

HOBBS OCD

DEC 12 2011

OCD-HOBBS

ATS-11-503

Form 3160-3
(August 2007)

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UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

Split Estate

FORM APPROVED
OMB No 1004-0137
Expires July 31, 2010

APPLICATION FOR PERMIT TO DRILL OR REENTER

1a. Type of work: <input type="checkbox"/> DRILL <input checked="" type="checkbox"/> REENTER		7. If Unit or CA Agreement, Name and No COOPER JAL NMNM-070926X	
1b. Type of Well: <input checked="" type="checkbox"/> Oil Well <input type="checkbox"/> Gas Well <input type="checkbox"/> Other <input type="checkbox"/> Single Zone <input checked="" type="checkbox"/> Multiple Zone		8. Lease Name and Well No. <306443> COOPER JAL UNIT 129	
2. Name of Operator RESACA OPERATING COMPANY		9. API Well No. 30-025-11152	
3a. Address 1331 LAMAR, SUITE 1450 HOUSTON, TX 77010-3039	3b. Phone No. (include area code) 4263848 713 650-1246	10. Field and Pool, or Exploratory JALMAT TY7RO & LANGLIE M7RQG	
4. Location of Well (Report location clearly and in accordance with Onshore Oil and Gas Order No. 1) At surface 1653' FNL & 1583' FWL Unit 1 At proposed prod. zone SAME		11. Sec., T. R. M. or Blk. and Survey or Area SENW 19-24S-37E NMMPM	
14. Distance in miles and direction from nearest town or post office* 6 AIR MILES NORTH OF JAL, NM		12. County or Parish LEA	13. State NM
15. Distance from proposed* location to nearest property or lease line, ft (Also to nearest drig. unit line, if any) 987'	16. No. of acres in lease 312.45	17. Spacing Unit dedicated to this well SENW = 40 acres	
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. 660' (Cooper Jal 208)	19. Proposed Depth 3,730'	20. BLM/BIA Bond No. on file NM B005247624	
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3,302' UNGRADED	22. Approximate date work will start* 07/22/2011	23. Estimated duration 1 WEEK	
24. Attachments			

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, must be attached to this form

- Well plat certified by a registered surveyor.
- A Drilling Plan.
- A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office).
- Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).
- Operator certification
- Such other site specific information and/or plans as may be required by the BLM.

25. Signature B. Wood	Name (Printed/Typed) BRIAN WOOD (505 466-8120)	Date 06/11/2011
Title CONSULTANT (FAX 505 466-9682)		
Approved by (Signature) /s/ James Stovall	Name (Printed/Typed)	Date DEC 06 2011
Title FIELD MANAGER	Office CARLSBAD FIELD OFFICE	

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

APPROVAL FOR TWO YEARS

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

R.5590 for DHC

*(Instructions on page 2)

Capitan Controlled Water Basin

Oil Conservation Division

Conditions of approval: Approval for drilling/workover ONLY--- CANNOT produce Downhole Commingled until DHC is approved in Santa Fe.

Kc
12/13/11SEE ATTACHED FOR
CONDITIONS OF APPROVALApproval Subject to General Requirements
& Special Stipulations Attached

DEC 13 2011

REVISED RE-ENTRY PROGNOSIS

Resaca Operating Co.
Cooper Jal Unit #129
API No. 30-025-11152
1,650' FNL, 1,587' FWL
Section 19, T-24S, R-37E
Lea Co., New Mexico

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DESCRIPTION OF OPERATION

Resaca proposes to re-enter and deepen subject well which was drilled in 1954 and plugged in 2001 as part of an effort to re-develop certain acreage within the Cooper Jal Unit, an existing Secondary Recovery project. The Unitized Interval includes both the Jalmat and the Langlie Mattix pools. Subject well will be commingled as to these intervals, and utilized as a producing well. Commingling authority will be obtained prior to production.

1) SURFACE DESCRIPTION

The surface is a mildly undulating dunal plain consisting of Quaternary alluvium sediments. Vegetation is sparse, and includes snakeweed, shinoak, yucca cactus, assorted grasses and, on a more limited basis, other flora. The ground elevation at the wellsite is 3,310' above sea level.

