| Forn/3160-5<br>(March 2012)   | UNITED STATES   | OCD Hobbs   | BS OCD                  | O  | DRM APPROVED<br>MB No. 1004-0137       |
|---|---|---|-------------------------|--|--|
|   | DEPARTMENT OF THE INTE<br>UREAU OF LAND MANAGE  |   | 19201                   | 5. Lease Serial No.<br>NMLC 058395       | ires: October 31, 2014                 |
|   | Y NOTICES AND REPORTS   |   |                         | 6. If Indian, Allottee or                | Tribe Name                             |
| Do not use thi  | s form for proposals to dri<br>I.  Use Form 3160-3 (APD)  | ill or to re-enter an                                 | ECEIVED                 | N/A                                      |  |
|   |   |   | 5.                      | 7. If Unit of CA/Agreen                  | pent Name and/or No                    |
| I. Type of Well   | SMIT IN TRIPLICATE – Other instru   | ictions on page 2.                                    |                         | N/A                                      |  |
|   | as Well Other   |   |                         | 8. Well Name and No.                     | <u> </u>                               |
| 2. Name of Operator<br>ConocoPhillips Co. (P10  | )-4-4054)   |   |                         | 9. API Well No.<br>30-025-40596          | /                                      |
| 3a. Address   | 3b. P   | hone No. (include area cod                            | le)                     | 10. Field and Pool or Ex                 | ploratory Area                         |
| 600 N. Dairy Ashford Ro   |   | (281)206-5281   |                         | Maljamar; Yeso                           |  |
| 4. Location of Well <i>(Footage, Sec.</i> ,<br>1195' FSL & 800' FEL; U  | <i>T.,R.,M., or Survey Description)</i><br>JL P, Sec. 22, T17S, R32E  |   |                         | 11. County or Parish, Sta<br>Lea County  | NM                                     |
| 12. CH  | ECK THE APPROPRIATE BOX(ES)   | TO INDICATE NATURE                                    | OF NOTIC                | E, REPORT OR OTHER                       | R DATA                                 |
| TYPE OF SUBMISSION  |   | TYI   | PE OF ACTI              | ON                                       |  |
| X Notice of Intent  | Acidize   | Deepen  | Produ                   | ction (Start/Resume)                     | Water Shut-Off                         |
|   | Alter Casing  | Fracture Treat  | Recla                   | mation                                   | Well Integrity                         |
| Subsequent Report   | Casing Repair   | New Construction                                      | Recor                   | -  | Other                                  |
| Final Abandonment Notice  | Change Plans  | Plug and Abandon Plug Back                            |                         | orarily Abandon<br>Disposal              |  |
| determined that the site is ready<br>ConocoPhillips Company<br>plan for this well. The fol<br>program.<br>Please find the attached<br>-Updated Operator Certir<br>-Updated Drilling Plan<br>-Variance from Onshore<br>-Updated H2S Continger<br>-Changes to the Surface | y, as most recent operator of<br>lowing changes are necessa<br>documents:<br>fication<br>Order 2, III.A.2.b<br>ncy Plan | record, respectfully<br>ry to drill this well as      | requests<br>s part of o | s approval to chan                       | ge the approved<br>development         |
| 14. I hereby certify that the foregoing i   | s true and correct. Name (Printed/Typed)  | )   |                         |  |  |
| Susan B. Maunder  |   | Title Senior F  | Regulator               | y Specialist                             |  |
| Signature Sugar P   | 5. Mourder  | Date 10   | 23/13                   |  |  |
|   | THIS SPACE FOR  |   | TE OFFI                 | CE USE                                   |  |
| Approved by   | LIEN J. CAFFEY  |   |                         | W  | IAR 1 7 2014                           |
| that the applicant holds legal or equitable   | EPHEN J. CAFFEY<br>red. Approval of this notice does not war<br>e title to those rights in the subject lease v          | Fitle           rant or certify           which would | <del></del>             | Date                                     |  |
|   | ns thereon.<br>13 U.S.C. Section 1212, make it a crime for<br>presentations as to any matter within its ju              |   | willfully to            | make to any department or                | agency of the United States any false, |
| (Instructions on page 2)  |   |   |                         | an a | /                                      |
|   |   |   |                         | М  | AR 2 4 2014                            |

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## **Operator Certification**

## SC Federal #9 API #30-025-40596

HOBBS OCD

MAR 1 9 2014

**CONOCOPHILLIPS COMPANY** 

#### **CERTIFICATION:**

I hereby certify that I, or persons under my direct supervision, have inspected the proposed drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of State and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application with bond coverage provided by Nationwide Bond ES0085. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

Susan B. Maunder Senior Regulatory Specialist Date: 10 23 13

RECEIVED

## Request Approval to Change Drill Plan ConocoPhillips Company Maljamar; Yeso

HOBBS OCD

MAR 1 9 2014

SC Federal 9 Lea County, New Mexico

RECEIVED

## Request:

ConocoPhillips Company respectfully requests approval to revise the casing and cementing program, pressure control equipment, the proposed mud systems, diagram and schematic for BOP and choke manifold equipment, location schematic and rig layout, and updated H2S contingency plan. This request is made under the provision of Onshore Order No. 2 and No. 6.

### 1. Proposed casing program:

|                                    |              |       |                              |          |              |      |              |       |       |        |             | Safety Fa                 |                                      |
|------------------------------------|--------------|-------|------------------------------|----------|--------------|------|--------------|-------|-------|--------|-------------|---------------------------|--------------------------------------|
| Tune                               | Hole<br>Size | N     | Interval<br>ID RKB (ft)      | OD       | Wt           | Gr   | Conn         | MIY   | Col   | Jt Str | Calcu       | lated per Co<br>Corporate | onocoPhillips<br>Criteria            |
| Туре                               | (in)         | From  | То                           | (inches) | (lb/ft)      |      | Com          | (psi) | (psi) | (klbs) | Burst<br>DF | Collapse<br>DF            | Jt Str DF<br>(Tension)<br>Dry/Buoyar |
| Cond                               | 20           | 0     | 40' – 85'<br>(30' – 75' BGL) | 16       | 0.5"<br>wall | В    | Line<br>Pipe | N/A   | N/A   | N/A    | NA          | NA                        | NA                                   |
| Alt.<br>Cond                       | 20           | 0     | 40' 85'<br>(30' 75' BGL)     | 13-3/8   | 48#          | H-40 | PE           | 1730  | 740   | N/A    | NA          | NA                        | NA                                   |
| Surf                               | 12-1/4       | 0     | 880' - 905'                  | .8-5/8   | 24#          | J-55 | STC          | 2950  | 1370  | 244    | 1.55        | <b>3.40</b>               | 3.54                                 |
| Option:<br>Prod w/<br>Bond<br>Coat | 7-7/8        | 3000' | 4000'                        | 5-1/2    | 17#          | L-80 | LTC          | 7740  | 6290  | 338    | NA          | NA                        | NA                                   |
| Prod                               | 7-7/8        | 0     | 7045' – 7102'                | 5-1/2    | 17#          | L-80 | LTC          | 7740  | 6290  | 338    | 2.10        | 2.49                      | 1.97                                 |

The casing will be suitable for H<sub>2</sub>S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

ConocoPhillips Company respectfully requests the option to run bond coated production casing with the two-stage cementing option for the intension to protect the casing from corrosion if needed.

