UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT

OCD - HOBBS 06|17|2020 RECEIVED

FORM APPROVED

OMB N	No. 100)4- 01	137
Expires: J	anuary	31,	2018

6. If Indian, Allotee or Tribe Name

5. Lease Serial No. NMNM132079

A DDI ICATION		DDII I	OR REFNTER

1a. Type of work: PIDRILL RI	EENTER			7. If Unit or CA Agr	reement, Na	ame and No.
1b. Type of Well: Oil Well Gas Well Ot	ther			8. Lease Name and	Wall No	
1c. Type of Completion: Hydraulic Fracturing Sin	ngle Zone	Multiple Zone				204
,, , <u>, , , , , , , , , , , , , , , , ,</u>	C			UNCLE CHES 21	[32621	
				25511		
2. Name of Operator MATADOR PRODUCTION COMPANY [228937]				9. API Well No. 3	0-025-	47339
3a. Address		No. (include area cod	le)	10. Field and Pool,	_	
5400 LBJ Freeway, Suite 1500 Dallas TX 75240	(972)371	-5200		JENNINGS; BONE	SPRING	, WEST / AN1
4. Location of Well (Report location clearly and in accordance w	with any Sta	ate requirements.*)		11. Sec., T. R. M. or		•
At surface SWSE / 260 FSL / 2333 FEL / LAT 32.5521	126 / LON	IG -103.4612937		SEC 21 / T20S / R	35E / NMI	2
At proposed prod. zone NWNE / 240 FNL / 2311 FEL / L/	AT 32.579	8012 / LONG -103.4	612337			
14. Distance in miles and direction from nearest town or post office 12 miles	ice*			12. County or Parisl LEA	l l	13. State
15. Distance from proposed* 260 feet	16. No of	acres in lease	17. Spaci	ng Unit dedicated to t	his well	
location to nearest property or lease line, ft.	160		640			
(Also to nearest drig. unit line, if any)						
18. Distance from proposed location*	19. Propo	sed Depth	20. BLM	/BIA Bond No. in file		
to nearest well, drilling, completed, applied for, on this lease, ft.	12222 fe	et / 22271 feet	FED: N	MB001079		
21. Elevations (Show whether DF, KDB, RT, GL, etc.)		oximate date work will	start*	23. Estimated durati	ion	
3712 feet	08/01/20	19		30 days		
	24. Att	achments				
The following, completed in accordance with the requirements of (as applicable)	f Onshore O	Dil and Gas Order No.	1, and the l	Hydraulic Fracturing r	ule per 43 (CFR 3162.3-3
1. Well plat certified by a registered surveyor.		4. Bond to cover the	he operation	ns unless covered by a	n existing b	ond on file (see
2. A Drilling Plan.		Item 20 above).	1	,	J	
3. A Surface Use Plan (if the location is on National Forest System				. 1/ 1		. 11 . 4
SUPO must be filed with the appropriate Forest Service Office)>	BLM.	pecific into	rmation and/or plans as	may be rec	luested by the
25. Signature	Nar	me (Printed/Typed)			Date	
(Electronic Submission)	Lara	a Thompson / Ph: (5	05)431-26	78	02/22/20	19
Title						
Project Manager						
Approved by (Signature)		me (Printed/Typed)	004 5050		Date	200
(Electronic Submission)		ly Layton / Ph: (575)	∠34-5959 		06/16/20	
Title Assistant Field Manager Lands & Minerals	Offi	ice RLSBAD				
Application approval does not warrant or certify that the applican			hose rights	in the subject lease w	hich would	l entitle the
applicant to conduct operations thereon.	0	•	0	, and the second		
Conditions of approval, if any, are attached.						
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, m	nake it a cri	me for any person kno	wingly and	I willfully to make to a	any departn	nent or agency

GCP Rec 06/17/2020

SL



of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.





NAME: Lara Thompson

Title: Project Manager

Phone:

Email address:

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Operator Certification Data Report

Signed on: 10/04/2018

Operator Certification

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

,		
Street Address: 564	7 Jefferson Street NE	
City: Albuquerque	State: NM	Zip: 87109
Phone: (505)431-267	'8	
Email address: Lara	.Thompson@swca.com	
Field Repre	esentative	
Representative Nam	ıe:	
Street Address:		
City:	State:	Zip:



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Application Data Report

06/17/2020

APD ID: 10400034879 **Submission Date:** 02/22/2019

Operator Name: MATADOR PRODUCTION COMPANY

Well Number: 233H

recent changes
Show Final Text

Highlighted data reflects the most

Well Type: OIL WELL Well Work Type: Drill

Section 1 - General

Well Name: UNCLE CHES 2116 FED COM

BLM Office: CARLSBAD User: Lara Thompson Title: Project Manager

Federal/Indian APD: FED Is the first lease penetrated for production Federal or Indian? FED

Lease number: NMNM132079 Lease Acres: 160

Surface access agreement in place? Allotted? Reservation:

Agreement in place? NO Federal or Indian agreement:

Agreement number:

Agreement name:

Keep application confidential? YES

Permitting Agent? YES APD Operator: MATADOR PRODUCTION COMPANY

Operator letter of designation:

Operator Info

Operator Organization Name: MATADOR PRODUCTION COMPANY

Operator Address: 5400 LBJ Freeway, Suite 1500
Zip: 75240

Operator PO Box:

Operator City: Dallas State: TX

Operator Phone: (972)371-5200

Operator Internet Address: amonroe@matadorresources.com

Section 2 - Well Information

Well in Master Development Plan? NO Master Development Plan name:

Well in Master SUPO? NO Master SUPO name:

Well in Master Drilling Plan? NO Master Drilling Plan name:

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H Well API Number:

Field Pool or Exploratory? Field and Pool Field Name: JENNINGS; BONE Pool Name: ANTELOPE

SPRING, WEST RIDGE; BONE SPRING

Is the proposed well in an area containing other mineral resources? NATURAL GAS,OIL

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

Is the proposed well in an area containing other mineral resources? NATURAL GAS,OIL

Is the proposed well in a Helium production area? N Use Existing Well Pad? NO New surface disturbance?

Number of Legs: 1

Type of Well Pad: MULTIPLE WELL Multiple Well Pad Name: SLOT Number: 2

Well Class: HORIZONTAL

Well Work Type: Drill
Well Type: OIL WELL
Describe Well Type:
Well sub-Type: INFILL

Describe sub-type:

Distance to town: 12 Miles Distance to nearest well: 30 FT Distance to lease line: 260 FT

Reservoir well spacing assigned acres Measurement: 640 Acres

Well plat: Matador_Uncle_Ches_233H_20181004135825.pdf

Well work start Date: 08/01/2019 Duration: 30 DAYS

Section 3 - Well Location Table

Survey Type: RECTANGULAR

Describe Survey Type:

Datum: NAD83 Vertical Datum: NAVD88

Survey number: Reference Datum:

	_																		
Wellbore	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD	Will this well produce from this lease?
SHL	260	FSL	233	FEL	20S	35E	21	Aliquot	32.55211	-	LEA	NEW	NEW	F	NMNM	371	0	0	
Leg			3					SWSE	26	103.4612		MEXI	MEXI		132079	2			
#1										937		CO	CO						
KOP	260	FSL	233	FEL	20S	35E	21	Aliquot	32.55211	-	LEA	NEW	NEW	F	NMNM	-	116	116	
Leg			3					SWSE	26	103.4512		MEXI	MEXI		132079	793	54	46	
#1										937		CO	CO			4			
PPP	330	FSL	330	FW	20S	35E	21	Aliquot	32.55230	-	LEA	NEW	NEW	F	NMNM	-	125	122	
Leg				L				SWSE	5	103.4612		I	MEXI		132079	851	63	22	
#1-1										29		СО	СО			0			

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

Wellbore	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD	Will this well produce from this lease?
PPP	260	FSL	330	FW	20S	35E	21	Aliquot	32.55855	-	LEA	NEW	NEW	F	NMNM	-	148	122	
Leg	3			L				NWSE	42	103.4612		MEXI	ı		132078	851	36	22	
#1-2										29		СО	СО			0			
PPP	128	FSL	330	FW	20S	35E	21	Aliquot	32.55492	-	LEA	NEW	NEW	F	NMNM	-	135	122	
Leg	1			L				SWSE	25	103.4612		MEXI		7	137465	851	14	22	
#1-3										28		СО	СО			0			
EXIT	330	FNL	330	FW	20S	35E	16	Aliquot	32.57955		LEA		NEW	S	STATE	-	221	122	
Leg				L				NWNE	38	103.4612		MEXI	l .			851	81	22	
#1										337		СО	СО			0			
BHL	240	FNL	231	FEL	20S	35E	16	Aliquot	32.57980		LEA		NEW	S	STATE	-	222	122	
Leg			1					NWNE	12	103.4612		MEXI				851	71	22	
#1										337		СО	СО			0			



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Drilling Plan Data Report

06/17/2020

APD ID: 10400034879

Submission Date: 02/22/2019

Highlighted data reflects the most recent changes

Operator Name: MATADOR PRODUCTION COMPANY

Well Name: UNCLE CHES 2116 FED COM

Well Number: 233H

Show Final Text

Well Type: OIL WELL

Well Work Type: Drill

Section 1 - Geologic Formations

Formation			True Vertical				Producing
ID	Formation Name	Elevation	Depth	Depth	Lithologies	Mineral Resources	Formation
390047	RUSTLER	1767	1971	1971		NONE	N
390048	SALADO	-551	2318	2318		NONE	N
390049	DELAWARE	-4462	6229	6229		NATURAL GAS, OIL	N
390050	BRUSHY CANYON	-5559	7326	7326		NATURAL GAS, OIL	N
390051	BONE SPRING LIME	-6725	8492	8492		NATURAL GAS, OIL	N
390052	BONE SPRING 1ST	-7809	9576	9576		NATURAL GAS, OIL	N
390053	BONE SPRING 2ND	-8266	10033	10033		NATURAL GAS, OIL	N
390054	BONE SPRING 3RD	-9128	10895	10895		NATURAL GAS, OIL	N
390055	WOLFCAMP	-9878	11645	11645		NATURAL GAS, OIL	Y

Section 2 - Blowout Prevention

Pressure Rating (PSI): 5M Rating Depth: 12000

Equipment: A 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams. An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed.

Requesting Variance? YES

Variance request: Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used. Matador is requesting a variance to use a speed head for setting the intermediate (9-5/8") casing. In the case of running a speed head with landing mandrel for 9-5/8" casing, BOP test pressures after setting surface casing will be 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. The BOPE will be tested within 500 feet of the top of the Wolfcamp formation if the time between the setting of the Intermediate casing and reaching this depth exceeds 20 days. A diagram of the speed head is attached.

Testing Procedure: Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

and collars will be available on the rig floor in the open position. A third party company will test the BOPs. After setting surface casing, and before drilling below the surface casing shoe, BOPE will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high. After setting 9-5/8" casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. After setting 7-5/8" x 7" Casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will tested to 250 psi low and 5000 psi high.

Choke Diagram Attachment:

BLM_Choke_Mod_20181004152602.pdf

BOP Diagram Attachment:

809_CoFlex_Certs___Uncle_Ches_Copy_20181004152625.pdf BOP_809_001_20181004152626.pdf

Section 3 - Casing

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	20	13.375	NEW	API	N	0	1984	0	1984			1984	J-55			1.12 5	1.12 5	DRY	1.8	DRY	1.8
2	INTERMED IATE	12.2 5	9.625	NEW	API	N	0	5900	0	5900			5900	J-55	-		1.12 5	1.12 5	DRY	1.8	DRY	1.8
3	INTERMED IATE	8.75	7.625	NEW	API	Υ	0	12400	0	12199			12400	P- 110			_	1.12 5	BUOY	1.8	BUOY	1.8
4	PRODUCTI ON	6.12 5	5.5	NEW	API	Y	0	22270	0	12222			22270	P- 110	-		1.12 5	1.12 5	DRY	1.8	DRY	1.8

Casing Attachments

Operator Name: MATADOR PRODUCTION COMPANY Well Name: UNCLE CHES 2116 FED COM Well Number: 233H **Casing Attachments** Casing ID: 1 String Type: SURFACE **Inspection Document: Spec Document: Tapered String Spec:** Casing Design Assumptions and Worksheet(s): BLM_Casing_Design_Assumptions_4_string_Wolfcamp_20181004133257.docx Casing ID: 2 String Type: INTERMEDIATE **Inspection Document: Spec Document: Tapered String Spec:** Casing Design Assumptions and Worksheet(s): BLM_Casing_Design_Assumptions_4_string_Wolfcamp_20181009131752.docx Casing ID: 3 String Type: INTERMEDIATE **Inspection Document: Spec Document: Tapered String Spec:** 7.625in_29.7__P110EC_VAM_HTF_NR_20190222112017.PDF

Casing Design Assumptions and Worksheet(s):

BLM_Casing_Design_Assumptions_4_string_Wolfcamp_20181004133215.docx

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

Casing Attachments

Casing ID: 4 String Type: PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

5.5in_20__P110IC_TXP_20190222112046.pdf

Casing Design Assumptions and Worksheet(s):

 $BLM_Casing_Design_Assumptions_4_string_Wolfcamp_20181009131803.docx$

Section 4 - Cement

		•									
String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1984	2188	1.75	13.5	3829	100	С	3% NaCl + LCM
SURFACE	Tail		0	1984	694	1.38	14.8	958	100	С	5% NaCl + LCM
INTERMEDIATE	Lead		0	5900	1344	1.81	13.5	2433	100	С	Bentonite + 1% CaCL2 + 8% NaCl + LCM
INTERMEDIATE	Tail		0	5900	536	1.38	14.8	740	100	С	5% NaCl + LCM
INTERMEDIATE	Lead		4900	1240 0	940	2.36	11.5	2218	35	TXI	Fluid Loss + Dispersant + Retarder + LCM
INTERMEDIATE	Tail		4900	1240 0	166	1.38	13.2	229	35	TXI	Fluid Loss + Dispersant + Retarder + LCM
PRODUCTION	Lead		1140 0	2227 0	816	1.38	15.8	1126	35	Н	Fluid Loss + Dispersant + Retarder + LCM

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

Describe what will be on location to control well or mitigate other conditions: All necessary mud products for weight addition and fluid loss control will be on location at all times. Mud program subject to change due to hole conditions.

Describe the mud monitoring system utilized: The Mud Monitoring System is an electronic Pason system satisfying requirements of Onshore Order 1.

Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (lbs/gal)	Max Weight (lbs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	НА	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
0	2227 0	OIL-BASED MUD	12	12							
0	1240 0	OTHER : FW/Cut Brine	9	9							
0	1984	SPUD MUD	8.4	8.4							
0	5900	SALT SATURATED	10	10							

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

- Mud Logging Program: 2 man unit from 1984 TD
- Electric Logging Program: No electric logs are planned at this time. GR will be collected through the MWD tools from Inter. Csg to TD
- No DSTs or cores are planned at this time
- CBL w/ CCL from as far as gravity will let it fall to TOC

List of open and cased hole logs run in the well:

CBL,GR,MWD,MUDLOG

Well Name: UNCLE CHES 2116 FED COM Well Number: 233H

Coring operation description for the well:

NA

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 6110 Anticipated Surface Pressure: 3421.16

Anticipated Bottom Hole Temperature(F): 170

Anticipated abnormal pressures, temperatures, or potential geologic hazards? NO

Describe:

Contingency Plans geoharzards description:

Contingency Plans geohazards attachment:

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations plan:

H2S_Emergency_Contacts_20181004142259.docx

MRC_Energy_Co__Drilling_Contingency_plan_20181004142300.doc

Matador_Hydrogen_Sulfide_Drilling_Uncle_Ches_20181004142300.docx

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

Matador_UncleChesFed_233H_PrelimA_20181004142130.PDF

Matador_UncleChesFed_233H_PrelimA_WPReport_20181004142130.pdf

Matador_UncleChesFed_233H_PrelimA_ACReport_20181009132148.pdf

Other proposed operations facets description:

Other proposed operations facets attachment:

Other Variance attachment:

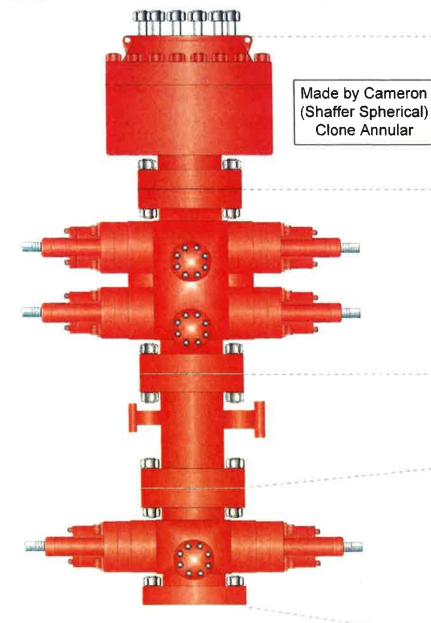
4_String_Wellhead_Diagram_20181004142159.pdf
Close_Loop_System_20181004142216.docx
Uncle_Ches_Fed__233H_MTDR_Drill_Plan_4.13.20_20200413164958.pdf



Exhibit E-1: BOP Uncle Ches Fed Com #233H Matador Resources Company

RIG:

809



PATTERSON-UTI # PS2-628

STYLE: New Shaffer Spherical

BORE 13 5/8" PRESSURE 5,000

HEIGHT: 48 ½" WEIGHT: 13,800 lbs

PATTERSON-UTI # PC2-128

STYLE: New Cameron Type U

BORE 13 5/8" PRESSURE 10,000

RAMS: TOP 5" Pipe BTM Blinds

HEIGHT: 66 5/8" WEIGHT: 24,000 lbs

DSA _____4" 10M x 2" 10M

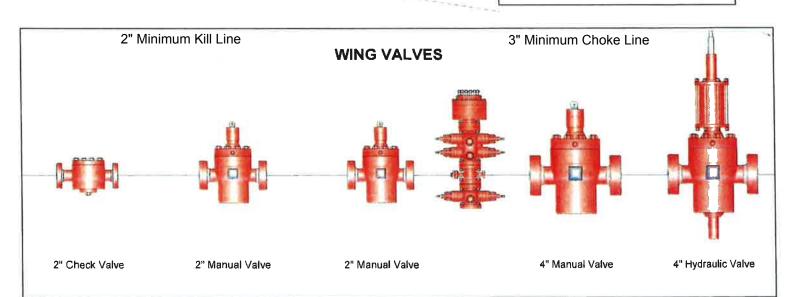
PATTERSON-UTI # PC2-228

STYLE: New Cameron Type U

BORE 13 5/8" PRESSURE 10,000

RAMS: 5" Pipe

HEIGHT: 41 5/8" WEIGHT: 13,000 lbs



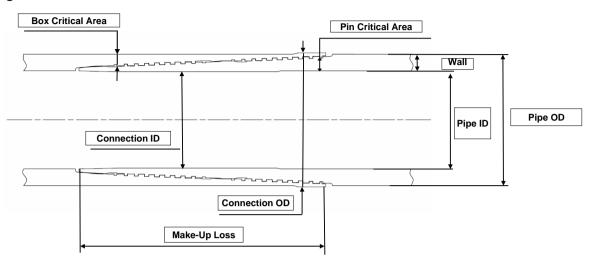
CONNECTION DATA SHEET (Imperial Units)



Connection: VAM® HTF-NR 7,625" 29,70# P110EC

Alternate Drift: 6.750"

Drawing: PD-101836P PD-101836B Isolated connection



OD WEIGHT WALL GRADE API DRIFT 7,625" 29,70 lb/ft 0,375" P110EC 6,750"

	DY PROP	ERTIES:	CONNECT	ION PR	OPER1	TES:
Outside Diameter	inch	7,625	Connection OD (nom)	inch		7,701
Internal Diameter	inch	6,875	Connection ID	inch		6,782
			Coupling Length	inch		N/A
Nominal Area	sqin.	8,541	Make-up Loss	inch		4,657
			Box critical area	%PBYS		58%
			Pin critical area	%PBYS		67%
Yield Strength	klb	1 068	Yield Strength	klb		619
Ultimate Strength	klb	1 153	Ultimate strength	klb		669
			Structural compression	klb		776
			Compression with sealability	klb		371
MIYP	psi	10 760	MIYP	psi		10 760
Collapse Pressure	psi	5 670	Ext Pressure Resistance	psi		5 670
			Regular Make-up Torque	ft.lb		
				Min		9 600
				Opt		11 300
				Max		13 000
			Maximum Torque with Seal	ability	ft.lb	58 500
			Maximum Torsional Value		ft.lb	73 000

uk@vamfieldservice.com dubai@vamfieldservice.com angola@vamfieldservice.com singapore@vamfieldservice.com



usa@vamfieldservice.com brazil@vamfieldservice.com canada@vamfieldservice.com mexico@vamfieldservice.com

80 VAM Specialists available worldwide 24/7 for Rig Site Assistance



Designed by : X. MENCAGLIA

Reference: VRCC16-1177

Revision: 0

Date : July 19, 2016

For the latest performance data, always visit our website: www.tenaris.com

July 15 2015



Size: 5.500 in. **Wall**: 0.361 in.