2) FORMATION TOPS

Formation	Estimated Top - MD (ft)	Lithology	Fluid Content
Alluvium	0	Sand, Caliche	Fresh Water
Ogalalla	146	Red Beds	None
Rustler	1,188	Anhydrite	None
Salado	1,293	Salt	None
Tansill	2,936	Anhydrite, Dolomite	None
Yates	3,001	Sandstone, Dolomite	Oil
Seven Rivers	3,226	Sandstone, Dolomite	Oil
Queen	3,635	Sandstone, Dolomite	Oil

The surface casing previously set and cemented in this well isolates and thereby protects the fresh water interval. The production casing previously set and cemented in this well isolates various productive intervals. It is not anticipated that any additional casing or remedial cementing will be required. The deepened portion of the well will extend the existing open-hole interval.

The Jalmat Pool is defined, in this area, as the interval from the top of the Tansill formation to a point 250' above the base of the Seven Rivers formation, thereby including all of the Yates formation. The top of the Tansill formation is at a depth of 2,936' in subject well.

The Langlie Mattix Pool is defined as the interval from 100' above the base of the Seven Rivers formation to the base of the Queen formation. The base of the Queen formation is estimated from offset well logs to be below the proposed total depth of subject well.

3) WELL CONTROL EQUIPMENT

A 2M system (as defined by BLM Onshore Oil and Gas Order No. 2), including a 3,000 PSI dual ram BOP dressed with 2-7/8" pipe rams and blind rams and choke manifold will be utilized throughout the proposed operations. The configuration and components of the BOP stack are set forth on Exhibit A, attached hereto. The configuration and components of the choke manifold are set forth on Exhibit B, attached hereto. The serial number and a copy of the test certificate for the rubber hose which will connect the BOP stack to the choke manifold will be provided by sundry notice prior to commencement of operations. *See COA* Flex line request will be approved when sundry submitted.*

All blowout prevention equipment will meet the minimum standards outlined in BLM Onshore Oil and Gas Order 2. A schematic indicating the routing to the choke manifold and the closed loop system is attached hereto as Exhibit C. A safety valve and crossovers to facilitate make-up to each workstring component will be kept on or near the rig floor.

The blowout preventers and choke manifold will be tested in accordance with the provisions of BLM Onshore Oil and Gas Order 2 upon installation. Pipe rams will be function tested once each 24-hour period, and blind rams will be function tested each time the workstring is out of the hole.

4) WELL CONSTRUCTION

Surface and production casing were set and cemented when the well was drilled in 1954. A 3,000 psi socket weld wellhead will be installed on the 8-5/8" surface casing, and a 3,000 psi socket weld tubing head will be installed on the 5-1/2" production casing.

Existing casing is as follows:

Hole Size (in)	Setting Depth (ft)	Outer Diameter (in)	Weight (ppf)	Grade	Threads
Unknown	330	8.625	Unknown	Unknown	Unknown
Unknown	3,386	5.500	Unknown	Unknown	Unknown

A casing design audit has been conducted as follows:

- Maximum collapse loading was assumed to occur at the bottom of each casing string. An external pressure equivalent to that which would be exerted by a column of 10 ppg brine water (0.520 psi/ft), and an internal pressure of 0 psi were assumed.
- Maximum burst loading was assumed to occur at the top of each casing string. An internal pressure equivalent to that which would be exerted at setting depth by a column of 10 ppg brine water (0.520 psi/ft), and an external pressure of 0 psi were assumed.

- Tensile loading was not evaluated as both casing strings have been run and are cemented in place.
- To the extent the casing weight and grade are unknown, the lowest API standard weight and grade were assumed.

Based upon these evaluation criteria, the surface casing was determined to have a collapse safety factor of 9.56 and a burst safety factor of 14.39, and the production casing was determined to have a collapse safety factor of 1.49 and a burst safety factor of 1.77.

The surface casing was cemented with 175 sacks of cement of unknown composition and yield. Available well records do not document circulation of the cement to surface; however, the calculated cement top, based on an assumed hole size of 12-1/4", yield of 1.18 ft³/sk (neat Class A), and hole enlargement factor of 20 percent, is at the surface.

The production casing was cemented in two stages. For the first stage, 200 sacks of cement of unknown composition and yield were pumped. Available well records do not document the top of cement; however, the calculated cement top, based on an assumed hole size of 7-7/8", yield of 1.18 ft³/sk (neat Class A), and hole enlargement factor of 20 percent, is at 2,297'. A DV tool was set at an unknown depth, and for the second stage, 100 sacks of cement of unknown composition and yield were pumped. Available well records do not document circulation of the cement to surface. It is noted that the actual cement top is obviously below 400', as during plugging operations, the production casing was perforated at 400', and cement was circulated to the surface through the annulus.

