| | | ATS-13- 1103 |
|--|--|--|
| HOBBSOU | | |
| HOBBS OCD Form 3160-3 (August 2007) NOV 2 0 2013) UNITED ST | OCD Hobbs | FORM APPROVED OMB No. 1004-0137 Evices luty 21 - 2010 |
| | ATES THE INTERIOR | Expires July 31, 2010 5. Lease Serial No. NM LC 029405B |
| BUREAU OF LAND | MANAGEMENI | 6. If Indian, Allotee or Tribe Name N/A |
| la. Type of work: DRILL | EENTER | 7. If Unit or CA Agreement, Name and No N/A |
| 1b. Type of Well: 🔽 Oit Well 🛄 Gas Well 🛄 Other | Single Zone 🖌 Multiple Zone | 8. Lease Name and Well No. 386 Ruby Federal 33 |
| 2. Name of Operator ConocoPhillips Company | (217817) | 9. API Well No. 30-025-41505 |
| 3a. Address P.O. Box 51810 Midland, TX 79710-1810 | 3b. Phone No. (include area code) 432-688-6913 | 10. Field and Pool, or Exploratory Maljamar; Yeso West |
| Location of Well (Report location clearly and in accordance At surface ULG, Sec.18, T17S, R32E; 1725' FNL | | 11. Sec., T. R. M. or Blk. and Survey or Area Sec.18, T17S, R32E; |
| At proposed prod. zone UL G, Sec. 18, T17S, R32E; 2 | 2211' FNL & 1658' FEL | |
| Distance in miles and direction from nearest town or post offi Approximately 3 miles south of Maljamar, New Mexic | | 12. County or Parish13. StateLea CountyNM |
| Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) | 16. No. of acres in lease 17. Sp 1601.9 6 40 ar | pacing Unit dedicated to this well cres |
| 18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. | 19. Proposed Depth 20. B 6939' TVD/6978'MD ES0 | LM/BIA Bond No. on file 085 |
| 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3970' GL | 22. Approximate date work will start* 01/01/2014 | 23. Estimated duration9 days |
| - | 24. Attachments | |
| The following, completed in accordance with the requirements of | Onshore Oil and Gas Order No.1, must be attached | to this form: |
| Well plat certified by a registered surveyor. A Drilling Plan. A Surface Use Plan (if the location is on National Forest S SUPO must be filed with the appropriate Forest Service Official Surveyor) | Item 20 above).System Lands, the5. Operator certification | rations unless covered by an existing bond on file c information and/or plans as may be required by |
| 25. Signature Sugar B. Maun | Name (Printed/Typed) Susan B. Maunder | Date 2 |
| Title Senior Regulatory Specialist | | |
| Approved by (Signature) | Name (Printed/Typed) | NOV 15 |
| Title /S/ STEPHEN J. CAFFEY | | FIELD OFFICE |
| FIELD MANAGER Application approval does not warrant or certify that the applica conduct operations thereon. Conditions of approval, if any, are attached. | ant holds legal or equitable title to those rights in the | e subject lease which would entitle the applicant to APPROVAL FOR TWO YEA |
| Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, mak States any false, fictitious or fraudulent statements or representat | te it a crime for any person knowingly and willfully tions as to any matter within its jurisdiction. | to make to any department or agency of the Unit |
| (Continued on page 2) | OK KE 11/22/13 | *(Instructions on page Roswell Controlled Water I |

& Special Stipulations Attached

Pr

NOV 262013

Drilling Plan ConocoPhillips Company <u>Maljamar; Grayburg-San Andres, Yeso (west)</u>

Ruby Federal #33

Lea County, New Mexico

1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The datum for these depths is RKB (which is 13' above Ground Level).

| Formations | Top Depth FT TVD | Top Depths FT MD | Contents |
|-------------------------------|------------------------|------------------------|--|
| Quaternary | Surface | Surface | Fresh Water |
| Rustler | 715 | 715 | Anhydrite |
| Salado (top of salt) | 887 | 887 | Salt |
| Tansill (base of salt) | 1882 | 1882 | Gas, Oil and Water |
| Yates | 2082 | 2082 | Gas, Oil and Water |
| Seven Rivers | 2372 | 2373 | Gas, Oil and Water |
| Queen | 3015 | 3025 | Gas, Oil and Water |
| Grayburg | 3451 | 3468 | Gas, Oil and Water |
| San Andres | 3805 | 3827 | Gas, Oil and Water |
| Glorieta | 5275 | 5314 | Gas, Oil and Water |
| Paddock | 5351 | 5390 | Gas, Oil and Water |
| Blinebry | 5730 | 5769 | Gas, Oil and Water |
| Tubb | 6739 | 6778 | Gas, Oil and Water |
| Deepest estimated perforation | 6739 | 6778 | Deepest estimated perf. is ~ Top of Tubb |
| Total Depth (maximum) | 6939 | 6978 | 200' below deepest estimated perforation |

All of the water bearing formations identified above will be protected by setting of the <u>8-5/8</u> surface casing <u>25' – 70' into the Rustler formation</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the <u>5-1/2</u>" production casing <u>10' off bottom of TD</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

Ruby Federal #33

1.1

(Date: 8/8/2013)

2. Proposed casing program:

| Tuno | Hole Size | M | Interval D RKB (ft) | OD | Wt | Gr | Conn | MIY | Col | Jt Str | | Safety Fa lated per Co Corporate (| nocoPhillips |
|--------------|--------------|------|--------------------------------|----------|--------------|------|--------------|-------|-------|--------|-------------|--|---------------------------------------|
| Туре | (in) | From | То | (inches) | (lb/ft) | G | Com | (psi) | (psi) | (klbs) | Burst DF | Collapse DF | Jt Str DF (Tension) Dry/Buoyant |
| Cond | 20 | 0 | 40' – 85' (30' – 75' BGL) | 16 | 0.5" wall | В | Line Pipe | N/A | N/A | N/A | NA | NA | NA |
| Alt. Cond | 20 | 0 | 40' – 85' (30' – 75' BGL) | 13-3/8 | 48# | H-40 | PE | 1730 | 740 | N/A | NA | NA | NA |
| Surf | 12-1/4 | 0 | '740' – <u>785'</u> | 8-5/8 | 24# | J-55 | STC | 2950 | 1370 | 244 | 1.60 | 3.93 | 3.67 |
| Prod | 7-7/8 | 0 | 6923' – 6968' | 5-1/2 | 17# | L-80 | LTC | 7740 | 6290 | 338 | 2.14 | 2.52 | 2.00 |

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

| Туре | Depth | Wt | MIY | Col | Jt Str | Drill Fluid | Burst | Collapse | Tensile-Dry | Tens-Bouy |
|-------------------|-------|----|------|------|--------|-------------|-------|----------|-------------|-----------|
| Surface Casing | 785 | 24 | 2950 | 1370 | 244000 | 8.5 | 8.50 | 3.95 | 13.0 | 14.9 |
| Production Casing | 6977 | 17 | 7740 | 6290 | 338000 | 10 | 2.14 | 1.74 | 2.85 | 3.37 |

