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HOBBS OCD

OCD Hobbs

NOV 10 2014

Form 3160-3
(March 2012)

RECEIVED

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

APPLICATION FOR PERMIT TO DRILL OR REENTER

NORTH DOK
LOCATION

FORM APPROVED
OMB No. 1004-0137
Expires October 31, 2014

5. Lease Serial No.
NMNM100567

6. If Indian, Allottee or Tribe Name

7. If Unit or CA Agreement, Name and No.

8. Lease Name and Well No.
RAGIN CAJUN 12 FED 2H

9. API Well No.

10. Field and Plot, or Exploratory
BRUSHY CANYON, DELAWARE

11. Sec., T. R. M. or Blk. and Survey or Area
Sec 12, T26S, R34E

12. County or Parish
LEA

13. State
NM

1a. Type of work: ☒ DRILL ☐ REENTER

1b. Type of Well: ☒ Oil Well ☐ Gas Well ☐ Other ☒ Single Zone ☐ Multiple Zone

2. Name of Operator Devon Energy Production Company, L.P.

3a. Address 333 W. Sheridan
Oklahoma City, OK 73102

3b. Phone No. (include area code)
405.552.7848

4. Location of Well (Report location clearly and in accordance with any State requirements.)*

At surface 10 FSL & 1135 FWL, Unit M

PP: 10 FSL & 1345 FWL

At proposed prod. zone 330 FNL & 1980 FWL, Unit C

14. Distance in miles and direction from nearest town or post office*
Approximately 17 miles SW Jal, NM

15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any)
See attached map

16. No. of acres in lease
640 acres

17. Spacing Unit dedicated to this well
160 acres

18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft.
See attached map

19. Proposed Depth
TVD: 9,050'; MD: 13,904'

20. BLM/BIA Bond No. on file
CO-1104; NBM-000801

21. Elevations (Show whether DF, KDB, RT, GL, etc.)
3,277.6' GL

22. Approximate date work will start*
10/15/2014

23. Estimated duration
45 Days

24. Attachments To be pad drilled w/ Ragin Cajun 12 Fed 3H

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No. 1, must be attached to this form:

1. Well plat certified by a registered surveyor.

2. A Drilling Plan.

3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office).

4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).

5. Operator certification

6. Such other site specific information and/or plans as may be required by the BLM.

25. Signature

Name (Printed/Typed)
David H. Cook

Date
05/07/2014

Title

Regulatory Compliance Professional

Approved by (Signature)

Steve Caffey

Name (Printed/Typed)

NOV - 5 2014

Title

FIELD MANAGER

Office

CARLSBAD FIELD OFFICE

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.
Conditions of approval, if any, are attached.

APPROVAL FOR TWO YEARS

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

*(Instructions on page 2)

Carlsbad Controlled Water Basin

Ka
11/06/14

PM

SEE ATTACHED FOR
CONDITIONS OF APPROVAL

Approval Subject to General Requirements
& Special Stipulations Attached

NOV 12 2014
13

DRILLING PROGRAM

Devon Energy Production Company, L.P.
Ragin Cajun 12 Fed 2H

1. Geologic Name of Surface Formation: Quaternary

2. Estimated Tops of Geological Markers & Depths of Anticipated FW, Oil, or Gas:

a. Fresh Water	180'	
b. Rustler	1070'	Barren
c. Top of Salt	1450'	Barren
d. Base of Salt	5061'	Barren
e. Delaware	5390'	Oil / Gas
f. Bell Canyon	5429'	Oil
g. Cherry Canyon	6415'	Oil
h. Brushy Canyon	7755'	Oil
Total Depth	9050' TVD	13904' MD

3. Pressure Control Equipment:

A 3M 13-5/8" BOP system (Double Ram and Annular preventer) will be installed and tested prior to drilling out the surface casing shoe. The BOP system used to drill the intermediate hole will be tested per BLM Onshore Oil and Gas Order 2.

A 3M 13-5/8" BOP system (Double Ram and Annular preventer) will be installed and tested prior to drilling out the intermediate casing shoe. The BOP system used to drill the production hole will be tested per BLM Onshore Oil and Gas Order 2.

The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.

See
COA

Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line). The line will be kept as straight as possible with minimal turns and will be secured with anchors and/or safety clamps as per the manufacturer's requirements. (See attached spec sheets).

Auxiliary Well Control and Monitoring Equipment:

- a. A Kelly cock will be in the drill string at all times.
- b. A full opening drill pipe stabbing valve having the appropriate connections will be on the rig floor at all times.

4. **Casing Program:**

Hole Size	Hole Interval	Casing OD	Casing Interval	Weight (lb/ft)	Collar	Grade	Collapse Design Factor	Burst Design Factor	Tension Design Factor
17-1/2"	0 – 1,100'	13-3/8"	0 - 1,100'	48	STC	H-40	1.57	3.52	10.25
12-1/4"	1,100-5,250'	9-5/8"	0 - 5,250'	40	BTC	HCK-55	1.55	1.45	4.41
8-3/4"	5,250-13,904'	5-1/2"	0 - 13,904'	17	BTC	P-110	1.72	2.45	3.68

Casing Notes:

- All casing is new and API approved

Maximum Lateral TVD: 9,070'

5. **Proposed mud Circulations System:**

Depth	Mud Weight	Viscosity	Fluid Loss	Type System
0-1,100'	8.4-8.6	30-34	N/C	FW
1,100-5,250'	10.0	28-32	N/C	Brine
5,250-13,904'	8.6-9.2	28-32	N/C	FW

The necessary mud products for weight addition and fluid loss control will be on location at all times. Visual mud monitoring equipment will be in place to detect volume changes indicating loss or gain of circulating fluid volume. If abnormal pressures are encountered, electronic/mechanical mud monitoring equipment will be installed.

