on the fixed monitor which sensing device has detected the release of the H<sub>2</sub>S gas.
  - They will utilize the hand-held sniffer type device at the particular sensing point disclosed on the fixed monitor to corroborate the fact that H<sub>2</sub>S gas has actually been released. This will rule out the possibility of a false alarm. This will be done with a buddy and under mask after reporting to the Safe Briefing Area for roll call and instructions by on-site MRC Foreman.

6. Refer to the Emergency Phone Numbers and call emergency personnel.
7. Take the necessary steps to suppress the release of H<sub>2</sub>S gas into the ambient air. Comply with the MRC Energy Co. Representative to physically suppress the release of H<sub>2</sub>S gas at the actual release point.
8. Check all of MRC Energy Co.'s monitoring devices and increase gas-monitoring activities with the portable hand-operated H<sub>2</sub>S and gas detector units.

**Do Not Panic!**

The MRC Energy Co. representative will assess the situation and with assistance of the Contractor's Representative and Total Safety's H<sub>2</sub>S Safety Technician or on site designee, will assign duties to each person to bring the situation under control.

**B. RESPONSIBILITIES OF WELL-SITE PERSONNEL**

In the event of a release of potentially hazardous amounts of H<sub>2</sub>S, all personnel will immediately don their protective breathing apparatus, the well will be shut in and personnel will proceed upwind to the nearest designated safe briefing area for roll call and instructions by MRC Foreman. Consideration will be given to evacuating Out of Scope Personnel, as situation warrants.

**1. MRC ENERGY CO.'S Well-site Representatives**

- a. If MRC Energy Co.'s well-site representative is incapacitated or not on location, this responsibility will fall to the Toolpusher/Driller.
- b. Immediately upon assessing the situation, set this plan into Action by initiating the proper procedures to contain the gas and notify the appropriate people and agencies.
- c. Ensure that the alarm area indicated by the fixed H<sub>2</sub>S Monitor is checked and verified with a portable H<sub>2</sub>S detector. (Safety Technician if on location or MRC assigned designee with a buddy utilizing SCBA's)
- d. Consult Pusher/driller of remedial actions as needed.

- e. Ensure that non-essential personnel proceed to the safe briefing area.
- f. Ensure location entrance barricades are positioned. Keep the number of persons on location to a minimum during hazardous operations.
- g. Consult each contractor, Service Company and all others allowed to enter the site, that H<sub>2</sub>S gas may be encountered and the potential hazards that may exist.
- h. Authorize the evacuation of local residents if H<sub>2</sub>S threatens Their safety.
- i. Non essential personnel should be evacuated from location if Situation warrants.

## **2. Toolpusher**

- a. Toolpusher/Driller will assume responsibilities of MRC Energy Co.'s well-site representative if that person is incapacitated or not on location.
- b. Ensure that the alarm area indicated by the fixed H<sub>2</sub>S monitor is checked and verified with a portable H<sub>2</sub>S gas detector. (Alarm area indicated by the monitor will be Checked by the H<sub>2</sub>S Technician and a buddy, under mask.) This will be done after checking in and roll call at the Upwind Safe Briefing Area.
- c. Confer with MRC Energy Co.'s well-site representative or superintendent and direct remedial action to suppress the H<sub>2</sub>S and control the well.
- d. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- e. Ensure that personnel at the drill floor area are instructed on emergency actions required.
- f. Ensure that all personnel observe the appropriate safety and emergency procedures.

- g. Ensure that all persons are accounted for and provided emergency assistance as necessary.

**3. Mud Engineer**

- a. Run a sulfide check on the flowline mud.
- b. Take steps to determine the source of the H<sub>2</sub>S and suppress it. Lime and H<sub>2</sub>S scavenger shall be added to the mud as necessary.

**4. Total H<sub>2</sub>S Safety Technician, if on location, or MRC Designee**

- a. H<sub>2</sub>S Safety Technician or designee don nearest SCBA and report to Safe Briefing Area for roll call, take a buddy masked up and check monitor and verify with a portable H<sub>2</sub>S detector the alarm area indicated by the fixed H<sub>2</sub>S monitor. Advise the Toolpusher/Driller and MRC Energy Co.'s well-site representative of findings. Record all findings.
- b. If H<sub>2</sub>S is flared, check for sulfur dioxide (SO<sub>2</sub>) near the flare as necessary. Take hourly readings at different perimeters, log readings and record on location.
- c. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- d. Ensure that the appropriate warning flags are displayed.
- e. Ensure that all personnel are in S.C.B.A. as necessary.
- f. Ensure that all persons are accounted for and provide emergency assistance as necessary.

- g. Be prepared to evacuate rig if order is issued.

## **5. General Personnel & Visitors**

- a. All In Scope Personnel, if not specifically designated to shut the well in or control the well, shall proceed to the (upwind) safe briefing area. All Out of Scope Personnel shall immediately proceed to the appropriate (upwind) safe briefing area or evacuate the site as conditions warrant.
- b. During any emergency, use the “buddy” system to prevent anyone from entering or being left in a gas area alone, even wearing breathing apparatus.
- c. Provide assistance to anyone who may be injured or overcome by toxic gases. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering a potentially H<sub>2</sub>S contaminated area.
- d. Remain in safe briefing area and wait for instructions.

## **C. INSTRUCTIONS FOR IGNITING THE WELL**

- 1. The Toolpusher/Driller will confer with MRC Energy Co.'s well-site representative who will secure the approval of the “Texas Wells Delivery Manager, prior to igniting the well, if at all possible.

The Toolpusher/Driller will be responsible for igniting the well in the event of severe well control problems. This decision should be made only as a last resort in situations where it is clear that:

- a. Human life and property are endangered, or
  - b. There is no hope of controlling the well under current conditions.
- 2. Once the decision has been made, the following procedures should be followed:



- a. Two people wearing self-contained breathing apparatus will be needed for the actual lighting of the well. They must first establish the flammable perimeter by using an explosimeter. This should be established at 30% to 40% of the lower flammable limits.
- b. After the flammable perimeter has been established and everyone removed from the area, the ignition team should select a site upwind of the well from which to ignite the well. This site should offer the maximum protection and have a clear path for retreat from the area.
- c. The ignition team should have safety belts and lifeline attached and manned before attempting ignition. If the leak is not ignited on the first attempt, move in 20 to 30 feet and fire again. Continue to monitor with the explosimeter and NEVER fire from an area with over 75% of the Lower Explosive Limit (LEL). If having trouble igniting the well, try firing 40 degrees to 90 degrees on either side of the well.
- d. If ignition is not possible due to the makeup of the gas, the toxic perimeter must be established and evacuation continued until the well is contained.
- e. All personnel must act only as directed by the person in charge of the operations.

NOTE: After the well is ignited, burning hydrogen sulfide ( $H_2S$ ) will convert to sulfur dioxide ( $SO_2$ ), which is also a highly toxic gas.

**DO NOT ASSUME THE AREA IS SAFE AFTER THE WELL IS IGNITED**

#### **D. CORING PROCEDURES**

Only essential personnel shall be on the rig floor. Ten (10) stands prior to retrieving core barrel; all personnel on drill floor and in derrick shall confirm self-Contained breathing apparatus available and ready for use.

A Total H<sub>2</sub>S Technician will don a SCBA with a buddy assigned from the rig crew, and continuously monitor for H<sub>2</sub>S at each connection. Any levels detected will require operations to be shut down and all involved

personnel to don SCBAs. Precautions will remain in place until barrel is laid down.

All involved personnel will don SCBAs when removing the inner barrel from the outer barrel. SCBAs can be removed once the absence of H<sub>2</sub>S is confirmed by the Total H<sub>2</sub>S Technician.

Cores will be appropriately marked and sealed for transportation.

## **Normal Operations**

### **1. Responsibilities of well-site personnel**

#### **a. Well-site Representative**

1. Notify H<sub>2</sub>S Technician of expected date to reach Contingency Plan implementation depth (Two (2) days prior to reaching suspected H<sub>2</sub>S bearing zone) or prior to starting well work.
2. Ensure H<sub>2</sub>S Safety Technician completes rig-up procedures prior to reaching Contingency Plan effective depth.
3. Restrict the number of personnel at the drilling rig or well site to a minimum while drilling, starting well work, testing or coring.
4. Ensure weekly H<sub>2</sub>S drills/training are performed, if possible.

#### **B. Toolpusher**

1. Ensure that necessary H<sub>2</sub>S safety equipment is provided on the rig, and that it is properly inspected and maintained.
2. Ensure that all personnel that work in the well area, are thoroughly trained in the use of H<sub>2</sub>S safety

equipment and periodic drills are held to maintain an adequate level of proficiency.

**C. In Scope Personnel**

1. Remain clean-shaven. Beards and long sideburns do not allow a proper facepiece seal.
2. Receive H<sub>2</sub>S safety training on location, or confirm prior training by certification that is one year within date.
3. Familiarize yourself with the rig's Contingency Plan.
4. Inspect and practice putting on your breathing apparatus.
5. Know the location of the "safe briefing areas".
6. Keep yourself "wind conscious". Be prepared to quickly move upwind and away in the event of any emergency involving release of H<sub>2</sub>S.

**D. Total Safety H<sub>2</sub>S Safety Technician or MRC Designee**

1. Conduct training as necessary to ensure all personnel working in well area are familiar with the contingency procedures and the operation of emergency equipment.
2. Check all H<sub>2</sub>S safety equipment to ensure that it is ready for emergency use:
  - Check pressure weekly for each shift on breathing apparatus (both 30-minute and hip-packs) to make sure they are charged to full volume.
  - Check pressure on cascade air bottles, if on location, to see that they are capable of recharging breathing apparatus.

- Check oxygen resuscitator, if on location, to ensure that it is charged to full volume.
  - Check H<sub>2</sub>S detectors weekly for each shift (fixed and portable), and explosimeter, to ensure they are working properly.
3. Provide a weekly report to MRC Energy Co.'s well-site representative documenting:
- Calibrations performed on H<sub>2</sub>S detectors.
  - Proper location and working order of H<sub>2</sub>S safety equipment.
  - Attendance of all personnel, trained or retrained, and their company.
  - Weekly drills, if held and a list of personnel participating and summary of actions.

### **OUT OF SCOPE PERSONNEL**

MRC Energy Co. policy will not require Out of Scope Personnel to be clean shaven, have processed medical questionnaires, fit testing, or have certified H<sub>2</sub>S Training.

## **SAFETY EQUIPMENT**

**All respirators will be designed, selected, used and maintained in conformance with ANSI Z88.2, American National Standard for respiratory protection.**

Personal protective equipment must be provided and used. Those who are expected to use respiratory equipment in case of an emergency will be carefully instructed in the proper use and told why the equipment is being used. Careful attention will be given to the minute details in order to avoid possible misuse of the equipment during periods of extreme stress.

Self-contained breathing apparatus provides complete respiratory and eye protection in any concentration of toxic gases and under any condition of oxygen deficiency. The wearer is independent of the surrounding atmosphere because he/she is breathing with a system admitting no outside air. It consists of a full face mask, breathing tube, pressure demand regulator, air supply cylinder, and harness. Pure breathing air from the supply cylinder flows to the mask automatically through the pressure demand regulator which reduces the pressure to a breathing level. Upon inhalation, air flows into the mask at a rate precisely regulated to the user's demand. Upon exhalation, the flow to the mask stops and the exhaled breath passes through a valve in the face piece to the surrounding atmosphere. The apparatus includes an alarm & gauge which warns the wearer to leave the contaminated area for a new cylinder of air or cylinder refill.

The derrickman is provided with a full face piece unit attached to a 5– minute escape cylinder. He will also have his own self-contained 30-minute unit breathing apparatus located on the drilling floor. He will use the 5-minute unit to exit the derrick to the floor, donning the 30-minute unit located on the floor, if needed.

All respiratory protective equipment, when not in use, should be stored in a clean, cool, dry place, and out of direct sunlight to retard the deterioration of rubber parts. After each use, the mask assembly will be scrubbed with soap and water, rinsed thoroughly, and dried. Air cylinders can be recharged to a full condition from a cascade system.

Personnel in each crew will be trained in the proper techniques of bottle filling.

The primary piece of equipment to be utilized, should anyone be overcome by hydrogen sulfide, is the oxygen resuscitator, if on location.

When asphyxiation occurs, the victim must be moved to fresh air and immediately given artificial respiration. In order to assure readiness, the bottles of oxygen will be checked at regular intervals and an extra tank kept on hand.

Hand-operated pump-type detectors incorporating detector tubes will give more accurate readings of hydrogen sulfide. The pump-type draws air to be tested through the detector

tube containing lead acetate-silica gel granules. Presence of hydrogen sulfide in the air sample is shown by the development of a dark brown stain on the granules, which is the scale reading of the concentration of hydrogen sulfide. By changing the type of detector tube used, this detector may also be used for sulfur dioxide (SO<sub>2</sub>) detection when hydrogen sulfide (H<sub>2</sub>S) is being burned in the flare area.

Provisions must be made for the storage of all safety equipment as is evident from the foregoing discussion. All equipment must be stored in an available location so that anyone engaged in normal work situations is no more than “one breath away” from a mask.

**V – TOXICITY OF VARIOUS GASES**

<b>Lethal Common Name ppm<sup>4</sup></b>	<b>Chemical Formula</b>	<b>Specific Gravity<sup>1</sup></b>	<b>PEL (OSHA)<sup>2</sup></b>	<b>STEL<sup>3</sup></b>
Hydrogen Cyanide 300	HCN	0.94	10	150
Hydrogen Sulfide 600	H <sub>2</sub> S	1.18	20	Peak- 50ppm
Note: The ACGIH(7) recommends a TWA(6) value of 10ppm as the TLV(5) for H <sub>2</sub> S and an STEL of 15ppm.				
Sulfur Dioxide 1000	SO <sub>2</sub>	2.21	2	5 ppm
Chlorine	CL <sub>2</sub>	2.45	1	
Carbon Monoxide 1000	CO	0.97	35	200/1 Hour
Carbon Dioxide 10%	CO <sub>2</sub>	1.52	5000	5%
Methane	CH <sub>4</sub>	0.55	90000	

<sup>1</sup> **Air = 1.0**

<sup>2</sup> **Permissible** - Concentration at which is believed that all workers may repeatedly be exposed, day after day, without adverse effect.

<sup>3</sup> **STEL** - Short Term Exposure Limit. A 15-minute time weighted average.

<sup>4</sup> **Lethal** - Concentration that will cause death with short-term exposure.

**TLV** – Threshold Limit Value; a concentration recommended by the American Conference of Governmental Industrial Hygienists (ACGIH)

**TWA** – Time Weighted Average; the average concentration of contaminant one can be exposed to over a given eight-hour period.

**ACGIH** – (American Conference of Governmental Industrial Hygienists) is an organization comprised of Occupational Health Professionals believed

by many to be the top experts in the field of Industrial Hygiene. They are recognized as an expert resource by OSHA. The ACGIH releases a bi-annual publication "Threshold Limit Values and Biological Indices" that many safety professionals consider to be the authoritative document on airborne contaminants.

Reference: API RP-49, September 1974 - Reissued August 1978

## **VI. PROPERTIES OF GASES**

### **A. CARBON DIOXIDE**

1. Carbon Dioxide (CO<sub>2</sub>) is usually considered inert and is commonly used to extinguish fires. It is 1.52 times heavier than air and will concentrate in low areas of still air. Humans cannot breathe air containing more than 10% CO<sub>2</sub> without losing conscience or becoming disorientation in a few minutes. Continued exposure to CO<sub>2</sub> after being affected will cause convulsions, coma, and respiratory failure.
2. The threshold limit of CO<sub>2</sub> is 5000 ppm. Short-term exposure to 50,000 ppm (5%) is reasonable. This gas is colorless, odorless, and can be tolerated in relatively high concentrations.

### **B. HYDROGEN SULFIDE**

1. Hydrogen Sulfide (H<sub>2</sub>S) is a colorless, transparent, flammable gas. It is heavier than air and, hence, may accumulate in low places.
2. Although the slightest presence of H<sub>2</sub>S in the air is normally detectable by its characteristic "rotten egg" odor, it is dangerous to rely on the odor as a means of detecting excessive concentrations because the sense of smell is rapidly lost, allowing lethal concentrations to be accumulated without warning. The following table indicates the poisonous nature of H<sub>2</sub>S.