Weight: 20.00 lbs/ft

Grade: P110-IC Min. Wall Thickness: 87.5 %

Connection: TenarisXP™ BTC **Casing/Tubing**: CAS

Coupling Option: REGULAR

		PIPE BODY	DATA		
		GEOMET	RY		
Nominal OD	5.500 in,	Nominal Weight	20.00 lbs/ft	Standard Drift Diameter	4.653 in,
Nominal ID	4.778 in.	Wall Thickness	0.361 in.	Special Drift Diameter	N/A
Plain End Weight	19.83 lbs/ft				
		PERFORM	ANCE		
Body Yield Strength	641 x 1000 lbs	Internal Yield	12630 psi	SMYS	110000 psi
Collapse	12100 psi				
	TER	NARISXP™ BTC CO	NNECTION D	ΔΤΔ	
49-11		GEOMET			
Connection OD	6.100 in.	Coupling Length	9.450 ln.	Connection ID	4.766 in.
Critical Section Area	5.828 sq. in.	Threads per in.	5.00	Make-Up Loss	4.204 in.
		PERFORM	ANCE		
Tension Efficiency	100 %	Joint Yield Strength	641 x 1000 lbs	Internal Pressure Capacity(1)	12630 psi
Structural Compression Efficiency	100 %	Structural Compression Strength	641 x 1000 lbs	Structural Bending ⁽²⁾	92 °/100 ft
External Pressure Capacity	12100 psi				
	E	STIMATED MAKE-	UP TORQUES	3)	
Minimum	11270 ft-lbs	Optimum	12520 ft-lbs	Maximum	13770 ft-lbs
		OPERATIONAL LI	MIT TORQUES	.	
Operating Torque	21500 ft-lbs	Yield Torque	23900 ft-lbs		

Grade

TXP® BTC Printed on: 05/26/2017



Outside Diameter 5.500 in. Min. Wall 87.5% Thickness

Wall Thickness 0.361 in. Connection OD

Option

P110-ICY* Drift API Standard

Type Casing

REGULAR

(*) Grade P110-ICY

COUPLING

Y

Body: White 1st Band: Pale Green

2nd Band: -3rd Band: -



PIPE BODY

1st Band: White 2nd Band: Pale Green 3rd Band: Pale Green 4th Band: -

GEOMETRY					
Nominal OD	5.500 in,	Nominal Weight	20 lbs/ft	Drift	4.653 in.
Nominal ID	4,778 in.	Wall Thickness	0.361 in.	Plain End Weight	19.83 lbs/ft
OD Tolerance	API				
PERFORMANCE					
Body Yield Strength	729 x1000 lbs	Internal Yield	14360 psi	SMYS	125000 psi
Collapse	12100 psi				
CONNECTION DATA					
GEOMETRY					
Connection OD	6.100 in.	Coupling Length	9.45 in.	Connection ID	4.766 in.
Make-up Loss	4.204 in _e	Threads per in	5	Connection OD Option	REGULAR
PERFORMANCE					
Tension Efficiency	100 %	Joint Yield Strength	729,000 x1000 lbs	Internal Pressure Capacity [1]	14360.000 psi
Compression Efficiency	100 %	Compression Strength	729.000 ×1000 lbs	Max. Allowable Bending	104 °/100 ft
External Pressure Capacity	12100.000 psi				
MAKE-UP TORQUES					
<i>l</i> inimum	11540 ft-lbs	Optimum	12820 ft-lbs	Maximum	14100 ft-lbs
OPERATION LIMIT TO	ORQUES				
Operating Torque	22700 ft-lbs	Yield Torque	25250 ft-lbs		

Notes

This connection is fully interchangeable with:

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Production Casing

Collapse: DF_c=1.125

• Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered.

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

• Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
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Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

 Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

 Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
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Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

• Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

• Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
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Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DFc=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

• Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Exhibit E-6: H2S Contingency Plan Emergency Contacts Uncle Ches Fed Com #233H

Matador Resources Company
UL: O, Sec. 21, 20S, 35E
Lea Co, NM

Company Office			
Matador Resources Company	(972)-371-5200		
Key Personnel			
Name	Title	Office	Mobile
Billy Goodwin	Vice President Drilling	972-371-5210	817-522-2928
Dee Smith	Drilling Superintendent	972-371-5447	972-822-1010
Toby Solis	Drilling Superintendent		817-372-7817
Patrick Walsh	Drilling Engineer Construction	972-371-5291	626-318-5808
Jimmy Benefield	Superintendent		318-548-6659
<u>Artesia</u>			
Ambulance		911	
State Police		575-746-2703	
City Police		575-746-2703	
Sheriff's Office		575-746-9888	
Fire Department		575-746-2701	
Local Emergency Planning Commit	tee	575-746-2122	
New Mexico Oil Conservation Divis	ion	575-748-1283	
Carlsbad			
Ambulance		911	
State Police		575-885-3137	
City Police		575-885-2111	
Sheriff's Office		575-887-7551	
Fire Department		575-887-3798	
Local Emergency Planning Committee		575-887-6544	
New Mexico Oil Conservation Division		575-887-6544	
Santa Fe			
New Mexico Emergency Response Comission (Santa Fe)		505-476-9600	
New Mexico Emergency Response Comission (Santa Fe) 24 hrs		505-827-9126	
New Mexico State Emergency Ope	rations Center	505-476-9635	
<u>National</u>			
National Emegency Response Cen	ter (Washington, D.C.)	800-424-8802	
<u>Medical</u>			
Flight for Life- 4000 24th St.; Lubbock, TX		806-743-9911	
Aerocare- R3, Box 49F; Lubbock, TX		806-747-8923	
Med Flight Air Amb- 2301 Yale Blvd S.E., D3; Albuquerque, NM		505-842-4433	
SB Air Med Service- 2505 Clark Ca NM	rr Loop S.E.; Albuquerque,	505-842-4949	
Other			
Boots & Coots IWC		800-256-9688	or 281-931- 8884 or 432-563-
Cudd Pressure Control		432-699-0139	3356
Haliburton		575-746-2757	

B.J. Services 575-746-3569

HYDROGEN SULFIDE CONTINGENCY PLAN Drilling, Testing, & Completion

MRC ENERGY CO.

Uncle Ches Fed Com #233H

Reviewers	Operations Manager
	Operations Supt.
	Staff RES
	Field Supv.
	Engineering

Latitude: 32.5519" N Longitude: 103.4646" W

(Surface Location)

H2S Contingency Plan # 0165 Revision# 0

This H2S Contingency Plan is subject to updating

Effective date: July 8, 2015

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INTRODUCTION

The H2S equipment will be rigged up 2 days prior to reaching a potential H2S containing zone. Drilling into any potential H2S zone shall not commence until the on-site MRC Drilling Supervisor has confirmed this plan in place.

The onsite Drilling Foreman will give Total Safety one week (7 days) notice to prepare for rig up of H2S equipment)

To be effective, the plan requires the cooperation and effort of each person participating in the drilling of an H_2S well. Each person must know his/her responsibilities and all emergency and safety procedures. He/she should thoroughly understand and be able to use with accuracy, all safety equipment while performing his/her normal duties, if the circumstance should arise. He/she should therefore familiarize himself/herself with the location of all safety equipment and check to see that it is properly stored, easily accessible at all times, and routinely maintained.

It is the intention of MRC ENERGY CO. and the Drilling Contractor to make every effort to provide adequate safeguards against harm to persons on the rig and in the immediate vicinity from the effects of hydrogen sulfide, which may be released into the atmosphere under emergency conditions. However, the initiative rests with the individual in utilizing the safeguards provided. The ideas and suggestions of the individuals involved in the drilling of this well are highly welcomed and act as a fundamental tool for providing the safest working conditions possible.

The drilling representative is required to enforce these procedures. They are set up for your safety and the safety of all others.

II. PURPOSE

It is MRC Energy Co.'s intent to provide a safe working place, not only for its employees, but also for other contractors who are aiding in the drilling of this well. The safety of the general public is of utmost concern. All precautions will be taken to keep a safe working environment and protect the public.

There is a possibility of encountering toxic hydrogen sulfide gas. Safety procedures must be adhered to in order to protect all personnel connected with the operations as well as people living within the area.

The MRC Energy Co. representative will enforce all aspects of the H2S Contingency Plan. This job will become easier by a careful study of the following pages and training and informing all personnel that will be working on the well, their duties and responsibilities.

A. OPERATING PROCEDURES

DEFINITIONS:

For purpose of this plan, on-site personnel shall be referred to as "In Scope Personnel" or "Out of Scope Personnel", per the following definitions:

In Scope Personnel – Personnel who will be working or otherwise present in potential H2S release areas, including the rig floor, cellar, pits, and shaker areas.

Out of Scope Personnel – Personnel who will not be working or Otherwise present in potential H2S areas. Such personnel include rig Site visitor, delivery and camp services personnel.

GENERAL:

Before this H₂S contingency plan becomes operational, all regularly assigned In Scope Personnel (primarily the MRC, drilling contractor, and certain service personnel,) shall be thoroughly trained in the use of breathing equipment, emergency procedures, and responsibilities. Total Safety Technician or a designee assigned by the MRC Drilling Foreman shall keep a list of all personnel who have been through the on-site H₂S training program at the drill site.

All In Scope Personnel shall be given H2S training and the steps to be taken during H2S conditions under which the well may be drilled. General information will be explained about toxic gases, as well as the physiological effects of H₂S and the various classified operating conditions. In addition, the reader will be informed his/her general responsibility concerning safety equipment and emergency procedures.

The Total Safety H₂S Safety Technician or MRC on-site RSE Technician shall make available the H2S Contingency Plan for all personnel to review.

Without exception, all personnel that arrive on location must proceed directly to and sign-in with the on-site MRC RSE Technician. In Scope Personnel will be required to complete an on-site H2S training and respirator fit testing before starting work, or produce evidence that they have received equivalent training. Out of Scope Personnel will be required to complete a site H2S awareness and general safety briefing. This

briefing will consist of a H2S hazard overview, alarm review and required response to alarms.

B. PROCEDURES TO BE INITIATED PRIOR TO H2S CONTINGENCY PLAN COMPLIANCE:

A list of emergency phone numbers and contacts will be on location and posted at the following locations:

- 1. MRC ENERGY CO.'S Representative's Office
- 2. Drilling Contractor's, Toolpusher Office
- 3. Living Quarters Area

All safety equipment and H₂S related hardware must be set up as required by MRC Energy Co. with regard to location of briefing areas, breathing equipment, etc. All safety equipment must be inspected periodically (at least weekly) with particular attention to resuscitators and breathing equipment.

In Scope Personnel working in the well site area will be assigned breathing apparatus. Operator and drilling contractor personnel required to work in the following areas will be provided with Self Contained Breathing Apparatus:

- 1. Rig Floor
- 2. Mud Pits
- 3. Derrick
- 4. Shale Shaker
- 5. Cellar

The Total Safety H₂S Safety Technician will be responsible for rigging up all H₂S continuous monitoring-type detectors. The Total Safety Technician will monitor and bump test the detector units periodically (at least at least once a week to test alarm function during drilling conditions. In the event H₂S is detected, or when drilling in a zone confirmed to contain H₂S, the units shall be bump tested at least once every 24 hours. A bump test/calibration log will be kept on location. All results will be reported to the MRC on-site Drilling Foreman.

All Total Safety H2S equipment will be maintained and inspected by a Total Safety Technician on at least a Weekly basis.

C. DRILLING BELOW CONTINGENCY PLAN DEPTH

H2S response drills will be held at least once per week if possible or as often as necessary to acquaint the crews and service company personnel of their responsibilities and the proper procedures to shut-in a well. Initial drills will be performed until crews demonstrate competency donning and working under mask. After the MRC Energy Co.'s representative is satisfied with initial blowout drill procedures, a drill will be conducted weekly with each crew, as necessary. The H2S Safety Technician or designee will conduct safety talks and maintain the safety equipment, consult and carry out the instructions of the drilling supervisor. All personnel allowed in the well work area during drilling or testing operations will be instructed in the use of breathing equipment until supervisory personnel are satisfied that they are capable of using it.

After familiarization, each person must perform a drill with breathing equipment. The drill should include getting the breathing equipment, donning the breathing apparatus, and performing expected duties for a short period. A record shall be kept of all personnel drilled and the date of the drill. H2S training records will be kept on location for all personnel.

Rig crews and service company personnel shall be made aware of the location of spare air bottles, resuscitation equipment, portable fire extinguishers, H₂S monitors and detectors. Knowledge of the location of the H₂S monitors and detectors are vital in determining as our gas location and the severity of the emergency conditions.

After any device has initially detected H2S, all areas of poor ventilation shall be inspected periodically by means of a portable H₂S detector instrument. The buddy system will be utilized. (When an alarm sounds, personnel will don an SCBA, shut the well in, and proceed to SBA for roll call. The H2S Technician or designee will mask up, with a buddy and will verify source of H2S and report back to the on-site MRC Foreman.)

D. PROCEDURES PROGRAM

1. Drill Site

- a. The drilling rig will be located to allow prevailing winds to blow across the reserve pit.
- b. A Safe Briefing Area will be provided with a breathing air cascade trailer and or 30-minute SCBA's at the Primary Area. Personnel will assemble at the most up-wind station under alarm conditions, or when so ordered by the MRC Energy Co. representative, the Contractor representative, or the Total Safety H₂S Safety Technician. Windsocks or streamers will be anchored to various strategic places on a pole about 10 feet high, so it is in easy view from the rig floor at all times.
- c. Warning signs will be posted on the perimeters. "No Smoking" signs will be posted by MRC Energy Co.as well.
- d. One multi-channel automatic H₂S monitor will be provided by Total Safety and the detector heads will be at the shale shaker, bell nipple, mud pits, rig floor, and quarter's area. The monitor will be located inside HSE or Company man trailer. Should the alarm be shut off to silence the sirens, the blinker light must continue to warn of H₂S presence. The Total Safety H2S Safety Technician or designee will continuously monitor the detectors and will reactivate the alarm if H₂S concentrations increase to a dangerous level.
- e. A method of escape will be open at all times.
- f. If available, land line telephone service will be provided or cell phones provided. (Primary communications provided)
- g. A rig communication system will be provided, as needed.
- h. A gas trap, choke manifold, and degasser will be installed.
- i. A kill line, securely anchored and of ample strength, will be laid to the well-head from a safe location. This line is to be used only in an emergency.

General

- a. The MRC Energy Co. representative and/or the Contractor's Toolpusher will be available at all times. The drilling supervisor, while on duty, will have complete charge of the rig and location operations and will take whatever action is deemed necessary to insure personnel safety, to protect the well, and to prevent damage.
- b b. A Mud Engineer will be on location at all times when
 - c drilling takes place at the depth H₂S may be expected. The mud engineer will be able to verify the presence or absence of H2S.

III. CONDITIONS AND EMERGENCY PROCEDURES A. DEFINITION OF OPERATIONAL "CONDITIONS"

CONDITION I "POSSIBLE DANGER"

Warning Flags Green

Alarms No Alarm. Less than 10 ppm

Characterized By: Drilling operations in zones that may

contain hydrogen sulfide. This condition remains in effect unless H₂S is detected and it becomes necessary to go to Condition II.

General Action: a. Be alert for a condition change

b. Check all safety equipment for availability and proper functioning.

c. Perform all drills for familiarization

and proficiency.

CONDITION II "MODERATE DANGER"

Warning Flags Yellow

Alarms: Actuates at 10 ppm. Continuous flashing

light.

Characterized By: Drilling operations in zones containing

hydrogen sulfide. This condition will remain in effect until adding chemicals to the mud system neutralizes the hydrogen sulfide or it becomes necessary to go to

Condition III.

General Action: a. Be alert for a condition change

b. WHEN DRILLING AHEAD - Driller

and designated crewmember will don 30 min SCBA, shut-in the well and immediately proceed to the Safe

Briefing Area.

WHEN TRIPPING – Driller and two designated crewmembers will don 30 min SCBA, shut in the well and

immediately proceed to the Safe Briefing Area. The Derrickman will don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

- c. All In Scope Personnel will proceed directly to the appropriate Safe Briefing Area.
- d. Remain in safe briefing area, take roll call and wait for instructions
- e. Contact the Total H2S Technician if not on location.
- f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H₂S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases.
- g. All Out of Scope Personnel will report to the appropriate Safe Briefing Area.

CONDITION III "EXTREME DANGER"

Warning Flags Red

Alarms Actuate at 15 ppm. Continuous Sirens and

Flashing Lights

Characterized by: Critical well operations which pose an

immediate threat of H₂S exposure to on-site personnel and a potential threat to the

public.

General Action: a. WHEN DRILLING AHEAD -

Driller and designated crewmember will don 30 min SCBA, shut-in the

well and immediately proceed to the Safe Briefing Area.

WHEN TRIPPING – Driller and two designated crewmembers will don 30 min SCBA, shut in the well and immediately proceed to the Safe Briefing Area. The Derrickman will don a 5-minute escape pack, descend to the rig floor, don a 30-min SCBA (if necessary) and immediately proceed to the Safe Briefing Area.

- All In Scope Personnel should don SCBA if nearby and immediately proceed to Safe Briefing Area. If SCBA in not nearby at time of alarm, DO NOT GO TOWARDS RIG AREA, but proceed directly to the Safe Briefing Area
- c. All out of Scope Personnel shall evacuate the location.
- d. Remain in the Safe Briefing Area, take roll call and wait for instructions.
- e. Contact the Total H2S Technician if not on location.
- f. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering an H₂S contaminated area to provide assistance to anyone who may be injured or overcome by toxic gases. Use the buddy system.
- g. Remain in safe briefing area, take roll call and wait for instructions.
- h. A cascade breathing air systems shall be mobilized and utilized to conduct

- any additional on rig work required to correct the H2S release condition.
- i. If well is ignited do not assume area is safe. SO2 is hazardous and not all H2S will burn.

H₂S EMERGENCY PROCEDURES; IN SCOPE PERSONNEL

A. Day To Day Drilling Operations

- 1. Upon discovering a release of H₂S gas in the ambient air by warning alarms or in any other way **Do Not Panic**.
- 2. Hold your breath donning the nearest Self Contained Breathing Apparatus and rapidly move up or across-wind away from the areas where H₂S sensing devices are in place, to the closest available safe briefing area. Continue to use breathing apparatus until it has been determined that the exposure of H₂S gas in the ambient air no longer exists. **Do Not Panic**!
- 3. Utilize the "Buddy System", i.e.; select and pair up each person participating in the drilling of an H₂S well prior to an emergency situation.
- 4. Help anyone who is overcome or affected by the H₂S gas by taking him/her up-wind out of the contaminated area. (This should be done utilizing an SCBA and with a buddy.)
- 5. Take necessary steps to confirm the release of the H₂S gas into the ambient air.
 - When an H2S alarm activates, two designated personnel using the buddy system, while wearing their self contained breathing apparatus, will determine by the read-out on the fixed monitor which sensing device has detected the release of the H₂S gas.
 - They will utilize the hand-held sniffer type device at the particular sensing point disclosed on the fixed monitor to corroborate the fact that H₂S gas has actually been released. This will rule out the possibility of a false alarm. This will be done with a buddy and under mask after reporting to the Safe Briefing Area for roll call and instructions by on-site MRC Foreman.

- 6. Refer to the Emergency Phone Numbers and call emergency personnel.
- 7. Take the necessary steps to suppress the release of H₂S gas into the ambient air. Comply with the MRC Energy Co. Representative to physically suppress the release of H₂S gas at the actual release point.
- 8. Check all of MRC Energy Co.'s monitoring devices and increase gasmonitoring activities with the portable hand-operated H₂S and gas detector units.

Do Not Panic!

The MRC Energy Co. representative will assess the situation and with assistance of the Contractor's Representative and Total Safety's H₂S Safety Technician or on site designee, will assign duties to each person to bring the situation under control.