6. Cementing Table:

String	Number of sx	Weight lbs/gal	Water Volume g/sx	Yield cf/sx	Stage; Lead/Tail	Slurry Description
13-3/8" Surface Casing	490	13.5	9.08	1.72	Lead	Class C Cement + 0.125 lbs/sack Poly-E-Flake + 4% bwoc Bentonite + 70.1% Fresh Water
	550	14.8	6.34	1.33	Tail	Class C Cement + 63.5% Fresh Water
9-5/8" Intermediate Casing	1230	12.9	9.82	1.85	Lead	(65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 lbs/sack Poly-E-Flake + 70.9 % Fresh Water
	430	14.8	6.32	1.33	Tail	Class C Cement + 0.125 lbs/sack Poly-E-Flake + 63.5% Fresh Water
5-1/2" Production Casing Tuned Light Cement Option	450	11	14.94	2.66	Lead	Tuned Light® Cement + 0.125 lb/sk Pol-E-Flake + 76.5% Fresh Water
	1400	14.5	5.31	1.20	Tail	(50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.25% bwoc CFR-3 + 0.1% bwoc HR-601 + 2% bwoc Bentonite + 58.8% Fresh Water

TOC for all Strings:

13-3/8" Surface Csg @ 0'
 9-5/8" Intermediate Csg @ 0'
 5-1/2" Production Csg @ 4,750'

Notes:

- Cement volumes Surface 100%, Intermediate 50%, Production based on at least 25% excess
- Actual cement volumes will be adjusted based on fluid caliper and caliper log data

7. Logging, Coring, and Testing Program:

- a. Drill stem tests will be based on geological sample shows.
- b. If a drill stem test is anticipated, a procedure, equipment to be used, and safety measures will be provided via sundry notice to the BLM.
- c. Resistivity and porosity logs are planned below the intermediate casing point. Stated logs run will be named in the Completion Report and submitted to the BLM.
- d. No coring program is planned
- e. Additional Testing will be initiated subsequent to setting the production casing. Specific intervals will be targeted based on log evaluation (if applicable), geological sample shows, and drill stem tests.

8. Potential Hazards:

- a. No abnormal pressures or temperatures are expected. There is no known presence of H₂S in this area, and none is anticipated to be encountered. If H₂S is encountered the operator will comply with the provisions of Onshore Oil and Gas Order No. 6. No lost circulation is expected to occur. All personnel will be familiar with all aspects of safe operation being used to drill this well. Estimated BHP: 4073 psi, and estimated BHT: 149 degrees.
- b. Hydrogen Sulfide detection equipment will be in operation after drilling out the 13-3/8" casing shoe until the 5-1/2" casing is cemented. Breathing equipment will be on location upon drilling the 13-3/8" shoe until total depth is reached.

9. Anticipated Starting Date and Duration of Operations:

- a. Road and location construction will begin after the BLM has approved the APD. Anticipated spud date will be as soon after BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 20 days. If production casing is run then an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.

devon

Ragin Cajun 12 Fed 2H
Lea Co, NM



Weatherford

Plan Data for Ragin Cajun 12 Fed 2H

Plan Point Information:									
Dogleg Severity Unit: °/100.00ft				Position offsets from Slot centre					
MD	Inc	Az	TVD	+N/-S	+E/-W	Northing	Easting	VSec	DLS
(USft)	(°)	(°)	(USft)	(USft)	(USft)	(USft)	(USft)	(USft)	(DLSU)
0.00	0.00	0.00	0.00	0.00	0.00	383348.85	821674.21	0.00	0.00
5400.00	0.00	0.00	5400.00	0.00	0.00	383348.85	821674.21	0.00	0.00
5900.07	10.00	87.89	5897.53	1.61	43.50	383350.46	821717.71	1.61	2.00
7986.18	10.00	87.89	7951.95	14.98	405.56	383363.83	822079.77	14.98	0.00
8486.25	0.00	0.00	8449.48	16.58	449.06	383365.43	822123.27	16.58	2.00
8585.91	0.00	0.00	8549.14	16.58	449.06	383365.43	822123.27	16.58	0.00
9406.40	90.25	31.65	9070.00	461.95	723.59	383810.80	822397.80	461.95	11.00
9694.15	90.25	0.00	9068.69	735.28	801.06	384084.13	822475.27	735.28	11.00
13904.15	90.25	0.00	9050.00	4945.24	801.06	388294.09	822475.27	4945.24	0.00