CONCENTRATION			EFFECTS
% H <sub>2</sub> S	PPM	GR/100 SCF <sup>1</sup>	
0.001	10	.65	Safe for 8 hours without respirator. Obvious and unpleasant odor.
0.0015	15	0.975	Safe for 15 minutes of exposure without respirator.
0.01	100	6.48	Kills smell in 3-15 minutes; may sting eyes and throat.
0.02	200	12.96	Kills smell quickly; stings eyes and throat.
0.05	500	32.96	Dizziness; breathing ceases in a few minutes; need prompt artificial respiration.
0.07	700	45.92	Rapid Unconsciousness; death will result if not rescued promptly.
0.1	1000	64.80	Instant unconsciousness, followed by death within



			minutes.
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<sup>1</sup> Grains per 100 Cubic Feet

## VII. Treatment Procedures for Hydrogen Sulfide Poisoning

- A. Remove the victim to fresh air.
- B. If breathing has ceased or is labored, begin resuscitation immediately.  
Note: This is the quickest and preferred method of clearing victim's lungs of contaminated air; however, under disaster conditions, it may not be practical to move the victim to fresh air. In such instances, where those rendering first aid must continue to wear masks, a resuscitator should be used.
- C. Apply resuscitator to help purge H<sub>2</sub>S from the blood stream.
- D. Keep the victim at rest and prevent chilling.
- E. Get victim under physician's care as soon as possible.

### C. SULPHUR DIOXIDE

1. Sulfur Dioxide (SO<sub>2</sub>) is a colorless, non-flammable, transparent gas.
2. SO<sub>2</sub> is produced during the burning of H<sub>2</sub>S. Although SO<sub>2</sub> is heavier than air, it can be picked up by a breeze and carried downwind at elevated temperatures. Since SO<sub>2</sub> is extremely irritating to the eyes and mucous membranes of the upper respiratory tract, it has exceptionally good warning powers in this respect. The following table indicates the toxic nature of SO<sub>2</sub>:

CONCENTRATION		EFFECTS
% SO <sub>2</sub>	PPM	
0.0005	3 to 5	Pungent odor, normally a person can detect SO <sub>2</sub> in this range.
0.0012	12	Throat irritation, coughing, constriction of the chest, tearing and smarting of eyes.
0.015	150	So irritating that it can only be endured for a few minutes.
.05	500	Causes a sense of suffocation, event with the first

		breath.
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## VIII. BREATHING AIR EQUIPMENT DRILLS FOR ON & OFF DUTY PERSONNEL

**An H<sub>2</sub>S Drill and Training Session must be given once a week to ALL on-duty personnel with off duty personnel. On-duty and Off-duty personnel will reverse roles on alternate drills.**

**An H<sub>2</sub>S drill and training session must be given once a week to all off-duty personnel in coincidence with on-duty personnel reversing roles on alternate drills.**

The purpose of this drill is to instruct the crews in the operation and use of breathing air and H<sub>2</sub>S related emergency equipment and to allow the personnel to become acquainted with using the equipment under working conditions. The crews should be trained to put on the breathing air equipment within one minute when required or requested to do so.

The following procedure should be used for weekly drills. The MRC supervisor must be satisfied that the crews are proficient with the equipment.

1. All personnel should be informed that a drill will be held.
2. The Total H<sub>2</sub>S Safety Technician or a designee assigned by the MRC Drilling Foreman should initiate the drill by signaling as he/she would if H<sub>2</sub>S was detected.
3. Personnel should don their breathing apparatus.
4. Once the breathing air equipment is on, the H<sub>2</sub>S Technician should check all personnel to insure proper operation.

A training and information session will be conducted after each drill to answer any H<sub>2</sub>S related questions and to cover any gaps identified from one of the following topics:

- Condition II, and III alerts and steps to be taken by all personnel.
- The importance of wind direction when dealing with H<sub>2</sub>S.
- Proper use and storage of all types of breathing equipment.
- Proper use and storage of oxygen resuscitators.
- Proper use and storage of H<sub>2</sub>S detectors (Mini Checks or equivalent).
- The "buddy system" and the procedure for rescuing a person overcome by H<sub>2</sub>S.
- Responsibilities and duties.
- Location of H<sub>2</sub>S safety equipment.
- Other parts of the "H<sub>2</sub>S Contingency Plan" that should be reviewed.

NOTE: A record of attendance must be kept for weekly drills and training sessions.

## **IX. HYDROGEN SULFIDE TRAINING CURRICULUM**

(FOR EMPLOYERS, VISITORS, AND CONTRACTORS)

EACH PERSON WILL BE INFORMED ON THE RESTRICTIONS OF HAVING BEARDS AND CONTACT LENS. THEY WILL ALSO BE INFORMED OF THE AVAILABILITY OF SPECTACLE KITS.

AFTER THE H2S EQUIPMENT IS RIGGED UP, ALL IN SCOPE PERSONNEL WILL BE H2S TRAINED AND PUT THROUGH A DRILL. ANY DEFICIENCIES WILL BE CORRECTED.

**Training Completion cards are good for one year and will indicate date of completion or expiration. Personnel previously trained on another facility and visiting, must attend a "supplemental briefing" on H2S equipment and procedures before beginning duty. Visitors who remain on the location more than 24 hours must receive full H2S training given all crew members. A "supplemental briefing" will include but not be limited to: Location of respirators, familiarization with safe briefing areas, alarms with instruction on responsibilities in the event of a release and hazards of H2S and (SO2, if applicable). A training and drill log will be kept.**

Topics for full H2S training shall include the following equipment if on location, but not be limited to the following:

1. **Brief Introduction on H2S**
  - A. Slide or Computer presentation (If Available)
  - B. H2S material will be distributed
  - C. Re-emphasize the properties, toxicity, and hazards of H2S
  - D. Source of SO2 (if applicable)
2. **H2S Detection**
  - A. Description of H2S sensors
  - B. Description of warning system (how it works & it's location)
  - C. Actual location of H2S sensors
  - D. Instruction on use of pump type detector (Gastec)
  - E. Use of card detectors, ampoules, or dosimeters
  - F. Use of combustible gas detector
  - G. Other personnel detectors used
  - H. Alarm conditions I & II,
  - I. SO2 alarms (if applicable)

3. **H2S Protection**
  - A. Types of breathing apparatus provided (30-minute SCBA & 5-minute SCBA (with voice diaphragms for communication if supplied)
  - B. Principle of how breathing apparatus works
  - C. Demonstration on how to use breathing apparatus
  - D. Location of breathing apparatus
4. **Cascade System**
  - A. Description of cascade system
  - B. How system works
  - C. Cascade location of rig with reference to briefing areas
  - D. How to use cascade system (with 5-minute hose work line units & refill, if supplied)
  - E. Importance of wind direction and actual location of Windssocks
  - F. Purpose of compressor/function (if one is on site)
5. **H2S Rescue and First Aid**
  - A. Importance of wind direction
  - B. Safe briefing area
  - C. Buddy system
  - D. H2S symptoms
  - E. Methods of rescue
6. **Hands on Training**
  - A. Donning/familiarization of SCBA 30-minute unit
  - B. Donning/familiarization of SKADA 5- MIN. Packs
  - C. Familiarization of cascades
  - D. Use of O2 resuscitator
  - E. Alarm conditions - upwind briefing areas, etc...
  - F. Duties and responsibilities of all personnel
  - G. Procedures for evacuation
  - H. Search and Rescue teams
7. **Certification**
  - A. Testing on material covered

**TOTAL SAFETY US INC., FIT TEST**

*X. EMPLOYEE INFORMATION*

Employee Name: \_\_\_\_\_ Date: \_\_\_\_\_

Date of Employee Medical Evaluation: \_\_\_\_\_

Medical Status (circle):      Unrestricted      Limitations on Use      Use Not Authorized

RESPIRATOR INFORMATION

Respirator Type (Dustmask, SCBA, etc): \_\_\_\_\_

Brand: \_\_\_\_\_

Size: (circle):      XS      S      M      L      XL

FIT TEST INFORMATION

Type of Fit Test Performed:

**Quantitative**

Porta Count  
Fittestest 3000

Fit Factor: \_\_\_\_\_  
Fit Factor: \_\_\_\_\_

**Qualitative**

Irritant Smoke  
Isoamyl Acetate (Banana Oil)  
Saccharin  
Bitrex

Passed / Failed  
Passed / Failed  
Passed / Failed  
Passed / Failed

I hereby certify that this fittestest was conducted in accordance with the OSHA Fit Testing Protocols found in Appendix A of 1910.134.

Fit Tester Name (Print): \_\_\_\_\_

Signature: \_\_\_\_\_ Date: \_\_\_\_\_

## **XI. H<sub>2</sub>S SAFETY SERVICES**

HYDROGEN SULFIDE SAFETY PACKAGE – Contained on location in Total Safety H<sub>2</sub>S Equipment Trailer, unless otherwise noted:

### **RESPIRATORY SAFETY SYSTEMS**

#### **QTY DESCRIPTION**

- 12 30-Minute Pressure Demand SCBA  
(4-Primary Safe Briefing Area, 4-Secondary Safe Briefing Area, 4-floor with one of these for derrick man)
- 9 Hose Line 5-minute Work Unit w/Escapes Cylinder (1 in derrick, 6 on drill floor, 1 in mud pit wt area, 1 in shaker area)

The following shall be part of the package if requested by the MRC Foremen (at least one trailer with cascade system is required to be located in the MRC Magnolia asset for use as needed)

- 1 Breathing air cascade of 10 bottles w/regulator
- 2 Refill lines to refill 30-minute units on location
- 1 6-Man manifold that can be rigged up to work area on floor, if needed
- 6 25 foot hose lines
- 2 50 foot hose lines
- 100 Feet of hose line to rig cascade up to 12 man manifold on floor
- 12 30-minute Self Contained Breathing apparatus

### **DETECTION AND ALARM SAFETY SYSTEM**

- 1 H<sub>2</sub>S Fixed Monitor w/8Channels (Loc determined at rig up) suggested.  
(Mud pit area, shaker area, bell nipple area, floor/driller area, & outside quarters)
- 5 H<sub>2</sub>S Sensors
- 3 Explosion Proof Alarms (Light and Siren)  
(1 on floor, 1 in work area, 1 in trailer area where quarters are located)
- 2 Personal H<sub>2</sub>S monitors
- 1 Portable Tri-Gas Hand Held Meter (O<sub>2</sub>, LEL, H<sub>2</sub>S)
- 1 Sensidyne/Gastech Manual Pump Type Detector
- 8 Boxes H<sub>2</sub>S Tubes Various Ranges
- 2 Boxes SO<sub>2</sub> Tubes Various Ranges
- 1 Calibration Gas
- 1 Set Paper Work for Records: Training, Cal, Inspection, other

**ADDITIONAL SAFETY RELATED EQUIPMENT**

**QTY DESCRIPTION**

2	Windssocks with Pole and Bracket
1	Set Well Condition Sign w/Green, Yellow, Red Flags
1	Primary Safe Briefing Area Sign
1	Secondary Safe Briefing Area Sign
6	Operating Condition Signs for Work Areas & Living Quarters

**TRAILER WITH BREATHING AIR CASCADE WILL  
ALSO INCLUDE THE FOLLOWING:**

This equipment will be part of the H2S equipment stored in the trailer, when on location

1	First aid kit
1	Fire Blanket
1	Eye wash station
2	Safety Harness w/150' safety line

## **XII. EMERGENCY PHONE NUMBERS (Updated March 18, 2009)**

### **EMERGENCY PHONE NUMBERS**

MRC Energy Co. Emergency Phone #

MRC Energy Co. Permian Operations Phone-----

**MRC Energy Co. Production**

113 Daw Rd

Mansfield LA 71052

<b>Title</b>	<b>Names</b>	<b>Phone</b>	<b>Cell</b>
Operations Manager			
Operation Supt.			
Operations Supervisor			
Operations Supervisor			
Office Supervisor			
HSE			
Scheduler Planner			

### **Hydrogen Sulfide Safety Consultants**

Total Safety W. Bender Blvd. Hobbs, NM	575-392-2973	After Hours 24 Hour Call Center Through Office Number
Tommy Throckmorton Operations Manager	575-392-2973	940-268-9614
Rodney Jourdan Sales Contact	575-392-2973	432-349-3928



**MRC Energy Co. MEDICAL RESPONSE PLAN AND IT'S MEDICAL PROTOCOLS WILL BE FOLLOWED**

**MEDICAL COORDINATOR # -----**

[Emergency Numbers & Directions](#)

**Hospitals (911)**

<b>Artesia General Hospital 702 N. 13<sup>th</sup> St. Artesia, NM 88210</b>	<b>Main Phone Number</b>	<b>575-748-3333</b>
<b>Nor-Lea General Hospital 1600 N. Main Ave. Lovington, NM 88260</b>	<b>Main Phone Number</b>	<b>575-396-6611</b>
<b>Lea Regional Medical Center 5419 N. Lovington Hwy Hobbs, NM 88240</b>	<b>Main Phone Number</b>	<b>575-492-5260</b>
<b>Carlsbad General Hospital 2430 W. Pierce St. Carlsbad, NM</b>	<b>Main Phone Number</b>	<b>575-887-4100</b>
<b>Lovelace Regional Hospital 117 E. 19<sup>th</sup> St Roswell, NM 88201</b>	<b>Main Phone Number</b>	<b>575-627-7000</b>
<b>Winkler Co. Memorial Hospital 821 Jeffee Dr. Kermit, Texas 79745</b>	<b>Main Phone Number</b>	<b>432-586-8299</b>
<b>Reeves County Hospital 2323 Texas St. Pecos, Texas 79772</b>	<b>Main Phone Number</b>	<b>432-447-3551</b>

**State Police (911)**

<b>Texas DPS Loving co. 225 N.Pecos Mentone, Texas 79754</b>	<b>Office Number</b>	<b>432-377-2411</b>
<b>Texas DPS Winkler Co. 100 E Winkler Kermit, Texas 79745</b>	<b>Office Number</b>	<b>432-586-3465</b>
<b>Texas DPS Pecos Co. 148 N I-20 Frontage RD Pecos, Texas 79772</b>	<b>Office Number</b>	<b>432-447-3532</b>
<b>New Mexico State Police 3300 W. Main St Artesia, NM</b>	<b>Office Number</b>	<b>575-748-9718</b>
<b>New Mexico State Police 304 N. Canyon St Carlsbad, NM 88220</b>	<b>Office Number</b>	<b>575-885-3137</b>
<b>New Mexico State Police 5100 Jack Gomez Blvd. Hobbs, NM 88240</b>	<b>Office Number</b>	<b>575-392-5588</b>

**Local Law Enforcement (911) (Sheriff)**

<b>Reeves Co. Sheriff 500 N. Oak ST Pecos, Texas 79722</b>	<b>Office Number</b>	<b>432-445-4901</b>
<b>Winkler Co. Sheriff 1300 Bellaire St. Kermit, Texas 79745</b>	<b>Office Number</b>	<b>432-586-3461</b>
<b>Loving Co. Sheriff Courthouse Mentone, Texas</b>	<b>Office Number</b>	<b>432-377-2411</b>

<b>Lea Co. Sheriff 1417 S. Commercial St. Lovington, NM 88260</b>	<b>Office Number</b>	
<b>Eddy Co. Sheriff 305 N 7th St. Artesia, NM 88210</b>	<b>Office Number</b>	<b>575-766-9888</b>
<b>Eddy Co. Sheriff 305 N 7th St. Carlsbad, NM 88220</b>	<b>Office Number</b>	<b>575-746-9888</b>

## Federal &amp; State Agencies

<b>OSHA Lubbock Area Office 1205 Texas Av. Room 806 Lubbock, Texas 79401</b>	<b>Main Number</b>	<b>806-472-7681 EXT 7685</b>
<b>New Mexico Environment Department 400 N Pennsylvania Roswell, NM 88201</b>	<b>Joe Fresquez</b>	<b>575-623-3935</b>
<b>Texas Railroad Commission Midland, Texas</b>	<b>Main Number</b>	<b>844-773-0305</b>
<b>BLM Carlsbad, NM Field Office 620 E. Green ST Carlsbad, NM 88220</b>	<b>Main Number</b>	<b>575-234-5972</b>
<b>BLM Hobbs Field Station 414 W. Taylor Rd. Hobbs, NM 88240</b>	<b>Main Number</b>	<b>575-393-3612</b>
<b>BLM Roswell District Office 2909 W. Second St. Roswell, NM 88201</b>	<b>Main Number</b>	<b>575-627-0272</b>

<b>TECQ Texas Commission on Environmental Quality</b>	<b>Main Number</b>	<b>800-832-8224</b>
<b>New Mexico OCD</b>		
<b>U.S. Environmental Protection Agency Region 6 Texas/New Mexico</b>	<b>Main Number</b>	<b>214-655-2222</b>
<b>National Response Center Toxic Chemicals &amp; Oil Spills</b>	<b>Main Number</b>	<b>800-424-8802</b>

**Rig Company**


**XIII. EVACUATION OF THE GENERAL PUBLIC**

The procedure to be used in alerting nearby persons in the event of any occurrence that could pose a threat to life or property will be arranged and completed with public officials in detail, prior to drilling into the hydrogen sulfide formations.