B. RESPONSIBILITIES OF WELL-SITE PERSONNEL

In the event of a release of potentially hazardous amounts of H_2S , all personnel will immediately don their protective breathing apparatus, the well will be shut in and personnel will proceed upwind to the nearest designated safe briefing area for roll call and instructions by MRC Foreman. Consideration will be given to evacuating Out of Scope Personnel, as situation warrants.

1. MRC ENERGY CO.'S Well-site Representatives

- a. If MRC Energy Co.'s well-site representative is incapacitated or not on location, this responsibility will fall to the Toolpusher/Driller.
- b. Immediately upon assessing the situation, set this plan into Action by initiating the proper procedures to contain the gas and notify the appropriate people and agencies.
- c. Ensure that the alarm area indicated by the fixed H₂S Monitor is checked and verified with a portable H₂S detector. (Safety Technician if on location or MRC assigned designee with a buddy utilizing SCBA's)
- d. Consult Pusher/driller of remedial actions as needed.

- e. Ensure that non-essential personnel proceed to the safe briefing area.
- f. Ensure location entrance barricades are positioned. Keep the number of persons on location to a minimum during hazardous operations.
- g. Consult each contractor, Service Company and all others allowed to enter the site, that H2S gas may be encountered and the potential hazards that may exist.
- h. Authorize the evacuation of local residents if H_2S threatens Their safety.
 - i. Non essential personnel should be evacuated from location if Situation warrants.

2. Toolpusher

- a. Toolpusher/Driller will assume responsibilities of MRC Energy Co.'s well-site representative if that person is incapacitated or not on location.
- b. Ensure that the alarm area indicated by the fixed H₂S monitor is checked and verified with a portable H₂S gas detector. (Alarm area indicated by the monitor will be Checked by the H2S Technician and a buddy, under mask.) This will be done after checking in and roll call at the Upwind Safe Briefing Area.
- c. Confer with MRC Energy Co.'s well-site representative or superintendent and direct remedial action to suppress the H₂S and control the well.
- d. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- e. Ensure that personnel at the drill floor area are instructed on emergency actions required.
- f. Ensure that all personnel observe the appropriate safety and emergency procedures.

g. Ensure that all persons are accounted for and provided emergency assistance as necessary.

3. Mud Engineer

- a. Run a sulfide check on the flowline mud.
- b. Take steps to determine the source of the H_2S and suppress it. Lime and H_2S scavenger shall be added to the mud as necessary.

4. Total H₂S Safety Technician, if on location, or MRC Designee

- a. H2S Safety Technician or designee don nearest SCBA and report to Safe Briefing Area for roll call, take a buddy masked up and check monitor and verify with a portable H₂S detector the alarm area indicated by the fixed H₂S monitor. Advise the Toolpusher/Driller and MRC Energy Co.'s well-site representative of findings. Record all findings.
- b. If H₂S is flared, check for sulfur dioxide (SO₂) near the flare as necessary. Take hourly readings at different perimeters, log readings and record on location.
- c. Ensure that personnel at the safe briefing area are instructed on emergency actions required.
- d. Ensure that the appropriate warning flags are displayed.
- e. Ensure that all personnel are in S.C.B.A. as necessary.
- f. Ensure that all persons are accounted for and provide emergency assistance as necessary.

g. Be prepared to evacuate rig if order is issued.

5. General Personnel & Visitors

- a. All In Scope Personnel, if not specifically designated to shut the well in or control the well, shall proceed to the (upwind) safe briefing area. All Out of Scope Personnel shall immediately proceed to the appropriate (upwind) safe briefing area or evacuate the site as conditions warrant.
- b. During any emergency, use the "buddy" system to prevent anyone from entering or being left in a gas area alone, even wearing breathing apparatus.
- c. Provide assistance to anyone who may be injured or overcome by toxic gases. Personnel shall ensure that their breathing apparatus is properly fitted and operational before entering a potentially H₂S contaminated area.
- d. Remain in safe briefing area and wait for instructions.

C. INSTRUCTIONS FOR IGNITING THE WELL

1. The Toolpusher/Driller will confer with MRC Energy Co.'s well-site representative who will secure the approval of the "Texas Wells Delivery Manager, prior to igniting the well, if at all possible.

The Toolpusher/Driller will be responsible for igniting the well in the event of severe well control problems. This decision should be made only as a last resort in situations where it is clear that:

- a. Human life and property are endangered, or
- b. There is no hope of controlling the well under current conditions.
- 2. Once the decision has been made, the following procedures should be followed:

- a. Two people wearing self-contained breathing apparatus will be needed for the actual lighting of the well. They must first establish the flammable perimeter by using an explosimeter. This should be established at 30% to 40% of the lower flammable limits.
- b. After the flammable perimeter has been established and everyone removed from the area, the ignition team should select a site upwind of the well from which to ignite the well. This site should offer the maximum protection and have a clear path for retreat from the area.
- c. The ignition team should have safety belts and lifeline attached and manned before attempting ignition. If the leak is not ignited on the first attempt, move in 20 to 30 feet and fire again. Continue to monitor with the explosimeter and NEVER fire from an area with over 75% of the Lower Explosive Limit (LEL). If having trouble igniting the well, try firing 40 degrees to 90 degrees on either side of the well.
- d. If ignition is not possible due to the makeup of the gas, the toxic perimeter must be established and evacuation continued until the well is contained.
- e. All personnel must act only as directed by the person in charge of the operations.

NOTE: After the well is ignited, burning hydrogen sulfide (H₂S) will convert to sulfur dioxide (SO₂), which is also a highly toxic gas.

DO NOT ASSUME THE AREA IS SAFE AFTER THE WELL IS IGNITED

D. CORING PROCEDURES

Only essential personnel shall be on the rig floor. Ten (10) stands prior to retrieving core barrel; all personnel on drill floor and in derrick shall confirm self-Contained breathing apparatus available and ready for use.

A Total H2S Technician will don a SCBA with a buddy assigned from the rig crew, and continuously monitor for H2S at each connection. Any levels detected will require operations to be shut down and all involved

personnel to don SCBAs. Precautions will remain in place until barrel is laid down.

All involved personnel will don SCBAs when removing the inner barrel from the outer barrel. SCBAs can be removed once the absence of H2S in confirmed by the Total H2S Technician.

Cores will be appropriately marked and sealed for transportation.

Normal Operations

1. Responsibilities of well-site personnel

a. Well-site Representative

- 1. Notify H₂S Technician of expected date to reach Contingency Plan implementation depth (Two (2) days prior to reaching suspected H₂S bearing zone) or prior to starting well work.
- 2. Ensure H₂S Safety Technician completes rig-up procedures prior to reaching Contingency Plan effective depth.
- 3. Restrict the number of personnel at the drilling rig or well site to a minimum while drilling, starting well work, testing or coring.
- 4. Ensure weekly H₂S drills/training are performed, if possible.

B. Toolpusher

- 1. Ensure that necessary H₂S safety equipment is provided on the rig, and that it is properly inspected and maintained.
- 2. Ensure that all personnel that work in the well area, are thoroughly trained in the use of H₂S safety

equipment and periodic drills are held to maintain an adequate level of proficiency.

C. In Scope Personnel

- 1. Remain clean-shaven. Beards and long sideburns do not allow a proper facepiece seal.
- 2. Receive H₂S safety training on location, or confirm prior training by certification that is one year within date.
- 3. Familiarize yourself with the rig's Contingency Plan.
- 4. Inspect and practice putting on your breathing apparatus.
- 5. Know the location of the "safe briefing areas".
- 6. Keep yourself "wind conscious". Be prepared to quickly move upwind and away in the event of any emergency involving release of H₂S.

D. Total Safety H₂S Safety Technician or MRC Designee

- 1. Conduct training as necessary to ensure all personnel working in well area are familiar with the contingency procedures and the operation of emergency equipment.
- 2. Check all H₂S safety equipment to ensure that it is ready for emergency use:
 - Check pressure weekly for each shift on breathing apparatus (both 30-minute and hippacks) to make sure they are charged to full volume.
 - Check pressure on cascade air bottles, if on location, to see that they are capable of recharging breathing apparatus.

- Check oxygen resuscitator, if on location, to ensure that it is charged to full volume.
- Check H₂S detectors weekly for each shift (fixed and portable), and explosimeter, to ensure they are working properly.
- 3. Provide a weekly report to MRC Energy Co.'s well-site representative documenting:
 - Calibrations performed on H₂S detectors.
 - Proper location and working order of H₂S safety equipment.
 - Attendance of all personnel, trained or retrained, and their company.
 - Weekly drills, if held and a list of personnel participating and summary of actions.

OUT OF SCOPE PERSONNEL

MRC Energy Co. policy will not require Out of Scope Personnel to be clean shaven, have processed medical questionnaires, fit testing, or have certified H2S Training.

SAFETY EQUIPMENT

All respirators will be designed, selected, used and maintained in conformance with ANSI Z88.2, American National Standard for respiratory protection.

Personal protective equipment must be provided and used. Those who are expected to use respiratory equipment in case of an emergency will be carefully instructed in the proper use and told why the equipment is being used. Careful attention will be given to the minute details in order to avoid possible misuse of the equipment during periods of extreme stress.

Self-contained breathing apparatus provides complete respiratory and eye protection in any concentration of toxic gases and under any condition of oxygen deficiency. The wearer is independent of the surrounding atmosphere because he/she is breathing with a system admitting no outside air. It consists of a full face mask, breathing tube, pressure demand regulator, air supply cylinder, and harness. Pure breathing air from the supply cylinder flows to the mask automatically through the pressure demand regulator which reduces the pressure to a breathing level. Upon inhalation, air flows into the mask at a rate precisely regulated to the user's demand. Upon exhalation, the flow to the mask stops and the exhaled breath passes through a valve in the face piece to the surrounding atmosphere. The apparatus includes an alarm & gauge which warns the wearer to leave the contaminated area for a new cylinder of air or cylinder refill.

The derrickman is provided with a full face piece unit attached to a 5– minute escape cylinder. He will also have his own self-contained 30-minute unit breathing apparatus located on the drilling floor. He will use the 5-minute unit to exit the derrick to the floor, donning the 30-minute unit located on the floor, if needed.

All respiratory protective equipment, when not in use, should be stored in a clean, cool, dry place, and out of direct sunlight to retard the deterioration of rubber parts. After each use, the mask assembly will be scrubbed with soap and water, rinsed thoroughly, and dried. Air cylinders can be recharged to a full condition from a cascade system.

Personnel in each crew will be trained in the proper techniques of bottle filling.

The primary piece of equipment to be utilized, should anyone be overcome by hydrogen sulfide, is the oxygen resuscitator, if on location.

When asphyxiation occurs, the victim must be moved to fresh air and immediately given artificial respiration. In order to assure readiness, the bottles of oxygen will be checked at regular intervals and an extra tank kept on hand.

Hand-operated pump-type detectors incorporating detector tubes will give more accurate readings of hydrogen sulfide. The pump-type draws air to be tested through the detector

tube containing lead acetate-silica gel granules. Presence of hydrogen sulfide in the air sample is shown by the development of a dark brown stain on the granules, which is the scale reading of the concentration of hydrogen sulfide. By changing the type of detector tube used, this detector may also be used for sulfur dioxide (SO_2) detection when hydrogen sulfide (H_2S) is being burned in the flare area.

Provisions must be made for the storage of all safety equipment as is evident from the foregoing discussion. All equipment must be stored in an available location so that anyone engaged in normal work situations is no more than "one breath away' from a mask.

V – TOXICITY OF VARIOUS GASES

Lothol	Chemical	Specific		
Lethal Common Name ppm ⁴	Formula	Gravity ¹	PEL (OSHA) ²	STEL ³
Hydrogen Cyanide 300	HCN	0.94	10	150
Hydrogen Sulfide 600	H ₂ S	1.18	20 Pea	ak- 50ppm
Note: The ACGIH(7) re	commends a TW	A(6) value of 10	opm as the TLV(5) for	H2S and an STEL of
15ppm. Sulfur Dioxide 1000	SO ₂	2.21	2	5 ppm
Chlorine	CL_2	2.45	1	
Carbon Monoxide 1000	СО	0.97	35	200/1 Hour
Carbon Dioxide 10%	CO ₂	1.52	5000	5%
Methane	CH ₄	0.55	90000	

¹ Air = 1.0

TLV – Threshold Limit Value; a concentration recommended by the American Conference of Governmental Industrial Hygienists (ACGIH)

TWA – Time Weighted Average; the average concentration of contaminant one can be exposed to over a given eight-hour period.

ACGIH – (American Conference of Governmental Industrial Hygienists) is an organization comprised of Occupational Health Professionals believed

² Permissible - Concentration at which is believed that all workers may repeatedly be exposed, day after day, without adverse effect.

³ **STEL -** Short Term Exposure Limit. A 15-minute time weighted average.

⁴ **Lethal -** Concentration that will cause death with short-term exposure.

by many to be the top experts in the field of Industrial Hygiene. They are recognized as an expert rexource by OSHA. The ACGIH releases a biannual publication "Threshold Limit Values and Biological Indices" that many safety professionals consider to be the authoritative document on airborne contaminants.

Reference: API RP-49, September 1974 - Reissued August 1978

VI. PROPERTIES OF GASES

A. <u>CARBON DIOXIDE</u>

- 1. Carbon Dioxide (CO₂) is usually considered inert and is commonly used to extinguish fires. It is 1.52 times heavier than air and will concentrate in low areas of still air. Humans cannot breathe air containing more than 10% CO₂ without losing conscience or becoming disorientation in a few minutes. Continued exposure to CO₂ after being affected will cause convulsions, coma, and respiratory failure.
- 2. The threshold limit of CO_2 is 5000 ppm. Short-term exposure to 50,000 ppm (5%) is reasonable. This gas is colorless, odorless, and can be tolerated in relatively high concentrations.

B. <u>HYDROGEN SULFIDE</u>

- 1. Hydrogen Sulfide (H_2S) is a colorless, transparent, flammable gas. It is heavier than air and, hence, may accumulate in low places.
- 2. Although the slightest presence of H₂S in the air is normally detectable by its characteristic "rotten egg" odor, it is dangerous to rely on the odor as a means of detecting excessive concentrations because the sense of smell is rapidly lost, allowing lethal concentrations to be accumulated without warning. The following table indicates the poisonous nature of H₂S.

CONCENTRATION		TRATION	EFFECTS	
% H ₂ S	PPM	GR/100 SCF ¹		
0.001	10	.65	Safe for 8 hours without respirator. Obvious and unpleasant odor.	
0.0015	15	0.975	Safe for 15 minutes of exposure without respirator.	
0.01	100	6.48	Kills smell in 3-15 minutes; may sting eyes and throat.	
0.02	200	12.96	Kills smell quickly; stings eyes and throat.	
0.05	500	32.96	Dizziness; breathing ceases in a few minutes; need prompt artificial respiration.	
0.07	700	45.92	Rapid Unconsciousness; death will result if not rescued promptly.	
0.1	1000	64.80	Instant unconsciousness, followed by death within	

			minutes.	
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¹ Grains per 100 Cubic Feet

VII. Treatment Procedures for Hydrogen Sulfide Poisoning

- A. Remove the victim to fresh air.
- B. If breathing has ceased or is labored, begin resuscitation immediately.

Note: This is the quickest and preferred method of clearing victim's lungs of contaminated air; however, under disaster conditions, it may not be practical to move the victim to fresh air. In such instances, where those rendering first aid must continue to wear masks, a resuscitator should be used.

- C. Apply resuscitator to help purge H₂S from the blood stream.
- D. Keep the victim at rest and prevent chilling.
- E. Get victim under physician's care as soon as possible.

C. SULPHUR DIOXIDE

- 1. Sulfur Dioxide (SO₂) is a colorless, non-flammable, transparent gas.
- 2. SO₂ is produced during the burning of H₂S. Although SO₂ is heavier than air, it can be picked up by a breeze and carried downwind at elevated temperatures. Since SO₂ is extremely irritating to the eyes and mucous membranes of the upper respiratory tract, it has exceptionally good warning powers in this respect. The following table indicates the toxic nature of SO₂:

CONCEN	TRATION	EFFECTS
% SO ₂	PPM	
0.0005	3 to 5	Pungent odor, normally a person can detect SO ₂ in this range.
0.0012	12	Throat irritation, coughing, constriction of the chest, tearing and smarting of eyes.
0.015	150	So irritating that it can only be endured for a few minutes.
.05	500	Causes a sense of suffocation, event with the first

	breath.

VIII. BREATHING AIR EQUIPMENT DRILLS FOR ON & OFF DUTY PERSONNEL

An H₂S Drill and Training Session must be given once a week to ALL on-duty personnel with off duty personnel. On-duty and Off-duty personnel will reverse roles on alternate drills. An H₂S drill and training session must be given once a week to all off-duty personnel in coincidence with on-duty personnel reversing roles on alternate drills.

The purpose of this drill is to instruct the crews in the operation and use of breathing air and H_2S related emergency equipment and to allow the personnel to become acquainted with using the equipment under working conditions. The crews should be trained to put on the breathing air equipment within one minute when required or requested to do so.

The following procedure should be used for weekly drills. The MRC supervisor must be satisfied that the crews are proficient with the equipment.

- 1. All personnel should be informed that a drill will be held.
- 2. The Total H2S Safety Technician or a designee assigned by the MRC Drilling Foreman should initiate the drill by signaling as he/she would if H2S was detected.
- 3. Personnel should don their breathing apparatus.
- 4. Once the breathing air equipment is on, the H2S Technician should check all personnel to insure proper operation.

A training and information session will be conducted after each drill to answer any H_2S related questions and to cover any gaps identified from one of the following topics:

- · Condition II, and III alerts and steps to be taken by all personnel.
- The importance of wind direction when dealing with H_2S .
- · Proper use and storage of all types of breathing equipment.
- · Proper use and storage of oxygen resuscitators.
- · Proper use and storage of H₂S detectors (Mini Checks or equivalent).
- The "buddy system" and the procedure for rescuing a person overcome by H_2S .
- Responsibilities and duties.
- · Location of H₂S safety equipment.
- · Other parts of the "H₂S Contingency Plan" that should be reviewed.

NOTE: A record of attendance must be kept for weekly drills and training sessions.

IX. HYDROGEN SULFIDE TRAINING CURRICULUM

(FOR EMPLOYERS, VISITORS, AND CONTRACTORS)

EACH PERSON WILL BE INFORMED ON THE RESTRICTIONS OF HAVING BEARDS AND CONTACT LENS. THEY WILL ALSO BE INFORMED OF THE AVAILABILITY OF SPECTACLE KITS.

AFTER THE H2S EQUIPMENT IS RIGGED UP, ALL IN SCOPE PERSONNEL WILL BE H2S TRAINED AND PUT THROUGH A DRILL. ANY DEFICIENCIES WILL BE CORRECTED.

Training Completion cards are good for one year and will indicate date of completion or expiration. Personnel previously trained on another facility and visiting, must attend a "supplemental briefing" on H2S equipment and procedures before beginning duty. Visitors who remain on the location more than 24 hours must receive full H2S training given all crew members. A "supplemental briefing" will include but not be limited to: Location of respirators, familiarization with safe briefing areas, alarms with instruction on responsibilities in the event of a release and hazards of H2S and (SO2, if applicable). A training and drill log will be kept.