### Casing Safety Factors - BLM Criteria:

| Туре              | Depth | Wt | MIY  | Col  | Jt Str | Drill Fluid | Burst | Collapse | Tensile-Dry | Tens-Bouy |
|-------------------|-------|----|------|------|--------|-------------|-------|----------|-------------|-----------|
| Surface Casing    | 905   | 24 | 2950 | 1370 | 244000 | 8.5         | 7.37  | 3.42     | 11.2        | 12.9      |
| Production Casing | 7102  | 17 | 7740 | 6290 | 338000 | 10          | 2.10  | 1.70     | 2.80        | 3.30      |

## Casing Safety Factors - Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

#### ConocoPhillips Corporate Criteria for Minimum Design Factors

|                       | Burst | Collapse | Axial |
|-----------------------|-------|----------|-------|
| Casing Design Factors | 1.15  | 1.05     | 1.4   |

Change to Drill Plan: SC Federal #9: .....July 2, 2013

| Suttens Carina (8.5/8* 249 1 55 CTC)   | 85   |   | 65 35 <b>00</b> 0  |   | Jt Str  | 4329   |                                  | Barst    | -                     | Ten<br>-    | _               |       |     |      |               |     |
|--|--|---|--|---|---|--|----------------------------------|----------|-----------------------|-------------|-----------------|-------|-----|------|---------------|-----|
| Surface Casing (8-5/8* 24# J-55 STC)<br>Production Casing (5-1/2* 17# L-80 LTC)  | 905<br>7102  |   | 24 2950<br>17 7740   |   | 0 244000<br>0 338000  |  |                                  |          |                       |             |                 |       |     |      |               |     |
|  |  |   |  |   |   |  |                                  |          |                       |             |                 |       |     |      |               |     |
| Burst ConocoPhillips Required Load Cases<br>The maximum internal (curst) bad on the Surface Casing occurs when the   | e surface cas  | sing is t   | ested to 1500  | ) psi (as   | per BLM Ons   | hore Order   | 2 - Q. Require                   | ments).  |                       |             |                 |       |     |      |               |     |
| The maximum Internal (burst) lead on the Production Casing occurs during   |  |   | ian where th   | e mexim   | im allowable  | working pr   | essure                           |          |                       |             |                 |       |     |      |               |     |
| (MAWP) is the pressure that woold fit ConocoPhilips Corporate Criteria for<br>Surface Casing Test Pressure =   | 1500   |   |  | Pred  | licted Pore Pr  | essure at T  | D (PPTC) =                       | 8.5      | 5 FFF 5               |             |                 |       |     |      |               |     |
| Surface Rated Working Pressure (BOPE) =  | 3000   |   |  | Predict   | ed Frac Gra:  | fient at Sho                                       | e (CSFG) =                       | 19.2     |                       |             |                 |       |     |      |               |     |
| Field SW =<br>Surface Casing Burst Safety Factor = API Burst Rating / Max  | anum Predict   |   |  |   |   | m Allowaki   | e Surface Pre                    | asore (1 | JASP)                 |             |                 |       |     |      |               |     |
| Production Casing MAWP for the Fracture Stimulation = API E  | Jurst Rating /   | / Corpoi  | ngte Minimum   | Burst De  | sign Factor   |  |                                  |          |                       |             |                 |       |     |      |               |     |
| Surface Casing Burst Safety Factor:<br>Case #1, MPSP (MWhyd next section) =  | 905  | x   | 0.052  | x   | 10  | =  | 471                              |          |                       |             |                 |       |     |      |               |     |
| Case #2_MPSP (Field SW @ Buthead <sub>CSFS</sub> + 200 psi) =  | 905  |   | 0.052  | x   | 19.23   | -  | 471                              | ÷        | 200                   | =           | 634             |       |     |      |               |     |
| Case #3. MPSP (Kick Vol @ next section TD) =   | 7102   |   | 0.052  | x   | 8.55  | -  | 619.7                            | -        | 400                   | =           | 2138            |       |     |      |               |     |
| Case #4. MPSP (PPTD - GG) =<br>Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) =   | 7102<br>905  |   | 0.052<br>0.052   | ×<br>×(   | 8.55<br>19.23   | -+   | 710.2<br>0.2                     | =<br>)=  | 2447<br>914           |             |                 |       |     |      |               |     |
| MASP (MWhyd + Test Pressure) =   | 905  |   | 0.052  | x   | 8.5   | ÷  | 1500                             | =        | 1900                  |             |                 |       |     |      |               |     |
| Burst Safety Factor (Max. MPSP or MASP) =  | 2950   | 1   | 1900   | =   | 1.55  |  |                                  |          |                       |             |                 |       |     |      |               |     |
| Production Casing Burst Safety Factor:<br>Case #1. MPSP (MWbyd TD) =   | 7102   | x   | 0.052  | x   | 10  | .=   | 3593.04                          |          |                       |             |                 |       |     |      |               |     |
| Case #4. MPSP (PPTD - GG) =  | 7102   |   | 0.052  | x   | 8.55  | -  | 710.2                            | =        | 2447                  |             |                 |       |     |      |               |     |
| Burst Safety Factor (Max, MPSP) =<br>MAWP for the Fracture Stimulation (Corporate Criteria) =  | 7740<br>7740   |   | 3693   | =   | 2.10<br>6730  |  |                                  |          |                       |             |                 |       |     |      |               |     |
|  |  |   |  |   |   |  |                                  |          |                       |             |                 |       |     |      |               |     |
| Collapse – ConocoPhillips Required Load Cases  |  |   |  |   |   |  |                                  |          |                       |             |                 |       |     |      |               |     |
| The maximum collapse had on the Surface Casing occurs when cementing   |  |   |  |   |   |  |                                  | f expos  | ure (full ev          | /acuation). |                 |       |     |      |               |     |
| The maximum collapse load on the Production Casing occurs when cement<br>literefore, the external pressure profile for the evacuation cases should be  |  |   |  |   |   |  |                                  | we 853   | umed to be            | PPTD.       |                 |       |     |      |               |     |
| Surface Casing Collacse Safety Factor = API Collacse Rating  | / Full Evacut  | ation 'O  | R' Cement Dis  | placeme   | nt during Cer   | nenting to S                                       | urface                           |          |                       |             |                 |       |     |      |               |     |
| Production Casing Colapse Safety Factor = API Colapse Rati<br>Cement Displacement Fluid (FW) =   | ng / Maximun<br>8.34   |   | ted Surface  |   |   | Displacem<br>Cement to 5                           | -                                | renting  | to Surface            | •           |                 |       |     |      |               |     |
| Surface Cement Lead =  | 13.6   | ppg   | Pro  |   | nt Lead = [   | 11.  | 8 crag                           |          |                       |             |                 |       |     |      |               |     |
| Surface Cement Tell =  | 14.8<br>300  |   |  |   | ent Tail =  |  | 4 FF9                            |          |                       |             |                 |       |     |      |               |     |
| Top of Surface Tail Cement =   |  | n   | Top of P   |   | ement =   | 520  | ojn                              |          |                       |             |                 |       |     |      |               |     |
| Surface Casing Collapse Safety Factor:   | 005  |   | 0.053  |   | 9 55  | =  | 100                              |          |                       |             |                 |       |     |      |               |     |
| Full Evacuation Diff Pressure =<br>Cementing Diff Lift Pressure =  | 905<br>[(  | ×<br>605  | 0.052<br>x   | ×<br>0.052  | 8.55<br>×   | 13.6   | 402<br>)+(                       | 300      | x                     | 0.052       | x               | 14.8  | ) - | 392  | ] = 2         | 66  |
| Collapse Safety Factor =   | 1370   | 1   | 402  | =   | 3.40  |  | • •                              |          |                       |             |                 |       |     |      | •             |     |