In the event of an actual emergency, the following steps will be immediately taken:

1. The MRC Energy Co.'s representative will dispatch sufficient personnel to immediately warn each resident and transients down-wind within radius of exposure from the well site. Then warn all residence in the radius of exposure. Additional evacuation zones may be necessary as the situation warrants.
2. The MRC Energy Co.'s representative will immediately notify proper authorities, including the Sheriff's Office, Highway Patrol, and any other public officials as described above and will enlist their assistance in warning residents and transients in the calculated radius of exposure.
3. The MRC Energy Co.'s representative will dispatch sufficient personnel to divert traffic in the vicinity away from the potentially dangerous area. A

guard to the entrance of the well site will be posted to monitor essential and non essential traffic.

4. General:

- A. The area included within the radius of exposure is considered to be the zone of maximum potential hazard from a hydrogen sulfide gas escape. Immediate evacuation of public areas, in accordance with the provisions of this contingency plan, is imperative. When it is determined that conditions exist which create an additional area (beyond the initial zone of maximum potential hazard) vulnerable to possible hazard, public areas in the additional hazardous area will be evacuated in accordance with the contingency plan.
- B. In the event of a disaster, after the public areas have been evacuated and traffic stopped, it is expected that local civil authorities will have arrived and within a few hours will have assumed direction of and control of the public, including all public areas. MRC Energy Co. will cooperate with these authorities to the fullest extent and will exert every effort by careful advice to such authorities to prevent panic or rumors.
- C. MRC Energy Co. will dispatch appropriate management personnel at the disaster site as soon as possible. The company's personnel will cooperate with and provide such information to civil authorities as they might require.
- D. One of the products of the combustion of hydrogen sulfide is sulfur dioxide (SO<sub>2</sub>). Under certain conditions this gas may be equally as dangerous as H<sub>2</sub>S. A pump type detector device, which determines the percent of SO<sub>2</sub> in air through concentrations in ppm, will be available. Although normal air movement is sufficient to dissipate this material to safe levels, the SO<sub>2</sub> detector should be utilized to check concentrations in the proximity of the well once every hour, or as necessary and the situation warrants. Also, if any low areas are suspected of having high concentrations, personnel should be made aware of these areas, and steps should be taken to determine whether or not these low areas are hazardous.



# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

<b>Project</b>	Lea County, NM		
<b>Map System:</b>	US State Plane 1927 (Exact solution)	<b>System Datum:</b>	Mean Sea Level
<b>Geo Datum:</b>	NAD 1927 (NADCON CONUS)		
<b>Map Zone:</b>	New Mexico East 3001		

Site		Uncle Ches 2116 Fed				
Site Position:		Northing:	565,604.00 usft	Latitude:	32.551980	
From:	Map	Easting:	766,403.00 usft	Longitude:	-103.468749	
Position Uncertainty:		0.00 usft	Slot Radius:	13-3/16 "	Grid Convergence:	0.47 °

Well	#232H					
Well Position	+N/-S	0.00 usft	Northing:	565,616.00 usft	Latitude:	32.551984
	+E/-W	0.00 usft	Easting:	767,694.00 usft	Longitude:	-103.464559
Position Uncertainty		0.00 usft	Wellhead Elevation:	usft	Ground Level:	3,717.00 usft

<b>Wellbore</b>	OH				
<b>Magnetics</b>	<b>Model Name</b>	<b>Sample Date</b>	<b>Declination (°)</b>	<b>Dip Angle (°)</b>	<b>Field Strength (nT)</b>
	HDGM	7/12/2018	6.65	60.48	48,146.50

<b>Design</b>	Prelim A				
<b>Audit Notes:</b>					
<b>Version:</b>	<b>Phase:</b>	PLAN	<b>Tie On Depth:</b>	0.00	
<b>Vertical Section:</b>	<b>Depth From (TVD) (usft)</b>	<b>+N/-S (usft)</b>	<b>+E/-W (usft)</b>	<b>Direction (°)</b>	
	0.00	0.00	0.00	359.52	

<b>Survey Tool Program</b>	<b>Date</b>	7/12/2018			
<b>From (usft)</b>	<b>To (usft)</b>	<b>Survey (Wellbore)</b>	<b>Tool Name</b>	<b>Description</b>	
0.00	22,324.69	Prelim A (OH)	MWD+HDGM	OWSG MWD + HRGM	

<b>Planned Survey</b>										
<b>Measured Depth (usft)</b>	<b>Inclination (°)</b>	<b>Azimuth (°)</b>	<b>Vertical Depth (usft)</b>	<b>+N/-S (usft)</b>	<b>+E/-W (usft)</b>	<b>Vertical Section (usft)</b>	<b>Dogleg Rate (°/100usft)</b>	<b>Build Rate (°/100usft)</b>	<b>Turn Rate (°/100usft)</b>	
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00	
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00	
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00	
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00	
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00	
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00	
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00	
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00	



# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

## Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	1.00	114.30	1,099.99	-0.36	0.80	-0.37	1.00	1.00	0.00
1,200.00	2.00	114.30	1,199.96	-1.44	3.18	-1.46	1.00	1.00	0.00
1,300.00	3.00	114.30	1,299.86	-3.23	7.16	-3.29	1.00	1.00	0.00
1,400.00	4.00	114.30	1,399.68	-5.74	12.72	-5.85	1.00	1.00	0.00
1,499.94	5.00	114.30	1,499.31	-8.97	19.87	-9.14	1.00	1.00	0.00
1,600.00	5.00	114.30	1,598.99	-12.56	27.81	-12.79	0.00	0.00	0.00
1,700.00	5.00	114.30	1,698.60	-16.15	35.76	-16.45	0.00	0.00	0.00
1,800.00	5.00	114.30	1,798.22	-19.73	43.70	-20.10	0.00	0.00	0.00
1,900.00	5.00	114.30	1,897.84	-23.32	51.64	-23.75	0.00	0.00	0.00
2,000.00	5.00	114.30	1,997.46	-26.91	59.58	-27.40	0.00	0.00	0.00
2,100.00	5.00	114.30	2,097.08	-30.49	67.52	-31.06	0.00	0.00	0.00
2,200.00	5.00	114.30	2,196.70	-34.08	75.47	-34.71	0.00	0.00	0.00
2,300.00	5.00	114.30	2,296.32	-37.67	83.41	-38.36	0.00	0.00	0.00
2,400.00	5.00	114.30	2,395.94	-41.25	91.35	-42.02	0.00	0.00	0.00
2,500.00	5.00	114.30	2,495.56	-44.84	99.29	-45.67	0.00	0.00	0.00
2,600.00	5.00	114.30	2,595.18	-48.43	107.24	-49.32	0.00	0.00	0.00
2,700.00	5.00	114.30	2,694.80	-52.01	115.18	-52.98	0.00	0.00	0.00
2,800.00	5.00	114.30	2,794.42	-55.60	123.12	-56.63	0.00	0.00	0.00
2,900.00	5.00	114.30	2,894.04	-59.19	131.06	-60.28	0.00	0.00	0.00
3,000.00	5.00	114.30	2,993.66	-62.77	139.01	-63.93	0.00	0.00	0.00
3,100.00	5.00	114.30	3,093.28	-66.36	146.95	-67.59	0.00	0.00	0.00
3,200.00	5.00	114.30	3,192.90	-69.95	154.89	-71.24	0.00	0.00	0.00
3,300.00	5.00	114.30	3,292.52	-73.53	162.83	-74.89	0.00	0.00	0.00
3,400.00	5.00	114.30	3,392.14	-77.12	170.77	-78.55	0.00	0.00	0.00
3,500.00	5.00	114.30	3,491.76	-80.70	178.72	-82.20	0.00	0.00	0.00
3,600.00	5.00	114.30	3,591.38	-84.29	186.66	-85.85	0.00	0.00	0.00
3,700.00	5.00	114.30	3,691.00	-87.88	194.60	-89.51	0.00	0.00	0.00
3,800.00	5.00	114.30	3,790.62	-91.46	202.54	-93.16	0.00	0.00	0.00
3,900.00	5.00	114.30	3,890.24	-95.05	210.49	-96.81	0.00	0.00	0.00
4,000.00	5.00	114.30	3,989.85	-98.64	218.43	-100.46	0.00	0.00	0.00
4,100.00	5.00	114.30	4,089.47	-102.22	226.37	-104.12	0.00	0.00	0.00
4,200.00	5.00	114.30	4,189.09	-105.81	234.31	-107.77	0.00	0.00	0.00
4,300.00	5.00	114.30	4,288.71	-109.40	242.25	-111.42	0.00	0.00	0.00
4,400.00	5.00	114.30	4,388.33	-112.98	250.20	-115.08	0.00	0.00	0.00
4,500.00	5.00	114.30	4,487.95	-116.57	258.14	-118.73	0.00	0.00	0.00
4,600.00	5.00	114.30	4,587.57	-120.16	266.08	-122.38	0.00	0.00	0.00
4,700.00	5.00	114.30	4,687.19	-123.74	274.02	-126.04	0.00	0.00	0.00
4,800.00	5.00	114.30	4,786.81	-127.33	281.97	-129.69	0.00	0.00	0.00
4,900.00	5.00	114.30	4,886.43	-130.92	289.91	-133.34	0.00	0.00	0.00
5,000.00	5.00	114.30	4,986.05	-134.50	297.85	-136.99	0.00	0.00	0.00



# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

## Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,100.00	5.00	114.30	5,085.67	-138.09	305.79	-140.65	0.00	0.00	0.00
5,200.00	5.00	114.30	5,185.29	-141.68	313.74	-144.30	0.00	0.00	0.00
5,300.00	5.00	114.30	5,284.91	-145.26	321.68	-147.95	0.00	0.00	0.00
5,400.00	5.00	114.30	5,384.53	-148.85	329.62	-151.61	0.00	0.00	0.00
5,500.00	5.00	114.30	5,484.15	-152.44	337.56	-155.26	0.00	0.00	0.00
5,600.00	5.00	114.30	5,583.77	-156.02	345.50	-158.91	0.00	0.00	0.00
5,700.00	5.00	114.30	5,683.39	-159.61	353.45	-162.57	0.00	0.00	0.00
5,800.00	5.00	114.30	5,783.01	-163.20	361.39	-166.22	0.00	0.00	0.00
5,900.00	5.00	114.30	5,882.63	-166.78	369.33	-169.87	0.00	0.00	0.00
6,000.00	5.00	114.30	5,982.25	-170.37	377.27	-173.52	0.00	0.00	0.00
6,100.00	5.00	114.30	6,081.87	-173.96	385.22	-177.18	0.00	0.00	0.00
6,200.00	5.00	114.30	6,181.48	-177.54	393.16	-180.83	0.00	0.00	0.00
6,300.00	5.00	114.30	6,281.10	-181.13	401.10	-184.48	0.00	0.00	0.00
6,400.00	5.00	114.30	6,380.72	-184.72	409.04	-188.14	0.00	0.00	0.00
6,500.00	5.00	114.30	6,480.34	-188.30	416.99	-191.79	0.00	0.00	0.00
6,600.00	5.00	114.30	6,579.96	-191.89	424.93	-195.44	0.00	0.00	0.00
6,700.00	5.00	114.30	6,679.58	-195.48	432.87	-199.10	0.00	0.00	0.00
6,739.96	5.00	114.30	6,719.39	-196.91	436.04	-200.55	0.00	0.00	0.00
6,800.00	4.40	114.30	6,779.23	-198.93	440.53	-202.62	1.00	-1.00	0.00
6,900.00	3.40	114.30	6,879.00	-201.73	446.72	-205.47	1.00	-1.00	0.00
7,000.00	2.40	114.30	6,978.87	-203.81	451.33	-207.59	1.00	-1.00	0.00
7,100.00	1.40	114.30	7,078.81	-205.18	454.35	-208.98	1.00	-1.00	0.00
7,200.00	0.40	114.30	7,178.80	-205.82	455.78	-209.63	1.00	-1.00	0.00
7,239.90	0.00	0.00	7,218.70	-205.88	455.91	-209.69	1.00	-1.00	0.00
7,300.00	0.00	0.00	7,278.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,400.00	0.00	0.00	7,378.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,500.00	0.00	0.00	7,478.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,600.00	0.00	0.00	7,578.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,700.00	0.00	0.00	7,678.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,800.00	0.00	0.00	7,778.80	-205.88	455.91	-209.69	0.00	0.00	0.00
7,900.00	0.00	0.00	7,878.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,000.00	0.00	0.00	7,978.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,100.00	0.00	0.00	8,078.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,200.00	0.00	0.00	8,178.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,300.00	0.00	0.00	8,278.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,400.00	0.00	0.00	8,378.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,500.00	0.00	0.00	8,478.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,600.00	0.00	0.00	8,578.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,700.00	0.00	0.00	8,678.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,800.00	0.00	0.00	8,778.80	-205.88	455.91	-209.69	0.00	0.00	0.00
8,900.00	0.00	0.00	8,878.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,000.00	0.00	0.00	8,978.80	-205.88	455.91	-209.69	0.00	0.00	0.00





# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

## Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,100.00	0.00	0.00	9,078.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,200.00	0.00	0.00	9,178.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,300.00	0.00	0.00	9,278.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,400.00	0.00	0.00	9,378.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,500.00	0.00	0.00	9,478.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,600.00	0.00	0.00	9,578.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,700.00	0.00	0.00	9,678.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,800.00	0.00	0.00	9,778.80	-205.88	455.91	-209.69	0.00	0.00	0.00
9,900.00	0.00	0.00	9,878.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,000.00	0.00	0.00	9,978.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,100.00	0.00	0.00	10,078.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,200.00	0.00	0.00	10,178.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,300.00	0.00	0.00	10,278.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,400.00	0.00	0.00	10,378.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,500.00	0.00	0.00	10,478.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,600.00	0.00	0.00	10,578.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,700.00	0.00	0.00	10,678.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,800.00	0.00	0.00	10,778.80	-205.88	455.91	-209.69	0.00	0.00	0.00
10,900.00	0.00	0.00	10,878.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,000.00	0.00	0.00	10,978.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,100.00	0.00	0.00	11,078.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,200.00	0.00	0.00	11,178.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,300.00	0.00	0.00	11,278.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,400.00	0.00	0.00	11,378.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,500.00	0.00	0.00	11,478.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,600.00	0.00	0.00	11,578.80	-205.88	455.91	-209.69	0.00	0.00	0.00
11,709.90	0.00	0.00	11,688.70	-205.88	455.91	-209.69	0.00	0.00	0.00
11,750.00	4.01	9.00	11,728.76	-204.49	456.13	-208.31	10.00	10.00	0.00
11,800.00	9.01	9.00	11,778.43	-198.90	457.02	-202.72	10.00	10.00	0.00
11,850.00	14.01	9.00	11,827.40	-189.05	458.58	-192.88	10.00	10.00	0.00
11,900.00	19.01	9.00	11,875.33	-175.02	460.80	-178.87	10.00	10.00	0.00
11,950.00	24.01	9.00	11,921.83	-156.92	463.67	-160.80	10.00	10.00	0.00
12,000.00	29.01	9.00	11,966.56	-134.88	467.16	-138.79	10.00	10.00	0.00
12,050.00	34.01	9.00	12,009.17	-109.08	471.24	-113.02	10.00	10.00	0.00
12,100.00	39.01	9.00	12,049.35	-79.71	475.89	-83.69	10.00	10.00	0.00
12,150.00	44.01	9.00	12,086.78	-46.99	481.08	-51.02	10.00	10.00	0.00
12,200.00	49.01	9.00	12,121.18	-11.17	486.75	-15.25	10.00	10.00	0.00
12,209.90	50.00	9.00	12,127.61	-3.73	487.93	-7.82	10.00	10.00	0.00
12,250.00	53.89	7.75	12,152.32	27.50	492.52	23.37	10.00	9.70	-3.11
12,300.00	58.75	6.36	12,180.04	68.78	497.61	64.61	10.00	9.73	-2.79
12,350.00	63.63	5.10	12,204.13	112.36	501.97	108.15	10.00	9.75	-2.51
12,400.00	68.52	3.95	12,224.41	157.90	505.57	153.66	10.00	9.78	-2.31



# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

## Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
12,450.00	73.41	2.87	12,240.71	205.07	508.37	200.80	10.00	9.79	-2.16
12,500.00	78.31	1.85	12,252.92	253.50	510.36	249.21	10.00	9.80	-2.05
12,550.00	83.22	0.86	12,260.94	302.82	511.52	298.53	10.00	9.81	-1.98
12,600.00	88.12	359.89	12,264.72	352.66	511.85	348.36	10.00	9.81	-1.94
12,619.15	90.00	359.52	12,265.03	371.81	511.75	367.51	10.00	9.81	-1.93
12,700.00	90.00	359.52	12,265.03	452.66	511.07	448.36	0.00	0.00	0.00
12,800.00	90.00	359.52	12,265.03	552.65	510.22	548.36	0.00	0.00	0.00
12,900.00	90.00	359.52	12,265.03	652.65	509.38	648.36	0.00	0.00	0.00
13,000.00	90.00	359.52	12,265.03	752.64	508.54	748.36	0.00	0.00	0.00
13,100.00	90.00	359.52	12,265.03	852.64	507.70	848.36	0.00	0.00	0.00
13,200.00	90.00	359.52	12,265.03	952.64	506.85	948.36	0.00	0.00	0.00
13,300.00	90.00	359.52	12,265.03	1,052.63	506.01	1,048.36	0.00	0.00	0.00
13,400.00	90.00	359.52	12,265.03	1,152.63	505.17	1,148.36	0.00	0.00	0.00
13,500.00	90.00	359.52	12,265.03	1,252.63	504.33	1,248.36	0.00	0.00	0.00
13,600.00	90.00	359.52	12,265.03	1,352.62	503.48	1,348.36	0.00	0.00	0.00
13,700.00	90.00	359.52	12,265.03	1,452.62	502.64	1,448.36	0.00	0.00	0.00
13,800.00	90.00	359.52	12,265.03	1,552.62	501.80	1,548.36	0.00	0.00	0.00
13,900.00	90.00	359.52	12,265.03	1,652.61	500.96	1,648.36	0.00	0.00	0.00
14,000.00	90.00	359.52	12,265.03	1,752.61	500.12	1,748.36	0.00	0.00	0.00
14,100.00	90.00	359.52	12,265.03	1,852.61	499.27	1,848.36	0.00	0.00	0.00
14,200.00	90.00	359.52	12,265.03	1,952.60	498.43	1,948.36	0.00	0.00	0.00
14,300.00	90.00	359.52	12,265.03	2,052.60	497.59	2,048.36	0.00	0.00	0.00
14,400.00	90.00	359.52	12,265.03	2,152.59	496.75	2,148.36	0.00	0.00	0.00
14,500.00	90.00	359.52	12,265.03	2,252.59	495.90	2,248.36	0.00	0.00	0.00
14,600.00	90.00	359.52	12,265.03	2,352.59	495.06	2,348.36	0.00	0.00	0.00
14,700.00	90.00	359.52	12,265.03	2,452.58	494.22	2,448.36	0.00	0.00	0.00
14,800.00	90.00	359.52	12,265.02	2,552.58	493.38	2,548.36	0.00	0.00	0.00
14,900.00	90.00	359.52	12,265.02	2,652.58	492.54	2,648.36	0.00	0.00	0.00
15,000.00	90.00	359.52	12,265.02	2,752.57	491.69	2,748.36	0.00	0.00	0.00
15,100.00	90.00	359.52	12,265.02	2,852.57	490.85	2,848.36	0.00	0.00	0.00
15,200.00	90.00	359.52	12,265.02	2,952.57	490.01	2,948.36	0.00	0.00	0.00
15,300.00	90.00	359.52	12,265.02	3,052.56	489.17	3,048.36	0.00	0.00	0.00
15,400.00	90.00	359.52	12,265.02	3,152.56	488.32	3,148.36	0.00	0.00	0.00
15,500.00	90.00	359.52	12,265.02	3,252.56	487.48	3,248.36	0.00	0.00	0.00
15,600.00	90.00	359.52	12,265.02	3,352.55	486.64	3,348.36	0.00	0.00	0.00
15,700.00	90.00	359.52	12,265.02	3,452.55	485.80	3,448.36	0.00	0.00	0.00
15,800.00	90.00	359.52	12,265.02	3,552.55	484.95	3,548.36	0.00	0.00	0.00
15,900.00	90.00	359.52	12,265.02	3,652.54	484.11	3,648.36	0.00	0.00	0.00
16,000.00	90.00	359.52	12,265.02	3,752.54	483.27	3,748.36	0.00	0.00	0.00
16,100.00	90.00	359.52	12,265.02	3,852.53	482.43	3,848.36	0.00	0.00	0.00
16,200.00	90.00	359.52	12,265.02	3,952.53	481.59	3,948.36	0.00	0.00	0.00
16,300.00	90.00	359.52	12,265.02	4,052.53	480.74	4,048.36	0.00	0.00	0.00



# Pro Directional Survey Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

## Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
16,400.00	90.00	359.52	12,265.02	4,152.52	479.90	4,148.36	0.00	0.00	0.00
16,500.00	90.00	359.52	12,265.02	4,252.52	479.06	4,248.36	0.00	0.00	0.00
16,600.00	90.00	359.52	12,265.02	4,352.52	478.22	4,348.36	0.00	0.00	0.00
16,700.00	90.00	359.52	12,265.02	4,452.51	477.37	4,448.36	0.00	0.00	0.00
16,800.00	90.00	359.52	12,265.02	4,552.51	476.53	4,548.36	0.00	0.00	0.00
16,900.00	90.00	359.52	12,265.02	4,652.51	475.69	4,648.36	0.00	0.00	0.00
17,000.00	90.00	359.52	12,265.02	4,752.50	474.85	4,748.36	0.00	0.00	0.00
17,100.00	90.00	359.52	12,265.02	4,852.50	474.01	4,848.36	0.00	0.00	0.00
17,200.00	90.00	359.52	12,265.02	4,952.50	473.16	4,948.36	0.00	0.00	0.00
17,300.00	90.00	359.52	12,265.02	5,052.49	472.32	5,048.36	0.00	0.00	0.00
17,400.00	90.00	359.52	12,265.02	5,152.49	471.48	5,148.36	0.00	0.00	0.00
17,500.00	90.00	359.52	12,265.02	5,252.48	470.64	5,248.36	0.00	0.00	0.00
17,600.00	90.00	359.52	12,265.02	5,352.48	469.79	5,348.36	0.00	0.00	0.00
17,700.00	90.00	359.52	12,265.02	5,452.48	468.95	5,448.36	0.00	0.00	0.00
17,800.00	90.00	359.52	12,265.01	5,552.47	468.11	5,548.36	0.00	0.00	0.00
17,900.00	90.00	359.52	12,265.01	5,652.47	467.27	5,648.36	0.00	0.00	0.00
18,000.00	90.00	359.52	12,265.01	5,752.47	466.43	5,748.36	0.00	0.00	0.00
18,100.00	90.00	359.52	12,265.01	5,852.46	465.58	5,848.36	0.00	0.00	0.00
18,200.00	90.00	359.52	12,265.01	5,952.46	464.74	5,948.36	0.00	0.00	0.00
18,300.00	90.00	359.52	12,265.01	6,052.46	463.90	6,048.36	0.00	0.00	0.00
18,400.00	90.00	359.52	12,265.01	6,152.45	463.06	6,148.36	0.00	0.00	0.00
18,500.00	90.00	359.52	12,265.01	6,252.45	462.21	6,248.36	0.00	0.00	0.00
18,600.00	90.00	359.52	12,265.01	6,352.45	461.37	6,348.36	0.00	0.00	0.00
18,700.00	90.00	359.52	12,265.01	6,452.44	460.53	6,448.36	0.00	0.00	0.00
18,800.00	90.00	359.52	12,265.01	6,552.44	459.69	6,548.36	0.00	0.00	0.00
18,900.00	90.00	359.52	12,265.01	6,652.44	458.84	6,648.36	0.00	0.00	0.00
19,000.00	90.00	359.52	12,265.01	6,752.43	458.00	6,748.36	0.00	0.00	0.00
19,100.00	90.00	359.52	12,265.01	6,852.43	457.16	6,848.36	0.00	0.00	0.00
19,200.00	90.00	359.52	12,265.01	6,952.42	456.32	6,948.36	0.00	0.00	0.00
19,300.00	90.00	359.52	12,265.01	7,052.42	455.48	7,048.36	0.00	0.00	0.00
19,400.00	90.00	359.52	12,265.01	7,152.42	454.63	7,148.36	0.00	0.00	0.00
19,500.00	90.00	359.52	12,265.01	7,252.41	453.79	7,248.36	0.00	0.00	0.00
19,600.00	90.00	359.52	12,265.01	7,352.41	452.95	7,348.36	0.00	0.00	0.00
19,700.00	90.00	359.52	12,265.01	7,452.41	452.11	7,448.36	0.00	0.00	0.00
19,800.00	90.00	359.52	12,265.01	7,552.40	451.26	7,548.36	0.00	0.00	0.00
19,900.00	90.00	359.52	12,265.01	7,652.40	450.42	7,648.36	0.00	0.00	0.00
20,000.00	90.00	359.52	12,265.01	7,752.40	449.58	7,748.36	0.00	0.00	0.00
20,100.00	90.00	359.52	12,265.01	7,852.39	448.74	7,848.36	0.00	0.00	0.00
20,200.00	90.00	359.52	12,265.01	7,952.39	447.90	7,948.36	0.00	0.00	0.00
20,300.00	90.00	359.52	12,265.01	8,052.39	447.05	8,048.36	0.00	0.00	0.00
20,400.00	90.00	359.52	12,265.01	8,152.38	446.21	8,148.36	0.00	0.00	0.00
20,500.00	90.00	359.52	12,265.01	8,252.38	445.37	8,248.36	0.00	0.00	0.00



# Pro Directional Survey Report



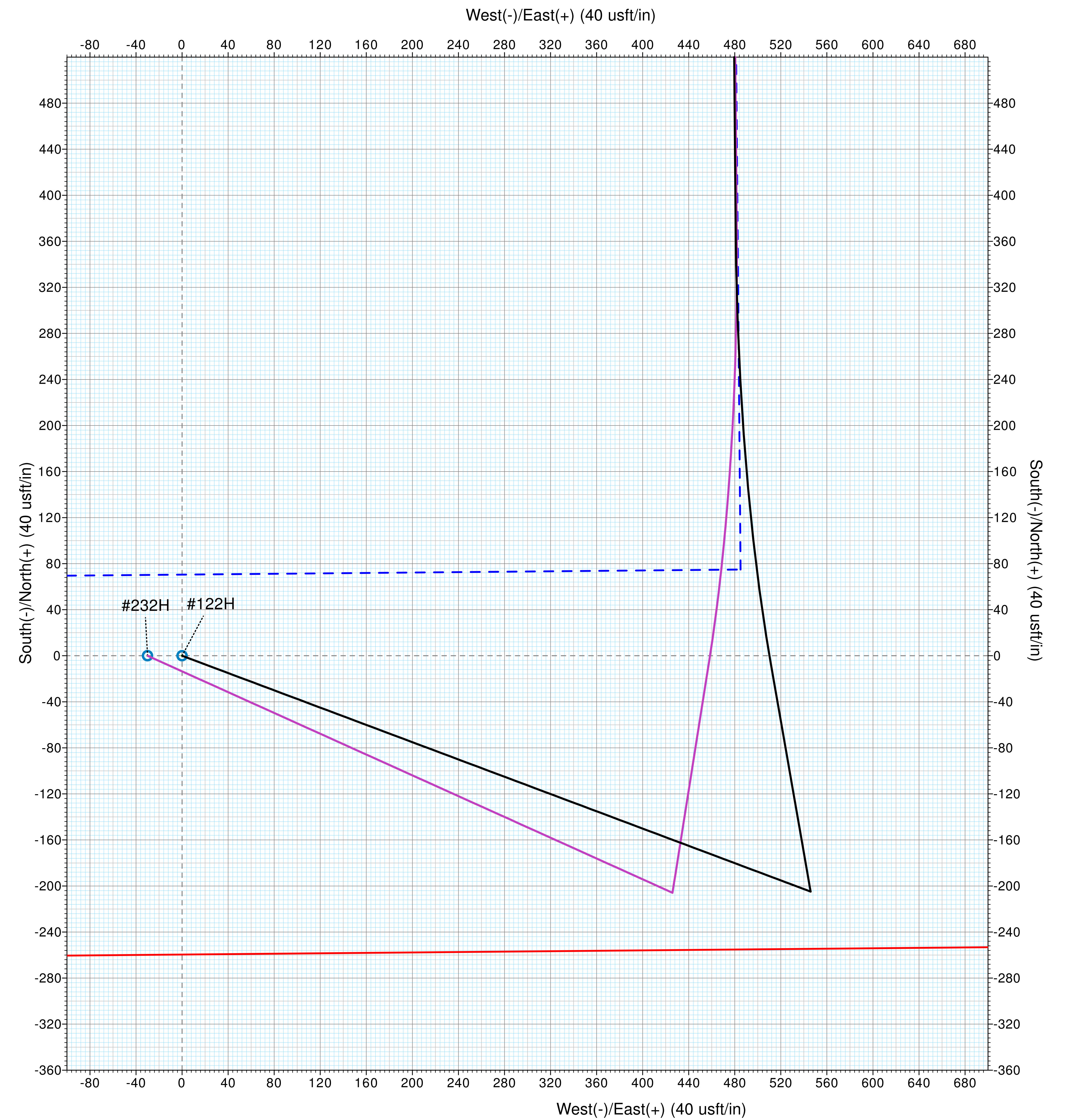
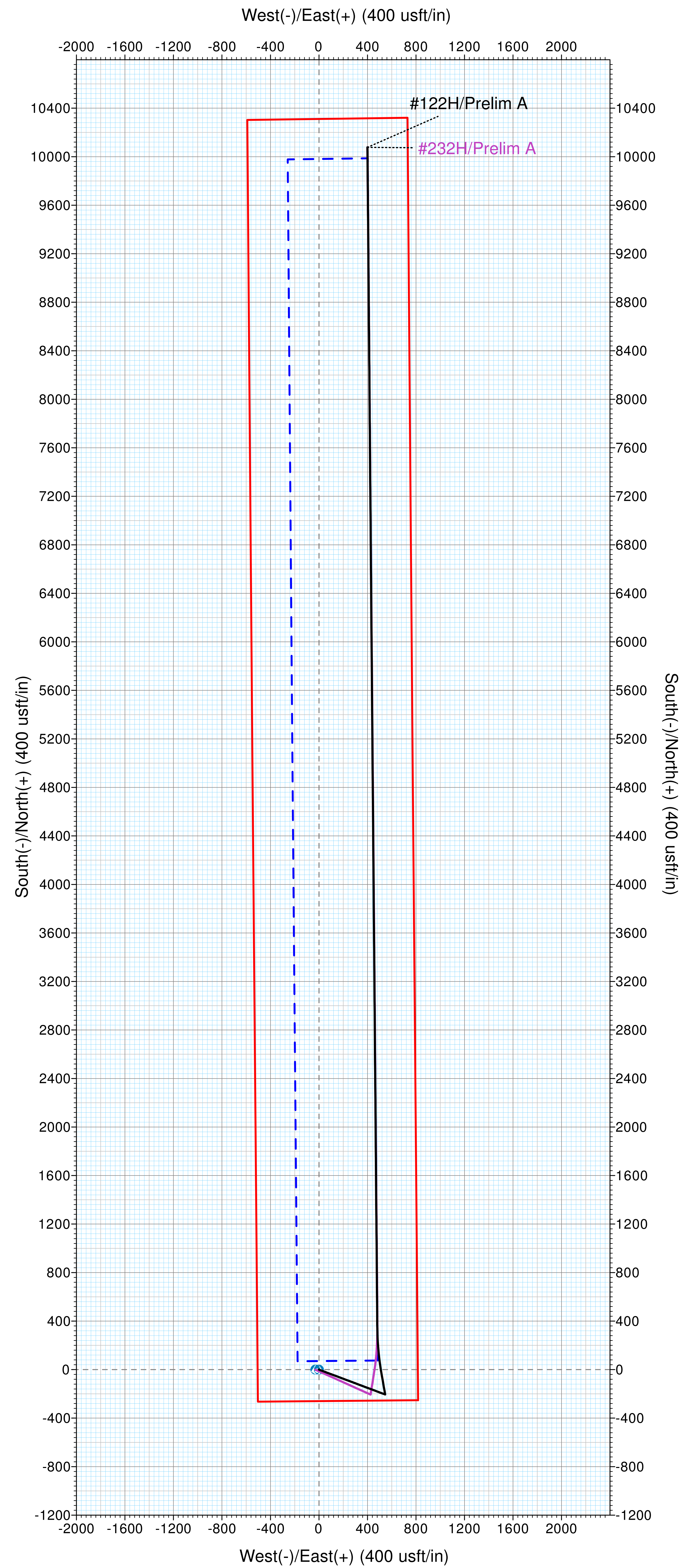
<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Well:</b>	#232H	<b>North Reference:</b>	Grid
<b>Wellbore:</b>	OH	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Design:</b>	Prelim A	<b>Database:</b>	WellPlanner1