Topics for full H2S training shall include the following equipment if on location, but not be limited to the following:

1. **Brief Introduction on H2S**

- A. Slide or Computer presentation (If Available)
- B. H2S material will be distributed
- C. Re-emphasize the properties, toxicity, and hazards of H2S
- D. Source of SO2 (if applicable)

2. **H2S Detection**

- A. Description of H2S sensors
- B. Description of warning system (how it works & it's location)
- C. Actual location of H2S sensors
- D. Instruction on use of pump type detector (Gastec)
- E. Use of card detectors, ampoules, or dosimeters
- F. Use of combustible gas detector
- G. Other personnel detectors used
- H. Alarm conditions I & II,
- I. SO2 alarms (if applicable)

3. **H2S Protection**

- A. Types of breathing apparatus provided (30-minute SCBA & 5-minute SCBA (with voice diaphragms for communication if supplied)
- B. Principle of how breathing apparatus works
- C. Demonstration on how to use breathing apparatus
- D. Location of breathing apparatus

4. Cascade System

- A. Description of cascade system
- B. How system works
- C. Cascade location of rig with reference to briefing areas
- D. How to use cascade system (with 5-minute hose work line units & refill, if supplied)
- E. Importance of wind direction and actual location of Windsocks
- F. Purpose of compressor/function (if one is on site)

5. **H2S Rescue and First Aid**

- A. Importance of wind direction
- B. Safe briefing area
- C. Buddy system
- D. H2S symptoms
- E. Methods of rescue

6. **Hands on Training**

- A. Donning/familiarization of SCBA 30-minue unit
- B. Donning/familiarization of SKADA 5- MIN. Packs
- C. Familiarization of cascades
- D. Use of O2 resuscitator
- E. Alarm conditions upwind briefing areas, etc...
- F. Duties and responsibilities of all personnel
- G. Procedures for evacuation
- H. Search and Rescue teams

7. **Certification**

A. Testing on material covered

TOTAL SAFETY US INC., FIT TEST

X. EMPLOYEE INFORMATION

Employee Na	Employee Name: Date:				
Date of Emplo	oyee Medical F	Evaluation:		<u> </u>	
Medical Statu	s (circle):	Unrestricted	Limitations or	n Use Use Not	Authorized
RESPIRATO	R INFORMAT	IOIN			
Respirator Ty	pe (Dustmask,	SCBA, etc):			
Brand:					
Size: (circle):	XS	S	M	L	XL
FIT TEST INF	FORMATION				
Type of Fit Te	est Performed:				
Quan	Porta Count		F	it Factor:	
	Fittester 3000)		it Factor:	
<u>Quali</u>					
	Irritant Smok		Passed / I		
	Saccharin	tate (Banana Oil)	Passed /]	raned Passed / Failed	
	Bitrex			Passed / Failed	
I hereby certify that the found in Appendix A		conducted in accord	lance with the O	SHA Fit Testir	g Protocols
Fit Tester Name (Prin	t):				
Signature:				Date:	

XI. H₂S SAFETY SERVICES

HYDROGEN SULFIDE SAFETY PACKAGE – Contained on location in Total Safety H2S Equipment Trailer, unless otherwise noted:

RESPIRATORY SAFETY SYSTEMS

QTY DESCRIPTION

- 30-Minute Pressure Demand SCBA (4-Primary Safe Briefing Area, 4-Secondary Safe Briefing Area, 4-floor with one of these for derrick man)
- 9 Hose Line 5-minute Work Unit w/Escape Cylinder (1 in derrick, 6 on drill floor, 1 in mud pit wt area, 1 in shaker area)

The following shall be part of the package if requested by the MRC Foremen (at least one trailer with cascade system is required to be located in the MRC Magnolia asset for use as needed)

- 1 Breathing air cascade of 10 bottles w/regulator
- 2 Refill lines to refill 30-minute units on location
- 6-Man manifold that can be rigged up to work area on floor, if needed
- 6 25 foot hose lines
- 2 50 foot hose lines
- 100 Feet of hose line to rig cascade up to 12 man manifold on floor
- 12 30-minute Self Contained Breathing apparatus

DETECTION AND ALARM SAFETY SYSTEM

- H2S Fixed Monitor w/8Channels (Loc determined at rig up) suggested. (Mud pit area, shaker area, bell nipple area, floor/driller area, & outside quarters)
- 5 H2S Sensors
- Explosion Proof Alarms (Light and Siren)
 (1 on floor, 1 in work area, 1 in trailer area where quarters are located)
- 2 Personal H2S monitors
- 1 Portable Tri-Gas Hand Held Meter (O2, LEL, H2S)
- 1 Sensidyne/Gastech Manual Pump Type Detector
- 8 Boxes H2S Tubes Various Ranges
- 2 Boxes SO2 Tubes Various Ranges
- 1 Calibration Gas
- 1 Set Paper Work for Records: Training, Cal, Inspection, other

ADDITIONAL SAFETY RELATED EQUIPMENT

QTY DESCRIPTION

- Windsocks with Pole and Bracket
- 1 Set Well Condition Sign w/Green, Yellow, Red Flags
- 1 Primary Safe Briefing Area Sign
- 1 Secondary Safe Briefing Area Sign
- 6 Operating Condition Signs for Work Areas & Living Quarters

TRAILER WITH BREATHING AIR CASCADE WILL ALSO INCLUDE THE FOLLOWING:

This equipment will be part of the H2S equipment stored in the trailer, when on location

- 1 First aid kit
- 1 Fire Blanket
- 1 Eye wash station
- 2 Safety Harness w/150' safety line

XII. EMERGENCY PHONE NUMBERS (Updated March 18, 2009)

EMERGENCY PHONE NUMBERS

MRC Energy Co. Emergency Phone #
MRC Energy Co. Permian Operations Phone-----MRC Energy Co. Production
113 Daw Rd
Mansfield LA 71052

Title	Names	Phone	Cell
Operations Manager			
Operation Supt.			
Operations			
Supervisor			
Operations			
Supervisor			
Office Supervisor			
HSE			
Scheduler Planner			

Hydrogen Sulfide Safety Consultants

_ • •		
Total Safety W. Bender	575-392-2973	After Hours 24 Hour Call
Blvd. Hobbs, NM		Center Through Office
		Number
Tommy Throckmorton	575-392-2973	940-268-9614
Operations Manager		
Rodney Jourdan Sales	575-392-2973	432-349-3928
Contact		

MRC Energy Co. MEDICAL RESPONSE PLAN AND IT'S MEDICAL PROTOCOLS WILL BE FOLLOWED

MEDICAL COORDINATOR # -----

Emergency Numbers & Directions

Hospitals (911)

Artesia General Hospital		
702 N. 13 th St.	Main Phone Number	575-748-3333
Artesia, NM 88210		
Nor-Lea General Hospital		
1600 N. Main Ave.	Main Phone Number	575-396-6611
Lovington, NM 88260		
Lea Regional Medical		
Center	Main Phone Number	575-492-5260
5419 N. Lovington Hwy		
Hobbs, NM 88240		
Carlsbad General Hospital		
2430 W. Pierce St.	Main Phone Number	575-887-4100
Carlsbad, NM		
Lovelace Regional Hospital		
117 E. 19 th St	Main Phone Number	575-627-7000
Roswell, NM 88201		
Winkler Co. Memorial		
Hospital	Main Phone Number	432-586-8299
821 Jeffee Dr.		
Kermit, Texas 79745		
Reeves County Hospital		
2323 Texas St.	Main Phone Number	432-447-3551
Pecos, Texas 79772		

State Police (911)

Office Number	432-377-2411
Office Number	432-586-3465
Office Number	432-447-3532
Office Number	575-748-9718
Office Number	575-885-3137
Office Number	575-392-5588
	Office Number Office Number Office Number

<u>Local Law Enforcement (911) (Sheriff)</u>

Reeves Co. Sheriff 500 N. Oak ST Pecos, Texas 79722	Office Number	432-445-4901
Winkler Co. Sheriff 1300 Bellaire St. Kermit, Texas 79745	Office Number	432-586-3461
Loving Co. Sheriff Courthouse Mentone, Texas	Office Number	432-377-2411

Lea Co. Sheriff		
1417 S. Commercial St.	Office Number	
Lovington, NM 88260		
Eddy Co. Sheriff		
305 N 7th St.	Office Number	575-766-9888
Artesia, NM 88210		
Eddy Co. Sheriff		
305 N 7th St.	Office Number	575-746-9888
Carlsbad, NM 88220		

Federal & State Agencies

OSHA Lubbock Area		
Office	Main Number	806-472-7681 EXT 7685
1205 Texas Av. Room 806		
Lubbock, Texas 79401		
New Mexico Environment		
Department	Joe Fresquez	575-623-3935
400 N Pennsylvania		
Roswell, NM 88201		
Texas Railroad		
Commission	Main Number	844-773-0305
Midland, Texas		
BLM Carlsbad, NM Field		
Office	Main Number	575-234-5972
620 E. Green ST		
Carlsbad, NM 88220		
BLM Hobbs Field Station		
414 W. Taylor Rd.	Main Number	575-393-3612
Hobbs, NM 88240		
BLM Roswell District		
Office	Main Number	575-627-0272
2909 W. Second St.		
Roswell, NM 88201		

TECQ Texas Commission on Environmental Quality	Main Number	800-832-8224
New Mexico OCD		
U.S. Environmental		
Protection Agency Region	Main Number	214-655-2222
6		
Texas/New Mexico		
National Response Center		
Toxic Chemicals & Oil	Main Number	800-424-8802
Spills		

Rig Company

g	

XIII. EVACUATION OF THE GENERAL PUBLIC

The procedure to be used in alerting nearby persons in the event of any occurrence that could pose a threat to life or property will be arranged and completed with public officials in detail, prior to drilling into the hydrogen sulfide formations.

In the event of an actual emergency, the following steps will be immediately taken:

- 1. The MRC Energy Co.'s representative will dispatch sufficient personnel to immediately warn each resident and transients down-wind within radius of exposure from the well site. Then warn all residence in the radius of exposure. Additional evacuation zones may be necessary as the situation warrants.
- 2. The MRC Energy Co.'s representative will immediately notify proper authorities, including the Sheriff's Office, Highway Patrol, and any other public officials as described above and will enlist their assistance in warning residents and transients in the calculated radius of exposure.
- 3. The MRC Energy Co.'s representative will dispatch sufficient personnel to divert traffic in the vicinity away from the potentially dangerous area. A

guard to the entrance of the well site will be posted to monitor essential and non essential traffic.

4. General:

- A. The area included within the radius of exposure is considered to be the zone of maximum potential hazard from a hydrogen sulfide gas escape. Immediate evacuation of public areas, in accordance with the provisions of this contingency plan, is imperative. When it is determined that conditions exist which create an additional area (beyond the initial zone of maximum potential hazard) vulnerable to possible hazard, public areas in the additional hazardous area will be evacuated in accordance with the contingency plan.
- B. In the event of a disaster, after the public areas have been evacuated and traffic stopped, it is expected that local civil authorities will have arrived and within a few hours will have assumed direction of and control of the public, including all public areas. MRC Energy Co. will cooperate with these authorities to the fullest extent and will exert every effort by careful advice to such authorities to prevent panic or rumors.
- C. MRC Energy Co. will dispatch appropriate management personnel at the disaster site as soon as possible. The company's personnel will cooperate with and provide such information to civil authorities as they might require.
- D. One of the products of the combustion of hydrogen sulfide is sulfur dioxide (SO₂). Under certain conditions this gas may be equally as dangerous as H₂S. A pump type detector device, which determines the percent of SO₂ in air through concentrations in ppm, will be available. Although normal air movement is sufficient to dissipate this material to safe levels, the SO₂ detector should be utilized to check concentrations in the proximity of the well once every hour, or as necessary and the situation warrants. Also, if any low areas are suspected of having high concentrations, personnel should be made aware of these areas, and steps should be taken to determine whether or not these low areas are hazardous.

Hydrogen Sulfide Drilling

Operations Plan

Matador Resources

1 H2S safety instructions to the following:

- Characteristics of H2S
- Physical effects and hazards
- Principal and operation of H2S detectors, warning system and briefing areas
- Evacuation procedures, routes and first aid
- Proper use of safety equipment & life support systems
- Essential personnel meeting medical evaluation criteria will receive additional training on the proper use of 30min pressure demand air packs

2 H2S Detection and Alarm Systems:

- H2S sensor/detectors to be located on the drilling rig floor, in the base of the sub structure / cellar area, on the mud pits in the shale shaker area. Additional H2S detectors may be placed as deemed necessary
- An audio alarm system will be installed on the derrick floor and in the doghouse

3 Windsocks and / Wind Streamers:

- Windsocks at mud pit area should be high enough to be visible
- Windsock on the rig floor and / top of doghouse should be high enough to be visible

4 Condition Flags and Signs:

- Warning sign on access road to location
- Flags to be displayed on sign at entrance to location
 - o Green Flag Normal Safe Operation Condition
 - o Yellow Flag Potential Pressure and Danger
 - o Red Flag Danger (H2S present in dangerous concentrations) Only H2S trained personnel admitted on location

5 Well Control Equipment:

See Exhibit E-1

6 Communication:

While working under masks chalkboards will be used for communications

- Hand signals will be used where chalk board is inappropriate
- Two way radio will be used to communicate off location in case of emergency help is required. In most cases cellular telephones will be available at most drilling foreman's trailer or living quarters.

7 <u>Drilling Stem Testing:</u>

No DST cores are planned at this time

8 Drilling contractor supervisor will be required to be familiar with the effects H2S has on tubulars good and other mechanical equipment

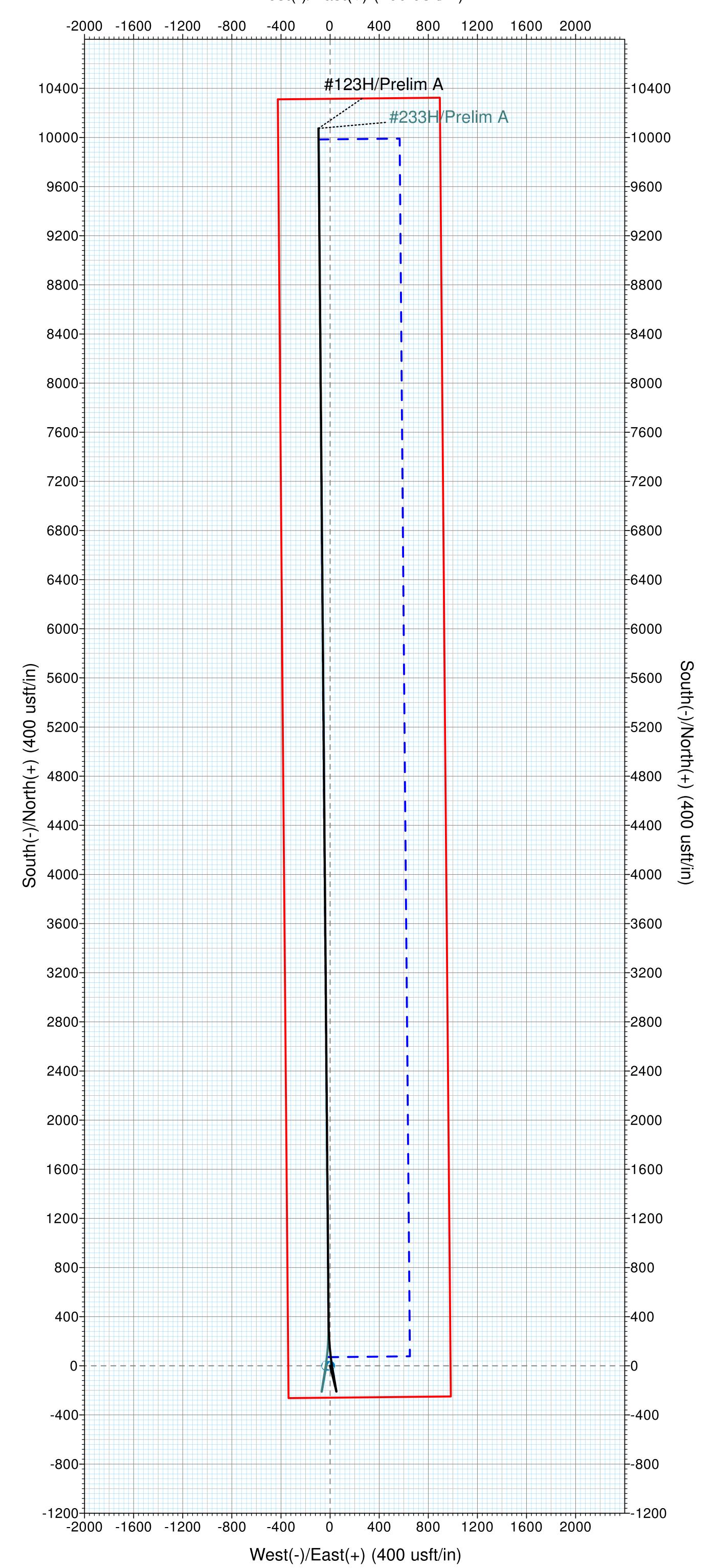
9 If H2S is encountered, mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H2S scavengers if necessary

11 Emergency Contacts

See exhibit E-6

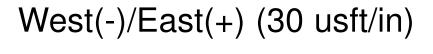


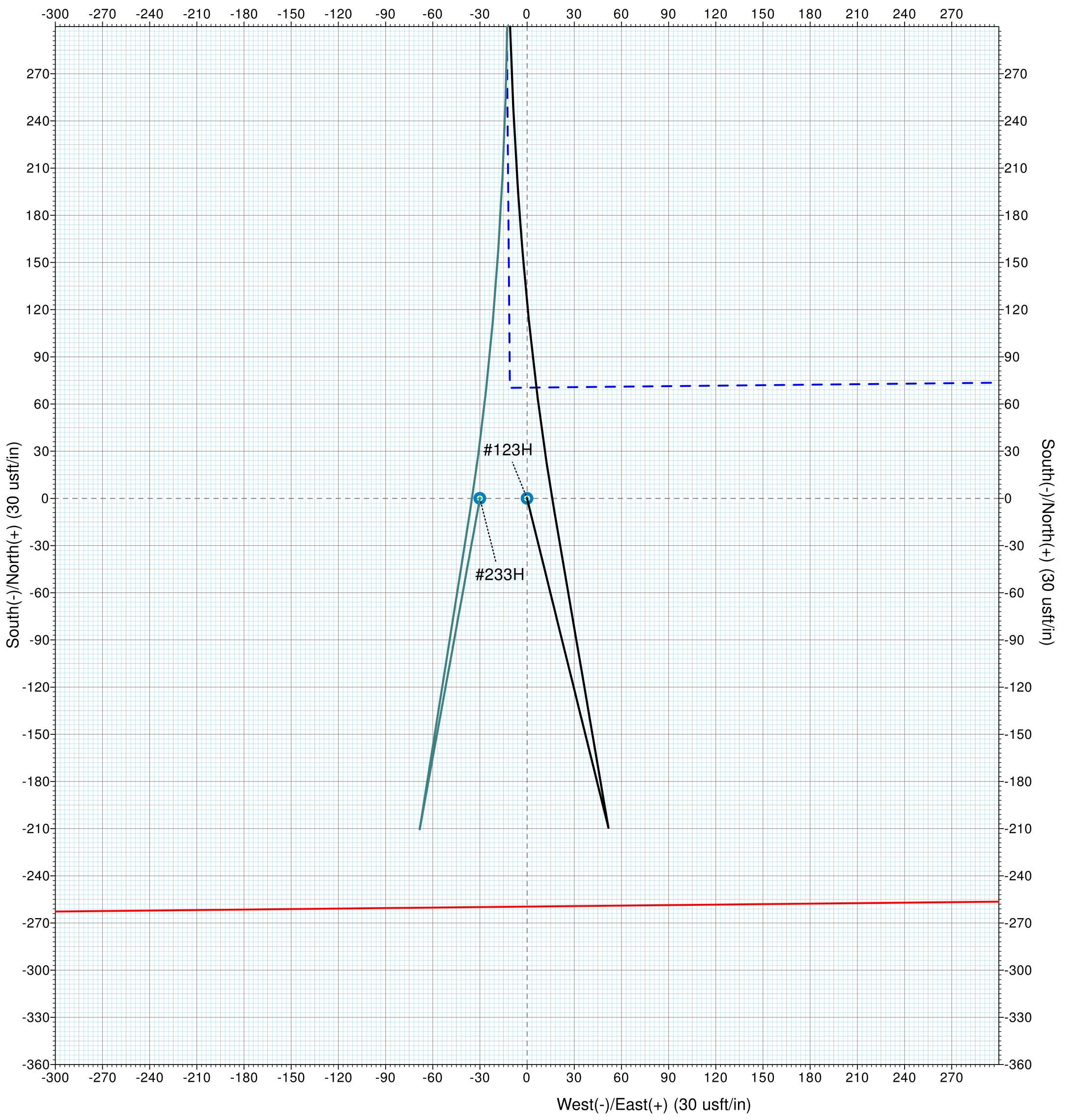
West(-)/East(+) (400 usft/in)



Matador Resources
Lea County, NM
Uncle Ches 2116 Fed
Slot 3 Pad
Prelim A
Patterson 809









Survey Report

MD Reference:



Matador Resources Company: Project: Lea County, NM

Site: Uncle Ches 2116 Fed

#233H Well: Wellbore: OH Design: Prelim A

Map Zone:

Local Co-ordinate Reference:

TVD Reference:

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

North Reference: Grid

Survey Calculation Method: Database:

Minimum Curvature

WellPlanner1

Project Lea County, NM

US State Plane 1927 (Exact solution) Map System: Geo Datum:

NAD 1927 (NADCON CONUS)