KB-3303
GL-3278

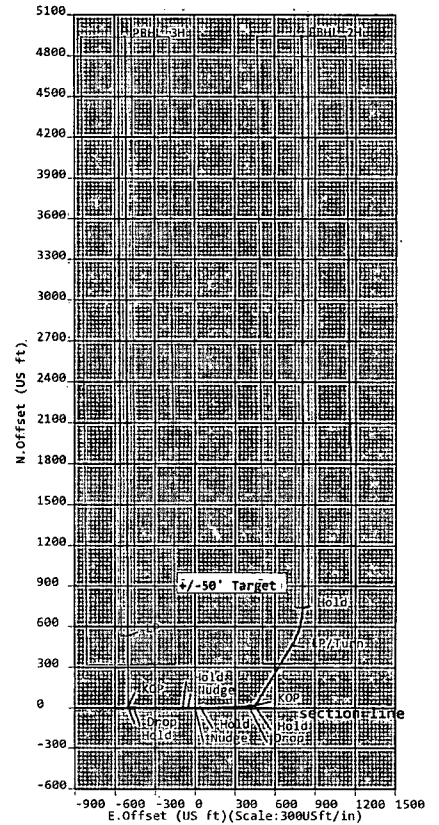
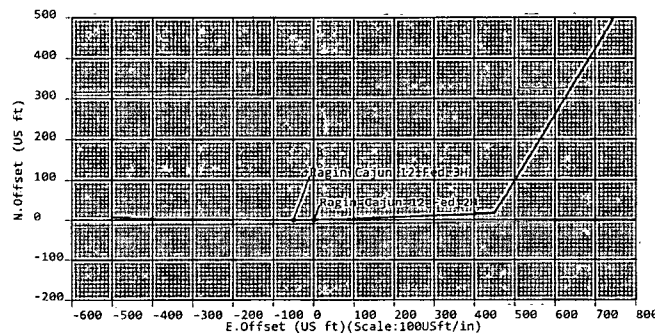
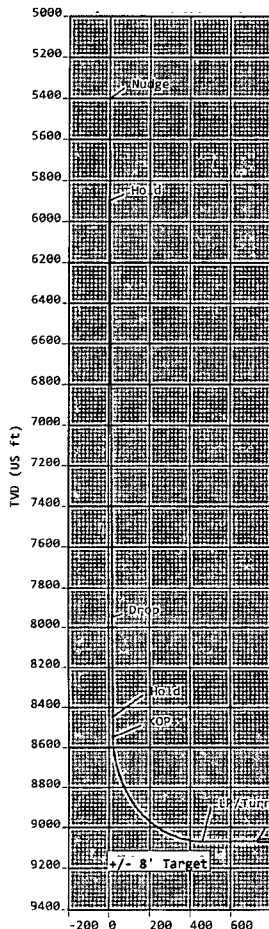
Plan Data for Ragin Cajun 12 Fed 2H

Slot: Ragin Cajun 12 Fed 2H
Position:
Offset is from Site centre
+N/-S: 0.00USft Northing: 383348.85USft Latitude: 32°3'2.4"
+E/-W: 0.00USft Easting: 821674.21USft Longitude: -103°25'42.6"
Elevation Above VRD: 3278.00USft

Plan Data for Ragin Cajun 12 Fed 2H

Target Set Information:
Name: Ragin Cajun 12 Fed 2
Position offsets from Slot centre
Name TVD +N/-S +E/-W Northing Easting Shape Comment
(USft) (USft) (USft) (USft) (USft)
PBHL 2H 9050.00 4945.24 801.06 388294.09 822475.27 Cuboid

Ragin Cajun 12 Fed 2H
Ragin Cajun 12 Fed 3H



PBHL 2H

VS (US ft)(Bearing:0.00° Scale:200USft/in)

Sign Off: Russell Joyner

SD Plan Report**Devon Energy**

Field Name: *Lea Co, NM Nad 83 NMEZ*
Site Name: *Ragin Cajun 12 Fed 2, 3H Pad*
Well Name: *Ragin Cajun 12 Fed 2*
Plan: *P1:V1*

30 April 2014



Ragin Cajun 12 Fed 2

Field Name Lea Co, NM Nad 83 NMEZ	Map Units : US ft Vertical Reference Datum (VRD) : Mean Sea Level Projected Coordinate System : NAD83 / New Mexico East (ftUS) Comment :	Company Name : Devon Energy
Site Name Ragin Cajun 12 Fed 2, 3H Pad	Units : US ft North Reference : Grid Convergence Angle : 0.48 Position Northing : 383348.85 US ft Latitude : 32° 3' 2.44" Easting : 821674.21 US ft Longitude : -103° 25' 42.62" Elevation above Mean Sea Level: 3278.00 US ft Comment :	
Slot Name Ragin Cajun 12 Fed 2H	Position (Offsets relative to Site Centre) +N / -S : 0.00 US ft Northing : 383348.85 US ft Latitude : 32° 3' 2.44" +E / -W : 0.00 US ft Easting : 821674.21 US ft Longitude : -103° 25' 42.62" Slot TVD Reference : Ground Elevation Elevation above Mean Sea Level : 3278.00 US ft Comment :	
Well Name Ragin Cajun 12 Fed 2	Type : Main well Rig Height / Drill Floor : 25.00 US ft Relative to Mean Sea Level: 3303.00 US ft Closure Distance : 5009.7 US ft Closure Azimuth : 9.2012° Vertical Section (Position of Origin Relative to Slot) +N / -S : 0.00 US ft +E / -W : 0.00 US ft Az : 0.00° Magnetic Parameters Model : BGGM Field Strength : 48220.4nT Dec : 7.24° Dip : 59.96° Date : 15/Jul/2014 UWI : Plan : P1:V1 Comment :	

Target Set

Name : Ragin Cajun 12 Fed 2 **Number of Targets :** 1

Comment :

Target Name PBHL 2H	Position (Relative to Slot centre) +N / -S : 4945.24 US ft Northing : 388294.09 US ft Latitude : 32° 3' 51.30" +E / -W : 801.06 US ft Easting : 822475.27 US ft Longitude : -103° 25' 32.83" Shape : TVD: (Drill Floor) : 9050.00 US ft Cuboid Orientation : Azimuth : 0.00° Inclination : 0.25° Dimensions Length : 8420.00 US ft Breadth : 100.00 US ft Height : 16.00 US ft
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Well path created using minimum curvature

Salient Points (Relative to Slot centre, TVD relative to Drill Floor)											
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	DLS (°/100 US ft)	VS (US ft)	B. Rate (°/100 US ft)	T. Rate (°/100 US ft)	T. Face (°)	Comment
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

