ak 1 =1						14-387	
Form 3160-3 (March 2012)		OCD Hobb	۰. ۲	· OMB	M APPROVEE No. 1004-0137	1	
UNITED STATES DEPARTMENT OF THE I BUREAU OF LAND MAN	INTERIOR		-	5. Lease Serial No. NMLC 0310			
LOCATION BUREAU OF LAND MAN APPLICATION FOR PERMIT TO				6. If Indian, Allote N/A	e or Tribe Na	ame	
la. Type of work: XDRILL REENTE	3R			7 If Unit or CA Ag Southeast N		TInit	
lb. Type of Well: X Oil Well Gas Well Other	X Si	ingle Zone 🔲 Multi	iple Zone	8. Lease Name and SEMU	Well No.	249	1670
2. Name of Operator ConocoPhillips Company (217817)				9. API Well No. 30-025-442	2020		
^{3a.} Address 600 N. Dairy Ashford Rd, Office	(201)2	0. (include area code) 206-5281	cD	10. Field and Pool, or Skaggs; Grayb	Exploratory		
Houston, TX 77079-1175 4. Location of Well (Report location clearly and in accordance with any At surface 1360' FNL & 242' FWL; Lot 2, Sec. 19,	y State requiren T20S, R3	nents.*) HOBBS O	2014	11. Sec., T. R. M. or Lot 2, Sec. 19			
At proposed prod. zone same as above		BE NO 0 5					
 Distance in miles and direction from nearest town or post office* Approximately 10 miles southwest of Hobbs, NM. 		μυ»	EIVED	12. County or Parish Lea County		3. State NM	
5. Distance from proposed* 1275' location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any)	16. No. of a 641.68		17. Spacin 40 acr	ng Unit dedicated to this	well		
8. Distance from proposed location* about 600' to nearest well, drilling, completed, applied for, on this lease, ft.	19. Proposed 4196' 7	d Depth FVD/MD	20. BLM/ ES008	BIA Bond No. on file 55			
 Elevations (Show whether DF, KDB, RT, GL, etc.) 3543' GL 	22. Approxi 06/14/	mate date work will sta /2014	 urt*	23. Estimated duration 7 days) <u>n</u>		
	24. Attac	chments				<u> </u>	
 Well plat certified by a registered surveyor. A Drilling Plan. A Surface Use Plan (if the location is on National Forest System I SUPO must be filed with the appropriate Forest Service Office). 	Lands, the	Item 20 above). 5. Operator certific	cation	ns unless covered by ar			
5. Signatur Sydan B Maunder		(Printed/Typed) an B. Maunder			Date //	6/14	
Senior Regulatory Specialist pproved by (Signatu Steve Caffey	Name	(Printed/Typed)			Dato	4 2014	
itle	Office	(171110113900)	CARIS	BAD FIELD OFFIC	AUG -	4 2014	
FIELD MANAGER						1' 1/	
pplication approval does not warrant or certify that the applicant holds onduct operations thereon. onditions of approval, if any, are attached.	legal of equil	lable title to those righ		ROVAL FOR			
tle 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a cri ates any false, fictitious or fraudulent statements or representations as to	me for any pe o any matter w	erson knowingly and within its jurisdiction.	willfully to n	ake to any department of	or agency of	the United	
Continued on page 2)				*(Inst	tructions c	on page 2)	
Lea County Controlled Water Basin		$\langle \nu \rangle$	t	K 2 15/04/14			
·		a	EE A'	TACHED	FOR		
Approval Subject to Genera & Special Stipulations	al Requirer s Attached	ments C	ee a COND	TIONS OF	APPR	OVAL	
a pheria orbriggin		·	AUC	•	$\mathcal{L}_{\mathbf{k}}$		

AUG 0 7 2014

Operator Certification

HOBBS OCD

CONOCOPHILLIPS COMPANY

AUG 0 5 2014

CERTIFICATION:

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I hereby certify that I, or persons under my direct supervision, have inspected the proposed drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of State and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application with bond coverage provided by Nationwide Bond ES0085. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

Date: 1

(Junder) Maunder

Susan B. Maunder Senior Regulatory Specialist

Drilling Plan ConocoPhillips Company <u>SEMU; Grayburg</u>

HOBBS OCD

SEMU #249

AUG 0 5 2014

Lea County, New Mexico

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1. Estimated tops of geological markers and estimated depths to water, oil, or gas formations:

The datum for these depths is RKB (which is 13' above Ground Level).

