Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

## State of New Mexico

Form C-122 Revised October, 1999

Energy Minerals and Natural Resources Oil Conservation Division

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				MUL	TIPOINT	AND ONE 1	2040 Sant	O South a Fe, N	Pacheco M 87505 K PRESSU		<i>30</i>	029	WEI:	37,7	7	
	<u> </u>				KAISER	FRANCIS O	il Company Lease or Unit Name									
Competion   Date   Protect   Prote	Type		. –	7			Test Da				Test Date	;				
T/20/05   T/20	Com				Spe	ecial	8/					7/05				
Set Al	7/00/10-															
The Size   With   d   Set At   11701   From:     11820   To:   11906   Lea   Peocl   Pool					Set At	-	Perfor	Perforations:								
109   207   27/8   6.5   2.441   11701   From:						From: 11820 To: 1				119	1000					
Type   Well   Single-Frademend-G   or GO   Multiple   SINGLE   Producing Thru   TUBING   Reservoir Temp   Mann Annual Temp.   60   112   TOTAL   Single-Frademend-G   or GO   Multiple   SINGLE   Producing Thru   TUBING   Reservoir Temp   Mann Annual Temp.   60   More Run   132   SALES   Single   Single   Single   SALES   Single   Single   Single   Sales   Single   Single   Sales		- 1				Perforations:										
Producing Thru    Reservoir Temp.   Maan Annual Temp.   Baro Press. P.   13.2   Connection SALES	l	1		1		From: _ To:					- Deudo South (C.)					
Producing Thrist   TuBING   Reservoir Temp.   Mean Annual Temp.   Go.	Type	Well-Single	e-Braden			le		Packer Set At – Usudo, South (Gas								
TUBING															:ow	
1.1863						13.2										
Prover Orifice				63		4.			1		Prover		7			
No.				<u> </u>		0.841	1 0	.598		DICD					1 .	
Size   Size   Size   P.S.i.g.   P.S.i.g.   P.S.i.g.   P.S.i.g.   P.S.i.g.   Flow   F	Nο	Prover Orifice			Press						12		ASING DATA		Duration	
SI	110.	A		e ,	p.s.1.g.	$h_{w}$			<b>.</b>	lemp	).			1 1		
1 3.067 X.875	SI						†		2550	+			<del>.</del>		Flow	
RATE OF FLOW CALCULATIONS  RATE OF FLOW CALCULATIONS  RATE OF FLOW CALCULATIONS  RATE OF FLOW CALCULATIONS  O		3.067 X .875		375	476	39.4		68	<del></del>	+	<del> </del>			<del> </del>	24 IIDC	
RATE OF FLOW CALCULATIONS   Rate of Flow		<del> </del>								1		+		<del> </del>	24 HRS	
RATE OF FLOW CALCULATIONS   COEFFICIENT   C44 Hour)		<del> </del>		-		<del></del>						<del>                                     </del>		<del> </del>		
RATE OF FLOW CALCULATIONS   Super Compress   Factor Ft   Gravity Factor   Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Factor Ft   Gravity Factor   Ft   Gravity						· · · · · · · · · · · · · · · · · · ·										
COEFFICIENT		<u> </u>				DATE	OFF	0117.0	17 67 - 1 -							
1	NTo.	CO	EFFICIE	ENT				JF FLOW CALCULATIONS 2031-12							2	
1		I .			$-\sqrt{h_{w}P_{m}}$	1		1		Super Compres		ss Rate of Ploy				
TOTAL   FLOW   METER									- Taking Factor	I g				V Q. McId 6.7		
A		TOTAL										73	¥			
Temp. R   Tr   Z   Gas Liquid Hydrocarbon Ratio   65   Mcf bbl.		IUIAL			FLOW	METER						4				
Temp. R												/2/		Q (20)		
A P. I. Gravity of Liquid Hydrocarbons   51 @60   Deg.	Vo.	P.	P. Temp R T 7		C. T.	Continuity										
Specific Gravity Separator Gas   Specific Gravity Flowing Fluid   N/A   XXXXXX	1	i iomp. K			11		<b>-</b> i	-		_		6	55		Mcf bbl.	
Specific Gravity Flowing Fluid   N/A   XXXXX	2				<del></del>	<del> </del> -										
Critical Pressure   673   P.S.I.A.   N/A   P.S.I.A.	3	TOTAL FLOW				-				3.714						
Critical Temperature 368 R. N/A R    P_c   2563.2   P_c^2   513.2	4															
No. $P_t^2$ $P_w$ $P_w^2$ $P_c^2 \cdot P_w^2$ (1) $P_c^2 = 1.043$ (2) $P_c^2 \cdot P_v^2$ $P_c^2 \cdot P_w^2$ AOF = Q $P_c^2 \cdot P_w^2$ $P_c^2 \cdot P_w^2$ AOF = Q $P_c^2 \cdot P_w^2$ $P_c^$		2502.0				Critical Temperature					_ I.S.	_				
1   518.7   269.1   6300.9														11/21	K	
1   318.7   269.1   6300.9	No.	P <sub>t</sub> *			$P_{\mathbf{w}}^{-2}$	$P_c^2 - P_w^2$	(1) P		$P_c^2 =$	<sup>2</sup> =		(2)	Р.	n =	1 043	
AOF = Q  P <sub>c</sub> <sup>2</sup> P <sub>c</sub>	1	···		518.7	269.1	6300.9			2 - 2			-		<u></u>	1.045	
AOF = Q P <sub>c</sub> = 0.678    P <sub>c</sub> - P <sub>w</sub>   F = 0.678	$\neg +$							Р	c - P <sub>w</sub>				$P_c^2 - 1$	$P_w^2$		
bosolute Open Flow 678 1 Mofd @ 15.025 Angle of Slope (): 45 Slope, n: 1  * WELL MADE 10 BBLS OF 51 API GRAVITY OIL DURING TEST.  * Opproved By Privision: Calculated By: Checked By:  PRO WELL TESTING  ** WERN PURCHED	3					$AOF = O \qquad \bigcap P^2$			P. 2	n = 0.678						
* WELL MADE 10 BBLS OF 51 API GRAVITY OIL DURING TEST.  **Conducted By:  **PRO WELL TESTING**  **Conducted By:  **PRO WELL TESTING**  **Conducted By:  **Conduc	4										c	-				
* WELL MADE 10 BBLS OF 51 API GRAVITY OIL DURING TEST.  **Conducted By:  **PRO WELL TESTING**  **Conducted By:  **PRO WELL TESTING**  **Conducted By:  **Conduc	5	<del></del>		,			]			$P_{\cdot}^{2}$	- P. 2				·	
* WELL MADE 10 BBLS OF 51 API GRAVITY OIL DURING TEST.  **Conducted By:  Calculated By:  PRO WELL TESTING  **WELL MADE 10 BBLS OF 51 API GRAVITY OIL DURING TEST.  Checked By:  PRO WELL TESTING	bsolu	te Open Flo	w	11	678	Mcfd @						45 Slone 2 1				
PRO WELL TESTING  Calculated By:  Checked By:  Checked By:	emark	s:			* V	VELL MADE	10 BBL				I. Di man		<u>-</u>	stope, n.	1	
PRO WELL TESTING MEDI DIFFCHED	pprov	ed By Divis	ion:	To	onducted By:	<del></del>										
		7,2 m	w/		PRO WI	ELL TESTING	<u>.                                    </u>	· ·				1				

## **KAISER FRANCIS**