5D Plan Report

Salient Points (Relative to Slot centre, TVD relative to Drill Floor)											Comment
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	DLS (°/100 US ft)	VS (US ft)	B. Rate (°/100 US ft)	T. Rate (°/100 US ft)	T. Face (°)	
5400.00	0.00	0.00	5400.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Nudge
5900.07	10.00	87.89	5897.53	1.61	43.50	2.00	1.61	2.00	0.00	87.89	Hold
7986.18	10.00	87.89	7951.95	14.98	405.56	0.00	14.98	0.00	0.00	0.00	Drop
8486.25	0.00	0.00	8449.48	16.58	449.06	2.00	16.58	-2.00	0.00	180.00	Hold
8585.91	0.00	0.00	8549.14	16.58	449.06	0.00	16.58	0.00	0.00	0.00	KOP
9406.40	90.25	31.65	9070.00	461.95	723.59	11.00	461.95	11.00	0.00	31.65	LP/Turn
9694.15	90.25	0.00	9068.69	735.28	801.06	11.00	735.28	0.00	-11.00	270.07	Hold
13904.15	90.25	0.00	9050.00	4945.24	801.06	0.00	4945.24	0.00	0.00	0.00	PBHL 2H

Interpolated Points (Relative to Slot centre, TVD relative to Drill Floor)											Comment
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	VS (US ft)	DLS (°/100 US ft)	Northing (US ft)	Easting (US ft)		
5400.00	0.00	0.00	5400.00	0.00	0.00	0.00	0.00	383348.85	821674.21		Nudge
5500.00	2.00	87.89	5499.98	0.06	1.74	0.06	2.00	383348.91	821675.95		
5600.00	4.00	87.89	5599.84	0.26	6.97	0.26	2.00	383349.11	821681.18		
5700.00	6.00	87.89	5699.45	0.58	15.68	0.58	2.00	383349.43	821689.89		
5800.00	8.00	87.89	5798.70	1.03	27.86	1.03	2.00	383349.88	821702.07		
5900.00	10.00	87.89	5897.47	1.61	43.49	1.61	2.00	383350.46	821717.70		
5900.07	10.00	87.89	5897.53	1.61	43.50	1.61	0.00	383350.46	821717.71		Hold
6000.00	10.00	87.89	5995.95	2.25	60.85	2.25	0.00	383351.10	821735.06		
6100.00	10.00	87.89	6094.43	2.89	78.20	2.89	0.00	383351.74	821752.41		
6200.00	10.00	87.89	6192.91	3.53	95.56	3.53	0.00	383352.38	821769.77		
6300.00	10.00	87.89	6291.39	4.17	112.91	4.17	0.00	383353.02	821787.12		
6400.00	10.00	87.89	6389.87	4.81	130.27	4.81	0.00	383353.66	821804.48		
6500.00	10.00	87.89	6488.35	5.45	147.62	5.45	0.00	383354.30	821821.83		
6600.00	10.00	87.89	6586.83	6.09	164.98	6.09	0.00	383354.94	821839.19		
6700.00	10.00	87.89	6685.31	6.73	182.34	6.73	0.00	383355.58	821856.55		
6800.00	10.00	87.89	6783.79	7.37	199.69	7.37	0.00	383356.22	821873.90		
6900.00	10.00	87.89	6882.27	8.02	217.05	8.02	0.00	383356.87	821891.26		
7000.00	10.00	87.89	6980.75	8.66	234.40	8.66	0.00	383357.51	821908.61		
7100.00	10.00	87.89	7079.23	9.30	251.76	9.30	0.00	383358.15	821925.97		
7200.00	10.00	87.89	7177.71	9.94	269.11	9.94	0.00	383358.79	821943.32		
7300.00	10.00	87.89	7276.19	10.58	286.47	10.58	0.00	383359.43	821960.68		
7400.00	10.00	87.89	7374.67	11.22	303.82	11.22	0.00	383360.07	821978.03		
7500.00	10.00	87.89	7473.15	11.86	321.18	11.86	0.00	383360.71	821995.39		
7600.00	10.00	87.89	7571.63	12.50	338.53	12.50	0.00	383361.35	822012.74		
7700.00	10.00	87.89	7670.11	13.14	355.89	13.14	0.00	383361.99	822030.10		
7800.00	10.00	87.89	7768.59	13.78	373.24	13.78	0.00	383362.63	822047.45		
7900.00	10.00	87.89	7867.07	14.42	390.60	14.42	0.00	383363.27	822064.81		
7986.18	10.00	87.89	7951.95	14.98	405.56	14.98	0.00	383363.83	822079.77		Drop
8000.00	9.73	87.89	7965.56	15.06	407.92	15.06	2.00	383363.91	822082.13		
8100.00	7.73	87.89	8064.40	15.62	423.08	15.62	2.00	383364.47	822097.29		
8200.00	5.73	87.89	8163.70	16.06	434.78	16.06	2.00	383364.91	822108.99		
8300.00	3.73	87.89	8263.36	16.36	443.01	16.36	2.00	383365.21	822117.22		
8400.00	1.73	87.89	8363.24	16.53	447.76	16.53	2.00	383365.38	822121.97		
8486.25	0.00	0.00	8449.48	16.58	449.06	16.58	2.00	383365.43	822123.27		Hold
8500.00	0.00	0.00	8463.23	16.58	449.06	16.58	0.00	383365.43	822123.27		
8585.91	0.00	0.00	8549.14	16.58	449.06	16.58	0.00	383365.43	822123.27		KOP
8600.00	1.55	31.65	8563.23	16.75	449.16	16.75	11.00	383365.60	822123.37		
8700.00	12.55	31.65	8662.32	27.18	455.59	27.18	11.00	383376.03	822129.80		
8800.00	23.55	31.65	8757.25	53.51	471.82	53.51	11.00	383402.36	822146.03		
8900.00	34.55	31.65	8844.54	94.78	497.26	94.78	11.00	383443.63	822171.47		
9000.00	45.55	31.65	8920.97	149.48	530.98	149.48	11.00	383498.33	822205.19		
9100.00	56.55	31.65	8983.73	215.58	571.72	215.58	11.00	383564.43	822245.93		
9200.00	67.55	31.65	9030.53	290.66	618.00	290.66	11.00	383639.51	822292.21		
9300.00	78.55	31.65	9059.64	371.96	668.12	371.96	11.00	383720.81	822342.33		
9400.00	89.55	31.65	9069.99	456.50	720.23	456.50	11.00	383805.35	822394.44		
9406.40	90.25	31.65	9070.00	461.95	723.59	461.95	11.00	383810.80	822397.80		LP/Turn
9500.00	90.26	21.35	9069.58	545.60	765.30	545.60	11.00	383894.45	822439.51		