Casing Safety Factors – Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

ConocoPhillips Corporate Criteria for Minimum Design Factors

| | eeiperate en | tonia for himmani Boolgin raotoro | |
|-----------------------|--------------|-----------------------------------|-------|
| | Burst | Collapse | Axial |
| Casing Design Factors | 1.15 | 1.05 | 1.4 |

| Conductor | | Wt | | Col | Jt Str F | ipe Yiel | | Burst | Col | Ten | - | | | | | | |
|--|--|---|---|--|--|---|---|-------------------|-----------------------|------------|-----------------|---------------|----|--------|--------------------|--|--|
| Surface Casing (8-5/8" 24# J-55 STC) | 85 785 | | 5 35000 4 2950 | 137 | 0 244000 | 432966 | | - 1.60 | 0 3.9 | 3 3.6 | 57 | | | | | | |
| Production Casing (5-1/2" 17# L-80 LTC) | 6968 | 1 | 7 7740 | | 0 336000 | 397000 | | | | | 0 | | | | | | |
| Burnt ConcerDhillion Denviced Lond Conce | | | | | | | | | | | | | | | | | |
| Burst - ConocoPhillips Required Load Cases The maximum internal (burst) load on the Surface Casing occurs when the | e surface cas | ung is te | sled to 1500 | psi (as j | per BLM Onahi | ore Order 2 | - iil Require | ments). | | | | | | | | | |
| The maximum internal (bursi) load on the Production Casing occurs during (MAWP) is the pressure that would fit ConocoPh@ps Corporate Criteria for | | | on where the | maximu | m allowable w | orking pres | sure | | | | | | | | | | |
| (MANNE) is the pressure that would be concerning a corporate cruent for Surface Casing Test Pressure = | 1500 | | | Pred | icted Pore Pres | sure at TD | (PPTD) = | 8.5 | 5 ppg | | | | | | | | |
| Surface Rated Working Pressure (BOPE) = Field SW = | 3000 | psi ppg | | Predict | ed Frac Gradie | nt at Shoe | (CSFG) = | 19.23 | 3 ppg | | | | | | | | |
| Surface Casing Burst Safety Factor = API Burst Rating / Max | kimum Predict | ed Surf | | | | Aliowable | Surface Pres | ssure (1 | (IASP) | | | | | | | | |
| Production Casing NAWP for the Fracture Stimulation = API E | Burst Rating / | Cerpon | ite Ummum B | Barst De | sign Factor | | | | | | | | | | | | |
| Surface Casing Burst Safety Factor: Case #1. MPSP (MWhyd next section) = | 785 | x | 0.052 | х | 10 | = | 408 | | | | | | | | | | |
| Case #2. MPSP (Field SW @ Bullhead _{CSFG} + 200 psi) = | 785 | х | 0.052 | х | 19.23 | • | 408 | + | 200 | = | 577 | | | | | | |
| Case #3. MPSP (Kick Vol @ next section TD) = Case #4. MPSP (PPTD - GG) = | 6968 6968 | X X | 0.052 0.052 | x x | 8.55 8.55 | : | 618.3 696.8 | - | 347 2401 | = | 2133 | | | | | | |
| Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) = | 785 | x | 0.052 | x(| 19.23 | + | 0.2 |)= | 793 | | | | | | | | |
| MASP (MWhyd + Test Pressure) = | 785 2950 | х / | 0.052 | х = | 8.5 1.60 | + | 1500 | = | 1847 | | | | | | | | |
| Burst Safety Factor (Max. MPSP or MASP) = Production Casing Burst Safety Factor: | 2900 | , | 1847 | - | 1.60 | | | | | | | | | | | | |
| Case #1, MPSP (MWhyd TD) = | 6968 | х | 0.052 | x | 10 | = | 3623.36 | | | | | | | | | | |
| Case #4. MPSP (PPTD - GG) = Burst Safety Factor (Max. MPSP) = | 6968 7740 | x 1 | 0.052 3623 | x = | 8.55 2.14 | - | 696.8 | = | 2401 | | | | | | | | |
| MAWP for the Fracture Stimulation (Corporate Criteria) = | 7740 | 1 | 1.15 | = | 6730 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| Collapse - ConocoPhillips Required Load Cases The maximum collapse load on the Surface Casing occurs when cementing | o to surface | 1/3 eva | cuation to the | next ca | sing setting de | oth ar dee | cest depth a | fexoos | sure (fuil es | acuation) | | | | | | | |
| The maximum collapse load on the Production Casing occurs when cemen | ting to surfac | e, or 1/3 | s evacuation t | to the de | epest depth o | t exposure; | ; and | | | | | | | | | | |
| therefore, the external pressure profile for the evacuation cases should be Surface Casing Collapse Safety Factor = API Collapse Rating | | | | | | | | we ass | umed to be | : PPTD. | | | | | | | |
| Production Casing Collapse Safety Factor = API Collapse Rating | | | | | | | | menting | to Surface | | | | | | | | |
| Cement Displacement Fluid (FW) = | 8.34 | | | | - | ement to Si | | | | | | | | | | | |
| Surface Cement Lead = Surface Cement Tail = | 13.6 14.6 | | | | niLead≂ ⊯ntTai= | | B ppg ppg | | | | | | | | | | |
| Top of Surface Tail Cement = | 300 | | Tep of P | rod Tail | Cement = | 5200 | | | | | | | | | | | |
| Surface Casing Collapse Safety Factor: | | | | | | | | | | | | | | | | | |
| Full Evacuation Diff Pressure = | 785 | X | 0.052 | x 0.000 | 8.55 | = | 349 | 200 | | 0.052 | | 11.0 | | 240 3 | | | |
| Cementing Diff Lift Pressure = Collapse Safety Factor = | [(1370 | 485 / | x 349 | 0.052 = | x 3.93 | 13.6 |) + (| 300 | x | 0.052 | x | 14.8 | ٠, | 340 J | = 233 | | |
| Production Casing Collapse Safety Factor: | | | | | | | | | | | | | | | | | |
| . 1/3 Evacuation Diff Pressure = Cementing Diff Lift Pressure = | ((((| 6968 1766 | | 0.052 | x x | 8.55 11.8 |) · () + (| 6968 5200 | / × | 3 0.052 | x x | 0.052 16.4 |). | |] ≕ 2091 = 2498 | | |
| Collapse Safety Factor = | 6290 | 1 | | 0.002 | | 11.0 | / · (| | <u> </u> | 0.002 | ~ | 10.4 | 1. | JOLF 1 | 2400 | | |
| • • | | ' | 2498 | = | 2.52 | | | | | | | | | | | | |
| | | , | 2498 | = | 2.52 | | | | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases | | | | = | 2.52 | | | | | | | | | | | | |
| <u>Tensial Strength - ConocoPhillips Required Load Cases</u> The maximum axial (tensian) load occurs if casing were to get stuck and p | ulled on to try | y to gel i | t unstuck. | | | actor | | | | | | | | | | | |
| <u>Tensial Strength – ConocoPhillips Required Load Cases</u> The maximum axial (lension) load occurs if casing were to get stuck and p Itaximum Allowable Axial Load for Pipe Vield = API Pipe Maximum Allowable Axial Load for Joint = API Joint Stre | ulled on to try Yield Streng ngth Rating / | y to gel i Ih Rating Corpora | t unstuck. 1 Corporate 1 te Minimum At | Minimum xisl Des | ı Axisi Design I ign Factor | factor | | | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases The maximum axial (lensian) load occurs if casing were to get stuck and p Maximum Alawyable Axial Load for Pipe Yield + API Pipe Maximum Alawyable Axial Load for Joint - API Johni Stre Maximum Alawyable Hook Load (Limited to 75% of Rig M | ulled on to try Yield Streng ngth Rating / (ax Load) = M | y to gel i Ih Rating Corpora Saximum | t unstuck. 1 / Corporate I te Minimum A Allowable Ap | Minimum xisl Des xisl Load | ı Axisi Design I ign Factor | factor . | | | | | | | | | | | |