5) WORKING FLUID

Working fluid will be fresh water with 2% KCl, with a density of 8.4 ppg. Gelled sweeps and lost circulation material will be utilized as necessary. Working volume will be approximately 500 barrels. Given the low anticipated bottom-hole pressure, use of weighting materials is not anticipated, and no circulating system monitoring equipment will be utilized.

6) LOGGING, CORING AND TESTING

No mud-logging, coring, or testing are anticipated. The Unitized Interval will be logged in whole or part. Specific logs to be run have not yet been determined.

7) ANTICIPATED PRESSURES AND DRILLING HAZARDS

All formations above the Unitized Interval are cased off. The previous producing intervals, as well as the interval through which the well will be deepened, are believed to be partially pressure depleted due to production from the Unit and surrounding wells.

Based on a static fluid level survey conducted in May 2009 in an offset well (the Cooper Jal #401), reservoir pressure was 247 psi at a depth of 3,330'. Since that time, increased injection rates have been sustained, and reservoir pressure is likely to have risen; however, it is anticipated that the working fluid will create an overbalanced condition, and lost circulation may occur.

Hydrogen Sulfide may be present in the Yates and Seven Rivers. H₂S equipment will be operational prior to drilling out any cement plugs, and all operations will be conducted in accordance with BLM Onshore Oil and Gas Order 6. An H₂S plan is attached.

GENERAL PROCEDURE

- 1) Remove dry hole marker. Dress casing as necessary. Install 3,000 psi socket weld wellhead on 8-5/8" casing. Install 3,000 psi socket weld tubing head on 5-1/2" casing. Install 3,000 psi drilling flange.
- 2) MIRU pulling unit and reverse unit. Closed loop system to be utilized. Install H₂S equipment.

- 3) N/U and test 2M BOP system as depicted on Exhibits A and B.

- 4) P/U 4-3/4" bit on 2-7/8" production tubing (BHA design to be determined), and drill out:

- a. Cement plug surface – 400' +/-
- b. Cement plug 1,070' – 1,300 +/- (previously tagged)
- c. Cement plug 2,700' – 2,975' (not previously tagged)
- d. CIBP @ 2,975'.

- 5) Clean out well to 3,670' (current TD). Drill new hole to 3,730'. Circulate well clean and POOH and L/D 4-3/4" bit.

- 6) Log per supplemental procedure.

- 7) P/U 5-1/2" tension packer and RIH to 2,970'. Set packer @ 2,970' and test casing to 500 psi. If leaks occur, isolate and repair per supplemental procedure. POOH and L/D packer.

- 8) Perforate well 2 spf (120 degree phasing) as follows:

- a. 3,369' – 3,372'
- b. 3,350' – 3,354'
- c. 3,332' – 3,337'
- d. 3,275' – 3,279'.

- 9) Frac well and flow back per supplemental procedure.

- 10) P/U 5-1/2" TAC and RIH w/ 2-7/8" production tubing. Space out and set TAC per supplemental procedure. Land tubing.

- 11) N/D BOPs. N/U pumping tee.

- 12) N/U rod stripper. P/U & RIH w/ downhole pump and rods (design to be determined). Seat pump. Hang off rods. N/D rod stripper and pack off rods.

See
COA

See
COA *

See COA
For CIT

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COA *

SEE EMAIL FROM Bob Porter

13) RDMO pulling unit and other equipment.