Planned Survey										
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	
20,600.00	90.00	359.52	12,265.01	8,352.38	444.53	8,348.36	0.00	0.00	0.00	
20,700.00	90.00	359.52	12,265.01	8,452.37	443.68	8,448.36	0.00	0.00	0.00	
20,800.00	90.00	359.52	12,265.01	8,552.37	442.84	8,548.36	0.00	0.00	0.00	
20,900.00	90.00	359.52	12,265.00	8,652.36	442.00	8,648.36	0.00	0.00	0.00	
21,000.00	90.00	359.52	12,265.00	8,752.36	441.16	8,748.36	0.00	0.00	0.00	
21,100.00	90.00	359.52	12,265.00	8,852.36	440.32	8,848.36	0.00	0.00	0.00	
21,200.00	90.00	359.52	12,265.00	8,952.35	439.47	8,948.36	0.00	0.00	0.00	
21,300.00	90.00	359.52	12,265.00	9,052.35	438.63	9,048.36	0.00	0.00	0.00	
21,400.00	90.00	359.52	12,265.00	9,152.35	437.79	9,148.36	0.00	0.00	0.00	
21,500.00	90.00	359.52	12,265.00	9,252.34	436.95	9,248.36	0.00	0.00	0.00	
21,600.00	90.00	359.52	12,265.00	9,352.34	436.10	9,348.36	0.00	0.00	0.00	
21,700.00	90.00	359.52	12,265.00	9,452.34	435.26	9,448.36	0.00	0.00	0.00	
21,800.00	90.00	359.52	12,265.00	9,552.33	434.42	9,548.36	0.00	0.00	0.00	
21,900.00	90.00	359.52	12,265.00	9,652.33	433.58	9,648.36	0.00	0.00	0.00	
22,000.00	90.00	359.52	12,265.00	9,752.33	432.73	9,748.36	0.00	0.00	0.00	
22,100.00	90.00	359.52	12,265.00	9,852.32	431.89	9,848.36	0.00	0.00	0.00	
22,200.00	90.00	359.52	12,265.00	9,952.32	431.05	9,948.36	0.00	0.00	0.00	
22,300.00	90.00	359.52	12,265.00	10,052.31	430.21	10,048.36	0.00	0.00	0.00	
22,324.69	90.00	359.52	12,265.00	10,077.00	430.00	10,073.04	0.00	0.00	0.00	

Design Targets										
Target Name	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude	
LPP(U C 2116 F #232	0.00	0.00	12,265.00	9,987.00	431.00	575,603.00	768,125.00	32.579424	-103.462895	
- hit/miss target										
- Shape										
- plan misses target center by 0.24usft at 22234.68usft MD (12265.00 TVD, 9987.00 N, 430.76 E)										
- Point										
BHL(U C 2116 F #232	0.00	0.00	12,265.00	10,077.00	430.00	575,693.00	768,124.00	32.579672	-103.462896	
- hit/miss target										
- Shape										
- plan hits target center										
- Point										
FPP(U C 2116 F #232	0.00	0.00	12,265.00	75.00	514.00	565,691.00	768,208.00	32.552179	-103.462889	
- hit/miss target										
- Shape										
- plan misses target center by 72.30usft at 12347.81usft MD (12203.16 TVD, 110.41 N, 501.80 E)										
- Point										

Checked By: \_\_\_\_\_ Approved By: \_\_\_\_\_ Date: \_\_\_\_\_







# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

<b>Reference</b>	Prelim A
<b>Filter type:</b>	NO GLOBAL FILTER: Using user defined selection & filtering criteria
<b>Interpolation Method:</b>	Stations
<b>Depth Range:</b>	Unlimited
<b>Results Limited by:</b>	Maximum center-center distance of 9,999.98 us
<b>Warning Levels Evaluated at:</b>	2.00 Sigma
<b>Error Model:</b>	ISCWSA
<b>Scan Method:</b>	Closest Approach 3D
<b>Error Surface:</b>	Pedal Curve
<b>Casing Method:</b>	Not applied

<b>Survey Tool Program</b>	<b>Date</b>	7/12/2018
<b>From (usft)</b>	<b>To (usft)</b>	<b>Survey (Wellbore)</b>
0.00	22,324.69	Prelim A (OH)
		<b>Tool Name</b>
		MWD+HDGM
		<b>Description</b>
		OWSG MWD + HRGM

Summary						
Site Name	Reference Measured Depth (usft)	Offset Measured Depth (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Separation Factor	Warning
Offset Well - Wellbore - Design						
Uncle Ches 2116 Fed						
#122H - OH - Prelim A	1,010.62	1,009.62	29.99	23.21	4.423	CC
#122H - OH - Prelim A	6,800.00	6,803.54	51.47	2.03	1.041	Level 2, ES, SF

<b>Offset Design</b>	Uncle Ches 2116 Fed - #122H - OH - Prelim A										<b>Offset Site Error:</b>	0.00 usft
<b>Survey Program:</b>	0-MWD+HDGM										<b>Offset Well Error:</b>	0.00 usft
<b>Reference</b>	<b>Offset</b>	<b>Semi Major Axis</b>		<b>Distance</b>		<b>Minimum Separation</b>		<b>Warning</b>				
<b>Measured Depth (usft)</b>	<b>Vertical Depth (usft)</b>	<b>Measured Depth (usft)</b>	<b>Vertical Depth (usft)</b>	<b>Reference (usft)</b>	<b>Offset (usft)</b>	<b>Highside Toolface (°)</b>	<b>Offset Wellbore Centre +N/-S (usft)</b>	<b>+E/-W (usft)</b>	<b>Between Centres (usft)</b>	<b>Between Ellipses (usft)</b>	<b>Minimum Separation (usft)</b>	<b>Separation Factor</b>
0.00	0.00	1.00	-1.00	0.00	0.00	90.00	0.00	30.00	30.00			
100.00	100.00	101.00	99.00	0.13	0.13	90.00	0.00	30.00	30.00	29.74	0.26	115.432
200.00	200.00	201.00	199.00	0.49	0.49	90.00	0.00	30.00	30.00	29.02	0.98	30.711
300.00	300.00	301.00	299.00	0.85	0.85	90.00	0.00	30.00	30.00	28.31	1.69	17.712
400.00	400.00	401.00	399.00	1.20	1.21	90.00	0.00	30.00	30.00	27.59	2.41	12.444
500.00	500.00	501.00	499.00	1.56	1.57	90.00	0.00	30.00	30.00	26.87	3.13	9.592
600.00	600.00	601.00	599.00	1.92	1.92	90.00	0.00	30.00	30.00	26.16	3.84	7.803
700.00	700.00	701.00	699.00	2.28	2.28	90.00	0.00	30.00	30.00	25.44	4.56	6.577
800.00	800.00	801.00	799.00	2.64	2.64	90.00	0.00	30.00	30.00	24.72	5.28	5.683
900.00	900.00	901.00	899.00	3.00	3.00	90.00	0.00	30.00	30.00	24.00	6.00	5.004
1,000.00	1,000.00	999.00	999.00	3.35	3.35	90.00	0.00	30.00	30.00	23.29	6.71	4.474
1,010.62	1,010.62	1,009.62	1,009.62	3.39	3.39	-24.31	0.00	30.00	29.99	23.21	6.78	4.423 CC
1,100.00	1,099.99	1,098.52	1,098.51	3.70	3.70	-24.42	-0.30	30.79	30.00	22.61	7.40	4.057
1,200.00	1,199.96	1,198.03	1,197.99	4.04	4.03	-24.74	-1.20	33.20	30.04	21.97	8.07	3.724
1,300.00	1,299.86	1,297.54	1,297.41	4.38	4.37	-25.26	-2.71	37.23	30.11	21.37	8.74	3.445
1,400.00	1,399.68	1,397.06	1,396.74	4.73	4.72	-25.98	-4.83	42.88	30.23	20.81	9.42	3.209
1,499.94	1,499.31	1,504.49	1,495.87	5.08	5.10	-26.89	-7.55	50.13	30.39	20.26	10.13	2.999
1,600.00	1,598.99	1,603.45	1,595.55	5.43	5.45	-27.85	-10.62	58.30	30.64	19.82	10.83	2.830
1,700.00	1,698.60	1,703.45	1,695.16	5.79	5.81	-28.79	-13.68	66.47	30.91	19.37	11.53	2.680
1,800.00	1,798.22	1,803.46	1,794.78	6.15	6.17	-29.71	-16.75	74.63	31.18	18.93	12.24	2.546
1,900.00	1,897.84	1,903.46	1,894.40	6.51	6.53	-30.62	-19.82	82.80	31.45	18.50	12.96	2.428
2,000.00	1,997.46	2,003.46	1,994.01	6.88	6.90	-31.51	-22.88	90.97	31.74	18.07	13.67	2.321
2,100.00	2,097.08	2,103.46	2,093.63	7.24	7.26	-32.38	-25.95	99.14	32.03	17.64	14.39	2.226

CC - Min centre to center distance or convergent point, SF - min separation factor, ES - min ellipse separation



# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Offset Design													Offset Site Error:	0.00 usft
Survey Program: 0-MWD+HDGM													Offset Well Error:	0.00 usft
Reference		Offset		Semi Major Axis			Distance							Warning
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbore Centre +N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor		
2,200.00	2,196.70	2,203.46	2,193.25	7.61	7.63	-33.24	-29.01	107.31	32.33	17.22	15.11	2.139		
2,300.00	2,296.32	2,296.54	2,292.87	7.98	7.97	-34.08	-32.08	115.47	32.64	16.83	15.81	2.064		
2,400.00	2,395.94	2,403.47	2,392.48	8.35	8.37	-34.91	-35.14	123.64	32.95	16.39	16.56	1.990		
2,500.00	2,495.56	2,503.47	2,492.10	8.72	8.74	-35.72	-38.21	131.81	33.28	15.98	17.29	1.924		
2,600.00	2,595.18	2,603.47	2,591.72	9.09	9.11	-36.51	-41.27	139.98	33.60	15.58	18.02	1.865		
2,700.00	2,694.80	2,703.47	2,691.33	9.46	9.48	-37.29	-44.34	148.14	33.94	15.18	18.75	1.810		
2,800.00	2,794.42	2,803.47	2,790.95	9.83	9.85	-38.06	-47.40	156.31	34.28	14.79	19.49	1.759		
2,900.00	2,894.04	2,903.47	2,890.57	10.20	10.22	-38.81	-50.47	164.48	34.62	14.40	20.22	1.712		
3,000.00	2,993.66	3,003.47	2,990.19	10.58	10.60	-39.54	-53.53	172.65	34.98	14.02	20.96	1.669		
3,100.00	3,093.28	3,103.48	3,089.80	10.95	10.97	-40.26	-56.60	180.81	35.33	13.64	21.69	1.629		
3,200.00	3,192.90	3,203.48	3,189.42	11.32	11.34	-40.97	-59.66	188.98	35.70	13.26	22.43	1.591		
3,300.00	3,292.52	3,303.48	3,289.04	11.70	11.72	-41.66	-62.73	197.15	36.06	12.89	23.17	1.556		
3,400.00	3,392.14	3,403.48	3,388.65	12.07	12.09	-42.33	-65.79	205.32	36.44	12.53	23.91	1.524		
3,500.00	3,491.76	3,503.48	3,488.27	12.45	12.47	-43.00	-68.86	213.49	36.82	12.16	24.65	1.493 Level 3		
3,600.00	3,591.38	3,603.48	3,587.89	12.82	12.84	-43.65	-71.92	221.65	37.20	11.80	25.40	1.465 Level 3		
3,700.00	3,691.00	3,703.49	3,687.50	13.20	13.22	-44.28	-74.99	229.82	37.59	11.45	26.14	1.438 Level 3		
3,800.00	3,790.62	3,803.49	3,787.12	13.57	13.59	-44.90	-78.05	237.99	37.98	11.10	26.88	1.413 Level 3		
3,900.00	3,890.24	3,896.51	3,886.74	13.95	13.94	-45.51	-81.12	246.16	38.38	10.77	27.60	1.390 Level 3		
4,000.00	3,989.85	4,003.49	3,986.36	14.32	14.34	-46.11	-84.18	254.32	38.78	10.40	28.37	1.367 Level 3		
4,100.00	4,089.47	4,103.49	4,085.97	14.70	14.72	-46.70	-87.25	262.49	39.18	10.06	29.12	1.346 Level 3		
4,200.00	4,189.09	4,203.49	4,185.59	15.08	15.10	-47.27	-90.31	270.66	39.59	9.72	29.87	1.326 Level 3		
4,300.00	4,288.71	4,296.50	4,285.21	15.45	15.45	-47.83	-93.38	278.83	40.01	9.41	30.59	1.308 Level 3		
4,400.00	4,388.33	4,403.50	4,384.82	15.83	15.85	-48.38	-96.44	287.00	40.42	9.06	31.36	1.289 Level 3		
4,500.00	4,487.95	4,503.50	4,484.44	16.20	16.22	-48.92	-99.51	295.16	40.84	8.73	32.11	1.272 Level 3		
4,600.00	4,587.57	4,603.50	4,584.06	16.58	16.60	-49.45	-102.57	303.33	41.27	8.40	32.86	1.256 Level 3		
4,700.00	4,687.19	4,696.50	4,683.68	16.96	16.95	-49.96	-105.64	311.50	41.69	8.11	33.59	1.241 Level 2		
4,800.00	4,786.81	4,803.50	4,783.29	17.33	17.35	-50.47	-108.71	319.67	42.12	7.76	34.36	1.226 Level 2		
4,900.00	4,886.43	4,903.51	4,882.91	17.71	17.73	-50.97	-111.77	327.83	42.56	7.44	35.11	1.212 Level 2		
5,000.00	4,986.05	5,003.51	4,982.53	18.09	18.11	-51.45	-114.84	336.00	43.00	7.13	35.87	1.199 Level 2		
5,100.00	5,085.67	5,103.51	5,082.14	18.46	18.48	-51.93	-117.90	344.17	43.44	6.82	36.62	1.186 Level 2		
5,200.00	5,185.29	5,203.51	5,181.76	18.84	18.86	-52.40	-120.97	352.34	43.88	6.51	37.37	1.174 Level 2		
5,300.00	5,284.91	5,303.51	5,281.38	19.22	19.24	-52.85	-124.03	360.50	44.33	6.20	38.12	1.163 Level 2		
5,400.00	5,384.53	5,403.51	5,381.00	19.60	19.62	-53.30	-127.10	368.67	44.77	5.90	38.88	1.152 Level 2		
5,500.00	5,484.15	5,503.52	5,480.61	19.97	19.99	-53.74	-130.16	376.84	45.23	5.60	39.63	1.141 Level 2		
5,600.00	5,583.77	5,596.48	5,580.23	20.35	20.34	-54.17	-133.23	385.01	45.68	5.32	40.36	1.132 Level 2		
5,700.00	5,683.39	5,696.48	5,679.85	20.73	20.72	-54.59	-136.29	393.18	46.14	5.03	41.11	1.122 Level 2		
5,800.00	5,783.01	5,803.52	5,779.46	21.10	21.12	-55.01	-139.36	401.34	46.60	4.70	41.89	1.112 Level 2		
5,900.00	5,882.63	5,903.52	5,879.08	21.48	21.50	-55.41	-142.42	409.51	47.06	4.41	42.65	1.103 Level 2		
6,000.00	5,982.25	6,003.52	5,978.70	21.86	21.88	-55.81	-145.49	417.68	47.52	4.12	43.40	1.095 Level 2		
6,100.00	6,081.87	6,103.52	6,078.32	22.24	22.26	-56.20	-148.55	425.85	47.99	3.83	44.15	1.087 Level 2		
6,200.00	6,181.48	6,203.53	6,177.93	22.61	22.63	-56.58	-151.62	434.01	48.45	3.54	44.91	1.079 Level 2		
6,300.00	6,281.10	6,303.53	6,277.55	22.99	23.01	-56.96	-154.68	442.18	48.92	3.26	45.67	1.071 Level 2		
6,400.00	6,380.72	6,403.53	6,377.17	23.37	23.39	-57.32	-157.75	450.35	49.40	2.98	46.42	1.064 Level 2		
6,500.00	6,480.34	6,496.47	6,476.78	23.75	23.74	-57.68	-160.81	458.52	49.87	2.72	47.15	1.058 Level 2		
6,600.00	6,579.96	6,603.53	6,576.40	24.13	24.14	-58.04	-163.88	466.69	50.35	2.41	47.93	1.050 Level 2		
6,700.00	6,679.58	6,703.53	6,676.02	24.50	24.52	-58.39	-166.94	474.85	50.83	2.14	48.69	1.044 Level 2		
6,739.96	6,719.39	6,736.43	6,715.83	24.65	24.65	-58.52	-168.17	478.12	51.02	2.05	48.96	1.042 Level 2		
6,800.00	6,779.23	6,803.54	6,775.63	24.88	24.90	-58.43	-170.01	483.02	51.47	2.03	49.44	1.041 Level 2, ES, SF		
6,900.00	6,879.00	6,896.44	6,875.23	25.25	25.25	-57.00	-173.07	491.19	52.97	2.85	50.12	1.057 Level 2		
7,000.00	6,978.87	7,003.63	6,974.78	25.61	25.66	-54.18	-176.14	499.35	55.51	4.69	50.82	1.092 Level 2		
7,100.00	7,078.81	7,103.78	7,074.25	25.97	26.03	-50.30	-179.20	507.50	59.27	7.82	51.45	1.152 Level 2		