| <u>Tensial Strength – ConocoPhillips Required Load Cases</u> The maximum axial (lension) load occurs if casing were to get stuck and p Itaximum Allowable Axial Load for Pipe Vield = API Pipe Maximum Allowable Axial Load for Joint = API Joint Stre | ulled on to try Yield Streng ngth Rating / lax Load) = M ble Hook Loa ength 'OR' Rig | y to gel i th Rating Corpora laximum d - Bouy Max Lo | t unstuck. 1 / Corporate I te Minimum A Allowable As ant Wt of the | Minimum xisl Des xist Load String | a Axial Design I ign Factor I | | verpuš Requi | ired) | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases The maximum axial (lension) load occurs if casing were to get stuck and p Haximum Alowable Axial Load for Pipe Yield = API Pipe Haximum Alowable Hook Lead (Limited to 75% of Rig M Maximum Alowable Hook Lead (Limited to 75% of Rig M Maximum Alowable Overput Hargin = Maximum Alowabl Tensial Safety Factor = API Pipe Yield 'OR' API Joint Stre | ulied on to try Yield Streng ngth Rating / lax Load) = M ble Hook Loa ength 'OR' Rig _225000 | y to get i Ih Rating Corpora laximum d - Bouy Max Lo Ibs - | t unstuck. 1 / Corporate I te Minimum A Allowable As ant Wt of the | Minimum xisl Des xist Load String | a Axial Design I ign Factor I | | verpuš Requ | ired) | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases The maximum axial (tension) load occurs if casing were to get stuck and p Maximum Allowable Axial Load for Pipa Yield = API Pipe Maximum Allowable Axial Load for Joint = API Joint Stre Maximum Allowable Overput Margin = Maximum Allow Tensial Safety Factor = API Pipe Yield 'OR' API Joint Stre Maximum Overput Required = | ulled on to try Yield Streng ngth Rating / lax Load) = M ble Hook Loa ength 'OR' Rig | y to get i Ih Rating Corpora laximum d - Bouy Max Lo Ibs - | t unstuck. 1 / Corporate I te Minimum A Allowable As ant Wt of the | Minimum xisl Des xist Load String | a Axial Design I ign Factor I | | verpuš Requ | ired) | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases The maximum axial (lension) load occurs if casing vere to get stuck and p Haximum Alovable Axial Load for Pipe Yield = API Pipe Haximum Alovable Hook Lead (Limited to 75% of Rig M Maximum Alovable Voerpul Nargin = Maximum Alovable Tensial Safety Factor = API Pipe Yield 'OR' API John's tr | vulled on to try Yield Streng ngih Rating / lax Load) = M bie Hook Loas ength 'OR' Rig _225000 _50000 | y to get i Ih Rating Corpora laximum d - Bouy Max Lo Ibs - | t unstuck. 1 / Corporate I te Minimum A Allowable As ant Wt of the | Minimum xisl Des xist Load String | a Axial Design I ign Factor I | | verpuš Requ | ired) | | | | | | | | | |
| Tensial Strength – ConocoPhillips Required Load Cases The maximum axial (tension) load occurs if casing were to get stuck and p Itaximum Allowable Axial Load for Pipa Yield = API Pipe Itaximum Allowable Axial Load for Joint = API Joint Stre Itaximum Allowable Overpul Hargin = Maximum Allow Itaximum Allowable Overpul Hargin = Maximum Allowable Tensial Safety Factor = API Pipe Yield 'OR' API Joint Stre Itaximum Overpul Required = | ulied on to try Yield Streng ngth Rating / lax Load) = M ble Hook Loa ength 'OR' Rig _225000 | y to get i Ih Rating Corpora laximum d - Bouy Max Lo Ibs - | t unstuck. 1 / Corporate I te Minimum A Allowable As ant Wt of the | Minimum xisl Des xist Load String | a Axial Design I ign Factor I | | verpuš Regu ~ | ired) | | | | | | | | | |
| Tensial Strength - ConocoPhillips Required Load Cases The maximum axial (lensian) load occurs if casing vere to get stuck and p Maximum Alovable Axial Load for Dipa Yield - API Pipe Maximum Alovable Axial Load for Dipa Yield - API Pipe Maximum Alovable Axial Load for Dipa Yield or Start - API Joint Stre Maximum Alovable Hook Lead (Limited to 75% of Rig M Maximum Alovable Hook Lead (Limited to 75% of Rig M Maximum Alovable Overpul Nargin = Maximum Alovable Tensial Safety Factor - API Pipe Yield 'OR' API Joint Stre Maximum Alovable Axia Load (300,000 Iba) x 75% + Maximum Alovable Axia Load (300,000 Iba) x 75% + Maximum Alovable Safety Factor: Air Wt = Bouyant Wt = Max. Allowable Axial Load (Pipe Yield) = | ulled on to try Yield Streng ngih Raitng / lax Load) = M bib Hook Loa: ngih 'DR' Rig 225000 50000 18840 18840 381000 | y to get i Ih Rating Corpora aximum d - Bcuy Max Lo Ibs Ibs X / | t unstuck. / Corporate i te Minimum A Allowable As ant Vt of the ad Rating / (t 0.870 1.40 | Ninimum xisl Des kisl Load String Bouyant = = = | Axial Dealgn I Ign Factor Wit of String + | | verpuš Requ | ired) | | | | . | | | | | |
| Tensial Strength - ConocoPhillips Required Load Cases The maximum axial (tensian) load occurs if casing vere to get stuck and p Maximum Alowable Axial Load for Dipa Vield - API Pipe Maximum Alowable Axial Load for Dipa Vield - API Pipe Maximum Alowable Axial Load for Dipa Vield - API Pipe Maximum Alowable Axial Load for Dipa Vield 10 75% of Rig M Maximum Alowable Procepul Margin = Maximum Abowable Tensial Safety Factor - API Pipe Vield 'OR' API Join Stre Maximum Alowable Axial Load (Solo Iba) x 75% = Maximum Alowable Axial Load (Solo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = Maximum Alowable Axial Load (Calo Iba) x 75% = | ulled on lo try Yield Streng Inglin Raling / As Lond) = Id ble Hook Loas engin 'OR' Rig 225000 50000 18840 13840 | y to get i Ih Rating Corpora aximum d - Bcuy Max Lo Ibs Ibs | i unstuck. I / Corporate I te Minimum A Adavable A ant Wt of the ad Rating / (1 | Winimum xisl Des xist Load String Bouyant | t Axis! Design I ign Factor Wt of String + | | verpuš Regu - | ired) | | | | | | | | | |
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3. Proposed cementing program:

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16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

| | Slurry | | vals MD | Weight ppg | Sx | Vol Cuft | Additives | Yield ft ³ /sx |
|------|---------|-------------|-------------|---------------|-----|-------------|--|------------------------------|
| Lead | Class C | Surface | 440' – 485' | 13.6 | 300 | 510 | 2% Extender 2% CaCl ₂ 0.125 lb/sx LCM if needed 0.2% Defoamer Excess ≕75% based on gauge hole volume | 1.70 |
| Tail | Class C | 440' – 485' | 740' – 785' | 14.8 | 200 | 268 | 1% CaCl2 Excess = 100% based on gauge hole volume | 1.34 |

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

5-1/2" Production Casing & Cementing Program:

The intention for the cementing program for the Production Casing is to:

- Place the Tail Slurry from the casing shoe to a point approximately 200' above the top of the Paddock,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

| | Slurry | • | rvals MD | Weight ppg | Sx | Vol Cuft | Additives | Yield ft ³ /sx |
|------|-------------|---------|---------------|---------------|-----|-------------|--|------------------------------|
| Lead | 50:50 Poz/C | Surface | 5200' | 11.8 | 700 | 1820 | 10% Bentonite 5% Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 220% or more if needed based on gauge hole volume | 2.6 |
| Tail | Class H | 5200' | 6923' – 6968' | 16.4 | 400 | 428 | 0.2% Fluid loss additive 0.3% Dispersant 0.15% Retarder 0.2% Antifoam Excess = 100% or more if needed based on gauge hole volume | 1.07 |

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Ruby Federal #33

(Date: 8/8/2013)

5-1/2" Production Casing & Cementing Program - TXI/LW Cementing Option for Grayburg-San Andres:

ConocoPhillips Company respectfully requests the options to our cementing program. This option will only be implemented in the cementing operation of wells requesting for co-mingling after approval and authorization by all agencies have been obtained. The intention for the alternative option to the cementing program for the Production Casing is to:

- Accommodate the additional frac'ing and stimulation of the Grayburg-San Andres by placement of the Tail Slurry from the casing shoe to the top of the Grayburg-San Andres formation,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

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| | Slurry | | vals MD | Weight ppg | Sx | Vol Cuft | Additives | Yield ft³/sx |
|------|-------------|---------|---------------|---------------|-----|-------------|--|-----------------|
| Lead | 50:50 Poz/C | Surface | 3000' | 11.8 | 500 | 1300 | 10% Bentonite 8 lbs/sx Salt 0.2%-0.4% Fluid loss additive 0.125 lb/sx LCM if needed Excess = 200% or more if needed based on gauge hole volume | 2.6 |
| Tail | TXI/LW | 3000' | 6923' – 6968' | 13.2 | 800 | 1120 | 0.5% Fluid loss additive 0.10% Retarder 0.2% Antifoam 0.125 lb/sx LCM if needed Excess = 150% or more if needed based on gauge hole volume | 1.40 |

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volume presented above are estimates based on gauge 7-7/8" hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

4. Pressure Control Equipment:

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A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- o Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. **See Attached BOPE Schematic.** A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

5. Proposed Mud System:

| DEPTH | TYPE | Density ppg | FV sec/qt | API Fluid Loss cc/30 min | рН | Vol bbl |
|----------------------------|---|----------------|--------------|--------------------------------|---------|------------|
| 0 – Surface Casing Point | Fresh Water or Fresh Water Native Mud in Steel Pits | 8.5 - 9.0 | 28 – 40 | N.C. | N.C. | 120 – 160 |
| Surface Casing Point to TD | Brine (Saturated NaCl ₂) in Steel Pits | 10 | 29 | N.C. | 10 – 11 | 500 – 1000 |
| Conversion to Mud at TD | Brine Based Mud (NaCl ₂) in Steel Pits | 10 | 33 – 40 | 5 – 10 | 10 – 11 | 0 – 750 |

The mud systems that are proposed for use are as follows:

Gas detection equipment and pit level flow monitoring equipment will be on location. A flow paddle will be installed in the flow line to monitor relative amount of mud flowing in the non-pressurized return line. Mud probes will be installed in the individual tanks to monitor pit volumes of the drilling fluid with a pit volume totalizer. Gas detecting equipment and H2S monitor alarm will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing. The gases shall be piped into the flare system. Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

6. Logging, Coring, and Testing Program:

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- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 2500': Resistivity, Density, and Gamma Ray
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Gamma Ray and Neutron
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - BHC or Dipole Sonic if needed (optional)
 - Spectral Gamma Ray if needed (optional)

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.
 - The bottom hole pressure is expected to be 8.55 ppg gradient.
 - The expected Bottom Hole Temperature is 115 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

| FORMATION / ZONE | H2S (PPM) | Gas Rate (MCFD) | ROE 100 PPM | ROE 500 PPM | |
|----------------------------------|--------------|--------------------|----------------|----------------|--|
| Grayburg / San Andres (from MCA) | 14000 | 38 | 59 | 27 | |
| Yeso Group | 400 | 433 | 34 | 15 | |

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6, Hydrogen Sulfide Operations. Also, ConocoPhillips will provide an H2S Contingency Plan (please see copy attached) and will keep this plan updated and posted at the wellsite during the drilling operation.

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill this well as early as 2014 after receiving approval of the APD.

Attachments:

- Attachment # 1 BOP and Choke Manifold Schematic 3M System
- Attachment # 2 Diagram of Choke Manifold Equipment

Contact Information:

Proposed 8 August 2013 by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647

