Submit 1 Copy To Appropriate District Form C-103 State of New Mexico Office Revised August 1, 2011 Energy, Minerals and Natural Resources District I - (575) 393-6161 WELL API NO. 1625 N. French Dr., Hobbs, NM 88240 District II - (575) 748-1283 30-025-38576 OIL CONSERVATION DIVISION 811 S. First St., Artesia, NM 88210 5. Indicate Type of Lease 1220 South St. Francis Dr. District III - (505) 334-6178 STATE 🖂 FEE \square 1000 Rio Brazos Rd., Aztec, NM 87410 Santa Fe, NM 87505 6. State Oil & Gas Lease No. District IV - (505) 476-3460 1220 S. St. Francis Dr., Santa Fe, NM V07530-0001 87505 SUNDRY NOTICES AND REPORTS ON WELLS 7. Lease Name or Unit Agreement Name (DO NOT USE THIS FORM FOR PROPOSALS TO DRILL OR TO DEEPEN OR PLUG BACK TO A Linam AGI DIFFERENT RESERVOIR. USE "APPLICATION FOR PERMIT" (FORM C-101) FOR SUCH PROPOSALS.) 8. Well Number 1 1. Type of Well: Oil Well Gas Well Other Injection 9. OGRID Number 36785 2. Name of Operator DCP Midstream LP 10. Pool name or Wildcat 3. Address of Operator 370 17th Street, Suite 2500, Denver, CO 80202 AGI - Wolfcamp 4. Well Location Unit Letter K: 1980 feet from the South line and 1980 feet from the west line Township 18S Range **NMPM** Section 30 County Lea 11. Elevation (Show whether DR, RKB, RT, GR, etc.) 3736 GR 12. Check Appropriate Box to Indicate Nature of Notice, Report or Other Data NOTICE OF INTENTION TO: SUBSEQUENT REPORT OF: PERFORM REMEDIAL WORK PLUG AND ABANDON REMEDIAL WORK ALTERING CASING [**TEMPORARILY ABANDON** П **CHANGE PLANS** COMMENCE DRILLING OPNS.□ P AND A П MULTIPLE COMPL П CASING/CEMENT JOB PULL OR ALTER CASING П DOWNHOLE COMMINGLE \Box OTHER: 13. Describe proposed or completed operations. (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion. Purpose of this workover is to describe the proposed procedure for the repair of the Linam AGI#1 to address tubing leak and weakened casing. While running in hole on 5/2/12 with replacement packer, the packer became stuck and set at approximately 830' in the 7" casing. Currently operator is milling out permanent packer to continue with modified completion operation which will result in returning well to original configuration with an additional corrosion inhibited packer fluid to protect section of weakened casing and aid in maintaining long term integrity of operation. Ultimately it is operator's intent to install a two packer system at next scheduled turnaround or if monitoring of well operation or result of MIT indicates loss of integrity. Please see attached detailed description and revised well bore diagram. 1. Run in hole with milling tool to mill out miss set new Inconel packer at approximately 830' Spear and remove packer from hole, inspect removed packer, check for casing damage Notify OCD and pressure test casing/tubing annulus to 500 psi. Chart for 30 minutes. 4. Run in hole with a new string of tubing and SSSV. Clean out annulus, treat and load annulus with inhibited diesel packer fluid 5. Install new injection tree. 6. 7. Remove blanking plugs 8. Notify OCD of MIT test. Pressure test casing/tubing annulus to 500 psi. Chart for 30 minutes. Bleed pressure 200# SICP at end of job. 10. File a C-103 subsequent report with the MIT. I hereby certify that the information above is true and complete to the best of my knowledge and belief. SIGNATURE TITLE Consultant to DCP Midstream DATE 05/03/2012 Type or print name Alberto A. Gutierrez, RG E-mail address: aag@geolex.com PHONE: 505-842-8000 For State Use Only

TITLE

APPROVED BY

Conditions of Approval (if any);

DATE 5-3-2012

MAY 0 3 2012



During a planned plant turn around at the Linam plant in Hobbs New Mexico the waste stream disposal well was pulled due to a known hole in tubing. When the equipment was pulled severe corrosion was observed on the tubing immediately above the packer. The initial investigation reviled primarily corrosion on the outside diameter of the tubing and consisted of CO_2 , H_2S and possible MIC corrosion. Sections of the corroded tubing have been collected to be submitted to 3^{rd} party metallurgical labs for further investigation.

During the previous installation the annulus of the well above the packer was circulated to surface with diesel fuel and did not contain additional corrosion inhibition chemicals. Some residual water was likely present above the packer which led to the corrosive environment. This area appears to also have been affected by some internal corrosion in the same two tubing ioints above the packer. A wall thickness survey of the entire tubing string revealed that there is no effective wall thickness reduction in the tubing except in the immediate area where the holes have developed in the lowermost two joints of tubing. A microvertilog was done inside the casing after removing the tubing string to evaluate the condition of the casing and only a portion of the lowermost joint has been affected. A pressure test (MIT) conducted on the casing at 1500 psi demonstrates that the casing, while weakened by the conditions which formerly existed immediately above the packer, still has integrity to pass required MIT. Since the attempt to run a new packer to have a stacked packer system was unsuccessful and replacement packer requires significant lead time, the decision has been made to modify the operation to get the well back online while taking substantive steps to protect and monitor the condition of the casing in this zone. Ultimately it is the operator's intent to address the reduction in wall thickness in this area by running an additional packer in the well immediately above the affected area of the casing, sting into the lower packer and provide enhanced protection of the well in addition to the proposed revisions in the packer fluid. The relative timing of inside and outside corrosion at this level are the continuing focus of a forensic investigation and root cause analysis. However we have developed a treatment and packer fluid strategy that addresses the multiple potential mechanisms of this failure that will minimize the potential for future corrosion.