SD Plan Report

Interpolated Points (Relative to Slot centre, TVD relative to Drill Floor)										
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N.Offset (US ft)	E.Offset (US ft)	VS (US ft)	DLS (%/100 US ft)	Northing (US ft)	Easting (US ft)	Comment
9600.00	90.26	10.36	9069.12	641.65	792.58	641.65	11.00	383990.50	822466.79	
9694.15	90.25	0.00	9068.69	735.28	801.06	735.28	11.00	384084.13	822475.27	Hold
9700.00	90.25	0.00	9068.67	741.13	801.06	741.13	0.00	384089.98	822475.27	
9800.00	90.25	0.00	9068.22	841.13	801.06	841.13	0.00	384189.98	822475.27	
9900.00	90.25	0.00	9067.78	941.13	801.06	941.13	0.00	384289.98	822475.27	
10000.00	90.25	0.00	9067.33	1041.13	801.06	1041.13	0.00	384389.98	822475.27	
10100.00	90.25	0.00	9066.89	1141.13	801.06	1141.13	0.00	384489.98	822475.27	
10200.00	90.25	0.00	9066.45	1241.13	801.06	1241.13	0.00	384589.98	822475.27	
10300.00	90.25	0.00	9066.00	1341.13	801.06	1341.13	0.00	384689.98	822475.27	
10400.00	90.25	0.00	9065.56	1441.13	801.06	1441.13	0.00	384789.98	822475.27	
10500.00	90.25	0.00	9065.11	1541.13	801.06	1541.13	0.00	384889.98	822475.27	
10600.00	90.25	0.00	9064.67	1641.13	801.06	1641.13	0.00	384989.98	822475.27	
10700.00	90.25	0.00	9064.23	1741.12	801.06	1741.12	0.00	385089.97	822475.27	
10800.00	90.25	0.00	9063.78	1841.12	801.06	1841.12	0.00	385189.97	822475.27	
10900.00	90.25	0.00	9063.34	1941.12	801.06	1941.12	0.00	385289.97	822475.27	
11000.00	90.25	0.00	9062.89	2041.12	801.06	2041.12	0.00	385389.97	822475.27	
11100.00	90.25	0.00	9062.45	2141.12	801.06	2141.12	0.00	385489.97	822475.27	
11200.00	90.25	0.00	9062.01	2241.12	801.06	2241.12	0.00	385589.97	822475.27	
11300.00	90.25	0.00	9061.56	2341.12	801.06	2341.12	0.00	385689.97	822475.27	
11400.00	90.25	0.00	9061.12	2441.12	801.06	2441.12	0.00	385789.97	822475.27	
11500.00	90.25	0.00	9060.67	2541.12	801.06	2541.12	0.00	385889.97	822475.27	
11600.00	90.25	0.00	9060.23	2641.12	801.06	2641.12	0.00	385989.97	822475.27	
11700.00	90.25	0.00	9059.79	2741.11	801.06	2741.11	0.00	386089.96	822475.27	
11800.00	90.25	0.00	9059.34	2841.11	801.06	2841.11	0.00	386189.96	822475.27	
11900.00	90.25	0.00	9058.90	2941.11	801.06	2941.11	0.00	386289.96	822475.27	
12000.00	90.25	0.00	9058.45	3041.11	801.06	3041.11	0.00	386389.96	822475.27	
12100.00	90.25	0.00	9058.01	3141.11	801.06	3141.11	0.00	386489.96	822475.27	
12200.00	90.25	0.00	9057.57	3241.11	801.06	3241.11	0.00	386589.96	822475.27	
12300.00	90.25	0.00	9057.12	3341.11	801.06	3341.11	0.00	386689.96	822475.27	
12400.00	90.25	0.00	9056.68	3441.11	801.06	3441.11	0.00	386789.96	822475.27	
12500.00	90.25	0.00	9056.23	3541.11	801.06	3541.11	0.00	386889.96	822475.27	
12600.00	90.25	0.00	9055.79	3641.11	801.06	3641.11	0.00	386989.96	822475.27	
12700.00	90.25	0.00	9055.35	3741.10	801.06	3741.10	0.00	387089.95	822475.27	
12800.00	90.25	0.00	9054.90	3841.10	801.06	3841.10	0.00	387189.95	822475.27	
12900.00	90.25	0.00	9054.46	3941.10	801.06	3941.10	0.00	387289.95	822475.27	
13000.00	90.25	0.00	9054.01	4041.10	801.06	4041.10	0.00	387389.95	822475.27	
13100.00	90.25	0.00	9053.57	4141.10	801.06	4141.10	0.00	387489.95	822475.27	
13200.00	90.25	0.00	9053.13	4241.10	801.06	4241.10	0.00	387589.95	822475.27	
13300.00	90.25	0.00	9052.68	4341.10	801.06	4341.10	0.00	387689.95	822475.27	
13400.00	90.25	0.00	9052.24	4441.10	801.06	4441.10	0.00	387789.95	822475.27	
13500.00	90.25	0.00	9051.79	4541.10	801.06	4541.10	0.00	387889.95	822475.27	
13600.00	90.25	0.00	9051.35	4641.10	801.06	4641.10	0.00	387989.95	822475.27	
13700.00	90.25	0.00	9050.91	4741.10	801.06	4741.10	0.00	388089.95	822475.27	
13800.00	90.25	0.00	9050.46	4841.09	801.06	4841.09	0.00	388189.94	822475.27	
13900.00	90.25	0.00	9050.02	4941.09	801.06	4941.09	0.00	388289.94	822475.27	
13904.15	90.25	0.00	9050.00	4945.24	801.06	4945.24	0.00	388294.09	822475.27	PBHL 2H