Ruby Federal #33

ConocoPhillips MCBU

Buckeye Ruby Federal Ruby Federal 33

Original Hole

Plan: S-Shape Plan

Standard Planning Report - Geographic

05 August, 2013

Planning Report - Geographic

| Database: | · · · · | Central Plannin | - | | Local Co-ordin | | | uby Federa | | |
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| Project: | Bucke | ýe _. | · . | | MD Reference: | | RKB @ |) 3983.0usf | t (PD 822) | |
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| Wellbore Magnetics Design Audit Notes: | i Origina Mo · S-Shap 1 | del Name BGGM2012 e Plan | Sample Phase epth From (TV | • Date 8/5/2013 : PRC | Declination (°) DTOTYPE +N/-S | Tie On Dep +E/-W | Dip Angle (°) | 60.60 0. Direc | () 0 tion | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: | i Origina Mo · S-Shap 1 | del Name BGGM2012 e Plan | Sample | • Date 8/5/2013 : PRC | Declination (°) DTOTYPE | Tie On Dep | Dip Angle (°) | 60.60 | () 0 tion | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: | i Origina Mo · S-Shap 1 | del Name BGGM2012 e Plan | Sample Phase epth From (TV | • Date 8/5/2013 : PRC | Declination (°) DTOTYPE +N/-S | Tie On Dep +E/-W | Dip Angle (°) | 60.60 0. Direc | (i 0 tion | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section | i Origina Mo · S-Shap 1 | del Name BGGM2012 e Plan | Sample Phase epth From (TV (usft) | • Date 8/5/2013 : PRC | Declination (°) DTOTYPE +N/-S (usft) | Tie On Dep +E/-W (usft) | Dip Angle (°) | 60.60 0. Direc (° | (i 0 tion | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections | i Origina Mo · S-Shap 1 | del Name BGGM2012 e Plan | Sample Phase epth From (TV (usft) 0.0 | • Date 8/5/2013 : PRC | Declination (°) DTOTYPE +N/-S (usft) 0.0 | Tie On Dep +E/-W (usft) 0.0 | Dip Angle (°) th: | 60.60 0. Direc (° 176. | (i 0 tion | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured | i Origina Mo S-Shap 1 n: | del Name BGGM2012 e Plan D | Sample Phase epth From (TV (usft) 0.0 Vertical | 2 Date 8/5/2013 :: PRC D) | Declination (°) DTOTYPE +N/-S (usft) 0.0 Do | Tie On Dep +E/-W (usft) 0.0 gleg Bui | Dip Angle (°) th: | 60.60 0. Direc (° 176. | (i 0 tion) 10 | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections | i Origina Mo S-Shap 1 n: Inclination | del Name BGGM2012 e Plan D | Sample Phase epth From (TV (usft) 0.0 | Date 8/5/2013 : PR(D) +N/-S | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W R | Tie On Dep +E/-W (usft) 0.0 gleg Bui ate Rat | Dip Angle (°) th: | 60.60 0. Direc (° 176. | ((0 tion) 10 TFO | Strength nT) |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth (usft) | i Origina Mo S-Shap 1 n: Inclination (°) | del Name BGGM2012 e Plan D Azimuth {°) | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) | +N/-S (usft) | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W R (usft) (°/10 | Tie On Dep +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) (°/100 | Dip Angle (°) th: ld Tu e Ra usft} (°/100 | 60.60 0. Direc (° 176. ite)usft) | (i 0 tion) 10 TFO (°) | Strength nT) 48,714 |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth {usft} 0.0 | i Origina Mo S-Shap 1 n: Inclination (°) 0.00 | del Name BGGM2012 e Plan D Azimuth (°) 0.00 | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) 0.0 | Date 8/5/2013 PRC D) +N/-S (usft) 0.0 | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W (usft) (°/10 (°/10 0.0 | Tie On Dep +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) (°/100/ 0.00 | Dip Angle (°) th: ld Tu e Ra usft} (°/100 0.00 | 60.60 0. Direc (° 176. ite Dusft) 0.00 | (i 0 tion) 10 TFO (°) 0.00 | Strength nT) 48,714 |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth (usft) 0.0 1,882.0 | i Origina Mo S-Shap 1 n: Inclination (°) 0.00 0.00 | del Name BGGM2012 e Plan D Azimuth {°) 0.00 0.00 | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) 0.0 1,882.0 | Date 8/5/2013 PRC D) +N/-S (usft) 0.0 0.0 0.0 | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W (usft) (°/10 0.0 0.0 0.0 | Tie On Deg +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) (°/1000 0.00 0.00 | Dip Angle (°) th: d Tu e Ra usft) (°/100 0.00 0.00 | 60.60 0. Direc (° 176. ite)usft) 0.00 0.00 | (i 0 tion) 10 TFO (°) 0.00 0.00 | Strength nT) 48,714 |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth (usft) 0.0 1,882.0 2,538.8 | i Origina Mo S-Shap 1 n: Inclination (°) 0.00 0.00 9.85 | Al Hole del Name BGGM2012 e Plan D Azimuth (°) 0.00 0.00 176.10 | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) 0.0 1,882.0 2,535.6 | Date 8/5/2013 PRC D) +N/-S (usft) 0.0 0.0 -56.2 | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W (usft) (°/10 0.0 0.0 0.0 3.8 | Tie On Deg +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) (°/100 0.00 0.00 1.50 | Dip Angle (°) th: d Tu e Ra usft} (°/100 0.00 0.00 1.50 | 60.60 0. Direc (° 176. ite Dusft) 0.00 0.00 0.00 | (i 0 tion) 10 TFO (°) 0.00 0.00 176.10 | Strength nT) 48,714 |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth (usft) 0.0 1,882.0 2,538.8 4,733.0 | i Origina Mo S-Shap 1 n: Inclination (°) 0.00 0.00 | del Name BGGM2012 e Plan D Azimuth {°) 0.00 0.00 | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) 0.0 1,882.0 | * Date 8/5/2013 * PRC D) +N/-S (usft) 0.0 0.0 -56.2 -430.8 | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W (usft) (°/10 0.0 0.0 0.0 3.8 29.3 | Tie On Dep +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) {°/100 0.00 0.00 1.50 0.00 | Dip Angle (°) th: d Tu e Ra usft) (°/100 0.00 0.00 1.50 0.00 | 60.60 0. Direc (° 176. ite Dusft) 0.00 0.00 0.00 0.00 0.00 | (i 0 tion) 10 TFO (°) 0.00 0.00 | Strength nT) 48,714 |
| Wellbore Magnetics Design Audit Notes: Version: Vertical Section Plan Sections Measured Depth (usft) 0.0 1,882.0 2,538.8 | i Origina Mo S-Shap 1 n: Inclination (°) 0.00 0.00 9.85 | Al Hole del Name BGGM2012 e Plan D Azimuth (°) 0.00 0.00 176.10 | Sample Phase epth From (TV (usft) 0.0 Vertical Depth (usft) 0.0 1,882.0 2,535.6 | • Date 8/5/2013 : PRC D) +N/-S (usft) 0.0 0.0 -56.2 | Declination (°) DTOTYPE +N/-S (usft) 0.0 +E/-W (usft) (°/10 0.0 0.0 0.0 3.8 | Tie On Deg +E/-W (usft) 0.0 gleg Bui ate Rat 0ùsft) (°/100 0.00 0.00 1.50 | Dip Angle (°) th: d Tu e Ra usft} (°/100 0.00 0.00 1.50 | 60.60 0. Direc (° 176. ite Dusft) 0.00 0.00 0.00 | (i) 0 tion) 10 TFO (°) 0.00 0.00 176.10 0.00 | Strength nT) 48,714 |

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Planning Report - Geographic