New Mexico East 3001

Mean Sea Level

Uncle Ches 2116 Fed Site

Site Position: Northing: 565,604.00 usft Latitude: 32.551980 766,403.00 usft Longitude: -103.468749 From: Мар Easting: 0.00 usft **Slot Radius:** 13-3/16 " Grid Convergence: 0.47° **Position Uncertainty:**

System Datum:

Well #233H

Well Position +N/-S 0.00 usft Northing: 565,627.00 usfl Latitude: 32.551989

0.00 usft 768.850.00 usfl -103.460807 +E/-W Easting: Longitude:

Position Uncertainty 0.00 usft Wellhead Elevation: usfl **Ground Level:** 3,712.00 usfl

Wellbore ОН

Magnetics **Model Name** Sample Date Declination Dip Angle Field Strength (°) (nT) (°) **HDGM** 7/12/2018 6.65 60.48 48,144.40

Prelim A Design

Audit Notes:

Version: Phase: **PLAN** Tie On Depth: 0.00

Vertical Section: Depth From (TVD) +N/-S +E/-W Direction (usft) (usft) (usft) (°)

0.00 0.00 0.00 359.52

Survey Tool Program Date 7/12/2018

From To (usft) (usft) Survey (Wellbore) **Tool Name** Description

0.00 22,270.69 Prelim A (OH) MWD+HDGM OWSG MWD + HRGM

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00



Survey Report



Company: Matador Resources
Project: Lea County, NM

Site: Uncle Ches 2116 Fed

Well: #233H Wellbore: OH Design: Prelim A Local Co-ordinate Reference:

TVD Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

MD Reference: GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

Well #233H

809)

North Reference: Grid

Survey Calculation Method:

Minimum Curvature

Database: WellPlanner1

Joigii.				Dutubuo	•				
anned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	1.00	190.31	1,099.99	-0.86	-0.16	-0.86	1.00	1.00	0.00
1,200.00	2.00	190.31	1,199.96	-3.43	-0.62	-3.43	1.00	1.00	0.00
1,300.00	3.00	190.31	1,299.86	-7.73	-1.41	-7.71	1.00	1.00	0.00
1,400.00	4.00	190.31	1,399.68	-13.73	-2.50	-13.71	1.00	1.00	0.00
1,499.80	5.00	190.31	1,499.17	-21.43	-3.90	-21.40	1.00	1.00	0.00
1,600.00	5.00	190.31	1,598.99	-30.02	-5.46	-29.98	0.00	0.00	0.00
1,700.00	5.00	190.31	1,698.61	-38.59	-7.02	-38.53	0.00	0.00	0.00
1,800.00	5.00	190.31	1,798.22	-47.17	-8.58	-47.09	0.00	0.00	0.00
1,900.00	5.00	190.31	1,897.84	-55.74	-10.14	-55.65	0.00	0.00	0.00
2,000.00	5.00	190.31	1,997.46	-64.31	-11.70	-64.21	0.00	0.00	0.00
2,100.00	5.00	190.31	2,097.08	-72.88	-13.26	-72.77	0.00	0.00	0.00
2,200.00	5.00	190.31	2,196.70	-81.45	-14.82	-81.32	0.00	0.00	0.00
2,300.00	5.00	190.31	2,296.32	-90.02	-16.38	-89.88	0.00	0.00	0.00
2,400.00	5.00	190.31	2,395.94	-98.59	-17.94	-98.44	0.00	0.00	0.00
2,500.00	5.00	190.31	2,495.56	-107.17	-19.50	-107.00	0.00	0.00	0.00
2,600.00	5.00	190.31	2,595.18	-115.74	-21.06	-115.56	0.00	0.00	0.00
2,700.00	5.00	190.31	2,694.80	-124.31	-22.61	-124.11	0.00	0.00	0.00
2,800.00	5.00	190.31	2,794.42	-132.88	-24.17	-132.67	0.00	0.00	0.00
2,900.00	5.00	190.31	2,894.04	-141.45	-25.73	-141.23	0.00	0.00	0.00
3,000.00	5.00	190.31	2,993.66	-150.02	-27.29	-149.79	0.00	0.00	0.00
3,100.00	5.00	190.31	3,093.28	-158.59	-28.85	-158.35	0.00	0.00	0.00
3,200.00	5.00	190.31	3,192.90	-167.17	-30.41	-166.91	0.00	0.00	0.00
3,300.00	5.00	190.31	3,292.52	-175.74	-31.97	-175.46	0.00	0.00	0.00
3,400.00	5.00	190.31	3,392.14	-184.31	-33.53	-184.02	0.00	0.00	0.00
3,454.57	5.00	190.31	3,446.50	-188.99	-34.38	-188.69	0.00	0.00	0.00
3,500.00	4.54	190.31	3,491.78	-192.70	-35.06	-192.40	1.00	-1.00	0.00
3,600.00	3.54	190.31	3,591.53	-199.64	-36.32	-199.33	1.00	-1.00	0.00
3,700.00	2.54	190.31	3,691.38	-204.87	-37.27	-204.55	1.00	-1.00	0.00
3,800.00	1.54	190.31	3,791.32	-208.37	-37.91	-208.05	1.00	-1.00	0.00
3,900.00	0.54	190.31	3,891.30	-210.17	-38.23	-209.84	1.00	-1.00	0.00
3,954.37	0.00	0.00	3,945.67	-210.42	-38.28	-210.09	1.00	-1.00	0.00
4,000.00	0.00	0.00	3,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,100.00	0.00	0.00	4,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,200.00	0.00	0.00	4,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,300.00	0.00	0.00	4,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,400.00	0.00	0.00	4,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,500.00	0.00	0.00	4,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,600.00	0.00	0.00	4,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,700.00	0.00	0.00	4,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
4,800.00	0.00	0.00	4,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00



Survey Report



Company: Matador Resources Project: Lea County, NM

Uncle Ches 2116 Fed Site:

#233H Well: Wellbore: ОН Design: Prelim A Local Co-ordinate Reference:

TVD Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

Well #233H

MD Reference: GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

Minimum Curvature

809)

North Reference: Grid

Survey Calculation Method:

WellPlanner1

Database:

Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
4,900.00	0.00	0.00	4,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,000.00	0.00	0.00	4,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,100.00	0.00	0.00	5,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,200.00	0.00	0.00	5,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,300.00	0.00	0.00	5,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,400.00	0.00	0.00	5,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,500.00	0.00	0.00	5,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,600.00	0.00	0.00	5,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,700.00	0.00	0.00	5,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,800.00	0.00	0.00	5,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
5,900.00	0.00	0.00	5,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,000.00	0.00	0.00	5,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,100.00	0.00	0.00	6,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,200.00	0.00	0.00	6,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,300.00	0.00	0.00	6,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,400.00	0.00	0.00	6,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,500.00	0.00	0.00	6,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,600.00	0.00	0.00	6,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,700.00	0.00	0.00	6,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,800.00	0.00	0.00	6,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
6,900.00	0.00	0.00	6,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,000.00	0.00	0.00	6,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,100.00	0.00	0.00	7,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,200.00	0.00	0.00	7,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,300.00	0.00	0.00	7,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,400.00	0.00	0.00	7,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,500.00	0.00	0.00	7,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,600.00	0.00	0.00	7,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,700.00	0.00	0.00	7,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,800.00	0.00	0.00	7,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
7,900.00	0.00	0.00	7,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,000.00	0.00	0.00	7,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,100.00	0.00	0.00	8,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,200.00	0.00	0.00	8,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,300.00	0.00	0.00	8,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,400.00	0.00	0.00	8,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,500.00	0.00	0.00	8,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,600.00	0.00	0.00	8,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,700.00	0.00	0.00	8,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,800.00	0.00	0.00	8,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
8,900.00	0.00	0.00	8,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,000.00	0.00	0.00	8,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00



Survey Report



Company: Matador Resources
Project: Lea County, NM

Site: Uncle Ches 2116 Fed

Well: #233H Wellbore: OH Design: Prelim A Local Co-ordinate Reference:

TVD Reference:

MD Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

North Reference: Grid

Survey Calculation Method:

Minimum Curvature WellPlanner1

Database: WellPlanne

Design.	allii A			Database	•		vveiir iai ii iei i		
Planned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,100.00	0.00	0.00	9,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,200.00	0.00	0.00	9,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,300.00	0.00	0.00	9,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,400.00	0.00	0.00	9,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,500.00	0.00	0.00	9,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,600.00	0.00	0.00	9,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,700.00	0.00	0.00	9,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,800.00	0.00	0.00	9,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
9,900.00	0.00	0.00	9,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,000.00	0.00	0.00	9,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,100.00	0.00	0.00	10,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,200.00	0.00	0.00	10,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,300.00	0.00	0.00	10,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,400.00	0.00	0.00	10,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,500.00	0.00	0.00	10,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,600.00	0.00	0.00	10,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,700.00	0.00	0.00	10,691.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,800.00	0.00	0.00	10,791.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
10,900.00	0.00	0.00	10,891.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,000.00	0.00	0.00	10,991.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,100.00	0.00	0.00	11,091.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,200.00	0.00	0.00	11,191.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,300.00	0.00	0.00	11,291.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,400.00	0.00	0.00	11,391.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,500.00	0.00	0.00	11,491.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,600.00	0.00	0.00	11,591.30	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,654.37	0.00	0.00	11,645.67	-210.42	-38.28	-210.09	0.00	0.00	0.00
11,700.00	4.56	9.00	11,691.25	-208.63	-38.00	-208.30	10.00	10.00	0.00
11,750.00	9.56	9.00	11,740.86	-202.56	-37.03	-202.24	10.00	10.00	0.00
11,800.00	14.56	9.00	11,789.74	-192.24	-35.40	-191.94	10.00	10.00	0.00
11,850.00	19.56	9.00	11,837.52	-177.75	-33.11	-177.47	10.00	10.00	0.00
11,900.00	24.56	9.00	11,883.85	-159.21	-30.17	-158.95	10.00	10.00	0.00
11,950.00	29.56	9.00	11,928.36	-136.75	-26.61	-136.52	10.00	10.00	0.00
12,000.00	34.56	9.00	11,970.72	-110.54	-22.46	-110.35	10.00	10.00	0.00
12,050.00	39.56	9.00	12,010.60	-80.79	-17.75	-80.63	10.00	10.00	0.00
12,100.00	44.56	9.00	12,047.71	-47.71	-12.51	-47.60	10.00	10.00	0.00
12,154.37	50.00	9.00	12,084.58	-8.27	-6.26	-8.22	10.00	10.00	0.00
12,200.00	54.43	7.59	12,112.53	27.40	-1.07	27.41	10.00	9.70	-3.09
12,250.00	59.29	6.21	12,139.86	68.95	3.94	68.92	10.00	9.73	-2.75
12,300.00	64.17	4.97	12,163.54	112.77	8.22	112.69	10.00	9.76	-2.49
12,350.00	69.06	3.83	12,183.38	158.51	11.73	158.41	10.00	9.78	-2.29
12,400.00	73.95	2.76	12,199.23	205.83	14.45	205.71	10.00	9.79	-2.14



Survey Report



Company: Matador Resources Project: Lea County, NM

Uncle Ches 2116 Fed Site:

Well: #233H Wellbore: ОН Design: Prelim A Local Co-ordinate Reference:

TVD Reference:

MD Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

North Reference: Grid

Survey Calculation Method:

Minimum Curvature Database: WellPlanner1

Pla	anned Survey									
	Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
	12,450.00	78.85	1.74	12,210.98	254.38	16.35	254.23	10.00	9.80	-2.04
	12,500.00	83.76	0.75	12,218.54	303.78	17.41	303.62	10.00	9.81	-1.97
	12,550.00	88.66	359.78	12,221.84	353.65	17.64	353.49	10.00	9.81	-1.94
	12,563.61	90.00	359.52	12,222.00	367.26	17.56	367.10	10.00	9.81	-1.93
	12,600.00	90.00	359.52	12,222.00	403.65	17.25	403.49	0.00	0.00	0.00
	12,700.00	90.00	359.52	12,222.00	503.65	16.41	503.49	0.00	0.00	0.00
	12,800.00	90.00	359.52	12,222.00	603.64	15.57	603.49	0.00	0.00	0.00
	12,900.00	90.00	359.52	12,222.00	703.64	14.73	703.49	0.00	0.00	0.00
	13,000.00	90.00	359.52	12,222.00	803.64	13.89	803.49	0.00	0.00	0.00
	13,100.00	90.00	359.52	12,222.00	903.63	13.05	903.49	0.00	0.00	0.00
	13,200.00	90.00	359.52	12,222.00	1,003.63	12.21	1,003.49	0.00	0.00	0.00
	13,300.00	90.00	359.52	12,222.00	1,103.63	11.37	1,103.49	0.00	0.00	0.00
	13,400.00	90.00	359.52	12,222.00	1,203.62	10.53	1,203.49	0.00	0.00	0.00
	13,500.00	90.00	359.52	12,222.00	1,303.62	9.69	1,303.49	0.00	0.00	0.00
	13,600.00	90.00	359.52	12,222.00	1,403.62	8.85	1,403.49	0.00	0.00	0.00
	13,700.00	90.00	359.52	12,222.00	1,503.61	8.01	1,503.49	0.00	0.00	0.00
	13,800.00	90.00	359.52	12,222.00	1,603.61	7.17	1,603.49	0.00	0.00	0.00
	13,900.00	90.00	359.52	12,222.00	1,703.60	6.33	1,703.49	0.00	0.00	0.00
	14,000.00	90.00	359.52	12,222.00	1,803.60	5.49	1,803.49	0.00	0.00	0.00
	14,100.00	90.00	359.52	12,222.00	1,903.60	4.65	1,903.49	0.00	0.00	0.00
	14,200.00	90.00	359.52	12,222.00	2,003.59	3.81	2,003.49	0.00	0.00	0.00
	14,300.00	90.00	359.52	12,222.00	2,103.59	2.97	2,103.49	0.00	0.00	0.00
	14,400.00	90.00	359.52	12,222.00	2,203.59	2.13	2,203.49	0.00	0.00	0.00
	14,500.00	90.00	359.52	12,222.00	2,303.58	1.29	2,303.49	0.00	0.00	0.00
	14,600.00	90.00	359.52	12,222.00	2,403.58	0.45	2,403.49	0.00	0.00	0.00
	14,700.00	90.00	359.52	12,222.00	2,503.58	-0.39	2,503.49	0.00	0.00	0.00
	14,800.00	90.00	359.52	12,222.00	2,603.57	-1.23	2,603.49	0.00	0.00	0.00
	14,900.00	90.00	359.52	12,222.00	2,703.57	-2.07	2,703.49	0.00	0.00	0.00
	15,000.00	90.00	359.52	12,222.00	2,803.57	-2.91	2,803.49	0.00	0.00	0.00
	15,100.00	90.00	359.52	12,222.00	2,903.56	-3.75	2,903.49	0.00	0.00	0.00
	15,200.00	90.00	359.52	12,222.00	3,003.56	-4.59	3,003.49	0.00	0.00	0.00
	15,300.00	90.00	359.52	12,222.00	3,103.56	-5.43	3,103.49	0.00	0.00	0.00
	15,400.00	90.00	359.52	12,222.00	3,203.55	-6.27	3,203.49	0.00	0.00	0.00
	15,500.00	90.00	359.52	12,222.00	3,303.55	-7.11	3,303.49	0.00	0.00	0.00
	15,600.00	90.00	359.52	12,222.00	3,403.54	-7.95	3,403.49	0.00	0.00	0.00
	15,700.00	90.00	359.52	12,222.00	3,503.54	-8.79	3,503.49	0.00	0.00	0.00
	15,800.00	90.00	359.52	12,222.00	3,603.54	-9.63	3,603.49	0.00	0.00	0.00
	15,900.00	90.00	359.52	12,222.00	3,703.53	-10.47	3,703.49	0.00	0.00	0.00
	16,000.00	90.00	359.52	12,222.00	3,803.53	-11.31	3,803.49	0.00	0.00	0.00
	16,100.00	90.00	359.52	12,222.00	3,903.53	-12.15	3,903.49	0.00	0.00	0.00
	16,200.00	90.00	359.52	12,222.00	4,003.52	-12.99	4,003.49	0.00	0.00	0.00
	16,300.00	90.00	359.52	12,222.00	4,103.52	-13.83	4,103.49	0.00	0.00	0.00



Survey Report



Company: Matador Resources Project: Lea County, NM

Uncle Ches 2116 Fed Site:

#233H Well: Wellbore: ОН Design: Prelim A Local Co-ordinate Reference:

TVD Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson MD Reference:

809)

North Reference: Grid

Survey Calculation Method:

Minimum Curvature

Database: WellPlanner1

nned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
16,400.00	90.00	359.52	12,222.00	4,203.52	-14.67	4,203.49	0.00	0.00	0.00
16,500.00	90.00	359.52	12,222.00	4,303.51	-15.51	4,303.49	0.00	0.00	0.00
16,600.00	90.00	359.52	12,222.00	4,403.51	-16.35	4,403.49	0.00	0.00	0.00
16,700.00	90.00	359.52	12,222.00	4,503.51	-17.19	4,503.49	0.00	0.00	0.00
16,800.00	90.00	359.52	12,222.00	4,603.50	-18.03	4,603.49	0.00	0.00	0.00
16,900.00	90.00	359.52	12,222.00	4,703.50	-18.87	4,703.49	0.00	0.00	0.00
17,000.00	90.00	359.52	12,222.00	4,803.50	-19.71	4,803.49	0.00	0.00	0.00
17,100.00	90.00	359.52	12,222.00	4,903.49	-20.56	4,903.49	0.00	0.00	0.00
17,200.00	90.00	359.52	12,222.00	5,003.49	-21.40	5,003.49	0.00	0.00	0.00
17,300.00	90.00	359.52	12,222.00	5,103.48	-22.24	5,103.49	0.00	0.00	0.00
17,400.00	90.00	359.52	12,222.00	5,203.48	-23.08	5,203.49	0.00	0.00	0.00
17,500.00	90.00	359.52	12,222.00	5,303.48	-23.92	5,303.49	0.00	0.00	0.00
17,600.00	90.00	359.52	12,222.00	5,403.47	-24.76	5,403.49	0.00	0.00	0.00
17,700.00	90.00	359.52	12,222.00	5,503.47	-25.60	5,503.49	0.00	0.00	0.00
17,800.00	90.00	359.52	12,222.00	5,603.47	-26.44	5,603.49	0.00	0.00	0.00
17,900.00	90.00	359.52	12,222.00	5,703.46	-27.28	5,703.49	0.00	0.00	0.00
18,000.00	90.00	359.52	12,222.00	5,803.46	-28.12	5,803.49	0.00	0.00	0.00
18,100.00	90.00	359.52	12,222.00	5,903.46	-28.96	5,903.49	0.00	0.00	0.00
18,200.00	90.00	359.52	12,222.00	6,003.45	-29.80	6,003.49	0.00	0.00	0.00
18,300.00	90.00	359.52	12,222.00	6,103.45	-30.64	6,103.49	0.00	0.00	0.00
18,400.00	90.00	359.52	12,222.00	6,203.45	-31.48	6,203.49	0.00	0.00	0.00
18,500.00	90.00	359.52	12,222.00	6,303.44	-32.32	6,303.49	0.00	0.00	0.00
18,600.00	90.00	359.52	12,222.00	6,403.44	-33.16	6,403.49	0.00	0.00	0.00
18,700.00	90.00	359.52	12,222.00	6,503.44	-34.00	6,503.49	0.00	0.00	0.00
18,800.00	90.00	359.52	12,222.00	6,603.43	-34.84	6,603.49	0.00	0.00	0.00
18,900.00	90.00	359.52	12,222.00	6,703.43	-35.68	6,703.49	0.00	0.00	0.00
19,000.00	90.00	359.52	12,222.00	6,803.42	-36.52	6,803.49	0.00	0.00	0.00
19,100.00	90.00	359.52	12,222.00	6,903.42	-37.36	6,903.49	0.00	0.00	0.00
19,200.00	90.00	359.52	12,222.00	7,003.42	-38.20	7,003.49	0.00	0.00	0.00
19,300.00	90.00	359.52	12,222.00	7,103.41	-39.04	7,103.49	0.00	0.00	0.00
19,400.00	90.00	359.52	12,222.00	7,203.41	-39.88	7,203.49	0.00	0.00	0.00
19,500.00	90.00	359.52	12,222.00	7,303.41	-40.72	7,303.49	0.00	0.00	0.00
19,600.00	90.00	359.52	12,222.00	7,403.40	-41.56	7,403.49	0.00	0.00	0.00
19,700.00	90.00	359.52	12,222.00	7,503.40	-42.40	7,503.49	0.00	0.00	0.00
19,800.00	90.00	359.52	12,222.00	7,603.40	-43.24	7,603.49	0.00	0.00	0.00
19,900.00	90.00	359.52	12,222.00	7,703.39	-44.08	7,703.49	0.00	0.00	0.00
20,000.00	90.00	359.52	12,222.00	7,803.39	-44.92	7,803.49	0.00	0.00	0.00
20,100.00	90.00	359.52	12,222.00	7,903.39	-45.76	7,903.49	0.00	0.00	0.00
20,200.00	90.00	359.52	12,222.00	8,003.38	-46.60	8,003.49	0.00	0.00	0.00
20,300.00	90.00	359.52	12,222.00	8,103.38	-47.44	8,103.49	0.00	0.00	0.00
20,400.00	90.00	359.52	12,222.00	8,203.38	-48.28	8,203.49	0.00	0.00	0.00
20,500.00	90.00	359.52	12,222.00	8,303.37	-49.12	8,303.49	0.00	0.00	0.00