CC - Min centre to center distance or convergent point, SF - min separation factor, ES - min ellipse separation





# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Offset Design													Offset Site Error:	0.00 usft
Survey Program: 0-MWD+HDGM													Offset Well Error:	0.00 usft
Reference		Offset		Semi Major Axis			Distance							Warning
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbore Centre +N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor		
7,200.00	7,178.80	7,204.04	7,173.61	26.32	26.41	-45.77	-182.25	515.65	64.48	12.42	52.06	1.239	Level 2	
7,239.90	7,218.70	7,235.73	7,213.23	26.46	26.53	70.42	-183.47	518.90	67.01	14.75	52.26	1.282	Level 3	
7,300.00	7,278.80	7,304.40	7,272.86	26.65	26.79	73.14	-185.31	523.79	71.10	18.46	52.64	1.351	Level 3	
7,400.00	7,378.80	7,404.79	7,372.10	26.98	27.17	77.02	-188.36	531.93	78.22	24.98	53.24	1.469	Level 3	
7,500.00	7,478.80	7,505.17	7,471.34	27.31	27.55	80.25	-191.41	540.06	85.63	31.78	53.85	1.590		
7,600.00	7,578.80	7,594.45	7,570.58	27.64	27.89	82.95	-194.47	548.20	93.27	38.83	54.44	1.713		
7,700.00	7,678.80	7,694.25	7,670.00	27.97	28.27	85.24	-197.52	556.34	101.08	45.99	55.09	1.835		
7,800.00	7,778.80	7,795.64	7,771.09	28.30	28.64	87.01	-200.25	563.60	108.05	52.29	55.75	1.938		
7,900.00	7,878.80	7,897.28	7,872.55	28.63	29.02	88.21	-202.35	569.20	113.46	57.04	56.42	2.011		
8,000.00	7,978.80	7,999.10	7,974.29	28.96	29.38	88.99	-203.82	573.11	117.27	60.18	57.09	2.054		
8,100.00	8,078.80	8,101.03	8,076.19	29.30	29.74	89.41	-204.65	575.33	119.44	61.69	57.75	2.068		
8,200.00	8,178.80	8,202.64	8,177.80	29.63	30.08	89.51	-204.86	575.89	119.98	61.59	58.39	2.055		
8,300.00	8,278.80	8,302.64	8,277.80	29.97	30.41	89.51	-204.86	575.89	119.98	60.92	59.07	2.031		
8,400.00	8,378.80	8,402.64	8,377.80	30.30	30.74	89.51	-204.86	575.89	119.98	60.25	59.74	2.009		
8,500.00	8,478.80	8,502.64	8,477.80	30.63	31.07	89.51	-204.86	575.89	119.98	59.57	60.41	1.986		
8,600.00	8,578.80	8,602.64	8,577.80	30.97	31.40	89.51	-204.86	575.89	119.98	58.90	61.09	1.964		
8,700.00	8,678.80	8,702.64	8,677.80	31.31	31.73	89.51	-204.86	575.89	119.98	58.22	61.76	1.943		
8,800.00	8,778.80	8,802.64	8,777.80	31.64	32.06	89.51	-204.86	575.89	119.98	57.55	62.44	1.922		
8,900.00	8,878.80	8,902.64	8,877.80	31.98	32.39	89.51	-204.86	575.89	119.98	56.87	63.11	1.901		
9,000.00	8,978.80	9,002.64	8,977.80	32.32	32.72	89.51	-204.86	575.89	119.98	56.19	63.79	1.881		
9,100.00	9,078.80	9,102.64	9,077.80	32.66	33.06	89.51	-204.86	575.89	119.98	55.51	64.47	1.861		
9,200.00	9,178.80	9,202.64	9,177.80	32.99	33.39	89.51	-204.86	575.89	119.98	54.83	65.15	1.842		
9,300.00	9,278.80	9,302.64	9,277.80	33.33	33.72	89.51	-204.86	575.89	119.98	54.15	65.83	1.823		
9,400.00	9,378.80	9,402.64	9,377.80	33.67	34.06	89.51	-204.86	575.89	119.98	53.47	66.51	1.804		
9,500.00	9,478.80	9,502.64	9,477.80	34.01	34.39	89.51	-204.86	575.89	119.98	52.79	67.19	1.786		
9,600.00	9,578.80	9,602.64	9,577.80	34.35	34.73	89.51	-204.86	575.89	119.98	52.11	67.88	1.768		
9,700.00	9,678.80	9,702.64	9,677.80	34.69	35.06	89.51	-204.86	575.89	119.98	51.43	68.56	1.750		
9,800.00	9,778.80	9,802.64	9,777.80	35.03	35.40	89.51	-204.86	575.89	119.98	50.74	69.24	1.733		
9,900.00	9,878.80	9,902.64	9,877.80	35.38	35.73	89.51	-204.86	575.89	119.98	50.06	69.93	1.716		
10,000.00	9,978.80	10,004.90	9,979.78	35.72	36.07	86.78	-199.18	574.90	119.19	48.58	70.62	1.688		
10,069.58	10,048.38	10,073.94	10,047.38	35.95	36.28	80.10	-185.53	572.52	118.37	47.10	71.27	1.661		
10,100.00	10,078.80	10,102.90	10,075.14	36.06	36.36	76.13	-177.44	571.10	118.68	47.08	71.60	1.658		
10,200.00	10,178.80	10,191.21	10,156.73	36.40	36.60	60.67	-144.39	565.34	127.28	55.15	72.12	1.765		
10,300.00	10,278.80	10,267.70	10,222.53	36.74	36.77	45.83	-106.07	558.65	153.53	83.17	70.36	2.182		
10,400.00	10,378.80	10,332.42	10,273.75	37.09	36.89	34.67	-67.14	551.85	198.19	131.40	66.79	2.967		
10,500.00	10,478.80	10,386.58	10,312.96	37.43	36.98	27.03	-30.37	545.44	256.89	193.84	63.05	4.074		
10,600.00	10,578.80	10,431.63	10,342.77	37.77	37.05	21.86	2.89	539.65	325.32	265.50	59.82	5.439		
10,700.00	10,678.80	10,468.89	10,365.40	38.12	37.09	18.38	32.11	534.99	400.60	343.40	57.20	7.003		
10,800.00	10,778.80	10,500.00	10,382.84	38.46	37.12	15.98	57.62	531.37	480.75	425.60	55.15	8.717		
10,900.00	10,878.80	10,527.66	10,397.17	38.80	37.15	14.17	81.08	528.38	564.44	510.81	53.64	10.524		
11,000.00	10,978.80	10,550.00	10,407.93	39.15	37.17	12.91	100.52	526.12	650.81	598.42	52.39	12.422		
11,100.00	11,078.80	10,571.28	10,417.48	39.49	37.18	11.84	119.43	524.10	739.25	687.73	51.52	14.348		
11,200.00	11,178.80	10,600.00	10,429.26	39.84	37.21	10.59	145.50	521.58	829.51	778.29	51.22	16.196		
11,300.00	11,278.80	10,600.00	10,429.26	40.18	37.21	10.59	145.50	521.58	920.76	870.59	50.17	18.354		
11,400.00	11,378.80	10,618.38	10,436.12	40.53	37.22	9.89	162.49	520.10	1,013.20	963.27	49.92	20.294		
11,500.00	11,478.80	10,630.68	10,440.41	40.87	37.23	9.46	173.97	519.17	1,106.56	1,056.90	49.66	22.283		
11,600.00	11,578.80	10,650.00	10,446.66	41.22	37.24	8.84	192.21	517.80	1,200.74	1,151.08	49.67	24.176		
11,709.90	11,688.70	10,650.00	10,446.66	41.60	37.24	8.84	192.21	517.80	1,304.80	1,255.46	49.34	26.446		
11,750.00	11,728.76	10,650.00	10,446.66	41.74	37.24	-0.13	192.21	517.80	1,342.54	1,293.31	49.23	27.269		
11,800.00	11,778.43	10,650.00	10,446.66	41.91	37.24	-0.11	192.21	517.80	1,388.38	1,339.32	49.06	28.297		

CC - Min centre to center distance or convergent point, SF - min separation factor, ES - min ellipse separation





# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Offset Design    Uncle Ches 2116 Fed - #122H - OH - Prelim A													Offset Site Error:    0.00 usft	
Survey Program: 0-MWD+HDGM													Offset Well Error:    0.00 usft	
Reference		Offset		Semi Major Axis			Distance							Warning
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbore Centre +N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor		
11,850.00	11,827.40	10,669.20	10,452.26	42.07	37.26	-0.41	210.53	516.55	1,432.23	1,383.06	49.17	29.126		
11,900.00	11,875.33	10,676.69	10,454.29	42.23	37.26	-0.47	217.72	516.10	1,474.39	1,425.34	49.05	30.060		
11,950.00	11,921.83	10,700.00	10,459.99	42.38	37.29	-0.69	240.29	514.80	1,514.74	1,465.62	49.12	30.835		
12,000.00	11,966.56	10,700.00	10,459.99	42.52	37.29	-0.63	240.29	514.80	1,552.34	1,503.51	48.83	31.789		
12,050.00	12,009.17	10,700.00	10,459.99	42.64	37.29	-0.58	240.29	514.80	1,587.71	1,539.17	48.54	32.706		
12,100.00	12,049.35	10,700.00	10,459.99	42.75	37.29	-0.53	240.29	514.80	1,620.74	1,572.47	48.27	33.578		
12,150.00	12,086.78	10,723.05	10,464.74	42.85	37.31	-0.69	262.81	513.68	1,650.70	1,602.46	48.24	34.218		
12,200.00	12,121.18	10,750.00	10,469.15	42.94	37.36	-0.85	289.38	512.60	1,678.36	1,630.12	48.24	34.795		
12,209.90	12,127.61	10,750.00	10,469.15	42.95	37.36	-0.84	289.38	512.60	1,683.35	1,635.18	48.18	34.941		
12,250.00	12,152.32	10,750.00	10,469.15	43.01	37.36	-0.58	289.38	512.60	1,702.55	1,654.58	47.97	35.492		
12,300.00	12,180.04	10,750.00	10,469.15	43.06	37.36	-0.35	289.38	512.60	1,724.13	1,676.38	47.75	36.109		
12,350.00	12,204.13	10,767.55	10,471.37	43.11	37.39	-0.25	306.77	512.02	1,742.67	1,694.99	47.68	36.548		
12,400.00	12,224.41	10,779.35	10,472.57	43.15	37.41	-0.17	318.51	511.69	1,758.20	1,710.60	47.60	36.938		
12,450.00	12,240.71	10,800.00	10,474.09	43.22	37.45	-0.13	339.10	511.22	1,770.71	1,723.12	47.59	37.210		
12,500.00	12,252.92	10,800.00	10,474.09	43.32	37.45	-0.06	339.10	511.22	1,779.89	1,732.37	47.52	37.455		
12,550.00	12,260.94	10,815.70	10,474.75	43.42	37.48	-0.04	354.78	510.96	1,785.95	1,738.39	47.55	37.556		
12,600.00	12,264.72	10,832.68	10,475.00	43.53	37.52	-0.03	371.76	510.77	1,788.82	1,741.20	47.62	37.562		
12,619.15	12,265.03	10,832.72	10,475.00	43.58	37.52	-0.03	371.80	510.77	1,789.03	1,741.38	47.65	37.543		
12,700.00	12,265.03	10,913.57	10,475.00	43.76	37.74	-0.03	452.65	510.10	1,789.03	1,741.15	47.89	37.361		
12,800.00	12,265.03	11,013.57	10,475.00	44.03	38.05	-0.03	552.64	509.27	1,789.03	1,740.82	48.22	37.105		
12,900.00	12,265.03	11,113.57	10,475.00	44.34	38.43	-0.03	652.64	508.44	1,789.03	1,740.44	48.60	36.815		
13,000.00	12,265.03	11,213.57	10,475.00	44.70	38.85	-0.03	752.64	507.60	1,789.03	1,740.01	49.02	36.493		
13,100.00	12,265.03	11,313.57	10,475.00	45.09	39.32	-0.03	852.63	506.77	1,789.03	1,739.53	49.50	36.144		
13,200.00	12,265.03	11,413.57	10,475.00	45.53	39.84	-0.03	952.63	505.94	1,789.03	1,739.01	50.02	35.768		
13,300.00	12,265.03	11,513.57	10,475.00	46.00	40.39	-0.03	1,052.63	505.11	1,789.03	1,738.45	50.58	35.370		
13,400.00	12,265.03	11,613.57	10,475.00	46.52	41.00	-0.03	1,152.62	504.28	1,789.03	1,737.84	51.19	34.951		
13,500.00	12,265.03	11,713.57	10,475.00	47.07	41.64	-0.03	1,252.62	503.44	1,789.03	1,737.20	51.83	34.516		
13,600.00	12,265.03	11,813.57	10,475.00	47.66	42.32	-0.03	1,352.62	502.61	1,789.03	1,736.51	52.52	34.065		
13,700.00	12,265.03	11,913.57	10,475.00	48.29	43.04	-0.03	1,452.61	501.78	1,789.03	1,735.79	53.24	33.603		
13,800.00	12,265.03	12,013.57	10,475.00	48.95	43.79	-0.03	1,552.61	500.95	1,789.03	1,735.03	54.00	33.131		
13,900.00	12,265.03	12,113.57	10,475.00	49.64	44.58	-0.03	1,652.61	500.11	1,789.03	1,734.24	54.79	32.651		
14,000.00	12,265.03	12,213.57	10,475.00	50.36	45.40	-0.03	1,752.60	499.28	1,789.03	1,733.41	55.62	32.166		
14,100.00	12,265.03	12,313.57	10,475.00	51.12	46.25	-0.03	1,852.60	498.45	1,789.03	1,732.55	56.48	31.677		
14,200.00	12,265.03	12,413.57	10,475.00	51.90	47.13	-0.03	1,952.60	497.62	1,789.03	1,731.66	57.36	31.187		
14,300.00	12,265.03	12,513.57	10,475.00	52.71	48.03	-0.03	2,052.59	496.79	1,789.03	1,730.75	58.28	30.697		
14,400.00	12,265.03	12,613.57	10,475.00	53.55	48.96	-0.03	2,152.59	495.95	1,789.03	1,729.80	59.22	30.207		
14,500.00	12,265.03	12,713.57	10,475.00	54.41	49.92	-0.03	2,252.58	495.12	1,789.03	1,728.83	60.19	29.721		
14,600.00	12,265.03	12,813.57	10,475.00	55.30	50.90	-0.02	2,352.58	494.29	1,789.03	1,727.84	61.19	29.238		
14,700.00	12,265.03	12,913.57	10,475.00	56.21	51.90	-0.02	2,452.58	493.46	1,789.03	1,726.82	62.21	28.759		
14,800.00	12,265.02	13,013.57	10,475.00	57.14	52.92	-0.02	2,552.57	492.62	1,789.02	1,725.78	63.25	28.286		
14,900.00	12,265.02	13,113.57	10,475.00	58.10	53.96	-0.02	2,652.57	491.79	1,789.02	1,724.72	64.31	27.819		
15,000.00	12,265.02	13,213.57	10,475.00	59.07	55.02	-0.02	2,752.57	490.96	1,789.02	1,723.63	65.39	27.359		
15,100.00	12,265.02	13,313.57	10,475.00	60.06	56.09	-0.02	2,852.56	490.13	1,789.02	1,722.53	66.49	26.906		
15,200.00	12,265.02	13,413.57	10,475.00	61.07	57.18	-0.02	2,952.56	489.30	1,789.02	1,721.41	67.61	26.460		
15,300.00	12,265.02	13,513.57	10,475.00	62.10	58.29	-0.02	3,052.56	488.46	1,789.02	1,720.27	68.75	26.023		
15,400.00	12,265.02	13,613.57	10,475.00	63.14	59.41	-0.02	3,152.55	487.63	1,789.02	1,719.12	69.90	25.593		
15,500.00	12,265.02	13,713.57	10,475.00	64.20	60.55	-0.02	3,252.55	486.80	1,789.02	1,717.95	71.07	25.172		
15,600.00	12,265.02	13,813.57	10,475.00	65.28	61.70	-0.02	3,352.55	485.97	1,789.02	1,716.77	72.26	24.759		
15,700.00	12,265.02	13,913.57	10,475.00	66.37	62.86	-0.02	3,452.54	485.13	1,789.02	1,715.57	73.46	24.355		
15,800.00	12,265.02	14,013.57	10,475.00	67.47	64.03	-0.02	3,552.54	484.30	1,789.02	1,714.35	74.67	23.960		
15,900.00	12,265.02	14,113.57	10,475.00	68.58	65.21	-0.02	3,652.54	483.47	1,789.02	1,713.13	75.89	23.573		