| Production Casing Collapse Safety Factor:<br>1/3 Evacuation Diff Pressure =  | K  | 7102  | ×  | 0.052   | x   | 8.55   | ) - (                            | 7102     | 1                     | 3           | x               | 0.052 | x   | 8.34 | )] = <b>2</b> | 131 |
| Cementing Diff Lift Pressure =   | ſ  | 1902  | x  | 0.052   | x   | 11.8   |                                  | 5200     | x                     | 0.052       | x               | 16,4  | ) - |      | j = 2         |     |
| Collapse Safety Factor =   | 6290   | 1   |  |   |   |  |                                  |          |                       |             |                 |       |     |      |               |     |
|  | 0230   | ,   | 2522   | =   | 2.49  |  |                                  |          |                       |             |                 |       |     |      |               |     |
|  | 0250   | ,   | 2522   | =   | 2.49  |  |                                  |          |                       |             |                 |       |     |      |               |     |
| Tensial Strength - ConocoPhillips Required Load Cases<br>The maximum axial (leasies) load accurs if casing were to get stuck and gu  |  |   |  | =   | 2.49  |  |                                  |          |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) bad occurs if casing were to get stuck and pu<br>Naximum Allowable Axial Load for Pipe Yield = API Pipe Y  | lled on io by<br>Yield Strength  | to get i<br>h Rating  | t unstuck.<br>1 Corporate I  | Minimum .   | Axial Design  | Factor   |                                  |          |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Uaximum Allowable Axial Load for Pipe Yield = API Pipe Y<br>Maximum Allowable Axial Load for Joint = API Joint Stren   | lled on to try<br>Yield Strength<br>gth Rating / C   | lo get i<br>h Rating<br>Corpora   | t unstuck.<br>1 / Corporate I<br>te Minimum A:   | Minimum .<br>xial Desig   | Axial Design  | Factor   |                                  |          |                       |             |                 |       |     |      |               |     |
| The maximum axial (Lensico) bad occurs if casing were to get stuck and pu<br>Haximum Allowable Axial Load for Pipe Yield = API Pipe Y  | Bed on to by<br>Yield Strength<br>gth Rating / C<br>x Load) = Ma   | to get i<br>h Rating<br>Corpora<br>aximum   | t unstuck.<br>1 / Corporate I<br>te Minimum A<br>Allowable Ax  | Vinimum<br>xial Desig<br>iial Load  | Axial Design  | Factor   |                                  |          |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensico) load accurs if casing were to get stuck and pu<br>Uaximum Alowable Axial Lead for Pipe Yield = API Pipe Y<br>Maximum Alowable Axial Lead for Joint = API Joint Sten<br>Maximum Alowable Hock Lead (Limbed to 75% of Rig Ma<br>Maximum Alowable Overpuil Margin = Maximum Alowabl<br>Tensial Safety Factor = API Pipe Yield 'OR' API Joint Strer  | lled on io try<br>Yield Strength<br>gth Rating / C<br>x Load) = Ma<br>le Hook Load<br>ngth 'OR' Rig  | to get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo   | t unstuck.<br>/ Corporate I<br>te Minimum A:<br>Allowable Au<br>ant WI of the  | Minimum .<br>xial Desig<br>xial Load<br>Sbring  | Axial Design<br>gn Factor   |  | iverpul Requi                    | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get shuck and pu<br>linximum Alowable Axial Land for Pice Yield - API Pipe Y<br>Maximum Alowable Axial Land at Juint = API Joint Stren<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Overput Margin = Maximum Alowable<br>Tensial Safety Factor = API Pipe Yield 'OR' API Joint Stren<br>Rig Max Laad (300,000 hs;) x 75% =  | lled on io by<br>Yield Strength<br>gth Rating / C<br>x Load) = Ma<br>le Hook Load<br>ngth 'OR' Rig<br>225000   1   | lo get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Its  | t unstuck.<br>/ Corporate I<br>te Minimum A:<br>Allowable Au<br>ant WI of the  | Minimum .<br>xial Desig<br>xial Load<br>Sbring  | Axial Design<br>gn Factor   |  | verpul Requi                     | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (Lensich) load occurs if casing were to get stuck and pu<br>Maximum Alovable Axial Load for Pice Yield - API Pipe 1<br>Maximum Alovable Axial Load for Joint Stem<br>Maximum Alovable Hock Load (Limbed to 75% of Rig Ma<br>Maximum Alovable Overpui Margin = Maximum Alovabl<br>Tensial Sofety Factor = API Pipe Yield 'OR' API Joint Stem<br>Rig Max Load (300,000 bs) x 75% =<br>Minimum Overpui Required =   | lled on io try<br>Yield Strength<br>gth Rating / C<br>x Load) = Ma<br>le Hook Load<br>ngth 'OR' Rig  | lo get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Its  | t unstuck.<br>/ Corporate I<br>te Minimum A:<br>Allowable Au<br>ant WI of the  | Minimum .<br>xial Desig<br>xial Load<br>Sbring  | Axial Design<br>gn Factor   |  | iverpul Requi                    | ret )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get shuck and pu<br>liandmum Alowable Axial Load of Load for Pice Yield - API Pipe ><br>Maximum Alowable Axial Load of Load at + API Aint Stren<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Aint Stren<br>Rig Max Load (300,000 hs) x 75% =<br>Minimum Overpuil Required =<br>Surface Casing Tensial Strength Safety Factor:  | Red on to try<br>Yield Strength<br>gth Rating / C<br>x Load) = Ma<br>He Hook Load<br>rigth 'OR' Rig<br>225000 1<br>50000 1   | lo get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Its  | t unstuck.<br>/ Corporate I<br>te Minimum A:<br>Allowable Au<br>ant WI of the  | Minimum .<br>xial Desig<br>xial Load<br>Sbring  | Axial Design<br>gn Factor   |  | iverpul Requi                    | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Maximum Alowable Axial Load for Pice Yiel = API Pice Y<br>Maximum Alowable Axial Load for Joint Stem<br>Maximum Alowable Host Load (Limited to 75% of Rig Ma<br>Maximum Alowable Overpul Margin = Maximum Alowable<br>Tensial Sofety Factor = API Pice Yiel 'OR API Joint Stem<br>Rig Max Load (300,000 bs) x 75% =<br>Minimum Overpul Required =<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =  | lled on to by<br>Yield Strength<br>gth Rating / L<br>k Load) = Me<br>te Hook Load<br>ngth 'OR' Rig<br>225000 1<br>50000 1<br>50000 1<br>21720<br>21720   | lo get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Its<br>Its<br>X  | t unstuck.<br>/ Corporate i<br>e Uinimum A:<br>Atlowable Ay<br>ant Wi of the<br>ad Rating / ( 1<br>0.870   | Minimum ,<br>xini Desig<br>xini Lond<br>Sbring<br>Bouyant 1<br>Bouyant 1  | Axial Design<br>gn Factor<br>Wt of String -<br>18901  |  | iverpul Requi                    | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Land for Pice Ytels - API Rips V<br>Maximum Alowable Maxial Land for Jint = API John Stren<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Vergraff Margin = Maximum Alowable<br>Tensial Safety Factor = API Pep Ytel VOR API John Stren<br>Rig Max Load (300,000 bs) x 75% =<br>Minimum Overpuil Required =<br>Sourface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =   | lied on to by<br>'ield Strength<br>gth Rating / C<br>x Load) = Ma<br>te Hoat Load<br>ngth 'OR' Rig<br>225000 1<br>50000 1<br>211720<br>21720<br>381000   | to get in<br>h Rating<br>Corpora<br>aximum<br>I- Bouy<br>Max Lo<br>Ins<br>Ins<br>Ins<br>Ins<br>X<br>/   | t unstuck.<br>/ Corporate i<br>te Minimum A<br>Allowable As<br>and Wi of the<br>ad Rafing / ( i<br>0.870<br>1.40   | Minimum (<br>xial Desig<br>xial Load<br>Sbring<br>Bouyant )<br>=<br>=<br>=  | Axial Design<br>gn Factor<br>Wt of String -<br>18901<br>272143  |  | iverpul Requi                    | ret )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Lead for Pice Yeld - API Rpo Y<br>Maximum Alowable Axial Load for Joint - API Aint Stren<br>Navimum Alowable Hock Load (Limited In 75% of Rig La<br>Maximum Alowable Hock Load (Limited In 75% of Rig La<br>Maximum Alowable Overpuil Margin - Maximum Alowable<br>Tensial Safety Factor - API Pipe Yeld OR API Joint Stren<br>Rig Max Lead (300,000 hs) x 75% -<br>Minimum Overpuil Required -<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =  | led on to try<br>field Strength<br>gth Rating / C<br>x Load) = Us<br>Hook Load<br>(225000)<br>225000)<br>21720<br>21720<br>21720<br>21720<br>247000<br>244000<br>244000  | lo get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Its<br>Its<br>X  | t unstuck.<br>/ Corporate I<br>te Minimum At<br>Absyrable As<br>ant W1 of the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40  | Minimum ,<br>xini Desig<br>xini Lond<br>Sbring<br>Bouyant 1<br>Bouyant 1  | Axial Design<br>gn Factor<br>Wt of String -<br>18901<br>272143<br>174286  |  |                                  | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Land for Pice Ytels - API Rips V<br>Maximum Alowable Maxia Land for Jint - API Ainti Stren<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (200,000 bs) x 75% =<br>Minimum Overpuil Required =<br>Surface Casing Tensial Strength Safety Factor:<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Overpuil Margin =   | Red on to by<br>Viet Strength<br>gth Raing / C<br>x Load) = Mae<br>te Hoak Load<br>igth '06'' Rig<br>225000  <br>50000  <br>21720<br>21720<br>21720<br>24720<br>381000<br>244000<br>174266   | to get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Ibs<br>bs<br>X<br>/<br>/<br>/  | t unstuck.