Formations	Top Depths FT MD	Contents						
Quaternary	Surface	Fresh Water						
Rustler	1371	Anhydrite						
Salado (top of salt)	1459	Salt						
Tansill (base of salt)	2569	Gas, Oil and Water						
Yates -	2676	Gas, Oil and Water						
Seven Rivers	2920	Gas, Oil and Water						
Queen	3493	Gas, Oil and Water						
Penrose	3624	Gas, Oil and Water						
Grayburg	3770	Gas, Oil and Water						
San Andres	3996	Gas, Oil and Water						
Deepest estimated perforation	3996	Deepest estimated perf. is above Top of San Andres						
Total Depth (maximum)	4196	200' below deepest estimated perforation						

All of the water bearing formations identified above will be protected by setting of the <u>8-5/8</u>" surface casing <u> $25^{\circ} - 70^{\circ}$ into the Rustler formation</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

The targeted oil and gas bearing formations identified above will be protected by setting of the <u>5-1/2</u>ⁿ production casing <u>10' off bottom of TD</u> and circulating of cement from casing shoe to surface in accordance with the provisions of Onshore Oil and Gas Order No. 2 and New Mexico Oil Conservation Division Title 19.

2. Proposed casing program:

Туре	Hole Size		Interval ID RKB (ft)	OD	Wt	Gr	Conn	MIY	Col	Jt Str	Calcu	Safety Fa lated per Co Corporate (nocoPhillips
, jpc	(in)	From	То	(inches)	(lb/ft)		CONIT	(psi)	(psi)	(klbs)	Burst DF	Collapse DF	Jt Str DF (Tension) Dry/Buoyant
Cond	20	0	40' – 85' (30' – 75' BGL)	16	0.5" [,] wall	В	Line Pipe	N/A	N/A	N/A	NA	NA	NA
Alt. Cond	20	0	40' – 85' (30' – 75' BGL)	13-3/8	48#	H-40 [′]	PE	1730	740 [.]	N/A	NA	NA	NA
Surf	12-1/4	0	⇒396 ' – 1441'	8-5/8	24#	J-55	STC	2950	1370	244	1.38	2.14	. 3.05
Prod	7-7/8	0	4141' – 4186'	5-1/2	17#	L-80	LTC	7740	6290	- 338	3.56	5.01	2.72

The casing will be suitable for H₂S Service. All casing will be new.

The surface and production casing will be set approximately 10' off bottom and we will drill the hole with a 45' range uncertainty for casing set depth to fit the casing string so that the cementing head is positioned at the floor for the cement job.

The production casing will be set 155' to 200' below the deepest estimated perforation to provide rathole for the pumping completion and for the logs to get deep enough to log the interval of interest.

Casing Safety Factors - BLM Criteria:

Туре	Depth	Wt	MIY	Col	Jt Str	Drill Fluid	Burst	Collapse	Tensile-Dry	Tens-Bouy
Surface Casing	1441	24	2950	1370	244000	8.5	4.63	2.15	7.1	8.1
Production Casing	4186	17	7740	6290	338000	10	3.56	2.89	4.75	5.61

Casing Safety Factors – Additional ConocoPhillips Criteria:

ConocoPhillips casing design policy establishes Corporate Minimum Design Factors (see table below) and requires that service life load cases be considered and provided for in the casing design.

		teria for Minimum Design Factors	
	Burst	Collapse	Axial
Casing Design Factors	1.15	1.05	1.4

