Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: DEVON ENERGY						Lease or Unit Name: OUTLAND ST. UNIT			
Type Test: ☑ Initial ☐ Annual ☐ Special						Test Date: 4/25/03		Well No.: 4	
Completion Date: 4/17/03		Total Depth: 13080		Plug Back TD: 13045		Elevation:		Unit Ltr - Sec - TWP - Rge: I 21S 34E	
Csg. Size: 4 1/2	Wt.: 13.5	d: 3.92	Set At: 13316	Perforations: From: 12304	To: 12324			County: LEA	
Tbg. Size: 2 3/8	Wt.: 4.7	d: 1.995	Set At: 12270	Perforations: From:	To:			Pool:	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE				Packer Set At: 12270				Formation: ATOKA	
Producing Thru: Tubing		Reservoir Temp. °F: 170.9		Mean Annual Temp. °F: 60		Baro. Press.-P_a: 13.2		Connection: SALES	
L: 12270	H: 12270	Gg: 0.611	%CO_2: 0.257	%N_2: 1.403	%H_2S: N/A	Prover: N/A	Meter Run: 4.026		Taps: FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp. °F	Press p.s.i.g.	Temp. °F	Press p.s.i.g.	Temp. °F	Duration of Flow
SI					5517	N/A	PKR	N/A	
1	4.026 X 1.500	581	8	67	5406				1 HR.
2	4.026 X 1.500	584	34	70	5385				1 HR.
3	4.026 X 1.500	596	104.1	63	5202				1 HR.
4	4.026 X 1.500	618	169.4	51	5081				1 HR.
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor P_s	Super Compress Factor P pv	Rate of Flow Q. Mcfd
1							998
2							2085
3	TOTAL	FLOW	METER				3621
4							4913
5							

No.	P_r	Temp. °R	T_r	Z
1				
2				
3	TOTAL	FLOW	METER	
4				
5				

Gas Liquid Hydrocarbon Ratio: N/A Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: N/A Deg.
Specific Gravity Separator Gas: 0.611 XXXXXXX
Specific Gravity Flowing Fluid: N/A XXXXX
Critical Pressure: 673 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 357 R. ____ R

P_s 5607.5 P_s^2 31444

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		5555.7	30865.8	578.2
2		5481.4	30045.7	1398.3
3		5371.7	28855.1	2588.9
4		5274.1	27288.7	4155.3
5				

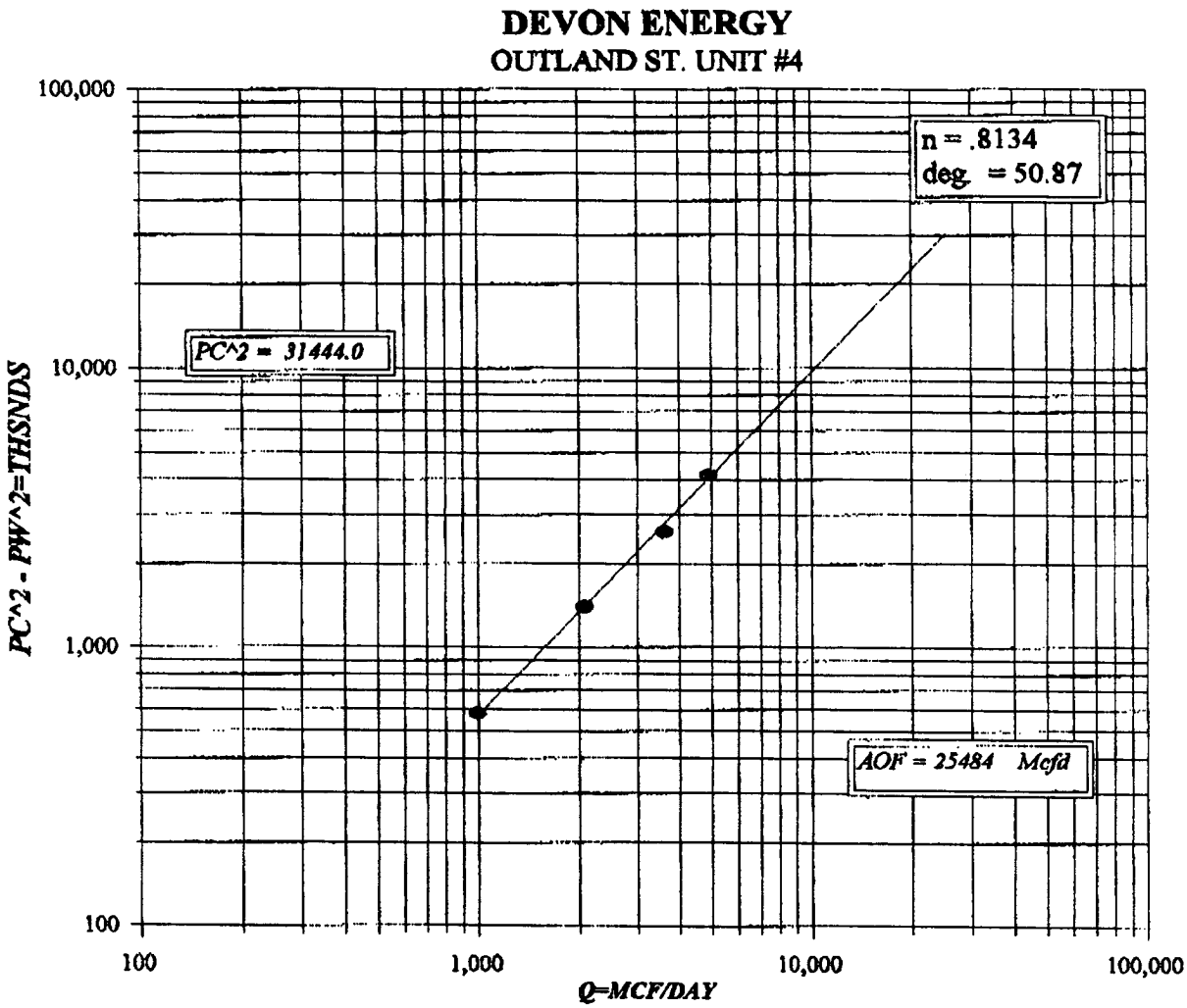
(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ 7.567 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 5.187