<br>/ Corporate i<br>te Minimum A<br>Allowable Az<br>and Wo of the<br>ad Rating / ( i<br>0.870<br>1.40<br>1.40<br>21720  | Ninimum ,<br>xial Desig<br>ital Lead<br>String<br>Jouyant 1<br>Jouyant 1<br>=<br>=<br>=<br>=                        | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174286<br>0.870  | ⊢ Minimum C  | 155384                           | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensice) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Lead for Pice Yeld - API Rpo Y<br>Maximum Alowable Axial Lead for Joint - API Aint Stren<br>Navimum Alowable Host Lead (Limited In 75% of Rig Ma<br>Maximum Alowable Host Lead (Limited In 75% of Rig Ma<br>Maximum Alowable Overpuil Margin - Maximum Alowable<br>Tensial Safety Factor - API Pipe Yeld OR API Joint Stren<br>Rig Max Lead (300,000 hs) x 75% -<br>Minimum Overpuil Required -<br>Max Minimum Overpuil Required -<br>Bouryant Wt =<br>Bouryant Wt =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Overpuil Margin =<br>Max. Allowable Overpuil Margin =<br>Tensial Safety Factor =   | Red on to by<br>Viet Strength<br>gth Raing / C<br>x Load) = Mae<br>te Hoak Load<br>igth '06'' Rig<br>225000  <br>50000  <br>21720<br>21720<br>21720<br>24720<br>381000<br>244000<br>174266   | logeti<br>hRating<br>Corpora<br>aximum<br>I-Bouy<br>Max Lo<br>Its<br>bs<br>bs<br>x<br>/<br>/  | t unstuck.<br>/ Corporate I<br>te Minimum At<br>Absyrable As<br>ant W1 of the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40  | Minimum,<br>xial Desig<br>ial Lead<br>Sbring<br>Bouyant 1<br>Souyant 1<br>=<br>=<br>=                               | Axial Design<br>gn Factor<br>Wt of String -<br>18901<br>272143<br>174286  | - Minimum C  |                                  | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Load for Pice Yiel - API Pipe Y<br>Maximum Alowable Axial Load for Joint Stem,<br>Maximum Alowable Axial Load for Joint 50% of Rig Ma<br>Maximum Alowable Overpul Margin = Maximum Alowable<br>Trensial Sofety Fector = API Pipe Yielt OR API Joint Stem,<br>Rig Hax Load (300,000 hs) x 75% =<br>Wintrum Overpul Required =<br>Max, Allowable Axial Load (Pipe Yield) =<br>Max, Allowable Axial Load (Joint) =<br>Max, Allowable Axial Load (Joint) =<br>Max, Allowable Overpull Margin =<br>Tensial Safety Factor =<br>roduction Casing Tensial Strength Safety Factor:   | led on 15 by<br>/i=W Strength<br>gth Rating / C<br>x Load) = Mae<br>Honk Load<br>(25000)<br>2000)<br>21720<br>21720<br>21720<br>21720<br>21720<br>244000<br>174286<br>244000<br>120734   | lo get i<br>h Rating<br>Corpora<br>aximum<br>I-Bouy<br>Max Lo<br>bis<br>bis<br>bis<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/   | t unstuck.<br>// Corporate i<br>le kinimum A<br>Abovable Ax<br>ad Walf the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40<br>1.40<br>1.40<br>1.801  | Winimum,<br>xiai Desig<br>Sbing<br>Bouyant 1<br>=<br>=<br>=<br>X<br>+   | Axial Design<br>gn Factor<br>18901<br>272143<br>174286<br>0.870<br>50000  | ⊢ Minimum C  | 155384                           | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get shuck and pu<br>Haximum Alowable Axial Lard for Pice Ytel - API Rpo Y<br>Maximum Alowable Axial Lard for Lint + API Aint Stren<br>Maximum Alowable Hack Load (Lintled Io 75% of Rig Ma<br>Maximum Alowable Hack Load (Lintled Io 75% of Rig Ma<br>Maximum Alowable Prest Margin - Maximum Alowable<br>Tensial Safety Factor - API Pipe Yteld OR API Joint Stren<br>Rig Max Lead (200,000 hs) x 75% -<br>Minimum Overpuil Required =<br>Uninum Overpuil Required =<br>Bouynant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Hook Load (Limited to 75% of Rig Max Load) =<br>Tensial Safety Factor =<br>Torduction Casing Tensial Strength Safety Factors:<br>Air Wt =  | Red on 10 by<br>Field Strengt<br>gth Rating / C<br>x: Load) = Uk<br>te Hook Load<br>ngth 'OR' Rig<br>225000 1<br>50000 1<br>24720<br>24720<br>244000<br>174266<br>174266<br>174266<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>174263<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17465<br>17   | to get i<br>h Rating<br>Corpora<br>aximum<br>I - Bouy<br>Max Lo<br>Ibs<br>bs<br>X<br>/<br>/<br>/  | t unstuck.<br>/ Corporate i<br>te Minimum AA<br>Adowable Aa<br>and Wi of the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40<br>21720<br>18901<br>0.847  | Ninimum ,<br>xial Desig<br>ital Lead<br>String<br>Jouyant 1<br>Jouyant 1<br>=<br>=<br>=<br>=                        | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174286<br>0.870  | ⊢ Minimum C  | 155384                           | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensico) load occurs if casing were to get stuck and pu<br>Maximum Alowable Axial Lead for Pice Yeld - API Pice Y<br>Maximum Alowable Axial Load for Joint Stern<br>Maximum Alowable Axial Load for Joint 50% of Rig Ma<br>Maximum Alowable Overpul Margin = Maximum Alowable<br>Tensial Sofety Factor = API Pice Yeld 'OR API Joint Stern<br>Rig Max Lead (30,000 fise) x 75% =<br>Minimum Overpul Required =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Overpul Margin =<br>Tensial Safety Factor:<br>Max. Allowable Overpul Margin =<br>Tensial Safety Factor =<br>Max. Allowable Safety Factor =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint Wit =   | led on ib try<br>riett Strengti<br>gih Rating / C<br>x Loady = Like<br>le Hook Load<br>rgth OR: Rig<br>225000  <br>50000  <br>50000  <br>24720<br>21720<br>21720<br>24720<br>24720<br>244000<br>174286<br>174286<br>244000<br>174286<br>244000<br>120734<br>120734<br>397000   | to get i<br>h Rating<br>Corpora<br>eximum<br>Hes Lo<br>Uns<br>bs<br>X<br>/<br>/<br>/<br>/<br>(<br>X   | t unstuck.<br>// Corporate i<br>le kinimum A<br>Abovable Ax<br>ad Walf the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40<br>1.40<br>1.40<br>1.801  | Minimum.<br>kiai Dasig<br>iai Load<br>Sbing<br>Jouyant<br>Souyant<br>=<br>=<br>=<br>x<br>+<br>+                     | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174285<br>0.870<br>50000<br>102301   | ⊢ Minimum C  | 155384                           | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>liaximum Alowable Axial Land for Pice Ytel - API Rips -<br>Maximum Alowable Axial Land for Jint - API Alori Stren<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Overput Required =<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Hook Load (Limited to 75% of Rig Max Load)<br>Production Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =  | Red on 10 by<br>/eH Strengt<br>gth Rating / C<br>x Load) = We<br>Hoth Load<br>ngth OR Rig<br>225000  <br>50000  <br>21720<br>21720<br>21720<br>244000<br>244000<br>244000<br>174286<br>244000<br>124266<br>244000<br>120734<br>120734<br>3378000<br>338000   | to get i<br>h Rating<br>corpora<br>corinsm<br>H-Bouy<br>Max Lo<br>Bas<br>K<br>to<br>S<br>- (<br>/<br>/<br>(<br>x<br>/<br>/<br>/<br>/                                    | t unstuck.<br>// Corporate i<br>te Winimum AA<br>Abovable Aa<br>and Wi of the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40   | Ninimum,<br>xini Deskj<br>sbring<br>Sbring<br>Souyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>=<br>=<br>=<br>=<br>=<br>= | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429   | ) =<br>) =   | 155384<br>3.54                   | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (Lensicn) load occurs if casing were to get stuck and pu<br>Baximum Allowable Axial Lead for Pice Yeld - API Pice Y<br>Maximum Allowable Axial Load for Joint Stern<br>Baximum Allowable Axial Load for Joint Stern<br>Baximum Allowable Overpul Margin = Maximum Allowable<br>Tensial Sofety Factor = API Pice Yeld 'OR API Joint Stern<br>Rig Max Lead (20,000 Bs) x 75% =<br>Winimum Overpul Required =<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Overpul Margin =<br>Tensial Safety Factor =<br>Production Casing Tensial Strength Safety Factor =<br>Bouyant Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Dimt Wt =<br>Bouyant Bout Bout Bout Bout Bout Bout Bout Bou | Red on 10 by<br>'rel Strengt<br>t Load) = Ue<br>te Hank Load<br>ngth 'OR' R0<br>225000<br>150000<br>24720<br>21720<br>21720<br>24720<br>24720<br>24720<br>24720<br>244000<br>174286<br>174286<br>244000<br>120734<br>120734<br>120734<br>338000<br>338000  | to get i<br>h Rating<br>Corpora<br>aximum<br>I-Bouy<br>Max Lo<br>Its<br>bs<br>X<br>/<br>/<br>/<br>/<br>(<br>/<br>/<br>(<br>X<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/    | t unstuck.<br>// Corporate in<br>the Minimum AA<br>Abovable Ay<br>ant Wi of the<br>ad Rating / (1<br>0.870<br>1.40<br>21720<br>18301<br>0.847<br>1.40  | Minimum.