CC - Min centre to center distance or convergent point, SF - min separation factor, ES - min ellipse separation



# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Offset Design      Uncle Ches 2116 Fed - #122H - OH - Prelim A													Offset Site Error:      0.00 usft	
Survey Program: 0-MWD+HDGM													Offset Well Error:      0.00 usft	
Reference		Offset		Semi Major Axis			Distance							Warning
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbore Centre +N/-S (usft)	+E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor		
16,000.00	12,265.02	14,213.57	10,475.00	69.71	66.40	-0.02	3,752.53	482.64	1,789.02	1,711.89	77.13	23.195		
16,100.00	12,265.02	14,313.57	10,475.00	70.85	67.61	-0.02	3,852.53	481.80	1,789.02	1,710.64	78.38	22.825		
16,200.00	12,265.02	14,413.57	10,475.00	72.00	68.82	-0.02	3,952.53	480.97	1,789.02	1,709.38	79.64	22.464		
16,300.00	12,265.02	14,513.57	10,475.00	73.16	70.04	-0.02	4,052.52	480.14	1,789.02	1,708.11	80.91	22.111		
16,400.00	12,265.02	14,613.57	10,475.00	74.32	71.27	-0.02	4,152.52	479.31	1,789.02	1,706.83	82.19	21.766		
16,500.00	12,265.02	14,713.57	10,475.00	75.50	72.51	-0.02	4,252.52	478.48	1,789.02	1,705.53	83.49	21.429		
16,600.00	12,265.02	14,813.57	10,475.00	76.69	73.75	-0.02	4,352.51	477.64	1,789.02	1,704.23	84.79	21.100		
16,700.00	12,265.02	14,913.57	10,475.00	77.89	75.01	-0.02	4,452.51	476.81	1,789.02	1,702.92	86.10	20.779		
16,800.00	12,265.02	15,013.57	10,475.00	79.09	76.26	-0.02	4,552.51	475.98	1,789.02	1,701.60	87.41	20.466		
16,900.00	12,265.02	15,113.57	10,475.00	80.31	77.53	-0.02	4,652.50	475.15	1,789.02	1,700.28	88.74	20.160		
17,000.00	12,265.02	15,213.57	10,475.00	81.53	78.80	-0.02	4,752.50	474.31	1,789.02	1,698.94	90.07	19.862		
17,100.00	12,265.02	15,313.57	10,475.00	82.76	80.08	-0.02	4,852.49	473.48	1,789.02	1,697.60	91.42	19.570		
17,200.00	12,265.02	15,413.57	10,475.00	83.99	81.36	-0.02	4,952.49	472.65	1,789.02	1,696.25	92.76	19.286		
17,300.00	12,265.02	15,513.57	10,475.00	85.23	82.65	-0.02	5,052.49	471.82	1,789.02	1,694.90	94.12	19.008		
17,400.00	12,265.02	15,613.57	10,475.00	86.48	83.94	-0.02	5,152.48	470.99	1,789.02	1,693.54	95.48	18.737		
17,500.00	12,265.02	15,713.57	10,475.00	87.74	85.24	-0.02	5,252.48	470.15	1,789.02	1,692.17	96.85	18.472		
17,600.00	12,265.02	15,813.57	10,475.00	89.00	86.55	-0.02	5,352.48	469.32	1,789.02	1,690.79	98.22	18.214		
17,700.00	12,265.02	15,913.57	10,475.00	90.26	87.85	-0.01	5,452.47	468.49	1,789.02	1,689.41	99.60	17.962		
17,800.00	12,265.01	16,013.57	10,475.00	91.53	89.17	-0.01	5,552.47	467.66	1,789.01	1,688.03	100.99	17.715		
17,900.00	12,265.01	16,113.57	10,475.00	92.81	90.48	-0.01	5,652.47	466.82	1,789.01	1,686.64	102.38	17.475		
18,000.00	12,265.01	16,213.57	10,475.00	94.09	91.80	-0.01	5,752.46	465.99	1,789.01	1,685.24	103.77	17.240		
18,100.00	12,265.01	16,313.57	10,475.00	95.37	93.13	-0.01	5,852.46	465.16	1,789.01	1,683.84	105.17	17.010		
18,200.00	12,265.01	16,413.57	10,475.00	96.66	94.45	-0.01	5,952.46	464.33	1,789.01	1,682.43	106.58	16.786		
18,300.00	12,265.01	16,513.57	10,475.00	97.96	95.78	-0.01	6,052.45	463.50	1,789.01	1,681.02	107.99	16.567		
18,400.00	12,265.01	16,613.57	10,475.00	99.26	97.12	-0.01	6,152.45	462.66	1,789.01	1,679.61	109.40	16.353		
18,500.00	12,265.01	16,713.57	10,475.00	100.56	98.45	-0.01	6,252.45	461.83	1,789.01	1,678.19	110.82	16.143		
18,600.00	12,265.01	16,813.57	10,475.00	101.87	99.79	-0.01	6,352.44	461.00	1,789.01	1,676.77	112.24	15.939		
18,700.00	12,265.01	16,913.57	10,475.00	103.18	101.14	-0.01	6,452.44	460.17	1,789.01	1,675.34	113.67	15.739		
18,800.00	12,265.01	17,013.57	10,475.00	104.49	102.48	-0.01	6,552.44	459.33	1,789.01	1,673.91	115.10	15.543		
18,900.00	12,265.01	17,113.57	10,475.00	105.81	103.83	-0.01	6,652.43	458.50	1,789.01	1,672.48	116.53	15.352		
19,000.00	12,265.01	17,213.57	10,475.00	107.13	105.18	-0.01	6,752.43	457.67	1,789.01	1,671.04	117.97	15.165		
19,100.00	12,265.01	17,313.57	10,475.00	108.45	106.54	-0.01	6,852.43	456.84	1,789.01	1,669.60	119.41	14.982		
19,200.00	12,265.01	17,413.57	10,475.00	109.78	107.89	-0.01	6,952.42	456.01	1,789.01	1,668.16	120.85	14.803		
19,300.00	12,265.01	17,513.57	10,475.00	111.11	109.25	-0.01	7,052.42	455.17	1,789.01	1,666.71	122.30	14.628		
19,400.00	12,265.01	17,613.57	10,475.00	112.44	110.61	-0.01	7,152.42	454.34	1,789.01	1,665.26	123.75	14.457		
19,500.00	12,265.01	17,713.57	10,475.00	113.77	111.97	-0.01	7,252.41	453.51	1,789.01	1,663.81	125.20	14.289		
19,600.00	12,265.01	17,813.57	10,475.00	115.11	113.34	-0.01	7,352.41	452.68	1,789.01	1,662.35	126.65	14.125		
19,700.00	12,265.01	17,913.57	10,475.00	116.45	114.70	-0.01	7,452.40	451.84	1,789.01	1,660.90	128.11	13.964		
19,800.00	12,265.01	18,013.57	10,475.00	117.80	116.07	-0.01	7,552.40	451.01	1,789.01	1,659.44	129.57	13.807		
19,900.00	12,265.01	18,113.57	10,475.00	119.14	117.44	-0.01	7,652.40	450.18	1,789.01	1,657.97	131.03	13.653		
20,000.00	12,265.01	18,213.57	10,475.00	120.49	118.82	-0.01	7,752.39	449.35	1,789.01	1,656.51	132.50	13.502		
20,100.00	12,265.01	18,313.57	10,475.00	121.84	120.19	-0.01	7,852.39	448.51	1,789.01	1,655.04	133.97	13.354		
20,200.00	12,265.01	18,413.57	10,475.00	123.19	121.56	-0.01	7,952.39	447.68	1,789.01	1,653.57	135.44	13.209		
20,300.00	12,265.01	18,513.57	10,475.00	124.55	122.94	-0.01	8,052.38	446.85	1,789.01	1,652.10	136.91	13.067		
20,400.00	12,265.01	18,613.57	10,475.00	125.90	124.32	-0.01	8,152.38	446.02	1,789.01	1,650.62	138.38	12.928		
20,500.00	12,265.01	18,713.57	10,475.00	127.26	125.70	-0.01	8,252.38	445.19	1,789.01	1,649.15	139.86	12.791		
20,600.00	12,265.01	18,813.57	10,475.00	128.62	127.08	-0.01	8,352.37	444.35	1,789.01	1,647.67	141.34	12.658		
20,700.00	12,265.01	18,913.57	10,475.00	129.98	128.47	-0.01	8,452.37	443.52	1,789.01	1,646.19	142.82	12.526		
20,800.00	12,265.01	19,013.57	10,475.00	131.35	129.85	0.00	8,552.37	442.69	1,789.01	1,644.70	144.30	12.398		
20,900.00	12,265.00	19,113.57	10,475.00	132.71	131.24	0.00	8,652.36	441.86	1,789.00	1,643.22	145.78	12.272		

CC - Min centre to center distance or convergent point, SF - min separation factor, ES - min ellipse separation



# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Offset Design													Offset Site Error:	0.00 usft
Survey Program: 0-MWD+HDGM													Offset Well Error:	0.00 usft
Reference		Offset		Semi Major Axis			Distance							Warning
Measured Depth (usft)	Vertical Depth (usft)	Measured Depth (usft)	Vertical Depth (usft)	Reference (usft)	Offset (usft)	Highside Toolface (°)	Offset Wellbore +N/-S (usft)	Centre +E/-W (usft)	Between Centres (usft)	Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor		
21,000.00	12,265.00	19,213.57	10,475.00	134.08	132.62	0.00	8,752.36	441.02	1,789.00	1,641.73	147.27	12.148		
21,100.00	12,265.00	19,313.57	10,475.00	135.45	134.01	0.00	8,852.36	440.19	1,789.00	1,640.25	148.76	12.026		
21,200.00	12,265.00	19,413.57	10,475.00	136.82	135.40	0.00	8,952.35	439.36	1,789.00	1,638.76	150.25	11.907		
21,300.00	12,265.00	19,513.57	10,475.00	138.19	136.79	0.00	9,052.35	438.53	1,789.00	1,637.27	151.74	11.790		
21,400.00	12,265.00	19,613.57	10,475.00	139.56	138.18	0.00	9,152.35	437.70	1,789.00	1,635.77	153.23	11.675		
21,500.00	12,265.00	19,713.57	10,475.00	140.94	139.58	0.00	9,252.34	436.86	1,789.00	1,634.28	154.72	11.563		
21,600.00	12,265.00	19,813.57	10,475.00	142.31	140.97	0.00	9,352.34	436.03	1,789.00	1,632.78	156.22	11.452		
21,700.00	12,265.00	19,913.57	10,475.00	143.69	142.36	0.00	9,452.34	435.20	1,789.00	1,631.29	157.72	11.343		
21,800.00	12,265.00	20,013.57	10,475.00	145.07	143.76	0.00	9,552.33	434.37	1,789.00	1,629.79	159.21	11.237		
21,900.00	12,265.00	20,113.57	10,475.00	146.45	145.16	0.00	9,652.33	433.53	1,789.00	1,628.29	160.71	11.132		
22,000.00	12,265.00	20,213.57	10,475.00	147.83	146.55	0.00	9,752.33	432.70	1,789.00	1,626.79	162.21	11.029		
22,100.00	12,265.00	20,313.57	10,475.00	149.22	147.95	0.00	9,852.32	431.87	1,789.00	1,625.29	163.72	10.928		
22,200.00	12,265.00	20,413.57	10,475.00	150.60	149.35	0.00	9,952.32	431.04	1,789.00	1,623.78	165.22	10.828		
22,300.00	12,265.00	20,513.57	10,475.00	151.98	150.75	0.00	10,052.31	430.21	1,789.00	1,622.28	166.72	10.730		
22,324.69	12,265.00	20,538.26	10,475.00	152.33	151.10	0.00	10,077.00	430.00	1,789.00	1,621.91	167.09	10.706		

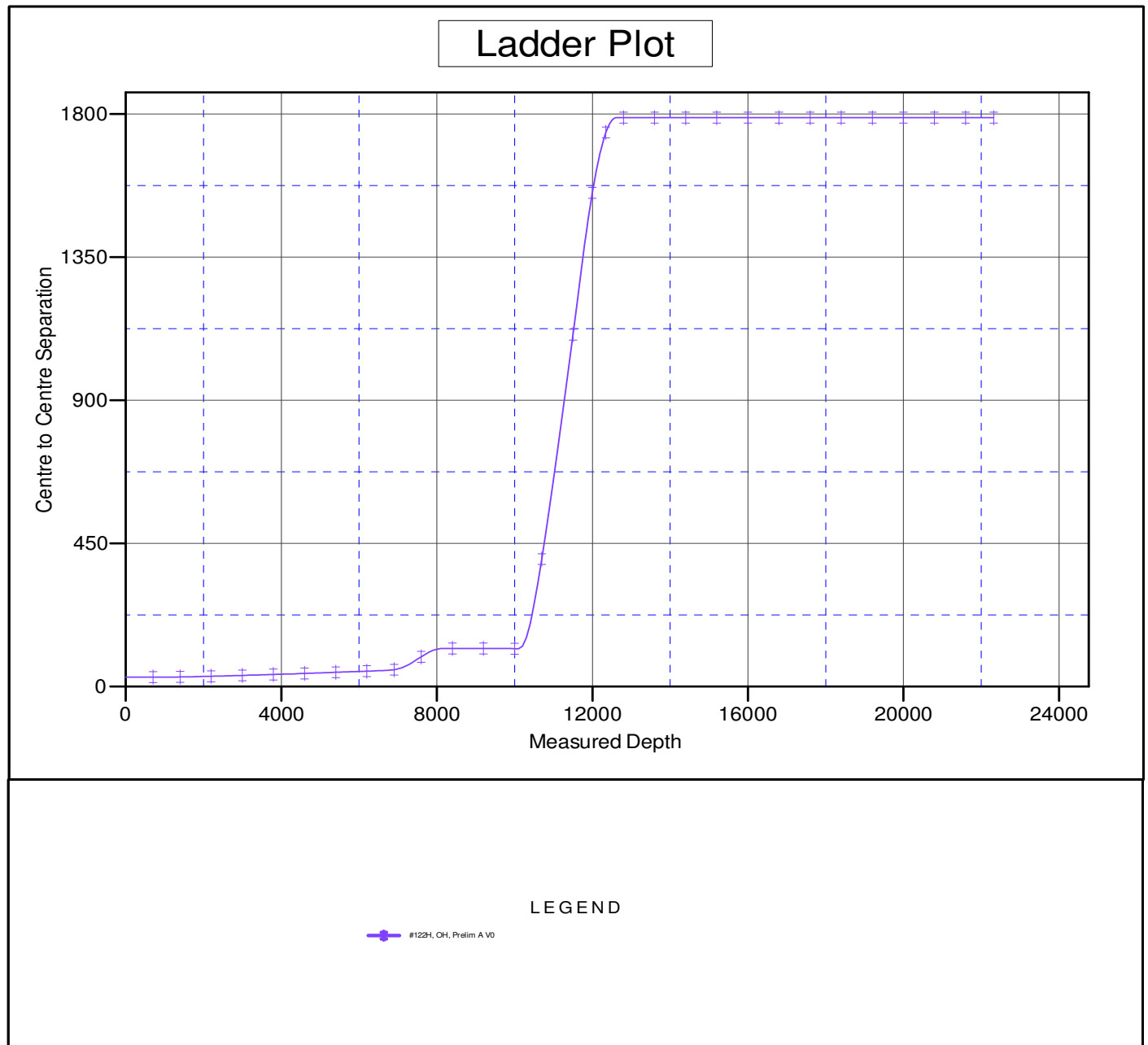


# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Reference Depths are relative to GL: 3717' + KB: 28.5' @ 3745.50usft Coordinates are relative to: #232H  
Offset Depths are relative to Offset Datum Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30  
Central Meridian is -104.333334 Grid Convergence at Surface is: 0.47°