	Depth		MIY	Col	Jt Str	Pipe Yie		Burs	t Col	Тел	_					
Conductor Surface Casing (8-5/8" 24# J-55 STC)	85 1441		5 3500 4 295		- 70 24400	4329 0 3810		5 1.3	- 38 2.1	4 3.0	15					
Production Casing (5-1/2" 17# L-80 LTC)	4186		7 774		90 33800											
: <u>Burst ConocoPhillips Required Load Cases</u>																
The maximum internal (burst) load on the Surface Casing occurs when the								ementa)	h.							
The maximum internal (burst) load on the Production Casing occurs during (ILAWP) is the pressure that would fit ConocoPhilips Corporate Criteria fo			on where i		um allowads	e working pr	essure									
Surface Casing Test Pressure =	1500					Pressure at 1			i5 ppg							
Surface Rated Working Pressure (BOPE) = Field SW =	3000	ps: ppg		Predic	ted Frac Gri	idient at Sho	e (CSFG) =	19.2	3 ppg							
Surface Casing Burst Safety Factor = API Burst Rating / Ma: Production Casing MAWP for the Fracture Stimulation = API							e Surface Pr	essure ((MASP)							
Surface Casing Burst Safety Factor: Case #1. MPSP (MWhyd next section) =	1441	x	0,052	x	10	2	749									
Case #2. MPSP (Field SW @ Bullhead _{CSFG} + 200 psi) =	1441	x	0.052		19.23	-	749	+	200	=	892					
Case #3. MPSP (Kick Vol @ next section TD) = Case #4. MPSP (PPTD - GG) =	4 186 4 186	x x	0.052		8.55 8.55	-	274.5 418.6	-	637 1442	7	950					
Case #3 & #4 Limited to MPSP (CSFG + 0.2 ppg) =	1441	x	0.052	x (19.23	+	0.2) =								
MASP (MWhyd + Test Pressure) = Burst Safety Factor (Max, MPSP or MASP) =	1441 2950	×	0.052 2137		8.5 1.38	+	1500	=	2137							
Production Casing Burst Safety Factor:		,														
Case #1. MPSP (MWhyd TD) = Case #4. MPSP (PPTD - GG) =	4186 4186	x x	0.052		10 8.55	· #	2176.72 418.6	! =	1442							
Burst Safety Factor (Max. MPSP) =	7740	î	2177		3.56		410.0	-	1442							
MAWP for the Fracture Stimulation (Corporate Criteria) =	7740	1	1.15	=	6730											
Collapse - ConocoPhillips Required Load Cases The maximum collapse load on the Surface Casing occurs when cementing	o to surface, '	1/3 evac	aution to t	he next c	asing setting	depth, or de	epest depth :	of excos	sure (fuil av	racuation).						
The maximum collapse load on the Production Casing occurs when cemen	ting to surface	e, ar 1/3	evacuatio	n to the d	eepest depti	1 of exposur	; and			-						
therefore, the external pressure profile for the evacuation cases should be Surface Casing Collapse Safety Factor = API Collapse Rating								we ass	sumed to be	PPTD.						
Production Casing Collapse Safety Factor = API Collapse Rat	ling / Maximum	n Predict		e Pressur	e 'OR' Ceme	nt Displacem	ent during Ca	menting	to Surface							
Cement Displacement Fluid (FW) = Surface Cement Lead =	8.34		Р		Cement = nt Lead =	Cement to 5	Surface 5 ppg									
Surface Cement Tail =	14.8	ppg		Prod Cen	ient Tal =	1	4 ppg									
Top of Surface Tail Cement =	350	ft	. Top of	Prod Tail	Cement =	300	Ujn									
Surface Casing Collapse Safety Factor:			0.050													
Full Evacuation Diff Pressure = Cementing Diff Lift Pressure =	144 1 [(.	x 1091	0.052 ×	× 0.052	8.55 ×	= 13.6	641)+(350	x	0.052	x	14.8	۱	625	1 =	416
Collapse Safety Factor =	1370	1	641	=	2.14		, ,						'		'	
Production Casing Collapse Safety Factor: 1/3 Evacuation Diff Pressure =	-II	4186	×	0.052	x	8.55) - (4186	1	3	x	0.052	x	8 34	1] =	1256
Cementing Diff Lift Pressure =	K	1186	x	0.052	x	11.5		3000		0.052	x	14			1=	
Collapse Safety Factor =						11.5) + (^	0,052	~	17) -	1013	1 -	10/6
· •	6290	1	1256	=	5.ÓÎ	11.5	<i>,</i> + (~	U.USZ	~	14] -	1015	1 -	1078
	6290	1				11.5	,+(^	0.092	*	14] -	1013	1 -	1078
Tensial Strength — ConocoPhillips Required Load Cases The maximum exist (lension) load accurs if casing were to get stuck and pu			1256			11.5	<i>)</i> + (~	U,U32	*) -	1013	1 -	1070
Tensial Strength — <u>ConocoPhillips Required Load Cases</u> The maximum axial (lension) load accurs if casing were to get stuck and pu Maximum Allowable Axial Load for Pipe Yield = API Pipe	ulled on to try Yield Strength	to get it Rating :	1256 unstuck / Corporate	= e Minimur	5.01 Axial Desig) , (Ň	0,052	*	14]-	1013	1 -	1078
<u>Tensial Strength - ConocoPhillips Required Load Cases</u> The maximum axial (tension) load occurs if casing were to get stuck and pu	ulled on to try Yield Strength 1gth Rating / C	to get it n Rating : Corporate	1256 unatuck / Corporati o Minimum	≕ e Minimurr Axial Dea	5.Ó1 Axial Desig Ign Factor		J + (Â	0.052	*] -	6101	1-	1076
Tensial Strength — ConocoPhillips Required Load Cases The maximum axial (lension) load accurs if casing were to get stuck and pu Maximum Aflowable Axial Load for Pipe Yield - API Pipe Maximum Aflowable Axial Load for John = API John Stren Maximum Aflowable Hoak Load (Limited to 75% of Rig Mr. Maximum Aflowable Overpul Margin = Maximum Aflowab	ulled on to try Yield Strength Igth Rating / C ax Load) = Ma Ne Hook Load	to get it Rating : Corporate Eximum A - Bouya	1256 unstuck. / Corporate Minimum Nowable / nt Wt of th	≕ e Minimum Axial Dea Axial Load e String	5.Ó1 Axial Desig Ign Factor 	n Factor			Â	0.052	*		J -	6101	1 -	
<u>Tensial Strength – ConocoPhillips Required Load Cases</u> The maximum axial (lension) load occurs If casing were to get stuck and pu Maximum Allowable Axial Load for Poe Yield – API Poe Maximum Allowable Axial Load for Joint – API Joint Stren Maximum Allowable Hook Load (Limited to 75% of Rig M	ulled on to try Yield Strength Igth Rating / C ax Load) = Ma Ne Hook Load	to get it i n Rating ; corporate uximum A - Bouya Max Loa	1256 unstuck. / Corporate Minimum Nowable / nt Wt of th	≕ e Minimum Axial Dea Axial Load e String	5.Ó1 Axial Desig Ign Factor 	n Factor			Â	0.052	*		, -	6191	1 -	
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3. Proposed cementing program:

16" or 13-3/8" Conductor:

Cement to surface with rathole mix, ready mix or Class C Neat cement. (Note: The gravel used in the cement is not to exceed 3/8" diameter) TOC at surface.

8-5/8" Surface Casing Cementing Program:

The intention for the cementing program for the Surface Casing is to:

- Place the Tail Slurry from the casing shoe to 350' above the casing shoe,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry	1	rvals MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Class C	Surface	1046' – 1091'	13.6	450	765	+ 2% Extender + 2% CaCl ₂ + 0.125 lb/sx Lost Circulation Control Agent + 0.2% Defoamer	1.70
							Excess =200% based on gauge hole volume	
Tail	Class C	1046' – 1091'	1396' – 1441'	14.8	300	402	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

Displacement: Fresh Water.

5-1/2" Production Casing Cementing Program – Single Stage Cementing Option:

The intention for the cementing program for the Production Casing – Single Stage Cementing Option is to:

- Place the Tail Slurry from the casing shoe to above the top of the Grayburg,
- Bring the Lead Slurry to surface.

Spacer: 20 bbls Fresh Water

	Slurry		rvals MD	Weight ppg	Sx	. Vol Cuft	Additives	Yield ft ³ /sx
Lead	C Gas Tight Slurry	Surface	3000'	11.5	400	1292	Class C 94 lb/sx 6% Extender 10% Gas Migration Control 2% Sodium Metasilicate (dry) 1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23
Tail	Poz/C Gas Tight Slurry	3000'	4141' – 4186'	14.0 .	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

Displacement: Fresh Water with approximately 250 ppm gluteraldehyde biocide.

5-1/2" Production Casing Cementing Program – Two-Stage Cementing Option (Shallow Flow):

ConocoPhillips Company respectfully requests the options to our cementing program. The intention for the cementing program for the Production Casing – Two-Stage Cementing Option is to:

- Provide a contingency plan for using a Stage Tool and Annulus Casing Packer(s) to isolate shallow saltwater or gas flow if either of these events occurs while drilling the well.
- Place the Stage 1 Cement from the casing shoe to surface.
- Proceed with Stage 2 Cement only if cement returns are contaminated or flow was observed after pumping 1st stage.