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 25484

Absolute Open Flow: 25484 Mcfd @ 15.025 | Angle of Slope θ: 50.87 | Slope n: 0.8134

Remarks: * NO LIQUID MADE DURING TEST. CALCULATED FROM KNOWN BOTTOM HOLE PRESSURES.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	MB


DEVON ENERGY
OUTLAND ST. UNIT #4
n = .8134
deg. = 50.87
PC^2 = 31444.0
AOF = 25484 Mcfd
PC^2 - PW^2=THSNDS
Q=MCF/DAY
100,000
10,000
1,000
100
100
1,000
10,000
100,000

C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	DEVON ENERGY		LEASE :	OUTLAND ST. UNIT	WELL NO. :	4			
UNIT :			SECTION :	1	TOWNSHIP :	21S			
L :	12270	H :	12270	L/H :	1	G/GMIX :	0.611		
%CO2 :	0.257	%N2 :	1.403	H2S :			DATE :	4/26/02	
G :	1.998	Fr :	0.018183	GH :	8197.0		RANGE :	34E	

VOL 1 :	998	PSIA 1 :	5419.2	RESV.TEMP	170.9
VOL 2 :	2085	PSIA 2 :	5898.2		
VOL 3 :	3621	PSIA 3 :	5215.2	SHUT-IN PRES =	5530.2
VOL 4 :	4919	PSIA 4 :	5094.2		
		PCR :	579		
		TCR :	348		

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.998	0.998	2.085	2.085	3.621	3.621	4.918	4.918
2	TW	534	534	534	534	534	534	534	534
3	T4	630.9	630.9	630.9	630.9	630.9	630.9	630.9	630.9
4	T	582.5	582.5	582.5	582.5	582.5	582.5	582.5	582.5
	PR (est)	7.98		7.95		7.68		7.50	
6	Z(est)	0.988	1.056	0.987	1.055	0.978	1.041	0.968	1.032
6	TZ	575.7	615.2	574.8	614.6	566.5	606.2	561.1	601.4
7	QM/TZ	14.298	13.323	14.262	13.838	14.470	13.823	14.609	13.651
8	a5	1.706	1.648	1.707	1.649	1.721	1.660	1.729	1.667
9	Hg-S	0.414	0.398	0.414	0.394	0.419	0.398	0.422	0.400
10	Pt	5419.2	5419.2	5898.2	5898.2	5215.2	5215.2	5094.2	5094.2
11	Pt2 /1000	29367.7	29367.7	29140.6	29140.6	27196.3	27196.3	26950.9	26950.9
12	Fr	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183
13	FcFrTZ	10.468	11.187	10.451	11.175	10.300	11.022	10.202	10.934
14	FcQm	10.45	11.16	21.79	23.30	37.30	39.91	50.12	53.72
15	L/H(FcQm)2	109.1	124.6	474.8	542.9	1391.1	1592.8	2512.9	2888.9
16	Fw	46.164618	49.016203	196.6756	219.65785	582.56172	638.84886	1059.7577	1154.94953
17	Pw2	29412.9	29416.7	29937.2	29384.2	27780.9	27831.9	27010.6	27105.8
18	Pt2	80166.4	48481.7	50082.1	48404.5	47797.7	46214.0	46714.9	46191.5
19	Pt	7082.8	6962.9	7076.9	6957.3	6913.6	6798.1	6834.8	6722.8
20	P	6281.0	6191.0	6237.5	6177.9	6064.4	6006.6	5964.5	5908.9
21	Pr	9.21	9.12	9.19	9.10	8.93	8.85	8.78	8.70
22	Tr	1.67	1.67	1.67	1.67	1.67	1.67	1.67	1.67
23	Z	1.056	1.051	1.055	1.050	1.041	1.036	1.032	1.028

Pc =	5607.8	Pc2 =	31444.0
Pt2 =	29367.7	Pw =	5556.7
	29140.6		5481.4
	27196.3		5371.7
	26950.9		5274.1
Pc2-Pw2=	578.2	Pw2 =	30865.8
	1398.3		30046.7
	2888.9		28555.1
	4156.3		27288.7
		n =	0.819
Pc2/(Pc2-Pw2) =			54.389
			22.487
			12.148
			7.867
(Pc2/Pc2-Pw2)n =			25.800
			12.580
			7.622
			5.187
AOF = Q			25.749
			26.228
			27.599
			25.484

FORM C122-D