SD Anti-Collision Report**Devon Energy****Field Name:** *Lea Co, NM Nad 83 NMEZ***Site Name:** *Ragin Cajun 12 Fed 2, 3H Pad***Well Name:** *Ragin Cajun 12 Fed 2*

30 April 2014




Weatherford

Ragin Cajun 12 Fed 2

Field Name Lea Co, NM Nad 83 NMEZ	Map Units : US ft		Company Name : Devon Energy	
	Vertical Reference Datum (VRD) : Mean Sea Level			
	Projected Coordinate System : NAD83 / New Mexico East (ftUS)			
	Comment :			
Site Name Ragin Cajun 12 Fed 2, 3H Pad	Units : US ft	North Reference : Grid	Convergence Angle : 0:48	
	Position	Northing : 383348.85 US ft	Latitude : 32° 3' 2.44"	
		Easting : 821674.21 US ft	Longitude : -103° 25' 42.62"	
	Elevation above Mean Sea Level: 3278.00 US ft		Comment :	
Slot Name Ragin Cajun 12 Fed 2H	Position (Offsets relative to Site Centre)			
	+N / -S : 0.00 US ft	Northing : 383348.85 US ft	Latitude : 32° 3' 2.44"	
	+E / -W : 0.00 US ft	Easting : 821674.21 US ft	Longitude : -103° 25' 42.62"	
	Slot TVD Reference : Ground Elevation			
Elevation above Mean Sea Level: 3278.00 US ft		Comment :		
Well Name Ragin Cajun 12 Fed 2	Type : Main well		UWI :	Plan : Working Plan
	Rig Height Drill Floor : 25.00 US ft		Comment :	
	Relative to Mean Sea Level: 3303.00 US ft			
	Closure Distance : 5009.7 US ft		Closure Azimuth : 9.2012°	
	Vertical Section (Position of Origin Relative to Slot)			
	+N / -S : 0.00 US ft		+E / -W : 0.00 US ft	Az : 0:00°
	Magnetic Parameters			
	Model : BGGM	Field Strength : 48220.4nT	Dec : 7.24°	Dip : 59:96° Date : 15/Jul/2014

Collision / Uncertainty Analysis				
Primary Well	Start MD (US ft)	End MD (US ft)	Collision Risk Interval	No. of Std Deviations in Error Computation
Ragin Cajun 12 Fed 2 (p)	0.00	13904.15	100.00	2

Secondary Well Names
Ragin Cajun 12 Fed 3H (p)

Anti-Collision Report Terminology
S.Minor, S.Major : Radii of the ellipse of uncertainty at the current location as seen in the along hole direction.
PHI : Angle between high-side vector and semi-minor axis
TVD Spread : Total TVD range of the ellipsoid of uncertainty at the current location
ES : Distance between the extremities of the primary and secondary uncertainty ellipsoids in the direction Cr-Cr
T.Face to Sec : Angle between the Hi-Side vector of the primary well at the current location and line of closest approach between the two wells

Separation factors calculated using Pedal Curve (Independent Uncertainty). Well path created using minimum curvature.

5D Anti-Collision Report

Anti Collision Proximity Summary (TVD relative to)

Secondary Well Name	Pri MD (US ft)	Sec MD (US ft)	TVD (US ft)	CC (US ft)	ES (US ft)	SF	Risk
Ragin Cajun 12 Fed 3H (p)	5400.00	5400.00	5400.00	50.00	25.24	2.02	