Spacer: 20 bbls Fresh Water

Stage	1 - Slurry		Intervals Ft MD	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	C Gas Tight Slurry	Surface	3000'	11.5	400	1292	Class C 94 lb/sx 6% Extender 10% Gas Migration Control 2% Sodium Metasilicate (dry) 1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23
Tail	Poz/C Gas Tight Slurry	3000'	4141' – 4186'	14.0	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

1st stage displacement: FW followed by Weighted Spacer

Spacer: Remaining Weighted Spacer in cementing lines from the 1st stage displacement

Sta	age 2 - Slurry	intervals Ft M		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Tail	Class C	Surface	Stage Tool ~1450'	14.8	300	402	1% CaCl2 Excess = 100% based on gauge hole volume	1.34

2nd stage displacement: Fresh Water

5-1/2" Production Casing Cementing Program – Two-Stage Cementing Option (Lower Zone Losses or Waterflow):

ConocoPhillips Company respectfully requests the options to our cementing program. The intention for the cementing program for the Production Casing – Two-Stage Cementing Option is to:

- Provide a contingency plan for using a Stage Tool and Annulus Casing Packer(s) to isolate losses or waterflow if either of these events occurs while drilling the well.
- Place the Stage 1 Cement from the casing shoe to the stage tool,
- Bring Stage 2 Cement from the stage tool to surface.

Spacer: 20 bbls Fresh Water See, COA

Stag	ge 1 – Slurry	Inter Ft N		Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	Poz/C Gas Tight Slurry	Stage Tool ~2900'	4141' – 4186'	14.0	320	438	(35:65) Poz:C 33 lb/sx 1% Sodium Metasilicate (dry) 1.5% Fluid Loss Control,	1.37

1st stage displacement: FW followed by Brine

Spacer: 20 bbls Fresh Water

Stag	je 2 - Slurry	1	vals ND	Weight ppg	Sx	Vol Cuft	Additives	Yield ft ³ /sx
Lead	C Gas Tight Slurry	Surface	Stage Tool ~2900'	11.5	400	1292	Class C 94 lb/sx 6% Extender 10% Gas Migration Control 2% Sodium Metasilicate (dry) 1% Cement Bonding Agent 3% Aluminum Silicate 0.125 lb/sx Cello Flake 3 lb/sx LCM-1	3.23

Displacement: Fresh Water

Proposal for Option to Adjust Production Casing Cement Volumes:

The production casing cement volumes for the proposed single stage and two-stage option presented above are estimates based on gauge hole. We will adjust these volumes based on the caliper log data for each well and our trends for amount of cement returns to surface. Also, if no caliper log is available for any particular well, we would propose an option to possibly increase the production casing cement volume to account for any uncertainty in regard to the hole volume.

4. Pressure Control Equipment:

A <u>11" 3M</u> system will be installed, used, maintained, and tested accordingly as described in Onshore Oil and Gas Order No. 2.

Our BOP equipment will be:

- Rotating Head
- o Annular BOP, 11" 3M
- o Blind Ram, 11" 3M
- Pipe Ram, 11" 3M

After nippling up, and every 30 days thereafter or whenever any seal subject to test pressure is broken followed by related repairs, blowout preventors will be pressure tested. BOP will be inspected and operated at least daily to insure good working order. All pressure and operating tests will be done by an independent service company and recorded on the daily drilling reports. BOP will be tested using a test plug to isolate BOP stack from casing. BOP test will include a low pressure test from 250 to 300 psi for a minimum of 10 minutes or until requirements of test are met, whichever is longer. Ram type preventers and associated equipment will be tested to 50 percent of rated working pressure of 3000 psi isolated by test plug. Annular type preventers will be tested to 50 percent of rated working pressure, and therefore will be tested to 1500 psi. Pressure will be held for at least 10 minutes or until provisions of test are met, whichever is longer. Valve on casing head below test plug will be open during testing of BOP stack. BOP will comply with all provisions of Onshore Oil and Gas Order No. 2 as specified. **See Attached BOPE Schematic.** A variance is respectfully requested to allow for the use of flexible hose. The variance request is included as a separate enclosure with attachments.