Survey Report



Company: Matador Resources
Project: Lea County, NM

Site: Uncle Ches 2116 Fed

Well: #233H
Wellbore: OH
Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson

809)

North Reference: Grid

Survey Calculation Method: Database:

Minimum Curvature WellPlanner1

WellPlanne

nned Survey									
Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
20,600.00	90.00	359.52	12,222.00	8,403.37	-49.96	8,403.49	0.00	0.00	0.00
20,700.00	90.00	359.52	12,222.00	8,503.36	-50.80	8,503.49	0.00	0.00	0.00
20,800.00	90.00	359.52	12,222.00	8,603.36	-51.64	8,603.49	0.00	0.00	0.00
20,900.00	90.00	359.52	12,222.00	8,703.36	-52.48	8,703.49	0.00	0.00	0.00
21,000.00	90.00	359.52	12,222.00	8,803.35	-53.32	8,803.49	0.00	0.00	0.00
21,100.00	90.00	359.52	12,222.00	8,903.35	-54.16	8,903.49	0.00	0.00	0.00
21,200.00	90.00	359.52	12,222.00	9,003.35	-55.00	9,003.49	0.00	0.00	0.00
21,300.00	90.00	359.52	12,222.00	9,103.34	-55.84	9,103.49	0.00	0.00	0.00
21,400.00	90.00	359.52	12,222.00	9,203.34	-56.68	9,203.49	0.00	0.00	0.00
21,500.00	90.00	359.52	12,222.00	9,303.34	-57.52	9,303.49	0.00	0.00	0.00
21,600.00	90.00	359.52	12,222.00	9,403.33	-58.36	9,403.49	0.00	0.00	0.00
21,700.00	90.00	359.52	12,222.00	9,503.33	-59.20	9,503.49	0.00	0.00	0.00
21,800.00	90.00	359.52	12,222.00	9,603.33	-60.05	9,603.49	0.00	0.00	0.00
21,900.00	90.00	359.52	12,222.00	9,703.32	-60.89	9,703.49	0.00	0.00	0.00
22,000.00	90.00	359.52	12,222.00	9,803.32	-61.73	9,803.49	0.00	0.00	0.00
22,100.00	90.00	359.52	12,222.00	9,903.32	-62.57	9,903.49	0.00	0.00	0.00
22,200.00	90.00	359.52	12,222.00	10,003.31	-63.41	10,003.49	0.00	0.00	0.00
22,270.69	90.00	359.52	12,222.00	10,074.00	-64.00	10,074.18	0.00	0.00	0.00

Design Targets									
Target Name - hit/miss target	Dip Angle I	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
FPP(U C 2116 F #230	0.00	0.00	12,222.0	70.00	19.00	565,697.00	768,869.00	32.552181	-103.460744
plan misses targetPoint	center by 72	2.37usft at	t 12291.12	usft MD (121	59.61 TVD,	104.84 N, 7.52 E)		
LPP(U C 2116 F #233	0.00	0.00	12,222.0	9,984.00	-63.00	575,611.00	768,787.00	32.579431	-103.460746
plan misses targetPoint	center by 0.	.24usft at 2	22180.69u	sft MD (1222	2.00 TVD, 9	984.00 N, -63.24	E)		
BHL(U C 2116 F #23	0.00	0.00	12,222.0 0	10,074.00	-64.00	575,701.00	768,786.00	32.579679	-103.460747
plan hits target cerPoint	nter								

Checked By:	Approved By:	Date:	
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Anticollision Report



Matador Resources Company: Project: Lea County, NM

Uncle Ches 2116 Fed Reference Site:

0.00 usft Site Error: Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

Survey Calculation Method: Minimum Curvature

Output errors are at

Database:

MD Reference:

North Reference:

Offset TVD Reference:

2.00 sigma WellPlanner1

Offset Datum

Prelim A Reference

NO GLOBAL FILTER: Using user defined selection & filtering criteria Filter type:

Interpolation Method: Stations **Error Model:**

Depth Range: Unlimited Scan Method: Closest Approach 3D

Maximum center-center distance of 9,999.98 us Pedal Curve Results Limited by: **Error Surface:** Warning Levels Evaluated at: 2.00 **Sigma Casing Method:** Not applied

Date 7/12/2018 **Survey Tool Program**

> From То

(usft)

(usft) Survey (Wellbore) **Tool Name**

Description

ISCWSA

0.00 22,270.69 Prelim A (OH) MWD+HDGM OWSG MWD + HRGM

Summary						
Site Name Offset Well - Wellbore - Design	Reference Measured Depth (usft)	Offset Measured Depth (usft)	Dista Between Centres (usft)	nce Between Ellipses (usft)	Separation Factor	Warning
Uncle Ches 2116 Fed						
#123H - OH - Prelim A #123H - OH - Prelim A #123H - OH - Prelim A	1,000.00 1,100.00 10,008.92	999.00 1,098.87 10,009.68	30.00 30.36 118.47	23.29 22.97 48.57	4.474 CC 4.110 ES 1.695 SF	

Offset D	esign	Uncle (Ches 211	6 Fed - #	123H - C)H - Prelim	Α						Offset Site Error:	0.00 usft
		WD+HDGM											Offset Well Error:	0.00 usft
Refer		Offs		Semi Major				<u>.</u> .	Dista					
Measured Depth	Vertical Depth	Measured Depth	Vertical Depth	Reference	Offset	Highside Toolface	Offset Wellbo		Between Centres	Between Ellipses	Minimum Separation	Separation Factor	Warning	
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(°)	+N/-S (usft)	+E/-W (usft)	(usft)	(usft)	(usft)	Factor		
0.00	0.00	1.00	-1.00	0.00	0.00	90.00	0.00	30.00	30.00					
100.00	100.00	101.00	99.00	0.13	0.13	90.00	0.00	30.00	30.00	29.74	0.26	115.432		
200.00	200.00	201.00	199.00	0.49	0.49	90.00	0.00	30.00	30.00	29.02	0.98	30.711		
300.00	300.00	301.00	299.00	0.85	0.85	90.00	0.00	30.00	30.00	28.31	1.69	17.712		
400.00	400.00	401.00	399.00	1.20	1.21	90.00	0.00	30.00	30.00	27.59	2.41	12.444		
500.00	500.00	501.00	499.00	1.56	1.57	90.00	0.00	30.00	30.00	26.87	3.13	9.592		
600.00	600.00	601.00	599.00	1.92	1.92	90.00	0.00	30.00	30.00	26.16	3.84	7.803		
700.00	700.00	701.00	699.00	2.28	2.28	90.00	0.00	30.00	30.00	25.44	4.56	6.577		
800.00	800.00	801.00	799.00	2.64	2.64	90.00	0.00	30.00	30.00	24.72	5.28	5.683		
900.00	900.00	901.00	899.00	3.00	3.00	90.00	0.00	30.00	30.00	24.00	6.00	5.004		
1,000.00	1,000.00	999.00	999.00	3.35	3.35	90.00	0.00	30.00	30.00	23.29	6.71	4.474 (CC	
1,100.00	1,099.99	1,098.87	1,098.87	3.70	3.69	-100.36	-0.83	30.20	30.36	22.97	7.39	4.110 E	ES	
1,200.00	1,199.96	1,198.74	1,198.70	4.02	4.02	-100.45	-3.35	30.83	31.45	23.41	8.04	3.911		
1,300.00	1,299.86	1,298.59	1,298.46	4.36	4.35	-100.56	-7.55	31.87	33.27	24.57	8.71	3.822		
1,400.00	1,399.68	1,398.42	1,398.10	4.69	4.69	-100.68	-13.44	33.32	35.82	26.44	9.38	3.819		
1,499.80	1,499.17	1,501.77	1,497.39	5.04	5.04	-100.81	-21.00	35.19	39.10	29.02	10.08	3.879		
1,600.00	1,598.99	1,601.86	1,597.14	5.39	5.39	-100.91	-29.47	37.28	42.75	31.98	10.78	3.968		
1,700.00	1,698.61	1,701.92	1,696.69	5.74	5.75	-101.00	-37.92	39.37	46.40	34.92	11.48	4.042		
1,800.00	1,798.22	1,801.99	1,796.24	6.09	6.10	-101.08	-46.38	41.46	50.05	37.86	12.19	4.105		
1,900.00	1,897.84	1,902.06	1,895.80	6.45	6.46	-101.14	-54.83	43.54	53.70	40.79	12.91	4.160		
2,000.00	1,997.46	2,002.12	1,995.35	6.81	6.82	-101.20	-63.28	45.63	57.35	43.72	13.63	4.208		
2,100.00	2,097.08	2,102.19	2,094.90	7.18	7.19	-101.25	-71.74	47.72	61.00	46.65	14.36	4.249		



Anticollision Report



Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

Site Error: 0.00 usft Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

North Reference:

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

Survey Calculation Method: Minimum Curvature

Output errors are at

Database:

Offset TVD Reference:

Offset D	esian	Uncle	Ches 21	16 Fed - #	123H - C)H - Prelim	Α						Offset Site Error:	0.00 usft
		/WD+HDGM											Offset Well Error:	0.00 usft
Refer		Offs	et	Semi Major	Axis				Dista	ance				
Measured		Measured	Vertical	Reference	Offset	Highside	Offset Wellbo			Between	Minimum		Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
2,200.00	2,196.70	2,202.26	2,194.46	7.54	7.55	-101.29	-80.19	49.81	64.65	49.57	15.08	4.286		
2,300.00			2,294.01	7.91	7.92	-101.33	-88.65	51.90	68.30	52.49	15.82			
2,400.00	-	2,402.39	2,393.56	8.28	8.29	-101.36	-97.10	53.99	71.95	55.40	16.55	4.348		
2,500.00	2,495.56	2,502.46	2,493.12	8.64	8.66	-101.40	-105.55	56.07	75.60	58.31	17.29	4.374		
2,600.00	2,595.18	2,602.52	2,592.67	9.01	9.03	-101.43	-114.01	58.16	79.25	61.23	18.02	4.397		
2,700.00	2,694.80	2,702.59	2,692.22	9.38	9.40	-101.45	-122.46	60.25	82.90	64.14	18.76	4.418		
2,800.00	2,794.42	2,802.66	2,791.77	9.75	9.77	-101.48	-130.91	62.34	86.55	67.04	19.51	4.437		
2,900.00		2,902.72	2,891.33	10.13	10.14	-101.50	-139.37	64.43	90.20	69.95	20.25	4.455		
3,000.00		3,002.79	2,990.88	10.50	10.51	-101.52	-147.82	66.51	93.85	72.86	20.99	4.471		
3,100.00		3,102.86	3,090.43	10.87	10.89	-101.54	-156.28	68.60	97.50	75.76	21.74	4.485		
3,200.00		3,202.92	3,189.99	11.25	11.26	-101.56	-164.73	70.69	101.15	78.67	22.48	4.499		
3,300.00			3,289.54	11.62	11.63	-101.57	-173.18	72.78	104.80	81.57	23.23	4.511		
3,400.00		3,396.94	3,389.09	11.99	11.99	-101.59	-181.64	74.87	108.45	84.49	23.95	4.527		
3,454.57		3,451.47	3,443.42	12.20	12.19	-101.60	-186.25	76.01	110.44	86.08	24.36	4.533		
3,500.00		3,496.97	3,488.74	12.37 12.74	12.36	-101.55 101.38	-190.06 -197.34	76.95	112.05	87.35	24.70 25.45	4.536		
3,600.00	ن. ۱ ۵ ۰, د	3,597.36	3,588.85	12.14	12.73	-101.38	-197.34	78.75	115.10	89.66	20.40	4.523		
3,700.00	3,691.38	3,697.78	3,689.11	13.10	13.10	-101.22	-202.92	80.12	117.42	91.24	26.18	4.485		
3,800.00	3,791.32	3,798.24	3,789.48	13.46	13.46	-101.06	-206.79	81.08	119.00	92.10	26.90	4.424		
3,900.00	3,891.30	3,898.71	3,889.93	13.82	13.82	-100.89	-208.96	81.62	119.86	92.25	27.61	4.341		
3,954.37		3,953.35	3,944.56	14.00	14.00	89.52	-209.42	81.73	120.01	92.03	27.98	4.289		
4,000.00	3,991.30	4,000.92	3,990.30	14.15	14.16	89.54	-209.46	81.74	120.02	91.73	28.29	4.243		
4,100.00	4,091.30	4,100.92	4,090.30	14.48	14.49	89.54	-209.46	81.74	120.02	91.08	28.95	4.146		
4,200.00		4,200.92	4,190.30	14.81	14.82	89.54	-209.46	81.74	120.02	90.41				
4,300.00		4,300.92	4,290.30	15.14	15.15	89.54	-209.46	81.74	120.02	89.75	30.27	3.965		
4,400.00		4,400.92	4,390.30	15.47	15.49	89.54	-209.46	81.74	120.02	89.09	30.94	3.879		
4,500.00	4,491.30	4,500.92	4,490.30	15.81	15.82	89.54	-209.46	81.74	120.02	88.42	31.61	3.797		
4,600.00		4,600.92	4,590.30	16.14	16.16	89.54	-209.46	81.74	120.02	87.75	32.28	3.719		
4,700.00		4,700.92 4,800.92	4,690.30	16.48	16.49	89.54	-209.46	81.74	120.02	87.08	32.95 33.62	3.643		
4,800.00 4,900.00		4,800.92	4,790.30 4,890.30	16.82 17.15	16.83 17.17	89.54 89.54	-209.46 -209.46	81.74 81.74	120.02 120.02	86.40 85.73	34.30	3.570 3.499		
5,000.00		5,000.92	4,990.30	17.19	17.50	89.54	-209.46	81.74	120.02	85.05	34.98	3.432		
0,000.00	4,001.00	0,000.02	4,000.00	11.40	17.00	00.04	200.40	01.74	120.02	00.00	04.00	0.402		
5,100.00	5,091.30	5,100.92	5,090.30	17.83	17.84	89.54	-209.46	81.74	120.02	84.37	35.65	3.366		
5,200.00	5,191.30	5,200.92	5,190.30	18.17	18.18	89.54	-209.46	81.74	120.02	83.69	36.33	3.303		
5,300.00		5,300.92	5,290.30	18.51	18.53	89.54	-209.46	81.74	120.02	83.01		3.242		
5,400.00		5,400.92	5,390.30	18.85	18.87	89.54	-209.46	81.74	120.02	82.32		3.184		
5,500.00	5,491.30	5,500.92	5,490.30	19.20	19.21	89.54	-209.46	81.74	120.02	81.64	38.38	3.127		
5,600.00	5,591.30	5,600.92	5,590.30	19.54	19.55	89.54	-209.46	81.74	120.02	80.95	39.07	3.072		
5,700.00		5,700.92	5,690.30	19.88	19.89	89.54	-209.46	81.74	120.02	80.27	39.76	3.019		
5,800.00	5,791.30	5,800.92	5,790.30	20.22	20.24	89.54	-209.46	81.74	120.02	79.58	40.44	2.968		
1 '	5,891.30		5,890.30	20.57	20.58	89.54	-209.46	81.74	120.02	78.89	41.13	2.918		
6,000.00	5,991.30	6,000.92	5,990.30	20.91	20.93	89.54	-209.46	81.74	120.02	78.20	41.82	2.870		
6 100 00	6 001 20	6 100 02	6 000 20	24.26	24 27	90 E4	200.46	01 74	120.02	77 F1	40 F4	2 022		
6,100.00 6,200.00		6,100.92 6,200.92		21.26 21.60	21.27 21.62	89.54 89.54	-209.46 -209.46	81.74 81.74	120.02 120.02	77.51 76.82		2.823 2.778		
6,300.00				21.00	21.02	89.54	-209.46 -209.46	81.74	120.02	76.62 76.13		2.776		
6,400.00		6,400.92		22.30	22.31	89.54	-209.46	81.74	120.02	75.44	44.59	2.734		
6,500.00		6,500.92	6,490.30	22.64	22.66	89.54	-209.46	81.74	120.02	74.74	45.28	2.651		
6,600.00		6,600.92	6,590.30	22.99	23.00	89.54	-209.46	81.74	120.02			2.611		
6,700.00		6,700.92	6,690.30	23.34	23.35	89.54	-209.46	81.74	120.02	73.35		2.572		
6,800.00				23.69	23.70	89.54	-209.46	81.74	120.02			2.534		
6,900.00		6,900.92		24.03	24.05	89.54	-209.46	81.74	120.02			2.497		
1,000.00	6,991.30			24.38	24.40	89.54	-209.46	81.74	120.02	71.26	48.76	2.462		



Anticollision Report



0.00 usft

Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

0.00 usft Site Error: Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH

Local Co-ordinate Reference:

TVD Reference:

North Reference:

Output errors are at

MD Reference:

Database:

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

Survey Calculation Method: Minimum Curvature

> 2.00 sigma WellPlanner1

Reference Design: Prelim A Offset TVD Reference: Offset Datum Offset Design Uncle Ches 2116 Fed - #123H - OH - Prelim A Offset Site Error:

	urvey Prog	gram: 0-M	IWD+HDGM Offs		Semi Major		711 1 10			Dista	anco			Offset Well Error:	0.00 usft
М	easured		Measured	Vertical	Reference		Highside	Offset Wellbo	re Centre	Between		Minimum	Separation	Marnina	
	Depth	Depth	Depth	Depth	Reference	Oliset	Toolface	+N/-S	+E/-W	Centres	Ellipses	Separation		Warning	
	(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)			
	7,100.00	7,091.30	7,100.92	7,090.30	24.73	24.75	89.54	-209.46	81.74	120.02	70.57	49.46	2.427		
	7,200.00	7,191.30	7,200.92	7,190.30	25.08	25.09	89.54	-209.46	81.74	120.02		50.16	2.393		
	7,300.00	7,291.30		7,290.30	25.43	25.44	89.54	-209.46	81.74	120.02			2.360		
	7,400.00	7,391.30		7,390.30	25.78	25.79	89.54	-209.46	81.74	120.02		51.55	2.328		
	7,500.00	7,491.30		7,490.30	26.13	26.14	89.54	-209.46	81.74	120.02			2.297		
	.,	.,	.,	.,							*****				
	7,600.00	7,591.30	7,600.92	7,590.30	26.48	26.49	89.54	-209.46	81.74	120.02	67.07	52.95	2.267		
	7,700.00	7,691.30	7,700.92	7,690.30	26.83	26.84	89.54	-209.46	81.74	120.02	66.37	53.65	2.237		
	7,800.00	7,791.30	7,800.92	7,790.30	27.18	27.19	89.54	-209.46	81.74	120.02	65.67	54.35	2.208		
	7,900.00	7,891.30	7,900.92	7,890.30	27.53	27.54	89.54	-209.46	81.74	120.02	64.97	55.06	2.180		
	8,000.00	7,991.30	8,000.92	7,990.30	27.88	27.89	89.54	-209.46	81.74	120.02	64.27	55.76	2.153		
	8,100.00	8,091.30	8,100.92		28.23	28.25	89.54	-209.46	81.74	120.02		56.46	2.126		
	8,200.00	8,191.30	8,200.92		28.58	28.60	89.54	-209.46	81.74	120.02			2.100		
1	8,300.00	8,291.30	8,300.92		28.93	28.95	89.54	-209.46	81.74	120.02			2.074		
1	8,400.00	8,391.30		8,390.30	29.29	29.30	89.54	-209.46	81.74	120.02			2.049		
	8,500.00	8,491.30	8,500.92	8,490.30	29.64	29.65	89.54	-209.46	81.74	120.02	60.75	59.27	2.025		
1	0 600 00	0 504 30	0 600 00	0 500 30	20.00	20.00	00.54	200.40	04 74	100.00	60.05	50.00	2.004		
1	8,600.00	8,591.30	8,600.92		29.99	30.00	89.54	-209.46	81.74	120.02			2.001		
	8,700.00	8,691.30	8,700.92		30.34	30.36	89.54	-209.46	81.74	120.02		60.68	1.978		
	8,800.00	8,791.30		8,790.30	30.69	30.71	89.54	-209.46	81.74	120.02		61.38	1.955		
	8,900.00	8,891.30	8,900.92		31.05	31.06	89.54	-209.46	81.74	120.02			1.933		
	9,000.00	8,991.30	9,000.92	8,990.30	31.40	31.41	89.54	-209.46	81.74	120.02	57.23	62.79	1.911		
	9,100.00	9,091.30	9,100.92	9,090.30	31.75	31.77	89.54	-209.46	81.74	120.02	56.52	63.50	1.890		
	9,200.00	9,191.30	9,200.92		32.10	32.12	89.54	-209.46	81.74	120.02			1.869		
	9,300.00	9,291.30		9,190.30	32.10	32.12	89.54	-209.46 -209.46	81.74	120.02			1.849		
	9,400.00	9,391.30	9,400.92		32.40	32.82	89.54	-209.46	81.74	120.02			1.829		
	9,500.00	9,491.30		9,490.30	33.16	33.18	89.54	-209.46	81.74	120.02		66.32	1.810		
	9,500.00	9,491.30	9,500.92	9,490.30	33.10	33.10	09.54	-209.40	01.74	120.02	33.70	00.32	1.610		
	9,600.00	9,591.30	9,600.92	9,590.30	33.52	33.53	89.54	-209.46	81.74	120.02	52.99	67.03	1.791		
	9,700.00	9,691.30	9,700.92		33.87	33.88	89.54	-209.46	81.74	120.02			1.772		
	9,800.00	9,791.30		9,790.30	34.22	34.24	89.54	-209.46	81.74	120.02			1.754		
	9,900.00	9,891.30	9,900.36	9,891.54	34.58	34.59	88.89	-208.10	81.51	119.82		69.14	1.733		
1	0,000.00	9,991.30			34.93	34.93	81.35	-192.59	78.86	118.49			1.697		
'	0,000.00	0,001.00	.0,0002	0,000.01	01.00	01.00	01.00	.02.00	. 0.00		10.00	00.01			
1	0,008.92	10,000.22	10,009.68	9,999.22	34.96	34.95	80.30	-190.46	78.49	118.47	48.57	69.90	1.695 S	SF	
1	0,100.00	10,091.30	10,093.63	10,078.48	35.28	35.22	67.25	-163.40	73.87	122.18	51.98	70.20	1.740		
		10,191.30	10,175.00		35.64	35.45	51.61	-126.56	67.57	140.73	71.87	68.86	2.044		
		10,291.30	10,244.38		35.99	35.64	38.88	-87.45	60.88	178.34	112.71		2.717		
		10,391.30	10,300.00		36.34	35.79	30.32	-51.39	54.72	231.93	170.26		3.761		
		10,491.30	10,351.31		36.70	35.92	23.90	-14.71	48.45	296.80	238.05		5.051		
		10,591.30	10,391.40		37.05	36.02	19.83	16.04	43.40	369.56	313.43		6.584		
	-	10,691.30	10,425.21		37.41	36.11	17.03	43.32	39.43	447.90	393.79	54.11	8.278		
		10,791.30	10,450.00		37.76	36.17	15.28	64.05	36.72	530.29	477.97	52.32	10.135		
1	0,900.00	10,891.30	10,478.84	10,357.18	38.12	36.24	13.53	88.87	33.76	615.62	564.24	51.37	11.984		
Ι.	1 000 00	10.004.00	10 500 00	10.000.01	00.47	20.00	40.40	407.51	04 74	700.07	650.01	50.40	40.000		
		.,		.,	38.47	36.29	12.42	107.54	31.74	703.27	652.81		13.938		
					38.83	36.34	11.53	124.58	30.04	792.72			15.922		
		11,191.30	10,535.37		39.18	36.38	10.83	139.52	28.65	883.60			17.930		
		11,291.30	10,550.00		39.53	36.42	10.26	153.01	27.48	975.66		48.92	19.943		
1	1,400.00	11,391.30	10,550.00	10,387.25	39.89	36.42	10.26	153.01	27.48	1,068.89	1,020.53	48.36	22.102		
1	1 500 00	11,491.30	10,574.23	10 395 67	40.24	36.48	9.41	175.65	25.68	1 162 48	1,113.97	48.51	23.964		
		11,591.30	10,600.00		40.60	36.54	8.62	200.12	23.00	1,102.46			25.799		
		11,645.67	10,600.00		40.00	36.54	8.62	200.12	23.97	1,308.70			26.927		
		11,691.25	10,600.00		40.79	36.54	-0.31	200.12	23.97		1,302.96		27.871		
			10,600.00				-0.31 -0.25		23.97		1,302.96		28.903		
1 1	1,730.00	11,740.00	10,000.00	10,403.39	41.12	36.54	-U.25	200.12	23.97	1,390.96	1,340.02	48.33	∠0.903		



Anticollision Report



Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

Site Error: 0.00 usft Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

North Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson 809)

GL: 3712' + KB: 28.5' @ 3740.50usft

Well #233H

(Patterson 809)

Grid

Survey Calculation Method:

Output errors are at

Database:

Offset TVD Reference:

Minimum Curvature

Offset D	esian	Uncle	Ches 21	16 Fed - #	123H - C)H - Prelim	A						Offset Site Error:	0.00 usft
		MWD+HDGM											Offset Well Error:	0.00 usft
Refer	rence	Offs	set	Semi Major					Dist	ance				
Measured		Measured	Vertical	Reference	Offset	Highside	Offset Wellbo			Between	Minimum		Warning	
Depth (usft)	Depth (usft)	Depth (usft)	Depth (usft)	(usft)	(usft)	Toolface (°)	+N/-S (usft)	+E/-W (usft)	Centres (usft)	Ellipses (usft)	Separation (usft)	Factor		
	11,789.74			41.29	36.54	-0.21	200.12	23.97	1,440.87			29.925		
1	11,837.52			41.45	36.54	-0.19	200.12	23.97	1,483.02		47.95	30.928		
	11,883.85		10,409.71	41.60	36.60	-0.45	222.15	22.61	1,522.61		48.04	31.692		
11,950.00	11,928.36	10,631.73	10,411.84	41.75	36.62	-0.50	230.70	22.13	1,560.19	1,512.27	47.92	32.560		
12,000.00	11,970.72	10,650.00	10,415.83	41.89	36.66	-0.63	248.50	21.22	1,595.43	1,547.54	47.89	33.316		
12,050.00	12,010.60	10,650.00	10,415.83	42.02	36.66	-0.59	248.50	21.22	1,627.90	1,580.27	47.64	34.174		
12.100.00	12.047.71	10,650.00	10.415.83	42.15	36.66	-0.55	248.50	21.22	1.657.91	1,610.51	47.40	34.975		
	12,084.58		10,420.02	42.29	36.72	-0.69	270.90	20.23	1,687.03		47.37	35.613		
	12,112.53			42.40	36.79	-0.58	297.80	19.27	1,709.30	1,661.90	47.40	36.060		
12,250.00	12,139.86	10,700.00	10,423.88	42.51	36.79	-0.34	297.80	19.27	1,730.25	1,683.05	47.20	36.656		
12,300.00	12,163.54	10,700.00	10,423.88	42.62	36.79	-0.18	297.80	19.27	1,748.51	1,701.47	47.05	37.165		
12 350 00	12,183.38	10,700.00	10 423 88	42.73	36.79	-0.06	297.80	19.27	1,764.03	1,717.08	46.94	37.580		
1	12,199.23			42.84	36.86	-0.06	327.17	18.49	1,775.75		46.99	37.788		
	12,210.98			42.94	36.91	-0.03	347.62	18.12	1,784.75		47.02	37.957		
	12,218.54			43.05	36.91	0.00	347.62	18.12	1,790.40		47.02	38.075		
	12,221.84			43.15	36.96	0.01	366.99	17.90	1,792.90	1,745.79	47.11			
10 500 61	10 000 00	10.760.65	10 400 00	40.47	26.06	0.04	267.26	17.00	1 702 00	1 745 00	47.40	20.045		
	12,222.00 12,222.00			43.17 43.25	36.96 37.05	0.01 0.01	367.26 403.65	17.90 17.59	1,793.00 1,793.00	1,745.88 1,745.78	47.13 47.22	38.045 37.967		
	12,222.00			43.48	37.03	0.01	503.65	16.74	1,793.00		47.52	37.907		
1 '	12,222.00			43.46	37.68	0.01	603.65	15.90	1,793.00	1,745.46	47.87	37.730		
	12,222.00			44.10	38.08	0.01	703.64	15.06	1,793.00		48.27	37.430		
12,000.00	12,222.00	11,100.04	10,420.00	44.10	00.00	0.01	700.04	10.00	1,700.00	1,11	10.21	07.140		
	12,222.00		10,428.00	44.47	38.52	0.01	803.64	14.21	1,793.00		48.71	36.810		
1 '	12,222.00			44.89	39.02	0.01	903.64	13.37	1,793.00		49.20	36.442		
1 '	12,222.00			45.35	39.56	0.01	1,003.63	12.53	1,793.00		49.74	36.049		
1	12,222.00			45.85	40.14	0.01	1,103.63	11.68	1,793.00	1,742.69	50.32	35.634		
13,400.00	12,222.00	11,606.04	10,428.00	46.39	40.77	0.01	1,203.63	10.84	1,793.00	1,742.06	50.94	35.199		
13,500.00	12,222.00	11,706.04	10,428.00	46.97	41.44	0.01	1,303.62	10.00	1,793.00	1,741.40	51.60	34.747		
13,600.00	12,222.00	11,806.04	10,428.00	47.59	42.15	0.01	1,403.62	9.15	1,793.00	1,740.70	52.30	34.281		
13,700.00	12,222.00	11,906.04	10,428.00	48.24	42.90	0.01	1,503.61	8.31	1,793.00	1,739.96	53.04	33.804		
13,800.00	12,222.00	12,006.04	10,428.00	48.92	43.68	0.01	1,603.61	7.46	1,793.00	1,739.19	53.82	33.318		
13,900.00	12,222.00	12,106.04	10,428.00	49.64	44.50	0.01	1,703.61	6.62	1,793.00	1,738.38	54.62	32.825		
14.000.00	12,222.00	12,206.04	10.428.00	50.39	45.34	0.01	1,803.60	5.78	1,793.00	1,737.54	55.46	32.327		
14,100.00	12,222.00			51.17	46.22	0.01	1,903.60	4.93	1,793.00		56.34	31.827		
14,200.00	12,222.00	12,406.04	10,428.00	51.98	47.12	0.01	2,003.60	4.09	1,793.00	1,735.77	57.24	31.325		
14,300.00	12,222.00	12,506.04	10,428.00	52.81	48.05	0.01	2,103.59	3.25	1,793.00	1,734.84	58.17	30.825		
14,400.00	12,222.00	12,606.04	10,428.00	53.67	49.01	0.01	2,203.59	2.40	1,793.00	1,733.88	59.12	30.326		
14,500.00	12,222.00	12,706.04	10.428.00	54.56	49.99	0.01	2,303.59	1.56	1,793.00	1,732.90	60.11	29.830		
	12,222.00			55.47	50.99	0.01	2,403.58	0.72	1,793.00		61.11			
	12,222.00			56.40	52.01	0.01	2,503.58	-0.13	1,793.00		62.14	28.852		
		13,006.04		57.35	53.05	0.01	2,603.58	-0.97		1,729.81		28.372		
		13,106.04		58.33	54.11	0.01	2,703.57	-1.82	1,793.00	1,728.73		27.899		
15 000 00	12 222 00	13,206.04	10 428 00	59.32	55.19	0.01	2,803.57	-2.66	1 703 00	1,727.64	65.36	27.432		
1	12,222.00			60.33	56.28	0.01	2,903.56	-3.50	1,793.00			26.973		
		13,406.04		61.36	57.39	0.01	3,003.56	-4.35	1,793.00			26.522		
1 '	12,222.00			62.40	58.52	0.01	3,103.56	-5.19	1,793.00		68.75	26.080		
	12,222.00			63.47	59.66	0.01	3,203.55	-6.03	1,793.00		69.91	25.646		
15 500 00	40,000,00			04.54	60.01		2 200 55	0.00	1 700 00		74.00	05.001		
1 '	12,222.00			64.54	60.81	0.01	3,303.55	-6.88 7.73	1,793.00			25.221		
	12,222.00	13,806.04 13,906.04		65.63 66.73	61.97 63.15	0.01 0.01	3,403.55 3,503.54	-7.72 -8.57	1,793.00 1,793.00			24.805 24.397		
	12,222.00			67.85	64.34	0.01	3,603.54	-6.57 -9.41		1,719.51 1,718.29	73.49 74.71			
1		14,106.04		68.98	65.53	0.01	3,703.54	-10.25		1,717.06	75.95	23.609		
10,000.00	12,222.00			00.90			aont point Cl							



Anticollision Report



Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

Site Error: 0.00 usft Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

Output errors are at

MD Reference:

Database:

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

North Reference: **Survey Calculation Method:** Minimum Curvature

	e Wellbe e Desig		m A				Offset 7	ΓVD Refe	rence:		Offset Dati			
Offset D	esian	Uncle	Ches 21	16 Fed - #	123H - C)H - Prelim	A						Offset Site Error:	0.00 us
		/WD+HDGM											Offset Well Error:	0.00 usf
Refer		Offs	set	Semi Major	r Axis				Dist	ance				
Measured	Vertical	Measured	Vertical	Reference	Offset	Highside	Offset Wellbo	re Centre	Between	Between	Minimum	Separation	Warning	
Depth (ueft)	Depth (ueft)	Depth (ueft)	Depth	(uoft)	(uoft)	Toolface	+N/-S	+E/-W	Centres	Ellipses	Separation (ueft)	Factor		
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)			
	12,222.00			70.12	66.74	0.01	3,803.53	-11.10	1,793.00			23.228		
	12,222.00			71.27	67.96	0.01	3,903.53	-11.94	1,793.00			22.856		
	12,222.00			72.43	69.18	0.01	4,003.53	-12.78	1,793.00			22.492		
	12,222.00			73.60	70.41	0.01	4,103.52	-13.63	1,793.00			22.137		
16,400.00	12,222.00	14,606.04	10,428.00	74.79	71.65	0.01	4,203.52	-14.47	1,793.00	1,710.72	82.28	21.790		
16.500.00	12,222.00	14,706.04	10.428.00	75.98	72.90	0.01	4,303.52	-15.31	1,793.00	1,709.42	83.58	21.452		
	12,222.00			77.18	74.16	0.01	4,403.51	-16.16	1,793.00			21.122		
	12,222.00			78.38	75.42	0.01	4,503.51	-17.00	1,793.00			20.799		
	12,222.00			79.60	76.69	0.01	4,603.50	-17.85	1,793.00			20.485		
	12,222.00			80.82	77.97	0.01	4,703.50	-18.69	1,793.00			20.178		
10,000.00	12,222.00	10,100.04	10,420.00	00.02	11.01	0.01	4,700.00	10.00	1,700.00	1,704.14	00.00	20.170		
17,000.00	12,222.00	15,206.04	10,428.00	82.05	79.25	0.01	4,803.50	-19.53	1,793.00	1,702.80	90.20	19.878		
	12,222.00			83.29	80.54	0.01	4,903.49	-20.38	1,793.00			19.586		
	12,222.00			84.53	81.83	0.01	5,003.49	-21.22	1,793.00			19.300		
	12,222.00			85.78	83.12	0.01	5,103.49	-22.06	1,793.00			19.022		
	12,222.00			87.04	84.43	0.01	5,203.48	-22.91	1,793.00			18.750		
,	,	.,	.,				.,		,	,				
17,500.00	12,222.00	15,706.04	10,428.00	88.30	85.73	0.01	5,303.48	-23.75	1,793.00	1,696.00	97.00	18.485		
17,600.00	12,222.00	15,806.04	10,428.00	89.57	87.04	0.01	5,403.48	-24.59	1,793.00	1,694.62	98.38	18.226		
17,700.00	12,222.00	15,906.04	10,428.00	90.84	88.36	0.01	5,503.47	-25.44	1,793.00	1,693.24	99.76	17.973		
17,800.00	12,222.00	16,006.04	10,428.00	92.12	89.68	0.00	5,603.47	-26.28	1,793.00	1,691.85	101.15	17.726		
17,900.00	12,222.00	16,106.04	10,428.00	93.40	91.00	0.00	5,703.47	-27.13	1,793.00	1,690.45	102.55	17.485		
18,000.00	12,222.00	16,206.04	10,428.00	94.69	92.33	0.00	5,803.46	-27.97	1,793.00	1,689.06	103.95	17.249		
18,100.00	12,222.00	16,306.04	10,428.00	95.98	93.66	0.00	5,903.46	-28.81	1,793.00	1,687.65	105.35	17.019		
18,200.00	12,222.00	16,406.04	10,428.00	97.28	94.99	0.00	6,003.45	-29.66	1,793.00	1,686.24	106.76	16.795		
18,300.00	12,222.00	16,506.04	10,428.00	98.58	96.33	0.00	6,103.45	-30.50	1,793.00	1,684.83	108.17	16.575		
18,400.00	12,222.00	16,606.04	10,428.00	99.88	97.67	0.00	6,203.45	-31.34	1,793.00	1,683.41	109.59	16.361		
	12,222.00			101.19	99.01	0.00	6,303.44	-32.19	1,793.00			16.151		
18,600.00	12,222.00			102.51	100.36	0.00	6,403.44	-33.03	1,793.00	1,680.56	112.44	15.947		
18,700.00	12,222.00	16,906.04	10,428.00	103.82	101.71	0.00	6,503.44	-33.88	1,793.00	1,679.13	113.87	15.746		
18,800.00	12,222.00	17,006.04	10,428.00	105.14	103.06	0.00	6,603.43	-34.72	1,793.00		115.30	15.551		
18,900.00	12,222.00	17,106.04	10,428.00	106.46	104.41	0.00	6,703.43	-35.56	1,793.00	1,676.26	116.74	15.359		
40.000.00	10 000 00	47.000.04	10 100 00	407.70	405.77	0.00	0.000.40	00.44	4 700 00	4 074 00	440.40	45.470		
	12,222.00			107.79	105.77	0.00	6,803.43	-36.41	1,793.00			15.172		
		17,306.04		109.12	107.13	0.00	6,903.42	-37.25	1,793.00			14.989		
	12,222.00			110.45	108.49	0.00	7,003.42	-38.09	1,793.00			14.810		
		17,506.04		111.78	109.85	0.00	7,103.42	-38.94	1,793.00			14.635		
19,400.00	12,222.00	17,606.04	10,428.00	113.12	111.22	0.00	7,203.41	-39.78	1,793.00	1,669.03	123.97	14.464		
10 500 00	10 000 00	17 700 01	10 400 00	111 10	110.50	0.00	7 000 44	40.00	4 700 00	1 607 50	405.40	44.000		
		17,706.04		114.46	112.58	0.00	7,303.41	-40.62	1,793.00			14.296		
		17,806.04		115.80	113.95	0.00	7,403.40	-41.47	1,793.00			14.132		
	12,222.00		10,428.00	117.15	115.32	0.00	7,503.40	-42.31	1,793.00			13.971		
	12,222.00			118.49	116.69	0.00	7,603.40	-43.16		1,663.20		13.813		
19,900.00	12,222.00	18,106.04	10,428.00	119.84	118.07	0.00	7,703.39	-44.00	1,793.00	1,661.73	131.27	13.659		
20 000 00	12,222.00	18 206 04	10 420 00	121 10	110 45	0.00	7 000 00	1101	1,793.00	1 660 07	122.74	13.508		
				121.19	119.45	0.00	7,803.39	-44.84 45.60						
	12,222.00		10,428.00	122.55	120.82	0.00	7,903.39	-45.69	1,793.00			13.360		
	12,222.00			123.90	122.20	0.00	8,003.38	-46.53	1,793.00			13.215		
	12,222.00			125.26	123.58	0.00	8,103.38	-47.37	1,793.00			13.073		
∠0,400.00	12,222.00	18,606.04	10,428.00	126.62	124.97	0.00	8,203.38	-48.22	1,793.00	1,654.37	138.63	12.934		
20 500 00	12,222.00	18,706.04	10 428 00	127.98	126.35	0.00	8,303.37	-49.06	1,793.00	1,652.89	140.11	12.797		
	12,222.00			129.35	127.73	0.00	8,403.37	-49.90	1,793.00			12.797		
	12,222.00			130.71					1,793.00			12.532		
					129.12	0.00	8,503.37	-50.75 51.50	1,793.00	-				
	12,222.00			132.08	130.51	0.00	8,603.36	-51.59				12.404		
ZU.900.00	12,222.00	19,106.04	10,428.00	133.45	131.90	0.00	8,703.36	-52.44	1,793.00	1,646.96	146.04	12.278		