Secondary Well : Ragin Cajun 12 Fed 3H (p) (TVD Relative to Drill Floor (Primary) ; All Azimuth Relative to GRID NORTH)								
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF
0:00	0:00	0:00	269:52	0:00	0:00	50:00	49:29	70:18
100:00	100:00	100:00	269:52	0:12	0:12	50:00	49:06	53:01
200:00	200:00	200:00	269:52	0:34	0:34	50:00	48:61	35:96
300:00	300:00	300:00	269:52	0:57	0:57	50:00	48:16	27:18
400:00	400:00	400:00	269:52	0:79	0:79	50:00	47:71	21:84
500:00	500:00	500:00	269:52	1:02	1:02	50:00	47:26	18:26
600:00	600:00	600:00	269:52	1:24	1:24	50:00	46:81	15:69
700:00	700:00	700:00	269:52	1:46	1:46	50:00	46:36	13:75
800:00	800:00	800:00	269:52	1:69	1:69	50:00	45:91	12:24
900:00	900:00	900:00	269:52	1:91	1:91	50:00	45:47	11:02
1000:00	1000:00	1000:00	269:52	2:14	2:14	50:00	45:02	10:03
1100:00	1100:00	1100:00	269:52	2:36	2:36	50:00	44:57	9:20
1200:00	1200:00	1200:00	269:52	2:59	2:59	50:00	44:12	8:50
1300:00	1300:00	1300:00	269:52	2:81	2:81	50:00	43:67	7:89
1400:00	1400:00	1400:00	269:52	3:04	3:04	50:00	43:22	7:37
1500:00	1500:00	1500:00	269:52	3:26	3:26	50:00	42:77	6:91
1600:00	1600:00	1600:00	269:52	3:49	3:49	50:00	42:32	6:51
1700:00	1700:00	1700:00	269:52	3:71	3:71	50:00	41:87	6:15
1800:00	1800:00	1800:00	269:52	3:94	3:94	50:00	41:42	5:83
1900:00	1900:00	1900:00	269:52	4:16	4:16	50:00	40:97	5:54
2000:00	2000:00	2000:00	269:52	4:39	4:39	50:00	40:52	5:27
2100:00	2100:00	2100:00	269:52	4:61	4:61	50:00	40:07	5:04
2200:00	2200:00	2200:00	269:52	4:84	4:84	50:00	39:62	4:82
2300:00	2300:00	2300:00	269:52	5:06	5:06	50:00	39:17	4:62
2400:00	2400:00	2400:00	269:52	5:29	5:29	50:00	38:72	4:43
2500:00	2500:00	2500:00	269:52	5:51	5:51	50:00	38:27	4:26
2600:00	2600:00	2600:00	269:52	5:73	5:73	50:00	37:82	4:11
2700:00	2700:00	2700:00	269:52	5:96	5:96	50:00	37:37	3:96
2800:00	2800:00	2800:00	269:52	6:18	6:18	50:00	36:93	3:82
2900:00	2900:00	2900:00	269:52	6:41	6:41	50:00	36:48	3:70
3000:00	3000:00	3000:00	269:52	6:63	6:63	50:00	36:03	3:58
3100:00	3100:00	3100:00	269:52	6:86	6:86	50:00	35:58	3:47
3200:00	3200:00	3200:00	269:52	7:08	7:08	50:00	35:13	3:36
3300:00	3300:00	3300:00	269:52	7:31	7:31	50:00	34:68	3:26
3400:00	3400:00	3400:00	269:52	7:53	7:53	50:00	34:23	3:17
3500:00	3500:00	3500:00	269:52	7:76	7:76	50:00	33:78	3:08
3600:00	3600:00	3600:00	269:52	7:98	7:98	50:00	33:33	3:00
3700:00	3700:00	3700:00	269:52	8:21	8:21	50:00	32:88	2:92
3800:00	3800:00	3800:00	269:52	8:43	8:43	50:00	32:43	2:85
3900:00	3900:00	3900:00	269:52	8:66	8:66	50:00	31:98	2:77
4000:00	4000:00	4000:00	269:52	8:88	8:88	50:00	31:53	2:71
4100:00	4100:00	4100:00	269:52	9:11	9:11	50:00	31:08	2:64
4200:00	4200:00	4200:00	269:52	9:33	9:33	50:00	30:63	2:58
4300:00	4300:00	4300:00	269:52	9:56	9:56	50:00	30:18	2:52
4400:00	4400:00	4400:00	269:52	9:78	9:78	50:00	29:73	2:47
4500:00	4500:00	4500:00	269:52	10:01	10:01	50:00	29:28	2:41
4600:00	4600:00	4600:00	269:52	10:23	10:23	50:00	28:83	2:36
4700:00	4700:00	4700:00	269:52	10:45	10:45	50:00	28:38	2:31
4800:00	4800:00	4800:00	269:52	10:68	10:68	50:00	27:94	2:27
4900:00	4900:00	4900:00	269:52	10:90	10:90	50:00	27:49	2:22
5000:00	5000:00	5000:00	269:52	11:13	11:13	50:00	27:04	2:18
5100:00	5100:00	5100:00	269:52	11:35	11:35	50:00	26:59	2:14