See COA

5. Proposed Mud System:

DEPTH	TYPE	Density ppg	FV sec/qt	API Fluid Loss cc/30 min	pН	Vol bbl
0 – Surface Casing Point	Fresh Water or Fresh Water Native Mud in Steel Pits	8.5 - 9.0	28 – 40	N.C.	N.C.	150 – 300
Surface Casing Point to TD	Brine (Saturated NaCl ₂) in Steel Pits	10	29	N.C.	10 – 11	300 – 1000
Conversion to Mud at TD	Brine Based Mud (NaCl₂) in Steel Pits	10	33 – 40	5 – 10	10 – 11	0 – 1000

The mud systems that are proposed for use are as follows:

Gas detection equipment and pit level flow monitoring equipment will be on location. A flow paddle will be installed in the flow line to monitor relative amount of mud flowing in the non-pressurized return line. Mud probes will be installed in the individual tanks to monitor pit volumes of the drilling fluid with a pit volume totalizer. Gas detecting equipment and H2S monitor alarm will be installed in the mud return system and will be monitored. A mud gas separator will be installed and operable before drilling out from the Surface Casing. The gases shall be piped into the flare system. Drilling mud containing H2S shall be degassed in accordance with API RP-49, item 5.14.

In the event that the well is flowing from a waterflow, then we would discharge excess drilling fluids from the steel mud pits through a fas-line into steel frac tanks at an offset location for containment. Depending on the rate of waterflow, excess fluids will be hauled to an approved disposal facility, or if in suitable condition, may be reused on the next well.

No reserve pit will be built.

Proposal for Option to Not Mud Up at TD:

FW, Brine, and Mud volume presented above are estimates based on gauge 12-1/4" or 7-7/8" holes. We will adjust these volume based on hole conditions. We do not plan to keep any weighting material at the wellsite. Also, we propose an option to not mud up leaving only brine in the hole if we have good hole stability.

6. Logging, Coring, and Testing Program:

- a. No drill stem tests will be done
- b. Remote gas monitoring planned for the production hole section (optional).
- c. No whole cores are planned
- d. The open hole electrical logging program is planned to be as follows:
 - Total Depth to 1700' MD: Spectral Gamma Ray, PE, Resistivity (laterologs), Bulk Density, and Sonic
 - Total Depth to surface Casing Shoe: Caliper
 - Total Depth to surface, Total Gamma Ray and Neutron
 - Total Depth to 2350' MD ; Mud Log (optional)
 - Total Depth to 2350' MD ; Dielectric Scanner (optional)
 - Formation pressure data (XPT) on electric line if needed (optional)
 - Rotary Sidewall Cores on electric line if needed (optional)
 - FMI (Formation MicroImager) if needed (optional)
 - UBI (Ultrasonic Borehole Imager) if needed (optional)
- e. Cement Bond Log (optional).

7. Abnormal Pressures and Temperatures:

- No abnormal pressures are expected to be encountered.
- Loss of circulation is a possibility in the horizons below the Top of Grayburg. We expect that normal Loss of Circulation Material will be successful in healing any such loss of circulation events.



- The bottom hole pressure is expected to be 7.8 ppg gradient.
- The expected Bottom Hole Temperature is 100 degrees F.
- The estimated H₂S concentrations and ROE calculations for the gas in the zones to be penetrated are presented in the table below for the various producing horizons in this area:

FORMATION / ZONE	H2S (PPM)	Gas Rate (MCFD)	ROE 100 PPM	ROE 500 PPM
Seven Rivers	6	50 - 100 MCFD	0	0
Grayburg / San Andres	18360	20 - 50 MCFD	95	43

ConocoPhillips will comply with the provisions of Oil and Gas Order # 6, Hydrogen Sulfide Operations. Also, ConocoPhillips will provide an H2S Contingency Plan (please see copy attached) and will keep this plan updated and posted at the wellsite during the drilling operation.

8. Anticipated starting date and duration of operations:

Well pad and road constructions will begin as soon as all agency approvals are obtained. Anticipated date to drill these wells begin in 2014 after receiving approval of the APD.