<br>kiai Deskj<br>iai Load<br>Sbing<br>Jouyant 1<br>=<br>=<br>=<br>=<br>X<br>+<br>+                         | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571   | ⊢ Minimum C  | 155384                           | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensice) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Lead for Pice Yell - API Pice Y<br>Maximum Alowable Axial Load for Joint - API Aint Strem<br>Haximum Alowable Hot Load (Limited In 75% of Rig Ma<br>Maximum Alowable Hot Load (Limited In 75% of Rig Ma<br>Maximum Alowable Overpuil Margin - Maximum Alowable<br>Tensial Safety Factor - API Pipe Yeld OR API Joint Strem<br>Rig Max Lead (300,000 fbs) x 75% -<br>Minimum Overpuil Required -<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Overpuil Margin =<br>Tensial Safety Factor =<br>roduction Casing Tensial Strength Safety Factors<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axield Axial Load (Pipe Yield  | Red on 10 by<br>Fell Strengt<br>gih Rating / C<br>x Load) = Like<br>te Hook Load<br>igth 'OR' Rig<br>225000 1<br>21720<br>21720<br>24720<br>244000<br>174286<br>244000<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>338000<br>225000   | to get i<br>h Rating<br>Corpora<br>aximum<br>I-Bouy<br>Max Lo<br>Its<br>bs<br>X<br>/<br>/<br>/<br>/<br>(<br>/<br>/<br>(<br>X<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/    | t unstuck.<br>// Corporate in<br>the Minimum AA<br>Adowshek AA<br>ant W1 of the<br>ad Rating / (1<br>0.870<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40  | Vinimum<br>xial Deskj<br>xial Load<br>Sbing<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>x<br>X          | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847                                | <pre>&gt; Minimum C ) = ) = ) =</pre>              | 155384<br>3.54<br>122699         | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensice) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Lead for Pice Yell - API Pice Y<br>Maximum Alowable Axial Load for Joint - API Aint Strem<br>Haximum Alowable Hot Load (Limited In 75% of Rig Ma<br>Maximum Alowable Hot Load (Limited In 75% of Rig Ma<br>Maximum Alowable Overpuil Margin - Maximum Alowable<br>Tensial Safety Factor - API Pipe Yeld OR API Joint Strem<br>Rig Max Lead (300,000 fbs) x 75% -<br>Minimum Overpuil Required -<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Overpuil Margin =<br>Tensial Safety Factor =<br>roduction Casing Tensial Strength Safety Factors<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axield Axial Load (Pipe Yield  | Red on 10 by<br>red Strengt<br>gth Rating / C<br>x Load) = Ua<br>E boot Load<br>100 225000<br>21720<br>21720<br>21720<br>21720<br>21720<br>24700<br>244000<br>174266<br>174266<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>12   | to get i<br>h Rating<br>Corpora<br>aximum<br>I-Bouy<br>Max Lo<br>Its<br>bs<br>X<br>/<br>/<br>/<br>/<br>(<br>/<br>/<br>(<br>X<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/    | t unstuck.<br>// Corporate in<br>the Minimum AA<br>Adowshek AA<br>ant W1 of the<br>ad Rating / (1<br>0.870<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40  | Vinimum<br>xial Deskj<br>xial Load<br>Sbing<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>x<br>X          | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847                                | <pre>&gt; Minimum C ) = ) = ) =</pre>              | 155384<br>3.54<br>122699         | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensich) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Load of Laint + API Aich Sten<br>Maximum Alowable Mack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hack Load (Limited to 75% of Rig Ma<br>Maximum Alowable Axial Load (Odd) (Limited to 75% of Rig Ma<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Hook Load (Limited to 75% of Rig Max Load) =<br>Max. Allowable Axial Load (Odint) =<br>Max. Allowable Strength Safety Factor =<br>Yroduction Cosing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Dint) =<br>Max   | led on ib by<br>riett Strengt<br>gih Raing / C<br>x Loady = Like<br>le Hook Load<br>rgh 'OR' Rig<br>225000]<br>1000<br>24720<br>21720<br>21720<br>21720<br>24720<br>24720<br>244000<br>174266<br>174266<br>174265<br>244000<br>120734<br>120734<br>120734<br>397000<br>308000<br>225000<br>300000<br>steps<br>sing is landed   | to get i<br>h Rating<br>Corpora<br>aximum<br>Hax Lo<br>bis<br>bis<br>tis<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>(<br>x<br>/<br>/<br>(<br>to bis<br>tis                   | t unstuck.<br>/ Corporate i<br>te kinimum A<br>Abweble As<br>and Wi of the<br>ad Rating / (1<br>0.870<br>1.40<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>120734<br>102301<br>conductor  | Vinimum<br>xial Deskj<br>xial Load<br>Sbing<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>x<br>X          | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847                                | <pre>&gt; Minimum C ) = ) = ) =</pre>              | 155384<br>3.54<br>122699         | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensico) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Lead for Pice Yell - API (per )<br>Maximum Alowable Axial Load for Joint - API Join Stren-<br>Bucimum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Maximum Alowable Hock Load (200,000 fbs) x 75% -<br>Minimum Overput Required -<br>Max Milowable Axial Load (30,000 fbs) x 75% -<br>Minimum Overput Required -<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Overput Margin =<br>Tensial Strength Safety Factor:<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Overput Margin =<br>Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Overput Margin =<br>Tensial Safety Factor =<br>Compression Strength ConocoPhillips Required Load Casing Compression Strength ConocoPhillips Required Load Casing Casing Compression Strength ConocoPhillips Required Load Casing Ca   | Red on 10 by<br>Field Strengt<br>gth Rating / C<br>x Load) = Uk<br>te Hoat Load<br>ngth OR Raj<br>225000 1<br>50000 1<br>24720<br>24720<br>244000<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>174266<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17466<br>17   | to get i<br>h Rating<br>Corpora<br>sximum<br>(- Bouy<br>Max Lo<br>bs<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/          | t unstuck.<br>// Corporate i<br>te klinimum AA<br>Adbovable AA<br>ant Wi of the<br>ad Rating / ( 1<br>0.870<br>1.40<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40   | Vinimum<br>xial Deskj<br>xial Load<br>Sbing<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>x<br>X          | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847                                | <pre>&gt; Minimum C ) = ) = ) =</pre>              | 155384<br>3.54<br>122699         | r년 )     |                       |             |                 |       |     |      |               |     |
| The maximum axial (lensich) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Load for Pice Ytel - API Rpo Y<br>Maximum Alowable Axial Load for Jint - API Aint Stren<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Overpuil Required =<br>Surface Casing Tensial Strength Safety Factor:<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Diont) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Dint) =<br>Max. Allowable  | led on ib by<br>ried Strengt<br>gih Rating / C<br>x Load) = like<br>le Hook Load<br>igh Orr Rej<br>225000 j<br>50000 j<br>21720<br>21720<br>21720<br>21720<br>247000<br>174286<br>174286<br>244000<br>174286<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>337000<br>338000<br>225000<br>338000<br>225000<br>338000<br>225000<br>338000<br>225000<br>338000<br>225000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>397000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>300000<br>3000000<br>3000000<br>300000000  | to get i<br>h Rating<br>Corpora<br>H-Bouy<br>Max Lo<br>bs<br>thes<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/        | t unstuck.