| atab | ase: | EDM | Central Plan | ning | | Local Co | o-ordinate Referen | ice: (We | Il Ruby Federal 33 | |
|------|------------|--------------|-------------------------|----------------|---|---------------------------------------|--------------------------|-------------------------------|---|---------------|
| | any: | | coPhillips MC | | | 1 | erence: | - + | B @ 3983.0usft (PD 822) | |
| rójé | | Buck | | | | MD Refe | | | B @ 3983.0usft (PD 822) | |
| - | | - 1 E | | | | | r | | | · . · |
| te: | | | Federal | | | | eference: | Gri | | • |
| ell: | | Ruby | Federal 33 | | | Survey C | Calculation Metho | di: Mir | nimum Curvature | |
| ellb | ore: | Origi | nal Hole | | | 1 | | | | |
| esig | n: | S-Sh | apë Plan | | | | · . · . · | • | | |
| | | | 44 | | مىيا سىرە ئىلىرىم مىلىكى لىكىغانىغا | | | · · · · · · · · · · · · · · · | م میلاد در بالای با بالا میکند به میکند. مرکز این از این این این میکند میکند این میکند. میکن این این این این میکند میکند میکند. | |
| lanr | ned Survey | | ، ئې د سري د سري د د | بې د چه سونۍ د | | | ي من الا مير دروي . ا | | ساورون غيور | |
| | · | · · . | | . * | | | | | and the second | |
| i M | leasured | | ÷., | Vertical | | | Мар | Мар | • • | |
| | Depth | Inclination | Azimuth | Depth | +N/-S | +E/-W | Northing | Easting | | |
| | (usft) | (°) | (°) | (usft) | (usft) | (usft) | (usft) | (usft) | Latitude | Longitude |
| •~ | | | | | | · · · · · · · · · · · · · · · · · · · | | | | |
| | 0.0 | 0.00 | 0.00 | 0.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | | 103° 48' 7.95 |
| | 79.0 | 0.00 | 0.00 | 79.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | Conduct | or | | | | | | | | |
| | 100.0 | 0.00 | 0.00 | 100.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 200.0 | 0.00 | 0.00 | 200.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 300.0 | 0.00 | 0.00 | 300.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 400.0 | 0.00 | 0.00 | 400.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | | 103° 48' 7.95 |
| | 500.0 | 0.00 | 0.00 | 500.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | | 103° 48' 7.95 |
| | 600.0 | 0.00 | 0.00 | 600.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | | 103° 48' 7.95 |
| | | | | | | | | | | |
| | 700.0 | 0.00 | 0.00 | 700.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | | 103° 48' 7.95 |
| | 715.0 | 0.00 | 0.00 | 715.0 | 0.0 | 0.0 | 668,652.10 | 663,133.6 | 0 32° 50′ 13.500 N | 103° 48' 7.95 |
| | Rustler | | | | | | | | | |
| | 785.0 | 0.00 | 0.00 | 785.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | Surface | | | | | • | | , | | |
| | 800.0 | 0.00 | 0.00 | 800.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 887.0 | 0.00 | 0.00 | 887.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | | 0.00 | 0.00 | 007.0 | 0.0 | 0.0 | 000,052.10 | 000,100.00 | 0 52 50 15.500 1 | 103 46 7.95 |
| | Salado | | | | | | | | | |
| | 900.0 | 0.00 | 0.00 | 900.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | 1,000.0 | 0.00 | 0.00 | 1,000.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 1,100.0 | 0.00 | 0.00 | 1,100.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 1,200.0 | 0.00 | 0.00 | 1,200.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 1,300.0 | 0.00 | 0.00 | 1,300.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 1,400.0 | 0.00 | 0.00 | 1,400.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | 1,500.0 | 0.00 | 0.00 | 1,500.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | 1,600.0 | 0.00 | 0.00 | 1,600.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | 1,700.0 | 0.00 | 0.00 | 1,700.0 | 0.0 | | | | | |
| | | | | | | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | 1,800.0 | 0.00 | 0.00 | 1,800.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | | 103° 48' 7.95 |
| | 1,882.0 | 0.00 | 0.00 | 1,882.0 | 0.0 | 0.0 | 668,652.10 | 663,133.60 | 0 32° 50' 13.500 N | 103° 48' 7.95 |
| | Tansill | | | | | | | | ****** | |
| | 1,900.0 | 0.27 | 176.10 | 1,900.0 | 0.0 | 0.0 | 668,652.05 | 663,133.61 | 1 32° 50' 13.500 N | 103° 48' 7.95 |
| | 2,000.0 | 1.77 | 176.10 | 2,000.0 | -1.8 | 0.1 | 668,650.28 | 663,133.73 | 3 32° 50' 13.482 N | 103° 48' 7.94 |
| | 2,082.1 | 3.00 | 176.10 | 2,082.0 | -5.2 | 0.4 | 668,646.87 | 663,133.96 | 6 32° 50' 13.448 N | 103° 48' 7.94 |
| | Yates | | | | | | | | | |
| | 2,100.0 | 3.27 | 176.10 | 2,099.9 | -6.2 | 0.4 | 668,645.89 | 663,134,02 | 2 32° 50' 13.439 N | 103° 48' 7.94 |
| | 2,200.0 | 4.77 | 176.10 | 2,035.5 | -13.2 | 0.4 | 668,638.90 | 663,134.50 | | 103° 48' 7.94 |
| | 2,200.0 | 4.77 6.27 | 176.10 | 2,199.8 | -13.2 -22.8 | | | 663,135.15 | | |
| | | | | | | 1.6 | 668,629.30 | | | 103° 48' 7.93 |
| | 2,373.4 | 7.37 | 176.10 | 2,372.0 | -31.5 | 2.1 | 668,620.61 | 663,135.75 | 5 32° 50' 13.188 N | 103° 48' 7.92 |
| | Seven Ri | | · · · | | | | | | | |
| | 2,400.0 | 7.77 | 176.10 | 2,398.4 | -35.0 | 2.4 | 668,617.11 | 663,135.99 | 9 32° 50' 13,154 N | 103° 48' 7.92 |
| | 2,500.0 | 9.27 | 176.10 | 2,497.3 | -49.8 | 3.4 | 668,602.33 | 663,136.99 | 9 32° 50' 13.007 N | 103° 48' 7.91 |
| | 2,538.8 | 9.85 | 176.10 | 2,535.6 | -56.2 | 3.8 | 668,595.90 | 663,137.43 | 3 32° 50' 12.944 N | 103° 48' 7.90 |
| | 2,600.0 | 9.85 | 176.10 | 2,595.9 | -66.6 | 4.5 | 668,585.45 | 663,138.14 | | 103° 48' 7.90 |
| | 2,700.0 | 9.85 | 176.10 | 2,694.4 | -83.7 | 5.7 | 668,568.38 | 663,139.30 | | 103° 48' 7.88 |
| | 2,800.0 | 9.85 | 176.10 | 2,792.9 | -100.8 | 6.9 | 668,551.31 | 663,140.47 | | 103° 48' 7.87 |
| | 2,900.0 | 9.85 | 176.10 | 2,891.4 | -117.9 | 8.0 | 668,534.24 | 663,141.63 | | 103° 48' 7.86 |
| | | | | | | | | | | |
| | 3,000.0 | 9.85 | 176.10 | 2,990.0 | -134.9 | 9.2 | 668,517.17 | 663,142.79 | | 103° 48' 7.85 |
| | 3,025.4 | 9.85 | 176.10 | 3,015.0 | -139.3 | 9.5 | 668,512.84 | 663,143.09 | 32° 50' 12.122 N | 103° 48' 7.84 |
| | Queen | | • • | | | | <u>.</u> | | | <i>,</i> · |
| | 3,100.0 | 9.85 | 176.10 | 3,088.5 | -152.0 | 10.4 | 668,500.10 | 663,143.95 | 5 32° 50' 11.996 N | 103° 48' 7.83 |
| | 3,200.0 | 9.85 | 176.10 | 3,187.0 | -169.1 | 11.5 | 668,483.03 | 663,145.12 | | 103° 48' 7.82 |
| | 3,300.0 | 9.85 | 176.10 | 3,285.5 | -186.1 | 12.7 | 668,465.96 | 663,146.28 | | 103° 48' 7.81 |
| | 3,400.0 | 9.85 | 176.10 | 3,384.1 | | | | | | |
| | 0.004 | 9.00 | 170.10 | 3,304.1 | -203.2 | 13.8 | 668,448.89 | 663,147.44 | 32° 50' 11.489 N | 103° 48' 7.80 |

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Planning Report - Geographic

| Database: | EDM Central Planning | ³ Local Co-ordinate Reference: | Well Ruby Federal 33 |
|-----------|----------------------|---|---------------------------|
| Company: | ConocoPhillips MCBU | TVD Reference: | RKB @ 3983.0usft (PD 822) |
| Project: | Buckeye | MD Reference: | RKB @ 3983.0usft (PD 822) |
| Site: | Ruby Federal | North Reference: | Grid |
| Well: | Ruby Federal 33 | Survey Calculation Method: | Minimum Curvature |
| Wellbore: | . Original Hole | · | |
| Design: | S-Shape Plan | | |