Anticollision Report



Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

Site Error: 0.00 usft Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

TVD Reference:

MD Reference:

North Reference:

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Well #233H

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

Survey Calculation Method: Minimum Curvature

Output errors are at

Database:

Offset TVD Reference:

Offset D	esign	Uncle	Ches 211	16 Fed - #	123H - C)H - Prelim	A						Offset Site Error:	0.00 usft
Survey Pro Refer		WD+HDGM	4	Comi Maio	. Auda				Diet				Offset Well Error:	0.00 usft
Measured	Vertical	Offs Measured	Vertical	Semi Major Reference	Offset	Highside	Offset Wellbo	re Centre	Dista Between	Between	Minimum	Separation	Warning	
Depth	Depth	Depth	Depth			Toolface	+N/-S	+E/-W	Centres	Ellipses	Separation	Factor	wanning	
(usft)	(usft)	(usft)	(usft)	(usft)	(usft)	(°)	(usft)	(usft)	(usft)	(usft)	(usft)			
21,000.00	12,222.00	19,206.04	10,428.00	134.82	133.29	0.00	8,803.36	-53.28	1,793.00	1,645.47	147.53	12.154		
21,100.00	12,222.00	19,306.04	10,428.00	136.19	134.68	0.00	8,903.35	-54.12	1,793.00	1,643.98	149.02	12.032		
21,200.00	12,222.00	19,406.04	10,428.00	137.56	136.07	0.00	9,003.35	-54.97	1,793.00	1,642.49	150.51	11.913		
21,300.00	12,222.00	19,506.04	10,428.00	138.94	137.46	0.00	9,103.34	-55.81	1,793.00	1,641.00	152.00	11.796		
21,400.00	12,222.00	19,606.04	10,428.00	140.31	138.86	0.00	9,203.34	-56.65	1,793.00	1,639.51	153.49	11.681		
21,500.00	12,222.00	19,706.04	10,428.00	141.69	140.25	0.00	9,303.34	-57.50	1,793.00	1,638.01	154.99	11.569		
21,600.00	12,222.00	19,806.04	10,428.00	143.07	141.65	0.00	9,403.33	-58.34	1,793.00	1,636.51	156.49	11.458		
21,700.00	12,222.00	19,906.04	10,428.00	144.45	143.05	0.00	9,503.33	-59.19	1,793.00	1,635.02	157.98	11.349		
21,800.00	12,222.00	20,006.04	10,428.00	145.83	144.45	0.00	9,603.33	-60.03	1,793.00	1,633.52	159.48	11.243		
21,900.00	12,222.00	20,106.04	10,428.00	147.22	145.85	0.00	9,703.32	-60.87	1,793.00	1,632.02	160.98	11.138		
22,000.00	12,222.00	20,206.04	10,428.00	148.60	147.25	0.00	9,803.32	-61.72	1,793.00	1,630.51	162.49	11.035		
22,100.00	12,222.00	20,306.04	10,428.00	149.99	148.65	0.00	9,903.32	-62.56	1,793.00	1,629.01	163.99	10.934		
22,200.00	12,222.00	20,406.04	10,428.00	151.37	150.05	0.00	10,003.31	-63.40	1,793.00	1,627.51	165.49	10.834		
22,270.69	12,222.00	20,476.73	10,428.00	152.35	151.04	0.00	10,074.00	-64.00	1,793.00	1,626.44	166.56	10.765		



Pro Directional Anticollision Report

MD Reference:

Database:

North Reference:

Output errors are at

Offset TVD Reference:



Matador Resources Company: Project: Lea County, NM

Reference Site: Uncle Ches 2116 Fed

0.00 usft Site Error: Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

Well #233H **TVD Reference:**

GL: 3712' + KB: 28.5' @ 3740.50usft (Patterson 809)

GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

Grid

Survey Calculation Method: Minimum Curvature

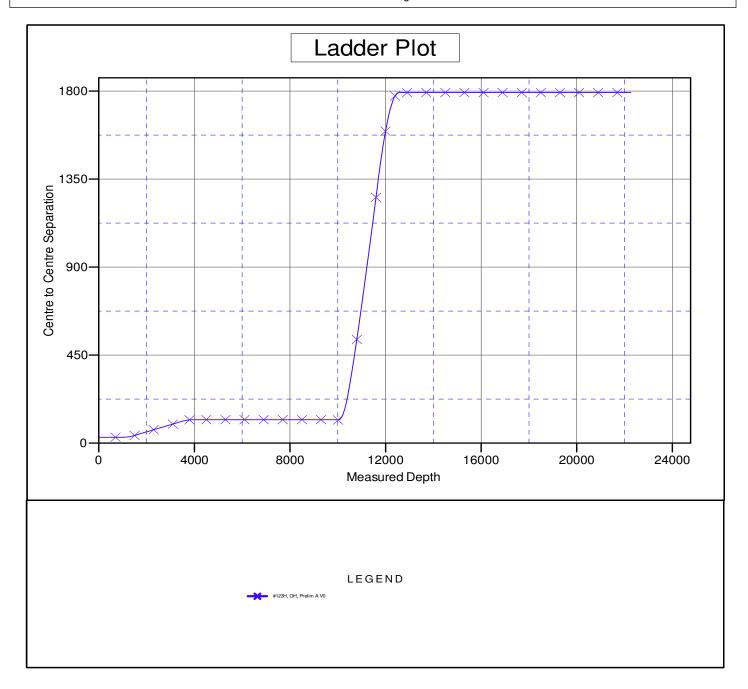
> 2.00 sigma WellPlanner1 Offset Datum

Reference Depths are relative to GL: 3712' + KB: 28.5' @ 3740.50usft Coordinates are relative to: #233H

Offset Depths are relative to Offset Datum

Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30

Central Meridian is -104.333334 Grid Convergence at Surface is: 0.47°





Pro Directional Anticollision Report



Matador Resources Company: Project: Lea County, NM

Uncle Ches 2116 Fed Reference Site:

0.00 usft Site Error: Reference Well: #233H Well Error: 0.00 usft Reference Wellbore OH Reference Design: Prelim A

Local Co-ordinate Reference:

Well #233H **TVD Reference:** GL: 3712' + KB: 28.5' @ 3740.50usft

(Patterson 809)

GL: 3712' + KB: 28.5' @ 3740.50usft **MD Reference:**

(Patterson 809)

Survey Calculation Method: Minimum Curvature

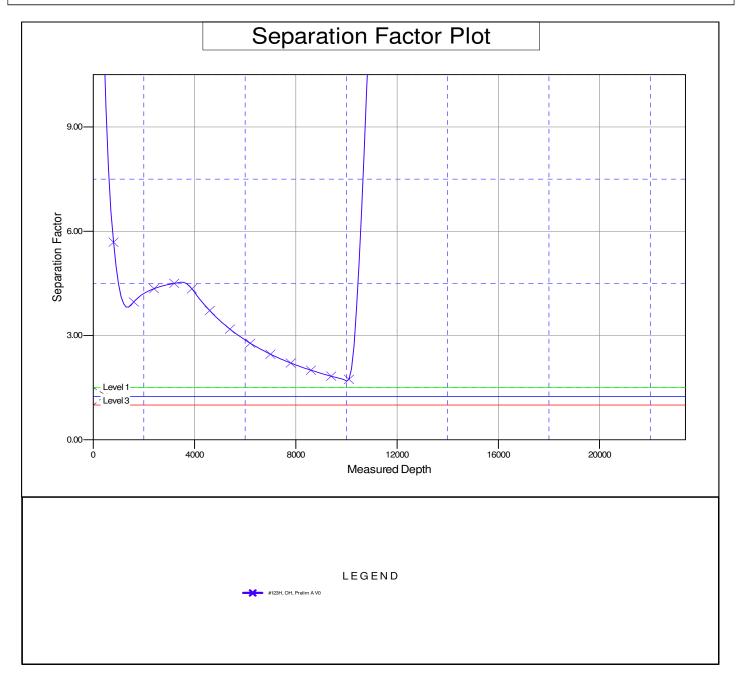
Output errors are at 2.00 sigma Database: WellPlanner1 Offset TVD Reference: Offset Datum

Reference Depths are relative to GL: 3712' + KB: 28.5' @ 3740.50usft Coordinates are relative to: #233H

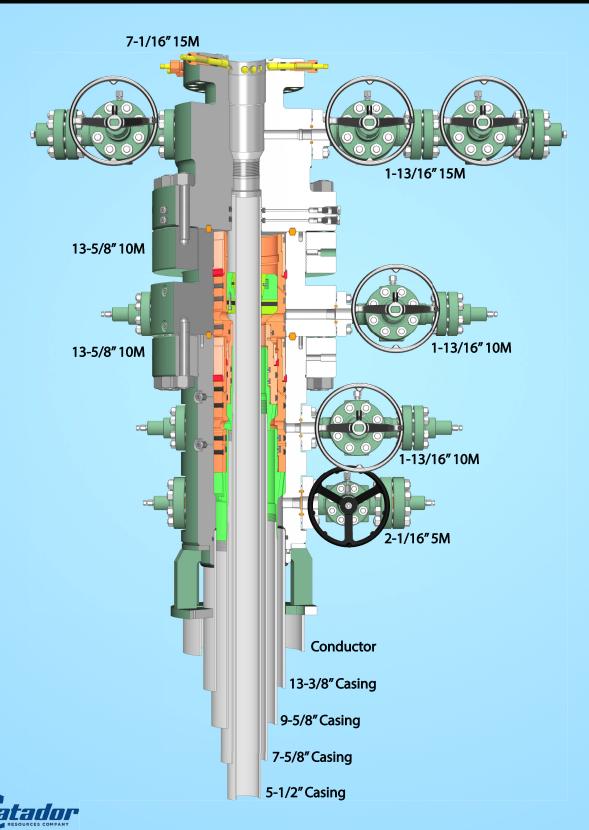
Offset Depths are relative to Offset Datum Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30

North Reference:

Central Meridian is -104.333334 Grid Convergence at Surface is: 0.47°







Closed-Loop System

Operating and Maintenance Plan:

During drilling operations, third party service companies will utilize solids control equipment to remove cuttings from the drilling fluids and collect it in haul-off bins. Equipment will be closely monitored at all times while drilling by the derrick man and the service company employees.

Closure Plan:

During drilling operations, third party service companies will haul off drill solids and fluids to an approved disposal facility. At the end of the well, all closed loop equipment will be removed from the location.

Drilling Operations Plan
Uncle Ches Fed Com #233H
Matador Resources Company
UL: O, Sec 21, 20S, 35E
Lea County, NM

Surface Location: 260' FSL & 2333' FEL, Sec. 21 Bottom Hole Location: 240' FNL & 2311' FEL, Sec. 16

Elevation Above Sea Level: 3712'

Type of Well: Horizontal well, No Pilot Hole, Drilled with conventional rotary tools

Proposed Drilling Depth: 22,270' MD / 12,222' TVD

Estimated Tops of Geological Markers w/ Mineral Bearing Formation:

Formation Name	SSTVD	TVD	Bearing
Rustler	1767	1971	Salt/Washout
Salado	1420	2318	Salt/Washout
Delaware	-2491	6229	Hydrocarbon/Loss Circ
Brushy Canyon	-3588	7326	Oil/Gas
Bone Spring Lime	-4754	8492	Oil/Gas
1st Bone Spring Carbonate	-5838	9576	Oil/Gas
1st Bone Spring Sand	-5961	9699	Oil/Gas
2nd Bone Spring Carbonate	-6295	10033	Oil/Gas
2nd Bone Spring Sand	-6640	10378	Oil/Gas
3rd Bone Spring Carbonate	-7157	10895	Oil/Gas
3rd Bone Spring Sand	-7707	11445	Oil/Gas
Wolfcamp A	-7907	11645	Oil/Gas
Wolfcamp B	-8018	11756	Oil/Gas
Wolfcamp C	-8254	11992	Oil/Gas
Wolfcamp D	-8434	12172	Oil/Gas

OSE Ground Water Estimated Depth: 877'

Casing Program

Name	Hole Size	Casing Size	Wt/Grade	Thread Collar	Setting Depth	Top Cement	
Surface	20"	13-3/8" (new)	54.5# J-55	BTC	1984	Surface	
Intermediate 1	12-1/4"	9-5/8" (new)	40# J-55 BTC		5900	Surface	
	8-3/4"	7-5/8" (new)	29.7# P-110	ВТС	0-5700		
Intermediate 2		7-5/8" (new)	29.7# P-110	VAM HTF-NR	5700-11604	4900'	
		7" (new)	29# P-110	ВТС	11604-12400	l	
Production	6-1/8"	5-1/2" (new)	20# P-110	Tenaris XP	0-11504	11400'	
		4-1/2" (new)	13.5# P-110	Tenaris XP	11504-22270		

Minimum Safety Factors: Burst: 1.125 Collapse: 1.125 Tension 1.8

Cementing Program

Drilling Operations Plan Uncle Ches Fed Com #233H Matador Resources Company UL: O, Sec 21, 20S, 35E

Lea County, NM

Name	Туре	Sacks	Yield	Weight	Blend		
Surface	Lead	2188	1.75	13.5	Class C + 3% NaCl + LCM		
	Tail	694	1.38	14.8	Class C + 5% NaCl + LCM		
TOC = 0'		100% Excess			Centralizers per Onshore Order 2.III.B.1f		
Intermediate 1	Lead	1344	1.81	13.5	Class C + Bentonite + 1% CaCL2 + 8% NaCl + LCM		
	Tail	536	1.38	14.8	Class C + 5% NaCl + LCM		
TOC = 0'		100% Excess			2 on btm jt, 1 on 2nd jt, 1 every 4th jt to surface		
Intermediate 2	Lead	940	2.36	11.5	TXI + Fluid Loss + Dispersant + Retarder + LCM		
	Tail	166	1.38	13.2	TXI + Fluid Loss + Dispersant + Retarder + LCM		
TOC = 4900'			35% Excess		2 on btm jt, 1 on 2nd jt, 1 every other jt to top of tail cement (500' above TOC), 1 every 4th jt to surface		
	- 						
Production	Tail	816	1.38	15.8	Class H + Fluid Loss + Dispersant + Retarder + LCM		
TOC = 11400'		10% Excess			2 on btm jt, 1 on 2nd jt, 1 every 4th jt to top of tail cement (1000' tie back)		

Matador requests the option to run a DV tool with annular packer as contingency in the intermediate section on 9-5/8" casing if lost circulation is encountered. If losses occur the DV tool with packer will be placed at least 100' above the loss zone to give the option to pump cement as either a single stage or two stage.

Pressure Control Equipment:

A 5000-psi BOP stack consisting of 3 rams with 2 pipe rams, 1 blind ram, and 1 annular preventer will be used below surface casing to TD. See attached BOP, choke manifold, co-flex hose, and speed head diagrams. An accumulator complying with Onshore Order 2 requirements for the BOP stack pressure rating will be present. Rotating head will be installed as needed. Pressure tests will be conducted before drilling out from under all casing strings. BOP will be inspected and operated as required in Onshore Order 2. Kelly cock and sub equipped with a full opening valve sized to fit the drill pipe and collars will be available on the rig floor in the open position. A third party company will test the BOPs.

After setting surface casing, and before drilling below the surface casing shoe, BOPE will be tested to 250 psi low and 2000 psi high. Annular will be tested to 250 psi low and 1000 psi high. After setting 9-5/8" casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high. After setting 7-5/8" x 7" Casing, pressure tests will be made to 250 psi low and 5000 psi high. Annular will tested to 250 psi low and 5000 psi high.

Drilling Operations Plan Uncle Ches Fed Com #233H Matador Resources Company UL: O, Sec 21, 20S, 35E

Lea County, NM

Matador requests a variance to drill this well using a co-flex line between the BOP and choke manifold. Certification for proposed co-flex hose is attached. Manufacturer does not require the hose to be anchored. If the specific hose is not available, then one of equal or higher rating will be used.

Matador is requesting a variance to use a speed head for setting the intermediate (9-5/8") casing. In the case of running a speed head with landing mandrel for 9-5/8" casing, BOP test pressures after setting surface casing will be 250 psi low and 5000 psi high. Annular will be tested to 250 psi low and 2500 psi high before drilling below the surface shoe. BOPE will be tested within 500 feet of the top of the Wolfcamp formation if the time between the setting of the Intermediate casing and reaching this depth exceeds 20 days. A diagram of the speed head is attached.

Proposed Mud System:

Name	Name Hole Size		Mud Weight Visc		Type Mud	
Surface	20"	8.40	28	NC	FW Spud Mud	
Intermediate 1	12-1/4"	10.00	30-32	NC	Brine Water	
Intermediate 2	8-3/4"	9.00	30-32	NC	FW/Cut Brine	
Intermediate 3	6-1/8"	12.00	50-60	<10	ОВМ	

All necessary mud products for weight addition and fluid loss control will be on location at all times. Mud program subject to change due to hole conditions.

The Mud Monitoring System is an electronic Pason system satisfying requirements of Onshore Order 1.

Testing, Logging & Coring Program:

- Mud Logging Program: 2 man unit from 1984 TD
- Electric Logging Program: No electric logs are planned at this time. GR will be collected through the MWD tools from Inter. Csg to TD
- No DSTs or cores are planned at this time
- CBL w/ CCL from as far as gravity will let it fall to TOC

Potential Hazards:

No abnormal pressures or temperatures are expected. In accordance with Onshore Order 6, Matador does not anticipate that there will be enough H₂S from the surface to the Bone Spring formations to meet the BLM's minimum requirements for the submission of an "H₂S Drilling Operation Plan" or "Public Protection Plan" for the drilling and completion of this well. Since we have an H₂S safety package on all wells, attached is an "H₂S Drilling Operations Plan". Adequate flare lines will be installed off the mud/gas separator where gas may be flared safely. All personnel will be familiar with all aspects of safe operation of equipment being used.

Estimated BHP: 6110 psi Estimated BHT: 170° F

Construction and Drilling:

Drilling Operations Plan
Uncle Ches Fed Com #233H
Matador Resources Company
UL: O, Sec 21, 20S, 35E
Lea County, NM

Road and location construction will begin after BLM approval of APD. Anticipated spud date as soon as approved. Drilling expected to take 35 days. If production casing is run an additional 30 days will be required to complete and construct surface facilities.

District I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720 District II 811 S. First St., Artesia, NM 88210 Phone: (575) 748-1283 Fax: (575) 748-9720 1000 Rio Brazos Road, Aztec, NM 87410 Phone: (505) 334-6178 Fax: (505) 334-6170 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505 Phone: (505) 476-3460 Fax: (505) 476-3462

640

State of New Mexico Energy, Minerals & Natural Resources Department OCD - HOBBS

OIL CONSERVATION DIVISION 1220 South St. Francis Dr.

Santa Fe, NM 87505

06|17|2020

FORM C-102 Revised August 1, 2011 Submit one copy to appropriate **District Office**

AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

30-025	^T API Numbe - 47339	r	98	² Pool Code 3 346		WC-025 G-09 S203521N; WOLFCAMP					
⁴ Property Code ⁵ Property Name						6W	⁶ Well Number				
326210							#	#233H			
OCIAD TANK						Elevation 3712'					
			·		¹⁰ Surface Lo	cation					
UL or let no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County		
0	21	20-S	35-E	-	260'	SOUTH	2333'	EAST	LEA		
	•		¹¹ Be	ottom Hole	Location If Di	fferent From Sur	face				
UL or lot no.	Section	Township	Range	Lot Idn	Feet from the	North/South line	Feet from the	East/West line	County		
0	16	20-S	35-E	-	240'	NORTH	2311'	EAST	LEA		
12Dedicated Acres	¹³ Joint or	Infill ¹⁴ Ce	nsolidation Code	15Order	No.	· · · · · · · · · · · · · · · · · · ·					

No allowable will be assigned to this completion until all interests have been consolidated or a non-standard unit has been approved by the division.