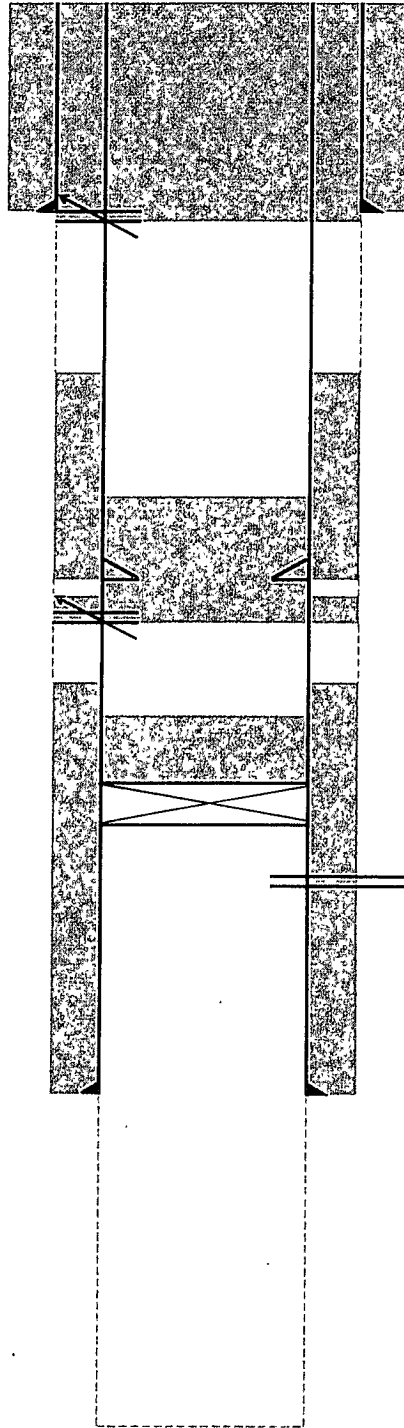
CURRENT WELLBORE SCHEMATIC

Operator: Resaca Operating Co.
Well Name: Cooper Jal #129
Well Location: 1650' FNL, 1587' FWL
Calls: F
Unit: 19
Section: 24S
Township: 37E
Range:

perf sqz holes @ 400'
sqz 155 sx cmt, circulated to surface

perf sqz holes @ 1300'
sqz 50 sx cmt
TOC tagged inside 5 1/2" @ 1070'

CIBP @ 2975' w/ 30 sx cmt



Surface Casing

Hole Size (in): Unknown
Casing Size (in): 8 5/8
Casing Weight (ppf): Unknown
Setting Depth (ft): 330
Amount Cement (sx): 175
Top of Cement (ft): Unknown
TOC Method: -----

DV Tool

Depth (ft): Unknown
Amount Cement (sx): 100
Top of Cement (ft): Unknown
TOC Method: -----

Perforations

Top (ft): 3018
Bottom (ft): 3215

Production Casing

Hole Size (in): Unknown
Casing Size (in): 5 1/2
Casing Weight (ppf): Unknown
Setting Depth (ft): 3386
Amount Cement (sx): 200
Top of Cement (ft): Unknown
TOC Method: -----

Open Hole

Hole Size (in): Unknown
Top (ft): 3386
Bottom (ft): 3670

Total Depth (ft) 3670

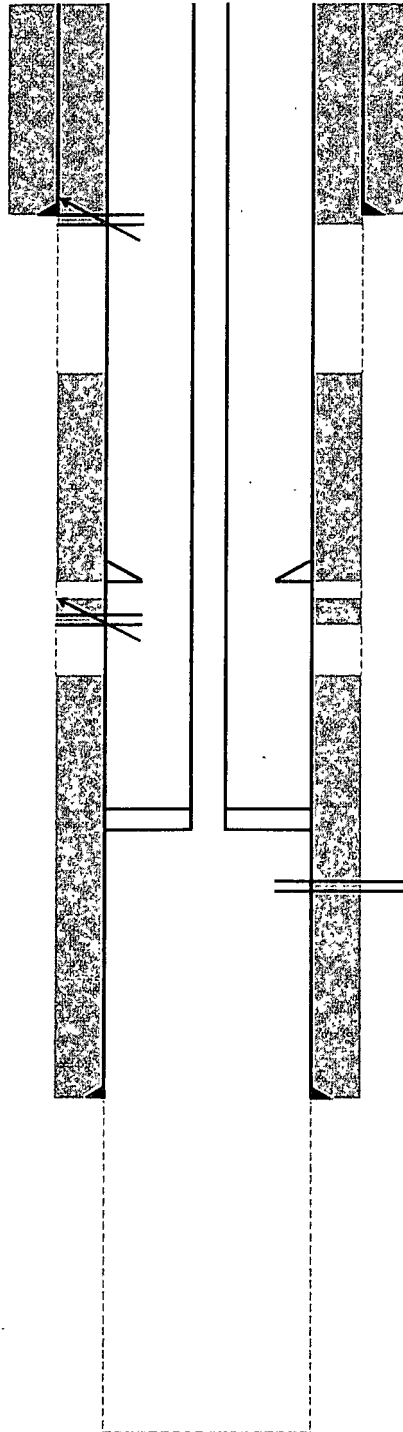
3730'