Attachments:

- Attachment # 1 Two-stage Cementing Schematic
- Attachment # 2 BOP and Choke Manifold Schematic 3M System
- Attachment # 3...... Diagram of Choke Manifold Equipment

Contact Information:

Proposed 9 January 2014 by: Steven Herrin Drilling Engineer, ConocoPhillips Company Phone (281) 206-5115 Cell (432) 209-7558 SEMU #249

(Date: 1/9/2014)







16 Surface Casing

Submitted by: Steven Herrin, Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company, 03-Jan-2014

Attachment # 3



ltem Description

- Manual Adjustable Choke, 2-1/16", 3M 1
- Remote Controlled Hydraulically Operated Adjustable Choke, 2-1/16", 3M 2
- 3 Gate Valve, 2-1/16" 5M
- Gate Valve, 2-1/16" 5M 4
- Gate Valve, 2-1/16" 5M 5
- Gate Valve, 2-1/16" 5M 6
- 7 Gate Valve, 3-1/8" 3M
- Gate Valve, 2-1/16" 5M 8
- Gate Valve, 2-1/16" 5M 9
- Gate Valve, 2-1/16" 5M 10
- 11 Gate Valve, 3-1/8" 3M
- Gate Valve, 2-1/16" 5M 12
- 13 Pressure Gauge
- 14 2" hammer union tie-in point for BOP Tester

We will test each valve to 3000 psi from the upstream side.

Submitted by: Steven Herrin Drilling Engineer, Mid-Continent Business Unit, ConocoPhillips Company Date: 3-January-2014

Request for Variance

ConocoPhillips Company

Lease Number: NMLC031670 (A) Well: SEMU #249 Location: Sec. 19, T20S, R38E Date: 1/9/2014

Request:

Zee COA ConocoPhillips Company respectfully requests a variance to install a flexible choke line instead of a straight choke line prescribed in the Onshore Order No. 2, III.A.2.b Minimum standards and enforcement provisions for choke manifold equipment. This request is made under the provision of Onshore Order No. 2, IV Variances from Minimum Standard. The rig to be used to drill this well is equipped with a flexible choke line if the requested variance is approved and determined that the proposed alternative meets the objectives of the applicable minimum standards.

Justifications:

The applicability of the flexible choke line will reduce the number of target tees required to make up from the choke valve to the choke manifold. This configuration will facilitate ease of rig up and BOPE Testing.

Attachments:

- Attachment # 1 Specification from Manufacturer
- Attachment # 2 Mill & Test Certification from Manufacturer

Contact Information:

Program prepared by: Steven Herrin Drilling Engineer, ConocoPhillips Company Phone: (281) 206-5115 Cell: (432) 209-7558 Date: 2 January 2014

Attachment # 1



Reliance Eliminator Choke & Kill

This hose can be used as a choke hose which connects the BOP stack to the bleed-off manifold or a kill hose which connects the mud stand pipe to the BOP kill valve.

The Reliance Eliminator Choke & Kill hose contains a specially bonded compounded cover that replaces rubber covered Asbestos, Fibreglass and other fire retardant materials which are prone to damage. This high cut and gouge resistant cover overcomes costly repairs and downtime associated with older designs.

The Reliance Eliminator Choke & Kill hose has been verified by an independent engineer to meet and exceed EUB Directive 36 (700°C for 5 minutes).

Nom, ID		Nom	Nom OD Weig		pht Min Bend Radi		us Max WP		
in.	mm.	in.	mm	lb/ft	kg/m	in.	mm	•	Mpa
3 3-1/2	76.2 88.9	5.11 5.79	129.79 147.06	14.5 20.14	21.46 29.80	48 54	1219 1371		34.4 34.4
				·					
Fittings			Flanges	·	Han	nmer Un	ions	Othe	r
RC4X5055 RC3X5055 RC4X5575			8 5000# AP 8 3000# AP		All Un	ilon Configu	irations	LP Threaded C Graylo Custom E	ck

Attachment # 2



Closed Loop System Design, Operating and Maintenance, and Closure Plan

ConocoPhillips Company Well: SEMU #249 Location: Sec. 19, T20S, R38E Date: 1/13/2014

ConocoPhillips proposes the following plan for design, operating and maintenance, and closure of our proposed closed loop system for the above named well:

1. We propose to use a closed loop system with steel pits, haul-off bins, and frac tanks for containing all cuttings, solids, mud, water, brine, and liquids. We will not dig a pit, nor will we use a drying pad, nor will we build an earth pit above ground level, nor will we dispose of or bury any waste on location.