Proposed Workover, Well Repair and Operating Procedure

DCP has developed a targeted systematic approach to mitigate potential corrosion issues in the annulus in the future. This approach consists of a two pronged approach to repair the damage encountered in the well. The strategy and plan are as follows:

- Make a mechanical repair of the well that replaces all tubulars in the well with the exception of the SSSV which is fully functional and whose integrity has not been affected (see attached well bore diagram).
- Implement a well annulus treatment and packer fluid introduction method and composition that addresses the potential multiple causes of the observed damage to the well tubulars over the entire string but especially in the areas where problems have been encountered in the well. (see attached MSDS for treatments and additives)
- 3. Conduct continued pressure, annular pressure, temperature and flow rate monitoring and monthly reporting to NMOCD of this monitoring data
- Conduct annual MITsunder NMOCD supervision until future turnaround allows for developing the stacked packer system every 6 months

The initial step of the well bore and annular fluid preparation strategy includes a remedial biocide treatment to accomplish a kill of bacteria that are potentially currently in the well bore. The biocide treatment will consist of 55 gallons of Bactron K-139 in a 50 bbl pill. The calculated



concentration of the biocide pill is ~2.6%. At this high concentration the biocide pill can be diluted back with water that is the wellbore and still maintain sufficient concentration to achieve a complete kill.

The second step of the strategy consists of a 200 gallon methanol pad treated 1 gallon of Cortron RU-160 oxygen inhibitor to aid in removing water from the annulus, separate the water and diesel to prevent water hold up, diesel/water emulsification and prevent oxygen induced corrosion.

The final step in the process is to circulate diesel to the surface with 360 bbls diesel treated with 275 gallons of Cortron R-2525. Cortron R-2525 is an oil soluble, highly water dispersal corrosion inhibitor that was found to partially partition to the water phase with the prescribed application.

All of the products and carrier fluids recommended have been tested in the lab for compatibility and have been found to be compatible (see attached MSDS).

Procedure for treatment and packer fluid preparation

- 1) Mix 55 gallons of Bactron K-139 in 50 bbls of 10 # Brine
- 2) Pump biocide pill down the tubing
- 3) Mix 1 gallon of Cortron RU-160 in 200 gallons of methanol
- 4) Pump methanol / Cortron RU-160 down mixture the tubing
- 5) Pump 360 bbls of diesel down the tubing treated on the fly with 275 gallons of Cortron R-2525
- 6) Set tubing in packer and close casing valves

DCP LINAM AGI #1 WELLBORE SCHEMATIC

Location:	1980' FSL, 1980' FWL					SURFACE CASING:	
STR	30-T18S-R37E					13 3/8", 48.00#/ft, H40, STC at 530'	
County, St.:	: LEA, NEW MEXICO						
				777	- !		
			مآن م کد		!		
	, , ,				! !	INTERMEDIATE CAS	SING:
			- 1 ° - 1		\$ •	9 5/8", 40.00#/ft, J55, LT	
	4° 3	이		J. 19 60 3	SSSV at 250'	20.0 , 1000	
		' '					
					!		
i^			121		Ī		
20.	13. J		, ,	1.	<u>}</u>		
r li	- '5				OH = 17.1/2"		
	1 4				OH = 17 1/2"	DD OD WOTTON G . ON	. ~
	,				·	PRODUCTION CASING:	
					13 3/8" at 530'	7", 26.00#/ft, L80, STC at 9200'	
وأساب			1	٠. ٠.		PBTD = 9137'	
	F .	1					
	10 Mg	ł					
1.5			1.5		OH = 12 1/4"		
i si		1	5 W.			TUBING:	
			~ .		9 5/8" at 4212'	Subsurface Safety Valve	at 250 ft
	33						
			آور	i	$OH = 8 \ 3/4"$	3 1/2", 9.2#/ft, L80, Hun	ting SLF at 8650'
	Į 1			1		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	1	l ,		1	DV Tool at 5686'		
	i I	1	1	i	2 . 10014.0000	PACKER:	
	-, ·	1		7	Primary TOC @ 5,955'	Permanent Production Pa	ocker
	10.3	l '		() 21	111111ary 100 (6, 5,755	Adjustable Choke	ierei
	ا رُدُا		1 :5	3		Check valve	
	1-1-2			i	•	Check valve	
			<u> </u>		2.1/20 0/50	BACKED ELLIP (COL	AN ACION INVINIMEN
	()	1		-	- 3 1/2" to 8650'	PACKER FLUID (CORROSION INHIBITED):	
			i i		Diesel w/ Cortron R-2525 (Corrosion inhibitor and		
	<i>-</i> ,	I	1 ."	•		oxygen scavenger)	
		이		: :	Profile Nipple		
	F 95	1	1.5	·Ì		PERFORATIONS:	
			;	ों			
	$: \; \boxtimes$	1	\mathbf{X}		Packer at 8650'	Primary Target	Secondary Target
			<u></u>	4			
		이	1	<u> </u>	Adjustable Choke (NA)	Lower Bone Springs	Brushy Canyon
				7	Check valve	8710' - 8730'	5000' to 5300'
	, i.					8755' - 8765'	(Not perforated)
	. 3.3			=	Perforations	8780' - 8795'	
		•			8710' to 9085'	8780' - 8890'	
				=	· · · ·	8925' - 8930'	
				季		8945' - 8975'	
				3		8985' - 9000'	
	; :						
				7		9045' - 9085'	
	4			. 1	70 DDTD -4 01370	· · · · · · · · · · · · · · · · · · ·	
TD	9213'				7" PBTD at 9137'		
ID:	7413						i