PROPOSED WELLBORE SCHEMATIC

Operator: Resaca Operating Co
 Well Name: Cooper Jal #129
 Well Location:
 Calls: 1650' FNL, 1587' FWL
 Unit: F
 Section: 19
 Township: 24S
 Range: 37E

perf sqz holes @ 400'
 sqz 155 sx cmt, circulated to surface

perf sqz holes @ 1300'
 sqz 50 sx cmt



Total Depth (ft) 3730

Surface Casing

Hole Size (in): Unknown
 Casing Size (in): 8 5/8
 Casing Weight (ppf): Unknown
 Setting Depth (ft): 330
 Amount Cement (sx): 175
 Top of Cement (ft): Unknown
 TOC Method: -----

DV Tool

Depth (ft): Unknown
 Amount Cement (sx): 100
 Top of Cement (ft): Unknown
 TOC Method: -----

Production Tubing

Tubing Size (in): 2 7/8
 Tubing Weight (ppf): 6.5
 TAC Depth (ft): 3000
 Setting Depth (ft): 3000

Perforations

Top (ft): 3018
 Bottom (ft): 3372

Production Casing

Hole Size (in): Unknown
 Casing Size (in): 5 1/2
 Casing Weight (ppf): Unknown
 Setting Depth (ft): 3386
 Amount Cement (sx): 200
 Top of Cement (ft): Unknown
 TOC Method: -----

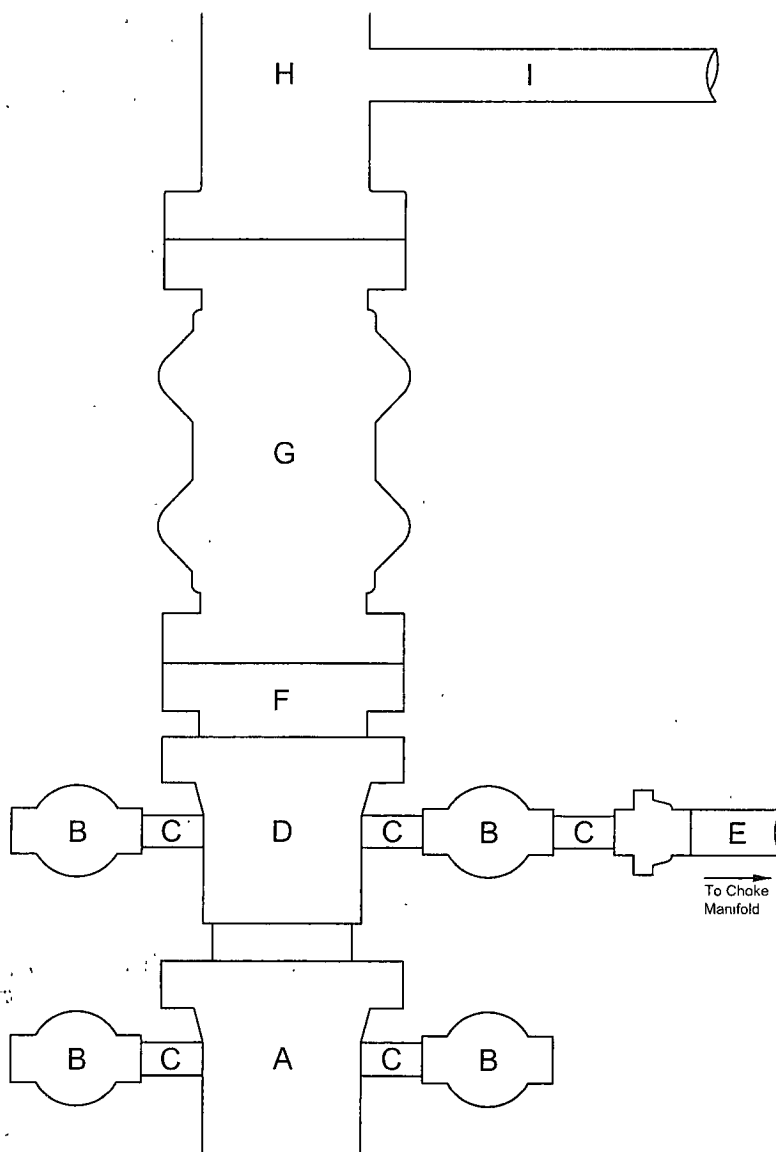
Open Hole

Hole Size (in): 4 3/4
 Top (ft): 3386
 Bottom (ft): 3730

REVISED EXHIBIT A:

2M BOP STACK CONFIGURATION - CJU #129

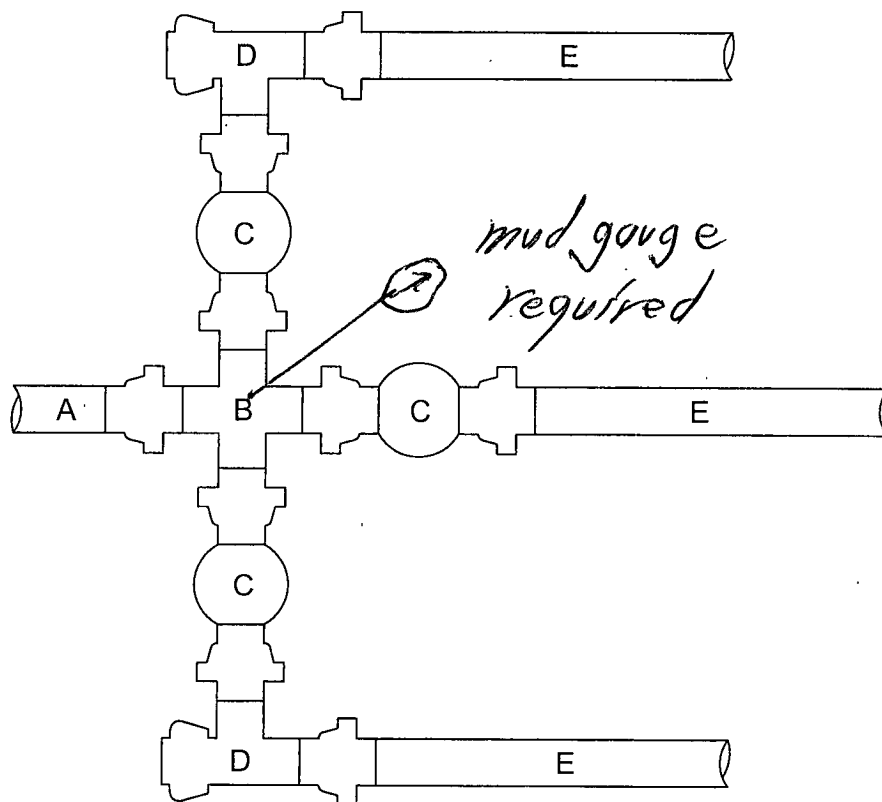
- See COA**
- A. 8 $\frac{5}{8}$ " SW x 10 $\frac{3}{4}$ " 3000 PSI WP Casing Mandrel w/ Threaded Outlets
 - B. 2 $\frac{1}{16}$ " 3000 PSI WP Ball Valve
 - C. 2" Schedule 80 Nipple
 - D. 5 $\frac{1}{2}$ " SW x 8 $\frac{5}{8}$ " 3000 PSI WP Tubing Head w/ Threaded Outlets
 - E. 2" 2500 PSI WP Rubber Hose — *see COA*
 - F. 8 $\frac{5}{8}$ " x 7 $\frac{1}{16}$ " 3000 PSI WP Drilling Flange
 - G. 7 $\frac{1}{16}$ " 3000 PSI WP Type "U" Double Ram Type BOP w/ Blind Rams & 2 $\frac{7}{8}$ " Pipe Rams
 - H. Bell Nipple
 - I. Fill-Up Line



REVISED EXHIBIT B:

2M CHOKE MANIFOLD CONFIGURATION

- A. 2" 2500 PSI WP Rubber Hose
- B. 2 $\frac{1}{16}$ " 3000 PSI WP Cross
- C. 2 $\frac{1}{16}$ " 3000 PSI WP Ball Valve
- D. 2 $\frac{1}{16}$ " 3000 PSI WP Manual Choke
- E. 2" Schedule 80 Line Pipe



Note: All connections are hammer unions.