<br>// Corporate in<br>te Minimum A<br>Abovable A<br>ant Wi of the<br>ad Rating / (1<br>0.870<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40   | Vinimum,<br>kial Desk<br>Sbring<br>Souyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>x<br>+                      | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000                       | <pre>&gt; Minimum C ) = ) = ) =</pre>              | 155384<br>3.54<br>122699         | r년 )     |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get shuck and pu<br>liaximum Alowable Axial Lead for Pice Yell - API Rpo Y<br>liaximum Alowable Hosk Lead (Linhed Io 75% of Rig La<br>liaximum Alowable Hosk Lead (Linhed Io 75% of Rig La<br>liaximum Alowable Hosk Lead (Linhed Io 75% of Rig La<br>liaximum Alowable Hosk Lead (Linhed Io 75% of Rig La<br>liaximum Alowable Hosk Lead (Linhed Io 75% of Rig La<br>liaximum Alowable Axial Lead (300,000 hs) x 75% -<br>liaminum Overput Required -<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Lead (Pipe Yield) =<br>Max. Allowable Axial Lead (Pipe Yield) =<br>Max. Allowable Axial Lead (Oint) =<br>Max. Allowable Axial Lead (Oint) =<br>Max. Allowable Axial Lead (Joint) =<br>Max. Allowable Axial Lead (Dipe Yield) =<br>Max. Allowable Axial Lead (Coint) =<br>Max. Allowable Axial Lead (Dipe Yield) =<br>Max. Allowable Axial Lead (Pipe Yield) =<br>Max. Allowable Oxerput Margin =<br>Tensial Safety Factor =<br>Compression Strength - ConocoPhillips Required Lead Car<br>The maximum axial (compression) bad for the well is where the surface cas<br>with a support of a phater theoring ring. The surface cashing is abo calculab<br>but not Minde. Any other axial bad such as a soubbing unt or other would  | Red on 15 by<br>Field Strengt<br>git Rating / C<br>x Load) = Uite<br>te Hook Load<br>rgth 'OR' Rig<br>2250000 1<br>221720<br>24720<br>24720<br>24720<br>174266<br>244000<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>338000<br>225000<br>308000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>50 | to get i<br>h Rating<br>Corpora<br>H-Bouy<br>Max Lo<br>bs<br>thes<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/        | t unstuck.<br>// Corporate in<br>te Minimum A<br>Abovable A<br>ant Wi of the<br>ad Rating / (1<br>0.870<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40   | Minimum,<br>kial Desk<br>Sbring<br>Bouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>X<br>+<br>X                           | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000                       | ) =<br>) =<br>) =                                  | 155384<br>3.54<br>122699         | r년 )     |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Load for Pice Yell - API (per<br>Maximum Alowable Axial Load for Joint - API Joint Stren-<br>Baximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Haximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Haximum Alowable Hock Load (Limited to 75% of Rig Ma<br>Haximum Alowable Hock Load (200,000 fbs) x 75% -<br>Winkrum Overpul Required -<br>Max. Allowable Axial Load (50,000 fbs) x 75% -<br>Minkrum Overpul Required -<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Overpul Margin =<br>Max. Allowable Overpul Margin =<br>Max. Allowable Overpul Margin =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Dint) =<br>Max. Allowable Axial Load (D   | led on 10 by<br>ried Strengt<br>git Rating / C<br>x Load) = Mis<br>e Hook Load<br>righ Orr Rej<br>225000 1<br>50000 1<br>21720<br>21720<br>21720<br>24720<br>174286<br>174286<br>174286<br>174286<br>174286<br>244000<br>174286<br>174286<br>120734<br>120734<br>120734<br>120734<br>397000<br>308000<br>225000<br>300000<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>1205<br>120   | to get i<br>h Rating<br>Corpora<br>H-Bouy<br>Max Lo<br>Its<br>bs<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/         | t unstuck.<br>/ Corporate in<br>te kinimum A<br>Abovable A<br>ant Wi of the<br>ad Rating / (1<br>0.870<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.20734<br>102301<br>1.55 be bad.<br>xinum Predict   | Minimum,<br>kial Desk<br>String<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>+                           | Axial Design<br>pr Factor<br>Vil of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000                       | ) =<br>) =<br>) =<br>) =                           | 155384<br>3.54<br>122699<br>1.97 | rस् )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>lixorinum Alowable Axial Load of Lait + API Alor M<br>lixorinum Alowable Axial Load of Lait + API Alor M<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>lixorinum Alowable Axial Load (Dir Alori Alori Alori<br>Rig Max Lead (200,000 hs) x 75% -<br>Linitrum Overpul Required -<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Dir Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Dirit) =<br>Max. A   | Red on 15 by<br>Field Strengt<br>gth Rating / C<br>x Load) = Mis<br>Rating / C<br>x Load) = Mis<br>225000<br>225000<br>244000<br>174286<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>120734<br>338000<br>225000<br>225000<br>225000<br>300000<br>ISES<br>sing is landed<br>at to bear 60<br>need to be ar<br>pe Yteld Ratin<br>3000   a  | to get i<br>h Rating<br>Corpora<br>Scimum<br>Has Lo<br>Bus<br>ts<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/         | t unstuck.<br>// Corporate i<br>te klinimum AA<br>Abwable AA<br>and Wi of the<br>ad Rating / ( 1<br>0.8670<br>1.40<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40  | Minimum,<br>xial Desk<br>ial Load<br>String<br>Bouyant 1<br>=<br>=<br>=<br>x<br>+<br>+<br>+<br>+<br>+<br>ted Load   | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000                       | ) =<br>) =<br>) =<br>) =                           | 155384<br>3.54<br>122699<br>1.97 | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>liaximum Alowable Axial Land for Jets Y Fel - API (pos Y<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Hack Load (Lintide Io 75% of Rig Ma<br>liaximum Alowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Allowable Axial Load Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Allowable Axial Load Allowable Axial Load Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Allowable Axial Load Joint) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load  | Red on 15 by<br>Field Strengt<br>gth Rating / C<br>x: Load) = Uite<br>Hoats Load<br>1000 1<br>2255000 1<br>227720<br>21720<br>21720<br>21720<br>247000<br>244000<br>174286<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120734<br>120746<br>120746<br>120746<br>120746<br>120746<br>120746<br>120746<br>1207   | to get i<br>h Rating<br>Corpora<br>I-Bouy<br>Max Lo<br>bas<br>bas<br>tas<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/ | t unstuck.<br>/ Corporate is<br>te Minimum AA<br>Abovable Ay<br>ant W1 of the<br>ad Rating / (1)<br>0.870<br>1.40<br>1.40<br>21720<br>18901<br>0.847<br>1.40<br>120734<br>102301<br>conductor<br>is bad<br>o the bad.<br>ximum Predict   | Minimum,<br>kial Desk<br>String<br>Jouyant 1<br>=<br>=<br>=<br>X<br>+<br>+<br>x<br>+<br>+                           | Axial Design<br>gn Factor<br>Vit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000                       | ) =<br>) =<br>) =<br>) =                           | 155384<br>3.54<br>122699<br>1.97 | red )    |                       |             |                 |       |     |      |               |     |
| The maximum axial (lension) load occurs if casing were to get stuck and pu<br>lixorinum Alowable Axial Load of Lait + API Rips V<br>lixorinum Alowable Axial Load of Lait + API Rips V<br>lixorinum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Maximum Alowable Hock Load (Linited to 75% of Rig Ma<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Hook Load (Linited to 75% of Rig Max Load) =<br>Max. Allowable Strength Safety Factor:<br>Air Wt =<br>Bouyant Wt =<br>Max. Allowable Axial Load (Pipe Yield) =<br>Max. Allowable Axial Load (Dint) =  | Red on 10 by<br>field Strengt<br>gth Rating / C<br>x Load) = Mike<br>Hoak Load<br>ngth OR Rig<br>225000<br>150000<br>174286<br>174286<br>174286<br>174286<br>244000<br>174286<br>174286<br>244000<br>120734<br>120734<br>120734<br>120734<br>338000<br>225000<br>225000<br>225000<br>300000<br>1885<br>sing is landed<br>ed to bear 60<br>need to bear<br>pe Yield Rati<br>30000 la<br>( 1<br>7102   | to get i<br>h Rating<br>Corpora<br>Scimum<br>Has Lo<br>Bus<br>ts<br>x<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/<br>/         | t unstuck.<br>// Corporate i<br>te Minimum AA<br>Abovable AA<br>and Wi of the<br>ad Rating / ( 1<br>0.6670<br>1.40<br>1.40<br>1.40<br>21720<br>18901<br>0.647<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40<br>1.40  | Minimum.<br>ital Desk<br>ital Load<br>String<br>Souyant 1<br>=<br>=<br>x<br>+<br>ted Load<br>0.870<br>0.877<br>x ×  | Axial Design<br>gn Factor<br>Wit of String -<br>18901<br>272143<br>174286<br>0.870<br>50000<br>102301<br>283571<br>241429<br>0.847<br>50000<br>0.847<br>50000     | ) =<br>) =<br>) =<br>) =<br>18901<br>102301<br>x   | 155384<br>3.54<br>122699<br>1.97 | red )    | 2.441                 | 42 =        | 11320           |       |     |      |               |     |
| The maximum axial (Lensich) load occurs if casing were to get stuck and pu<br>Haximum Alowable Axial Load for Pice Ytel - API (per<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Hock Load (Linthed Io 75% of Rig Ma<br>Maximum Alowable Axial Coad (Pipe Yteld OR API Joint Stern<br>Rig Max Lead (200,000 hs) x 75% -<br>Minimum Overpuil Required -<br>Surface Casing Tensial Strength Safety Factor:<br>Air Wt =<br>Max. Allowable Axial Load (Pipe Yteld) =<br>Max. Allowable Axial Load (Pipe Yteld) =<br>Max. Allowable Axial Load (Pipe Yteld) =<br>Max. Allowable Axial Load (Joint) =<br>Max. Allowable Axial Load (Pipe Yteld) =<br>Max. Allowable Axial Load (Pi   | Red on 10 by<br>Fell Strengt<br>gth Rating / C<br>x: Load) = Uk<br>te Hook Load<br>right OR 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## 2. Proposed cementing program:

### 16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

### 8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 300' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

|      | Slurry  |             | rvals<br>MD | Weight<br>ppg | Sx  | Vol<br>Cuft | Additives  | Yield<br>ft <sup>3</sup> /sx |
|------|---------|-------------|-------------|---------------|-----|-------------|--|------------------------------|
| Lead | Class C | Surface     | 560' – 605' | 13.6          | 300 | 510         | 2% Extender<br>2% CaCl <sub>2</sub><br>0.125 lb/sx LCM if needed<br>0.2% Defoamer<br>Excess =75% based on gauge<br>hole volume | 1.70                         |
| Tail | Class C | 560' – 605' | 860' 905'   | 14.8          | 200 | 268         | 1% CaCl2<br>Excess = 100% based on<br>gauge hole volume  | 1.34                         |

Displacement: Fresh Water.

Note: In accordance with the Pecos District Conditions of Approval, we will Wait on Cement (WOC) for a period of not less than 18 hrs after placement or until at least 500 psi compressive strength has been reached in both the Lead Slurry and Tail Slurry cements on the Surface Casing, whichever is greater.

#### 5-1/2" Production Casing Cementing Program – Single Stage Cementing Option:

The intention for the cementing program for the Production Casing - Single Stage Cementing Option is to:

- Place the Tail Slurry from the casing shoe to above the top of the Paddock,
- Bring the Lead Slurry to surface.

#### Spacer: 20 bbls Fresh Water

|      | Slurry      |         | rvals<br>MD   | Weight<br>ppg | Sx  | Vol<br>Cuft | Additives  | Yield<br>ft <sup>3</sup> /sx |
|------|-------------|---------|---------------|---------------|-----|-------------|--|------------------------------|
| Lead | 50:50 Poz/C | Surface | 5200'         | 11.8          | 700 | 1820        | 10% Bentonite<br>5% Salt<br>'0.2%-0.4% Fluid loss additive<br>0.125 lb/sx LCM if needed<br>Excess = 220% or more if<br>needed based on gauge hole<br>volume                              | 2.6                          |
| Tail | Class H     | 5200'   | 7045' – 7102' | 16.4          | 400 | 428         | <ul> <li>0.2% Fluid loss additive</li> <li>0.3% Dispersant</li> <li>0.15% Retarder</li> <li>0.2% Antifoam</li> <li>Excess = 100% or more if needed based on gauge hole volume</li> </ul> | 1.07                         |

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

## 5-1/2" Production Casing Cementing Program – Two-Stage Cementing w/ Comingle Option:

ConocoPhillips Company respectfully requests the options to our cementing program. The intention for the cementing program for the Production Casing – Two-Stage Cementing Option is to:

- Provide a contingency plan for using a Stage Tool and Annulus Casing Packer(s) to isolate losses or water flow if either of these events occurs while drilling the well.
- Place the Stage 1 Cement from the casing shoe to the stage tool,
- Bring Stage 2 Cement from the stage tool to surface.

#### Spacer: 20 bbls Fresh Water

| Stag | je 1 - Slurry |       | ervals<br>t MD | Weight<br>ppg | Sx  | Vol<br>Cuft | Additives  | Yield<br>ft <sup>3</sup> /sx |
|------|---------------|-------|----------------|---------------|-----|-------------|--|------------------------------|
| Lead | 50:50 Poz/H   | 3000' | 7045' – 7102'  | 13.2          | 800 | 1120        | <ul> <li>0.5% Fluid loss additive</li> <li>0.10% Retarder</li> <li>0.2% Antifoam</li> <li>0.125 lb/sx LCM if needed</li> <li>Excess = 150% or more if needed based on gauge hole volume</li> </ul> | 1.40                         |

| Staç | ge 2 - Slurry |         | rvals<br>MD           | Weight<br>ppg | Sx  | Vol<br>Cuft | Additives  | Yield<br>ft <sup>3</sup> /sx |
|------|---------------|---------|-----------------------|---------------|-----|-------------|--|------------------------------|
| Lead | 50:50 Poz/C   | Surface | Stage Tool<br>~ 3000' | 11.8          | 500 | 1300        | + 10 % Extender<br>+ 5 % NaCl<br>+ 0.2 % Defoamer<br>+ 5 lb/sx LCM/Extender<br>+ 0:125 lb/sx Lost Circulation<br>Control Agent<br>+ 0.5 % Fluid Loss<br>Excess = 50 % or more if<br>needed based on gauge hole<br>volume | 2.6                          |

Displacement: Fresh Water

#### Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volumes for the proposed single stage and two-stage option presented above are estimates based on gauge hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

#### 3. Pressure Control Equipment:

A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- o Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- o Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to the approved stack working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. **See Attached BOPE Schematic.** The BOPE may be configured to use flexible hose. Pressure test data and hose specification information will be provided to BLM prior to site construction.

#### 4. Proposed Mud System:

| DEPTH                      | TYPE  | Density<br>ppg | FV<br>sec/qt | API Fluid<br>Loss<br>cc/30 min | рН      | Vol<br>bbl  |
|----------------------------|---|----------------|--------------|--------------------------------|---------|-------------|
| 0 – Surface Casing Point   | Fresh Water or<br>Fresh Water Native<br>Mud in Steel Pits | 8.5 - 9.0      | 28 – 40      | N.C.                           | N.C.    | 120 – 160   |
| Surface Casing Point to TD | Brine (Saturated<br>NaCl <sub>2</sub> ) in Steel Pits     | 10             | 29           | N.C.                           | 10 – 11 | 1250 - 2500 |
| Conversion to Mud at TD    | Brine Based Mud<br>(NaCl <sub>2</sub> ) in Steel Pits     | 10             | 34 – 45      | 5 – 10                         | 10 11   | 0 - 1250    |

The mud systems that are proposed for use are as follows:  $\frac{1}{\sqrt{\frac{1}{2}}}$ 

#### Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole.

Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14. The gases shall be piped into the flare system. Gas detection equipment and pit level flow monitoring equipment will be on location. Gas detecting equipment will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

#### Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill these wells in 2013 after receiving approval of the APD.

# Attachments:

• Attachment # 1 ...... BOP and Choke Manifold Schematic – 3M System

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• Attachment # 2...... Diagram of Choke Manifold Equipment

# **Contact Information:**

Sundry Request proposed 16 October 2013 by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647







Drawn by: Steven O. Moore Chief Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company Date: 25-Sept-2012

#### **Request for Variance**

ConocoPhillips Company Lease Number: USA LC 058395 Well: SC Federal #9 Location: Sec. 22, T17S, R32E Date: 10-16-13

#### Request:

ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

#### Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

#### Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

#### Contact Information:

Program prepared by: James Chen Drilling Engineer, ConocoPhillips Company Phone (832) 486-2184 Cell (832) 768-1647 Date: 26 September 2012

## Attachment # 1

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|   |                                     |   |   |   |   |  | BOP stack to                                       |   | l-off   |
|   |                                     | 1                                       |   |   |   |  | io the BOP ki                                      |   |   |
| CO'   | ver that rep                        | olaces ru                               | bber cove   | ered Asbes                                  | tos, Fibre  | glass and                                    | ly bonded co<br>I other fire re                    | tardant   | ed  |
| ina<br>v  | aterials whi<br>ercomes co          | ich are pi<br>ostly repa                | rone to da<br>airs and do   | amage. Th<br>owntime a                      | is high cu<br>ssociated                           | ut.and.go<br>with old                        | uge resistan<br>er designs.                        | cover   |   |
|   |                                     | ;                                       | - Challen   |   |   |  |  |   |   |
| , Th  | e Reliance                          | Eliminat                                | or Choke  | & Kill hose                                 | has been  | verified                                     | by an indepe                                       | ndent   |   |
| Th<br>en  | e Reliance<br>gineer to n           | Eliminato<br>neet and                   | exceed E  | & Kill hose<br>UB Directiv                  | has been<br>ve 36 (70                             | verified 1<br>0°C for 5                      | by an indepe<br>minutes).                          | ndent   |   |
| Th<br>en  | e Reliance<br>gineer to n           | Eliminati<br>neet and                   | exceed E  | & Kill hose<br>UB Directiv                  | has been<br>ve 36 (70                             | verified<br>0°C for 5                        | by an indepe<br>minutes).                          | ndent   |   |
| i en  | e Reliance<br>gineer to n<br>m. ID  | neet and                                | exceed E  | UB Directiv                                 | ve 36 (70   | 0°C for 5                                    | by an indepe<br>minutes).<br>and Radius            | ndent<br>Max  | WP  |
| • en<br>Nor<br>in.  | gineer to n<br>m <b>. ID</b><br>mm. | neet and<br>Non<br>in.                  | exceed E<br>n OD<br>mm  | UB Directiv<br>Wei<br>16/ft                 | ve 36 (70<br>ght<br>kg/m                          | O°C for 5<br>Min Be<br>in.                   | minutes).<br>and Radius<br>mm.                     | <b>Max</b><br>psi   | Мра   |
| i en<br>Nor   | gineer to r<br>m. ID                | neet and<br>Non                         | exceed E<br>n OD<br>mm  | UB Directiv<br>Wei                          | ve 36 (70<br>ght                                  | 0°C for 5<br>Min Be                          | minutes).<br>and Radius                            | Max   |   |
| en<br>Nor<br>in<br>3  | gineer to n<br>m. ID<br>mm.<br>76.2 | neet and<br>Non<br>in.<br>5.11          | exceed E<br>n OD<br>mm<br>129.79                                    | UB Directiv<br>Wei<br>Ib/ft<br>14.5         | ve 36 (70<br>ght<br>kg/m<br>21.46                 | 0°C for 5<br>Min Be<br>in.<br>48             | minutes).<br>and Radius<br>mm.<br>1219.2           | Max<br>psi<br>5000  | Mpa<br>34.47  |
| en<br>Nor<br>in<br>3  | gineer to n<br>m. ID<br>mm.<br>76.2 | neet and<br>Non<br>in.<br>5.11          | exceed E<br>n OD<br>mm<br>129.79                                    | UB Directiv<br>Wei<br>Ib/ft<br>14.5         | ve 36 (70<br>ght<br>kg/m<br>21.46                 | 0°C for 5<br>Min Be<br>in.<br>48             | minutes).<br>and Radius<br>mm.<br>1219.2           | Max<br>psi<br>5000  | Mpa<br>34.47  |
| en<br>in.<br>3<br>3-1/2                                     | gineer to n<br>m. ID<br>mm.<br>76.2 | neet and<br>Non<br>in.<br>5.11          | exceed E<br>n OD<br>mm<br>129.79<br>147.06                          | Wei<br>Ib/ft<br>14.5<br>20.14               | ve 36 (70<br>ght<br>kg/m<br>21.46<br>29.80        | 0°C for 5<br>Min Be<br>in.<br>48<br>54       | minutes).<br>and Radius<br>mm.<br>1219.2<br>1371.6 | Max<br>psi<br>5000<br>5000  | Mpa<br>34.47<br>34.47   |
| en<br>in.<br>3<br>3-1/2<br>Fittings<br>RC4X5055             | gineer to n<br>m. ID<br>mm.<br>76.2 | Non<br>in.<br>5.11<br>5.79<br>R35 - 3-1 | exceed E<br>n OD<br>mm<br>129.79<br>147.06<br>Flanges<br>/8 5000# A | Wei<br>Ib/ft<br>14.5<br>20.14<br>Pl Type 6B | ve 36 (70<br>ght<br>kg/m<br>21.46<br>29.80<br>Han | 0°C for 5<br>Min Be<br>in.<br>48             | minutes).<br>and Radius<br>mm.<br>1219.2<br>1371.6 | Max<br>psi<br>5000<br>5000<br>000<br>Other<br>hreaded Ca            | Mpa<br>34.47<br>34.47<br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b> |
| en<br>in.<br>3<br>3-1/2<br>Fittings<br>RC4X5055<br>RC3X5055 | gineer to n<br>m. ID<br>mm.<br>76.2 | Non<br>in.<br>5.11<br>5.79<br>R35 - 3-1 | exceed E<br>n OD<br>mm<br>129.79<br>147.06<br>Flanges               | Wei<br>Ib/ft<br>14.5<br>20.14<br>Pl Type 6B | ve 36 (70<br>ght<br>kg/m<br>21.46<br>29.80<br>Han | 0°C for 5<br>Min Be<br>in.<br>48<br>54<br>54 | minutes).<br>and Radius<br>mm.<br>1219.2<br>1371.6 | Max<br>psi<br>5000<br>5000<br>5000<br>Dthe<br>hreaded Ca<br>Grayloc | Mpa<br>34.47<br>34.47<br><b>r</b><br>onnectio                                     |
| en<br>in.<br>3<br>3-1/2<br>Fittings<br>RC4X5055             | gineer to n<br>m. ID<br>mm.<br>76.2 | Non<br>in.<br>5.11<br>5.79<br>R35 - 3-1 | exceed E<br>n OD<br>mm<br>129.79<br>147.06<br>Flanges<br>/8 5000# A | Wei<br>Ib/ft<br>14.5<br>20.14<br>Pl Type 6B | ve 36 (70<br>ght<br>kg/m<br>21.46<br>29.80<br>Han | 0°C for 5<br>Min Be<br>in.<br>48<br>54<br>54 | minutes).<br>and Radius<br>mm.<br>1219.2<br>1371.6 | Max<br>psi<br>5000<br>5000<br>000<br>Other<br>hreaded Ca            | Mpa<br>34.47<br>34.47<br><b>r</b><br>onnectio                                     |

## Attachment # 2

1,