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Planned Survey

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| leasured Depth (usft) | Inclination (°) | Azimuth (°) | Vertical Depth (usft) | +N/-S (usft) | +E/-W (usft) | Map Northing (usft) | Map Easting (usft) | l atitud- | - بروند الم |
|-----------------------------|--------------------|----------------|-----------------------------|-----------------|-----------------|---------------------------|--------------------------|------------------|--------------|
| ~ - | · · · | | | (usit) | lusit | | | Latitude | Longitude |
| 3,467.9 | 9.85 | 176.10 | 3,451.0 | -214.8 | 14.6 | 668,437.30 | 663,148.23 | 32° 50' 11.374 N | 103° 48' 7.7 |
| Grayburg | | | | | | | | | |
| 3,500.0 | 9.85 | 176.10 | 3,482.6 | -220.3 | 15.0 | 668,431.82 | 663,148.60 | 32° 50' 11.320 N | 103° 48' 7.7 |
| 3,600.0 | 9.85 | 176.10 | 3,581.1 | -237.4 | 16.2 | 668,414.75 | 663,149.77 | 32° 50' 11.151 N | 103° 48' 7.7 |
| 3,700.0 | 9.85 | 176.10 | 3,679.6 | -254.4 | 17.3 | 668,397.68 | 663,150.93 | 32° 50' 10.982 N | 103° 48' 7.7 |
| 3,800.0 | 9.85 | 176.10 | 3,778.2 | -271.5 | 18.5 | 668,380.61 | 663,152.09 | 32° 50' 10.813 N | 103° 48' 7.7 |
| 3,827.2 | 9.85 | 176.10 | 3,805.0 | -276.2 | 18.8 | 668,375.96 | 663,152.41 | 32° 50' 10.767 N | 103° 48' 7.7 |
| San And | | | | | | | | | |
| 3,900.0 | 9.85 | 176.10 | 3,876.7 | -288.6 | 19.7 | 668,363.54 | 663,153.25 | 32° 50' 10.644 N | 103° 48' 7.7 |
| 4,000.0 | 9.85 | 176.10 | 3,975.2 | -305.6 | 20.8 | 668,346.47 | 663,154.42 | 32° 50′ 10.475 N | 103° 48' 7.7 |
| 4,100.0 | 9.85 | 176.10 | 4,073.7 | -322.7 | 22.0 | 668,329.40 | 663,155.58 | 32° 50' 10.306 N | 103° 48' 7.7 |
| 4,200.0 | 9.85 | 176.10 | 4,172.3 | -339.8 | 23.1 | 668,312.33 | 663,156.74 | 32° 50' 10.137 N | 103° 48' 7.6 |
| 4,300.0 | 9.85 | 176.10 | 4,270.8 | -356.9 | 24.3 | 668,295.26 | 663,157.90 | 32° 50' 9.968 N | 103° 48' 7.6 |
| 4,400.0 | 9.85 | 176.10 | 4,369.3 | -373.9 | 25.5 | 668,278.19 | 663,159.07 | 32° 50' 9.799 N | 103° 48' 7.6 |
| 4,500.0 | 9.85 | 176.10 | 4,467.8 | -391.0 | 26.6 | 668,261.12 | 663,160.23 | 32° 50' 9.630 N | 103° 48' 7.6 |
| 4,600.0 | 9.85 | 176.10 | 4,566.4 | -408.1 | 27.8 | 668,244.05 | 663,161.39 | 32° 50' 9.461 N | 103° 48' 7.6 |
| 4,700.0 | 9.85 | 176.10 | 4,664.9 | -425.1 | 29.0 | 668,226.98 | 663,162.56 | 32° 50' 9.292 N | 103° 48' 7.6 |
| 4,733.0 | 9.85 | 176.10 | 4,697.4 | -430.8 | 29.3 | 668,221.35 | 663,162.94 | 32° 50' 9.236 N | 103° 48' 7.6 |
| 4,800.0 | 8.85 | 176.10 | 4,763.5 | -441.6 | 30.1 | 668,210.49 | 663,163.68 | 32° 50' 9.129 N | 103° 48' 7.6 |
| 4,900.0 | 7.35 | 176.10 | 4,862.5 | -455.7 | 31.0 | 668,196.44 | 663,164.64 | 32° 50' 8.990 N | 103° 48' 7.6 |
| 5,000.0 | 5.85 | 176.10 | 4,961.9 | -467.1 | 31.8 | 668,184.98 | 663,165.42 | 32° 50' 8.876 N | 103° 48' 7.6 |
| 5,100.0 | 4.35 | 176.10 | 5,061.5 | -476.0 | 32.4 | 668,176.11 | 663,166.02 | 32° 50' 8.789 N | 103° 48' 7.5 |
| 5,200.0 | 2.85 | 176.10 | 5,161.3 | -482.3 | 32.8 | 668,169.85 | 663,166.45 | 32° 50' 8.727 N | 103° 48' 7.5 |
| 5,300.0 | 1.35 | 176.10 | 5,261.2 | -485.9 | 33.1 | 668,166.20 | 663,166.69 | 32° 50' 8.690 N | 103° 48' 7.5 |
| 5,313.8 | 1.14 | 176.10 | 5,275.0 | -486.2 | 33.1 | 668,165.90 | 663,166.72 | 32° 50' 8.687 N | 103° 48' 7.5 |
| Glorieta | | | | | | | | | |
| 5,389.8 | 0.00 | 0.00 | 5,351.0 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| Paddock | | | | | | | | | |
| 5,400.0 | 0.00 | - 0.00 | 5,361.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 5,500.0 | 0.00 | 0.00 | 5,461.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 5,600.0 | 0.00 | 0.00 | 5,561.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 5,700.0 | 0.00 | 0.00 | 5,661.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 5,768.8 | 0.00 | 0.00 | 5,730.0 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| Blinebry | · | | | | | | | | |
| 5,800.0 | 0.00 | 0.00 | 5,761.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 5,900.0 | 0.00 | 0.00 | 5,861.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,000.0 | 0.00 | 0.00 | 5,961.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,100.0 | 0.00 | 0.00 | 6,061.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,200.0 | 0.00 | 0.00 | 6,161.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,300.0 | 0.00 | 0.00 | 6,261.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,400.0 | 0.00 | 0.00 | 6,361.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | '32° 50' 8,680 N | 103° 48' 7.5 |
| 6,500.0 | 0.00 | 0.00 | 6,461.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,600.0 | 0.00 | 0.00 | 6,561.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,700.0 | 0.00 | 0.00 | 6,661.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,777.8 | 0.00 | 0,00 | 6,739.0 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| Tubb | | | | | | • | | | |
| 6,800.0 | 0.00 | 0.00 | 6,761.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,900.0 | 0.00 | | 6,861.2 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.5 |
| 6,968.0 | 0.00 | 0.00 | 6,929.2 | -487.0 | 33.2 | 668,165.15 | 663,166,77 | 32° 50' 8.680 N | 103° 48' 7.5 |
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Planning Report - Geographic