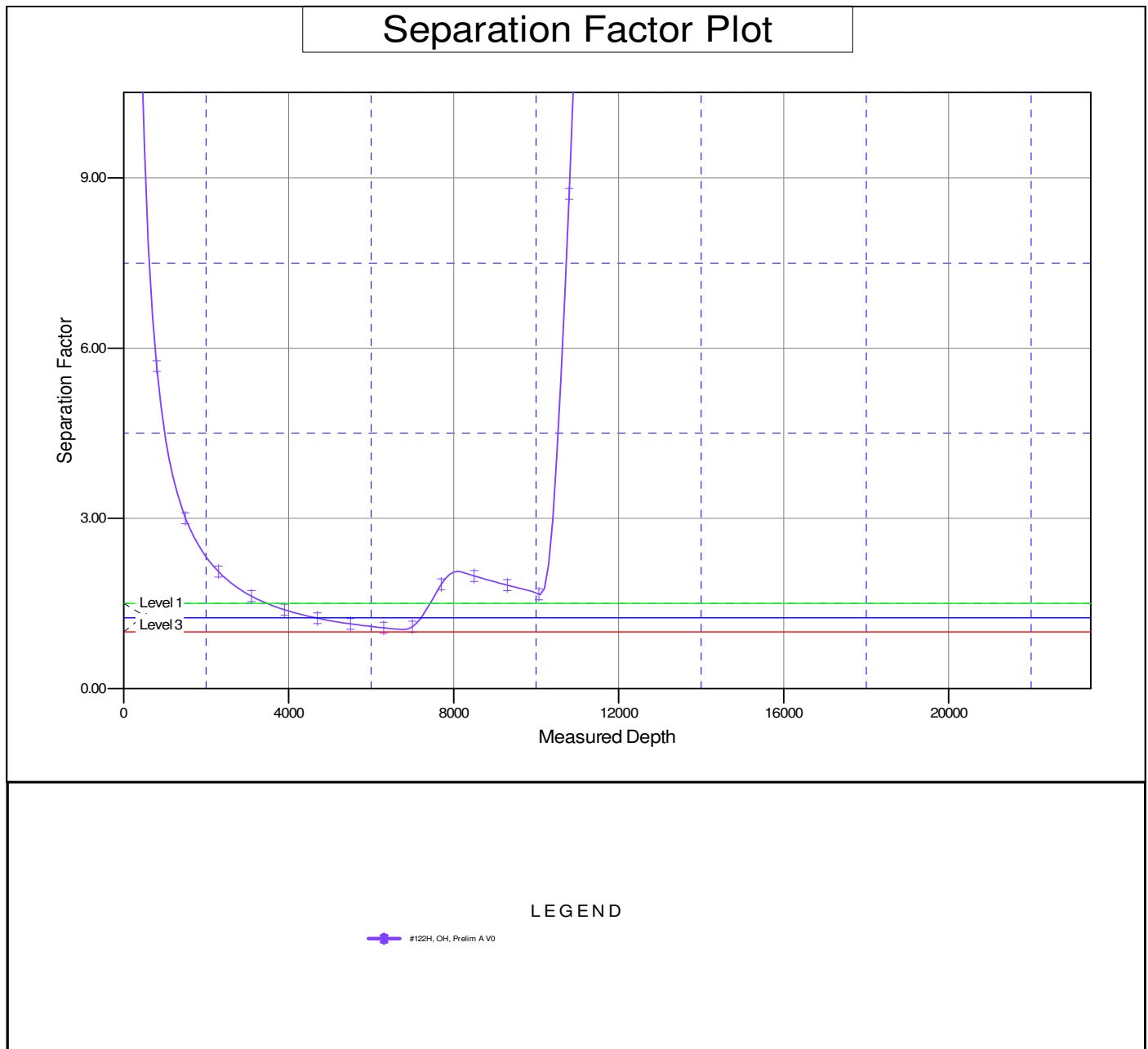


# Pro Directional Anticollision Report



<b>Company:</b>	Matador Resources	<b>Local Co-ordinate Reference:</b>	Well #232H
<b>Project:</b>	Lea County, NM	<b>TVD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Reference Site:</b>	Uncle Ches 2116 Fed	<b>MD Reference:</b>	GL: 3717' + KB: 28.5' @ 3745.50usft (Patterson 809)
<b>Site Error:</b>	0.00 usft	<b>North Reference:</b>	Grid
<b>Reference Well:</b>	#232H	<b>Survey Calculation Method:</b>	Minimum Curvature
<b>Well Error:</b>	0.00 usft	<b>Output errors are at</b>	2.00 sigma
<b>Reference Wellbore</b>	OH	<b>Database:</b>	WellPlanner1
<b>Reference Design:</b>	Prelim A	<b>Offset TVD Reference:</b>	Offset Datum

Reference Depths are relative to GL: 3717' + KB: 28.5' @ 3745.50usft Coordinates are relative to: #232H  
Offset Depths are relative to Offset Datum Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30  
Central Meridian is -104.333334 Grid Convergence at Surface is: 0.47°



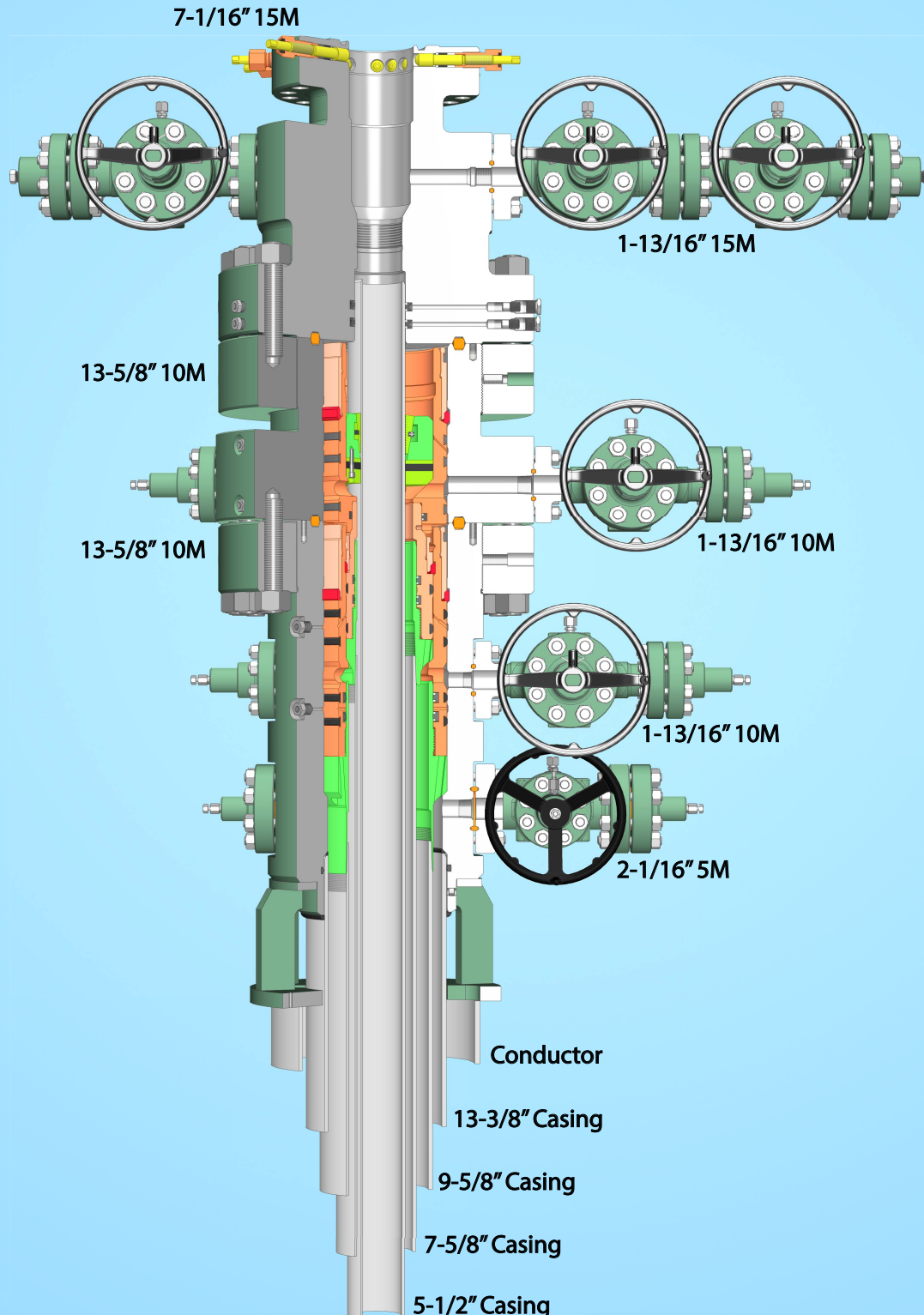
# **Closed-Loop System**

## **Operating and Maintenance Plan:**

During drilling operations, third party service companies will utilize solids control equipment to remove cuttings from the drilling fluids and collect it in haul-off bins. Equipment will be closely monitored at all times while drilling by the derrick man and the service company employees.

## **Closure Plan:**

During drilling operations, third party service companies will haul off drill solids and fluids to an approved disposal facility. At the end of the well, all closed loop equipment will be removed from the location.



Drilling Operations Plan  
Uncle Ches 2116 Fed Com #232H  
Matador Resources Company  
UL: N, Sec 21, 20S, 35E  
Lea County, NM

Surface Location: 260' FSL & 1797' FWL, Sec. 21  
Bottom Hole Location: 240' FNL & 2310' FWL, Sec. 16  
Elevation Above Sea Level: 3717'

Type of Well: Horizontal well, No Pilot Hole, Drilled with conventional rotary tools

Proposed Drilling Depth: 22,324' MD / 12,265' TVD

Estimated Tops of Geological Markers w/ Mineral Bearing Formation:

Formation Name	SSTVD	TVD	Bearing
Rustler	1774	1964	Salt/Washout
Salado	1431	2307	Salt/Washout
Delaware	-2555	6293	Hydrocarbon/Loss Circ
Brushy Canyon	-3606	7344	Oil/Gas
Bone Spring Lime	-4769	8507	Oil/Gas
1st Bone Spring Carbonate	-5870	9608	Oil/Gas
1st Bone Spring Sand	-6013	9751	Oil/Gas
2nd Bone Spring Carbonate	-6333	10071	Oil/Gas
2nd Bone Spring Sand	-6687	10425	Oil/Gas
3rd Bone Spring Carbonate	-7208	10946	Oil/Gas
3rd Bone Spring Sand	-7758	11496	Oil/Gas
Wolfcamp A	-7959	11697	Oil/Gas
Wolfcamp B	-8065	11803	Oil/Gas
Wolfcamp C	-8309	12047	Oil/Gas
Wolfcamp D	-8477	12215	Oil/Gas

OSE Ground Water Estimated Depth: 877'

Casing Program

Name	Hole Size	Casing Size	Wt/Grade	Thread Collar	Setting Depth	Top Cement
Surface	20"	13-3/8" (new)	54.5# J-55	BTC	1984	Surface
Intermediate 1	12-1/4"	9-5/8" (new)	40# J-55	BTC	5900	Surface
Intermediate 2	8-3/4"	7-5/8" (new)	29.7# P-110	BTC	0-5700	4900'
		7-5/8" (new)	29.7# P-110	VAM HTF-NR	5700-11659	
		7" (new)	29# P-110	BTC	11659-12450	
Production	6-1/8"	5-1/2" (new)	20# P-110	Tenaris XP	0-11559	11450
		4-1/2" (new)	13.5# P-110	Tenaris XP	11559-22324	

Minimum Safety Factors: Burst: 1.125 Collapse: 1.125 Tension 1.8

Cementing Program



Drilling Operations Plan  
Uncle Ches 2116 Fed Com #232H  
Matador Resources Company  
UL: N, Sec 21, 20S, 35E  
Lea County, NM

Name	Type	Sacks	Yield	Weight	Blend
Surface	Lead	2188	1.75	13.5	Class C + 3% NaCl + LCM
	Tail	694	1.38	14.8	Class C + 5% NaCl + LCM
TOC = 0'		100% Excess		Centralizers per Onshore Order 2.III.B.1f	
Intermediate 1	Lead	1344	1.81	13.5	Class C + Bentonite + 1% CaCL <sub>2</sub> + 8% NaCl + LCM
	Tail	536	1.38	14.8	Class C + 5% NaCl + LCM
TOC = 0'		100% Excess		2 on btm jt, 1 on 2nd jt, 1 every 4th jt to surface	
Intermediate 2	Lead	946	2.36	11.5	TXI + Fluid Loss + Dispersant + Retarder + LCM
	Tail	165	1.38	13.2	TXI + Fluid Loss + Dispersant + Retarder + LCM
TOC = 4900'		35% Excess		2 on btm jt, 1 on 2nd jt, 1 every other jt to top of tail cement (500' above TOC), 1 every 4th jt to surface	
Production	Tail	816	1.38	15.8	Class H + Fluid Loss + Dispersant + Retarder + LCM
TOC = 14450'		10% Excess		2 on btm jt, 1 on 2nd jt, 1 every 4th jt to top of tail cement (1000' tie back)	

Matador requests the option to run a DV tool with annular packer as contingency in the intermediate section on 9-5/8" casing if lost circulation is encountered. If losses occur the DV tool with packer will be placed at least 100' above the loss zone to give the option to pump cement as either a single stage or two stage.

**Pressure Control Equipment:**

A 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams. An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed. Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position. A third party company will test the BOPs.

After setting surface casing, and before drilling below the surface casing shoe, BOPE will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high. After setting 9-5/8" casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. After setting 7-5/8" x 7" Casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will tested to 250 psi low and 5000 psi high.

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Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used.

Matador is requesting a variance to use a speed head for setting the intermediate (9-5/8") casing. In the case of running a speed head with landing mandrel for 9-5/8" casing, BOP test pressures after setting surface casing will be 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. BOPE will be tested within 500 feet of the top of the Wolfcamp formation if the time between the setting of the Intermediate casing and reaching this depth exceeds 20 days. A diagram of the speed head is attached.

Proposed Mud System:

Name	Hole Size	Mud Weight	Visc	Fluid Loss	Type Mud
Surface	20"	8.40	28	NC	FW Spud Mud
Intermediate 1	12-1/4"	10.00	30-32	NC	Brine Water
Intermediate 2	8-3/4"	9.00	30-32	NC	FW/Cut Brine
Intermediate 3	6-1/8"	12.00	50-60	<10	OBM

All necessary mud products for weight addition and fluid loss control will be on location at all times. Mud program subject to change due to hole conditions.

The Mud Monitoring System is an electronic Pason system satisfying requirements of Onshore Order 1.

Testing, Logging & Coring Program:

- Mud Logging Program: 2 man unit from 1984 – TD
- Electric Logging Program: No electric logs are planned at this time. GR will be collected through the MWD tools from Inter. Csg to TD
- No DSTs or cores are planned at this time
- CBL w/ CCL from as far as gravity will let it fall to TOC

Potential Hazards:

No abnormal pressures or temperatures are expected. In accordance with Onshore Order 6, Matador does not anticipate that there will be enough H<sub>2</sub>S from the surface to the Bone Spring formations to meet the BLM's minimum requirements for the submission of an "H<sub>2</sub>S Drilling Operation Plan" or "Public Protection Plan" for the drilling and completion of this well. Since we have an H<sub>2</sub>S safety package on all wells, attached is an "H<sub>2</sub>S Drilling Operations Plan". Adequate flare lines will be installed off the mud/gas separator where gas may be flared safely. All personnel will be familiar with all aspects of safe operation of equipment being used.

Estimated BHP: 6132 psi  
Estimated BHT: 170° F

Construction and Drilling:

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Road and location construction will begin after BLM approval of APD. Anticipated spud date as soon as approved. Drilling expected to take 35 days. If production casing is run an additional 30 days will be required to complete and construct surface facilities.

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