All drilling waste and all drilling fluids (fresh water, brine, mud, cuttings, drill solids, cement returns, and any other liquid or solid that may be involved) will be contained on location in the rig's steel pits or in hauloff bins or in frac tanks as needed. The intent is as follows:

- We propose to use the rigs' steel pits for containing and maintaining the drilling fluids.
- We propose to remove cuttings and drilled solids from the mud by using solids control equipment and to contain such cuttings and drilled solids on location in haul-off bins.
- We propose that any excess water that may need to be stored on location will be stored in tanks.

The closed loop system components will be inspected daily by each tour and any needed repairs will be made immediately. Any leak in the system will be repaired immediately, and any spilled liquids and/or solids will be cleaned immediately, and the area where any such spill occurred will be remediated immediately.

2. Cuttings and solids will be removed from location in haul-off bins by an authorized contractor and disposed of at an authorized facility. For this well, we propose the following disposal facility:

R-360 Inc. 4507 West Carlsbad Hwy, Hobbs, NM 88240, P.O. Box 388; Hobbs, New Mexico 88241 Toll Free Phone: 877.505.4274, Local Phone Number: 432.638.4076

The physical address for the plant where the disposal facility is located is Highway 62/180 at mile marker 66 (33 miles East of Hobbs, NM and 32 miles West of Carlsbad, NM).

The Permit Number for R-360 is NM-01-0006.

A photograph showing the type of haul-off bins that will be used is attached.

- 3. Mud will be transported by vacuum truck and disposed of at R-360 Inc. at the facility described above.
- 4. Fresh Water and Brine will be hauled off by vacuum truck and disposed of at an authorized salt water disposal well. We propose the following for disposal of fresh water and brine as needed:
 - Nabors Well Services Company, 3221 NW County Rd; Hobbs, NM 88240, PO 5208 Hobbs, NM, 88241, Permit SWD 092. (Well Location: Section 3, T19S R37E)
 - Basic Energy Services, P.O. Box 1869; Eunice, NM 88231 Phone Number: 575.394.2545, Facility located at Hwy 18, Mile Marker 19; Eunice, NM.

Steven Herrin Drilling Engineer, ConocoPhillips Company Phone (281) 206-5115 Cell (432) 209-7558

SPECIFICATIONS

FLOOR = 3/16" PL one piece CROSS MEMBER: 3 x 4.1 channel 16" on center

WALLS: 3/16" PL solid welded with tubing lop, inside liner hooks

DOOR: 3/16/ PL with White frame FRONT: 3/16" PL slant formed PICK U P: Standard cable with 2" x 6" x 1/4" rails, gu sset at each crossmember WHEELS: 10 DIA:x 9 long with rease littings DOOR LATCH: 3 Independent ratchet binders: with chains; vertical second latch. CASKETIS: Extruded rubber seal with metal retainers

WELDS: All welds continuous except sub structur e crossmembers

FINISH: Coated Inside and out with direct to metal, rust inhibiting acrylic enamel color coat HYDROTESTING: Full capacity static test DIMEN SIONS: 22-11* long (21-8' inside), 99' wide (88' inside), see drawing for height OPTIONS: Steel gilt blast and special paint, Amplirell, Heil and Dino pickup

ROOF: 3/16" PL roof panels with tubing and channel support frame

LIDS: (2) 68" x 90" metal rolling lids spring

loaded, self raising ROLLERS: 4" V-groove rollers with definit bearings and grease fittings OPENING: (2) 60" x 82" openings

with 8" divider centered on container

LATCH:(2) independent ratchet binders with chains perlid GASKETS: Extruded rubber seal with metal relainers

Heavy Duty Split Metal Rolling Lid



CONT.	A	B
20 YD	41	53
25 YD	53	65
30 YD	65	77

31

ConocoPhillips

Location Schematic and Rig Layout for Closed Loop System Reviewed by: Steven Herrin Drilling Engineer, ConocoPhillips Company Date: updated January 2014

(PICTURE NOT TO SCALE)

NOTE: There are two muster areas depending on the prevailing wind direction, generally south in this area. The muster area that is furthest upwind/ crosswind will be the designated area for briefing and assessing the situation. In the event a full evacuation is deemed necessary, all personnel will exit the location via the access road. If the main access road is blocked off, they will exit via a secondary road (if available) or walk off route in the upwind/crosswind direction.

