Form 3.160 ₂ 5 (June 1990) DEPA BUREA	UNITED STATES N.M. OII Cons. I RTMENT OF THE INTERIOS N. French AU OF LAND MANAGEMENT HODDS, NM 882	Dr.
Do not use this form for proposals	NOTICES AND REPORTS ON WELLS s to drill or to deepen or reentry to a different reserv TION FOR PERMIT—" for such proposals SUBMIT IN TRIPLICATE	5. Lease Designation and Serial No.
Type of Well Oil Well Gas Well Other Other DEVON ENERGY PRODUCTION Address and Telephone No.		7. If Unit or CA, Agreement Designation 8. Well Name and No. Bradley A 1 9. API Well No.
4. Location of Well (Footage. Sec., T., R., M. at surface 1980 FNL & 1650 FWL		512 30-025-21168 10. Field and Pool, or Exploratory Area Bell lake Morrow South 11. County or Parish, State Lea, NM
	E BOX(s) TO INDICATE NATURE OF NOTIC	E, REPORT, OR OTHER DATA
TYPE OF SUBMISSION	TYPE OF	ACTION
 Notice of Intent Subsequent Report Final Abandonment Notice 	Abandonment Recompletion Plugging Back Casing Repair Altering Casing Other <u>Sidetrack</u>	Change of Plans Change of Plans New Construction Non-Routine Fracturing Water Shut-Off Conversion to Injection Dispose Water (Note: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)
13. Describe Proposed or Completed Operations (Cla subsurface locations and measured and true va	early state all pertinent details, and give pertinent dates, including estimated date rtical depths for all markers and zones pertinent to this work.)*	of starting any proposed work. If well is directionally drilled, give

Devon Energy request approval to change the proration unit on the referenced well from the W2 to the N2. We also request approval to cancel the APD on the Paloma Blanco 19 Federal #1 API #30-025-36065.

Devon Energy successfully reentered this plugged well and has determined that the well is a suitable candidate to perform a sidetrack. Devon requests approval to set a CIBP and whipstock at approximately 10,500' and make a casing exit in the existing 9-5/8" casing. An 8-3/4" hole will be drilled while building angle to ~40 degrees and at a depth of approximately 12,200' 7" casing will be run and cemented back to the 9-5/8" casing. A 6-1/8" hole will be drilled to penetrate the Morrow at a bottomhole location of 1980' FNL & 1980' FEL. If the well is productive, a 4-1/2" liner will be run and cemented back into the 7" casing. BOP 5000psi. See attached.

		APR (2003 61 10)
14. I hereby certify that the foregoing is true and correct		PETROLE GOULER
+	Karen A. Cottom	PETROLEUM ENSAue
Signed Clerken	Title Engineering Technician	Date April 2 20 CLOV 1 9 CHO
(This space for Federal or State office use)		
Approved by Conditions of approval, if any:	Title	Date
Title 18 U.S.C. Section 1001, makes it a crime for any person knowingly and willfully to any matter within its jurisdiction.	y to make to any department or agency of the	United States any false, fictitious or fraudulent statements or representations as

		-														
District I							State of	New	Mexico		-				For	m C-102
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District II		Energy, Minerals & Natural Resources Department					c	Submit to Appropriate District Office								
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Diendet III				10	20 South	h C+	Francis D	*					e Lease -	•		
1000 Rio Brazos Rd.,				14				1.				Fe	e Lease -	3 Copies		
District IV							Santa F	e, NI	M 87505					_		
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Well name: Operator: **N/A** String type: Intermediate: Prod'n

Bradley "A" #1

- I

Design parameters: <u>Collapse</u> Mud weight: 10.000 ppg Design is based on evacuated pipe.				Minimum design factors: <u>Collapse:</u> Design factor 1.125			Environm H2S consid Surface tem Bottom hole Temperatur	0.70 °F/100ft	
	anticipated		2,500 psi	<u>Burst:</u> Design fac	tor	1.00	Minimum se	ection length:	517 ft
Inter Calc	ressure: nal gradient ulated BHP backup mud	•	2,500 psi 0.427 psi/ft 7,625 psi	Tension: 8 Round S 8 Round L Buttress: Premium: Body yield: Tension is Neutral poi	TC: : based on air	1.80 (J) 1.80 (J) 1.60 (J) 1.50 (J) 1.60 (B) weight. 0,187 ft	Kick-off poin Departure a Maximum d Inclination a Re subseq Next set Next mu Next set Fracture Fracture	t shoe: ogleg: t shoe: u ent strings ting depth: d weight: ting BHP: mud wt:	10500 ft 697 ft 3 °/100ft 43.52 °
Run Seq 1	Segment Length (ft) 12200	Size (in) 7	Nominal Weight (Ibs/ft) 26.00	Grade HCP-110	End Finish LT&C	True Vert Depth (ft) 11996	Measured Depth (ft) 12200	Drift Diameter (in) 6.151	Est. Cost (\$) 126819
Run Seq 1	Collapse Load (psi) 6232	Collapse Strength (psi) 7800	Collapse Design Factor 1.25	Burst Load (psi) 7625	Burst Strength (psi) 9950	Burst Design Factor 1.30	Tension Load (kips) 311.9	Tension Strength (kips) 693	Tension Design Factor 2.22 J

Devon Energy

Date: April 8,2003 Oklahoma City, Oklahoma

Collapse is based on a vertical depth of 11996 ft, a mud weight of 10 ppg The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Remarks:

Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name: Operator: N/A String type: Liner: Production

Bradley "A" #1

Design parameters: <u>Collapse</u>	44 500	Minimum desigr <u>Collapse:</u>		Environment: H2S considered?	No
Mud weight: Design is based on evacu	11.500 ppg lated pipe.	Design factor	1.125	Surface temperature: Bottom hole temperatu Temperature gradient: Minimum section lengt	0.70 °F/100ft
		Burst:			
		Design factor	1.00		
Burst					
Max anticipated surface					
pressure:	2,348 psi			Liner top:	11.900 ft
Internal gradient:	0.427 psi/ft	Tension:		Directional Info - Build	
Calculated BHP	8,240 psi	8 Round STC:	1.80 (J)	Kick-off point	10500 ft
	•	8 Round LTC:	1.80 (J)	Departure at shoe:	2403 ft
No backup mud specified		Buttress:	1.60 (J)	Maximum dogleg:	3 °/100ft
		Premium:	1.50 (J)	Inclination at shoe:	43.52 °
		Body yield:	1.60 (B)		
		Tension is based o	n air weight.		
		Neutral point:	14,206 ft		

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (Ibs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost (\$)
1	2778	4.5	13.50	P-110	LT&C	13793	14678	3.795	15566
Run Seq 1	Collapse Load (psi) 8240	Collapse Strength (psi) 10680	Collapse Design Factor 1.30	Burst Load (psi) 8240	Burst Strength (psi) 12410	Burst Design Factor 1.51	Tension Load (kips) 27.2	Tension Strength (kips) 338	Tension Design Factor 12.43 J

Devon Energy

Date: April 8,2003 Oklahoma City, Oklahoma

For this liner string, the top is rounded to the nearest 100 ft. Collapse is based on a vertical depth of 13793 ft, a mud weight of 11.5 ppg The Collapse strength is based on the Westcott, Dunlop & Kernler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Remarks:

Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