| Database: | | ral Planning | | | | dinate Reference: | Well Ruby | | |
|--|--|---|--|-----------------------|------------------------|-------------------|-------------------|--|------------------|
| Company: | | illips MCBU | | | TVD Refere | | - | 83.0usft (PD 822) | |
| Project: | Buckeye | | | | MD Referen | | . – | 83.0usft (PD 822) | |
| Site: | Ruby Fede | | | | North Refer | | Grid | | |
| Nell: | Ruby Fede | | | | Survey Calo | ulation Method: | Minimum C | Curvature | |
| Wellbore: | Original Ho | | | | | | 1 | | |
| Design: | S-Shape P | | | - | | | | | |
| Design Targets | | | , a . | | • | - , | | • • • • | |
| Target Name | | | | | | | | | |
| hit/miss target | Dip Angl | e Dip Dir. | TVD | +N/-S | +E/-W | Northing | Easting | | |
| - Shape | (°) | (°) | (usft) | (usft) | (usft) | (usft) | (usft) | Latitude | Longitude |
| Ruby Federal 33 (Plat - plan hits target o - Circle (radius 0. | center | 00 0.00 | 5,351.0 | -487.0 | 33.2 | 668,165.15 | 663,166.77 | 32° 50' 8.680 N | 103° 48' 7.590 V |
| Ruby Federal 33 (Tar - plan misses tar - Circle (radius 15 | get center by 1 | 00 0.00 104.7usft at 53 | | -591.1 5351.0 TVD, | 43.6 -487.0 N, 33.2 | 668,060.99 E) | 663,177.22 | 32° 50' 7.649 N | 103° 48' 7.474 V |
| Casing Points | | ···· · · · | | | | | | | |
| . IV | feasured Depth (usft) | Vertical Depth (usft) | | | Name | | Cas Diam (" | eter Diamete | er . |
| | 79.0 | 79.0 | Conductor | | Name | | | 16 | 20 |
| | 785.0 | 785.0 | | | | | | | -1/4 |
| | 6,968.0 | 6,929.2 | | | | | | | - 1/4 -7/8 |
| | | | | | | | | | |
| | | A | | | | | • • • • • • • | 2 3 4 4 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 | |
| Formations | | • | | | | | •••• | · · · | |
| . Mea Do | asured epth usft) | Vertical Depth (usft) | | Name | | Litholog | | Dip Dip Direction (°) (°) | |
| . Mea Do | epth | Depth (usft) | Rustler | Name | | Litholog | | Dip Direction | |
| Mea | epth usft) | Depth (usft) 714.0 | Rustler Salado | Name | · · · · · · · · | Litholog | | Dip Direction (°) (°) | |
| Mea Di (L | epth usft) 715.0 | Depth (usft) 714.0 886.0 \$ | | Name | | Litholog | | Dip Direction (°) (°) 0.00 | |
| Mea Di (L | epth usft) 715.0 887.0 1,882.0 | Depth (usft) 714.0 886.0 1,881.0 | Salado | Name | | Litholog | | Direction (°) (°) 0.00 | |
| Mea Di (L | epth asft) 715.0 887.0 1,882.0 2,082.1 | Depth (usft) 714.0 4 886.0 5 1,881.0 7 2,081.0 7 | Salado Fansill | Name | | Litholog | | Direction (°) (°) 0.00 0.00 0.00 0.00 0.00 0.00 | |
| Mea Du (L | epth usft) 715.0 887.0 1,882.0 2,082.1 2,373.4 | Depth (usft) 714.0 4 886.0 5 1,881.0 7 2,081.0 7 2,371.0 5 | Salado Fansill Yates Seven Rivers | Name | | Litholog | | Direction (°) (°) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | |
| Mea Du (L | epth asft) 715.0 887.0 1,882.0 2,082.1 2,373.4 3,025.4 | Depth (usft) 714.0 4 886.0 5 1,881.0 7 2,081.0 7 2,371.0 5 3,014.0 6 | Salado Fansill Yates Seven Rivers Queen | Name | | Litholog | | Direction (°) (°) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | |
| Mea Du (L | epth asft) 715.0 887.0 1.882.0 2.082.1 2.373.4 3.025.4 3.467.9 | Depth (usft) 714.0 1 886.0 2 1,881.0 2 2,081.0 2 3,014.0 0 3,450.0 0 | Salado Tansill Yates Seven Rivers Queen Grayburg | Name | | Litholog | | Direction (°) (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) | |
| Mea Du (L | epth asft) 715.0 887.0 1,882.0 2,082.1 2,373.4 3,025.4 3,467.9 3,827.2 | Depth (usft) 714.0 1 886.0 2 1,881.0 2 2,081.0 2 3,014.0 2 3,450.0 2 3,804.0 2 | Salado Fansill Yates Seven Rivers Queen Grayburg San Andres | Name | | Litholog | | Direction (°) (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) | |
| Mea Du (L | epth asft) 715.0 887.0 1,882.0 2,082.1 2,373.4 3,025.4 3,467.9 3,827.2 5,313.8 | Depth (usft) 714.0 1 886.0 2 1,881.0 2 2,081.0 2 3,014.0 2 3,450.0 2 3,804.0 2 5,274.0 2 | Salado Fansill Yates Seven Rivers Queen Grayburg San Andres Glorieta | Name | | Litholog | | Direction (°) (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) | |
| Mea Du (L | epth asft) 715.0 887.0 1,882.0 2,082.1 2,373.4 3,025.4 3,467.9 3,827.2 5,313.8 5,389.8 | Depth (usft) 714.0 1 886.0 2 1,881.0 2 2,081.0 2 3,014.0 2 3,450.0 2 3,804.0 5 5,350.0 6 | Salado Fansill Yates Seven Rivers Queen Grayburg San Andres Glorieta Paddock | Name | | Litholog | | Direction (°) (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) | · · · · · |
| . Mea Du (L | epth asft) 715.0 887.0 1,882.0 2,082.1 2,373.4 3,025.4 3,467.9 3,827.2 5,313.8 5,389.8 5,768.8 | Depth (usft) 714.0 1 886.0 2 1,881.0 2 2,081.0 2 3,014.0 2 3,450.0 2 5,274.0 2 5,350.0 2 | Salado Fansill Yates Seven Rivers Queen Grayburg San Andres Glorieta Paddock Blinebry | Name | | Litholog | | Direction (°) (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) 0.00 (°) | · · · · · |
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Proposed Directional Well Plan

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Request for Variance

ConocoPhillips Company

Lease Number: NM LC 029405B Well: Ruby Federal #33 Location: Sec. 18, T17S, R32E Date: 6/14/2013

Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

Program prepared by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647 Date: 26 September 2012

Attachment # 1



Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

| Nor | n. ID | N | om OD | Wei | ght | Min Be | nd Radi | us | Мах | WP |
|--|--|---------------------|--|------------|-------|--------------------------------|---------|-------|----------------------|---------------|
| in. | mm. | iņ. | mm | íb/ft | kg/m | in. | mт | | psi | Mpa |
| .3 | 76.2 | 5.11 | 129.79 | 14.5 | 21.46 | 48 | 1219 | .2 | 5000 | 34.4 |
| 3-1/2 | 88.9 | 5.79 | 147.06 | 20.14 | 29.80 | 54 | 1371 | .6 | 5000 | 34.4 |
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Ruby Federal #33

Variance Request