5D Anti-Collision Report

Secondary Well : Ragin Cajun 12 Fed 3H (p) (TVD Relative to Drill Floor (Primary) ; All Azimuth Relative to GRID NORTH)									
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
5200.00	5200.00	5200.00	269.52	11.58	11.58	50.00	26.14	2.10	
5300.00	5300.00	5300.00	269.52	11.80	11.80	50.00	25.69	2.06	
5400.00	5400.00	5400.00	269.52	12.03	12.03	50.00	25.24	2.02	
5500.00	5498.15	5498.17	181.62	12.22	12.22	53.46	28.39	2.13	
5600.00	5595.49	5595.64	181.60	12.42	12.38	63.80	38.38	2.51	
5700.00	5691.23	5691.73	181.57	12.61	12.54	80.95	55.19	3.14	
5800.00	5784.64	5785.81	181.55	12.81	12.67	104.75	78.69	4.02	
5900.00	5875.08	5877.28	181.54	13.01	12.81	135.03	108.68	5.12	
6000.00	5966.58	5970.18	181.53	13.22	12.99	169.13	142.41	6.33	
6100.00	6059.13	6064.16	181.52	13.44	13.18	203.33	176.21	7.50	
6200.00	6151.67	6158.13	181.51	13.66	13.37	237.52	210.02	8.64	
6300.00	6244.22	6252.10	181.51	13.90	13.56	271.72	243.82	9.74	
6400.00	6336.76	6346.07	181.50	14.13	13.75	305.91	277.62	10.81	
6500.00	6429.30	6440.04	181.50	14.38	13.95	340.11	311.41	11.85	
6600.00	6521.85	6534.02	181.50	14.62	14.14	374.30	345.21	12.87	
6700.00	6614.39	6627.99	181.49	14.88	14.34	408.49	379.00	13.85	
6800.00	6706.94	6721.96	181.49	15.13	14.54	442.69	412.79	14.80	
6900.00	6799.48	6815.93	181.49	15.40	14.74	476.88	446.57	15.73	
7000.00	6892.03	6909.90	181.49	15.66	14.94	511.08	480.36	16.64	
7100.00	6984.57	7003.88	181.49	15.93	15.14	545.27	514.14	17.51	
7200.00	7077.11	7097.85	181.49	16.21	15.34	579.47	547.92	18.37	
7300.00	7169.66	7191.82	181.49	16.48	15.54	613.66	581.69	19.20	
7400.00	7262.20	7285.79	181.49	16.76	15.75	647.86	615.47	20.00	
7500.00	7354.75	7379.76	181.48	17.05	15.96	682.05	649.24	20.79	
7600.00	7447.29	7473.74	181.48	17.34	16.16	716.25	683.01	21.55	
7700.00	7539.83	7567.71	181.48	17.63	16.37	750.44	716.78	22.29	
7800.00	7632.38	7661.68	181.48	17.92	16.58	784.63	750.54	23.01	
7900.00	7724.92	7755.65	181.48	18.22	16.79	818.83	784.30	23.72	
8000.00	7817.48	7849.64	181.48	18.51	17.01	852.99	818.04	24.40	
8100.00	7910.74	7944.34	181.47	18.82	17.22	885.08	849.71	25.02	
8200.00	8026.03	8061.27	181.46	19.17	17.53	913.33	877.40	25.42	
8300.00	8169.24	8205.65	181.46	19.52	17.90	934.04	897.49	25.56	
8400.00	8316.52	8353.36	181.46	19.84	18.22	946.28	909.12	25.47	
8500.00	8463.23	8500.13	269.34	20.12	18.49	949.92	912.24	25.21	
8600.00	8563.29	8600.18	237.70	20.32	18.70	950.02	911.92	24.93	
8700.00	8663.81	8701.43	238.31	20.23	18.92	956.49	917.96	24.83	
8800.00	8759.03	8801.20	240.05	19.70	19.14	972.81	933.91	25.01	
8900.00	8844.63	8898.19	242.88	19.36	18.83	998.39	958.90	25.28	
9000.00	8917.85	8991.72	246.75	19.60	17.66	1032.31	992.38	25.85	
9100.00	8977.46	9081.75	251.55	19.91	16.42	1073.32	1032.65	26.39	
9200.00	9023.27	9168.85	257.13	20.31	15.20	1119.88	1078.38	26.99	
9300.00	9055.56	9254.02	263.21	20.77	14.19	1170.28	1127.82	27.56	
9400.00	9074.53	9338.66	269.47	21.32	13.51	1222.70	1179.07	28.02	
9500.00	9079.94	9428.56	269.60	21.94	13.34	1268.14	1223.25	28.25	
9600.00	9079.51	9524.51	269.58	22.84	13.53	1295.77	1249.21	27.83	
9700.00	9079.06	9623.96	269.54	23.73	13.77	1304.63	1256.34	27.02	
9800.00	9078.60	9723.96	269.55	24.85	14.05	1305.00	1254.71	25.95	
9900.00	9078.15	9823.96	269.55	25.97	14.36	1305.37	1252.89	24.88	
10000.00	9077.70	9923.96	269.55	27.11	14.70	1305.74	1251.05	23.88	
10100.00	9077.24	10023.96	269.55	28.43	15.07	1306.11	1248.98	22.86	
10200.00	9076.79	10123.96	269.55	29.80	15.48	1306.48	1246.67	21.84	
10300.00	9076.34	10223.96	269.55	31.19	15.90	1306.85	1244.33	20.90	
10400.00	9075.88	10323.96	269.55	32.62	16.36	1307.23	1241.95	20.03	
10500.00	9075.43	10423.96	269.55	34.07	16.83	1307.60	1239.54	19.21	
10600.00	9074.98	10523.96	269.55	35.55	17.32	1307.97	1237.03	18.44	
10700.00	9074.52	10623.96	269.55	37.05	17.84	1308.34	1234.39	17.69	
10800.00	9074.07	10723.96	269.55	38.57	18.36	1308.71	1231.72	17.00	
10900.00	9073.61	10823.96	269.55	40.11	18.88	1309.08	1229.04	16.36	

5D Anti-Collision Report

Secondary Well : Ragin Cajun 12 Fed 3H (p) (TVD Relative to Drill Floor (Primary) ; All Azimuth Relative to GRID NORTH)									
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
11000.00	9073.16	10923.95	269.55	41.67	19.42	1309.46	1226.26	15.74	
11100.00	9072.71	11023.95	269.55	43.30	19.97	1309.83	1223.41	15.16	
11200.00	9072.25	11123.95	269.55	44.95	20.55	1310.20	1220.62	14.63	
11300.00	9071.80	11223.95	269.55	46.61	21.13	1310.57	1217.62	14.10	
11400.00	9071.35	11323.95	269.55	48.28	21.72	1310.94	1214.66	13.62	
11500.00	9070.89	11423.95	269.55	49.96	22.29	1311.31	1211.71	13.17	
11600.00	9070.44	11523.95	269.55	51.65	22.84	1311.68	1208.75	12.74	
11700.00	9069.99	11623.95	269.56	53.35	23.48	1312.06	1205.78	12.35	
11800.00	9069.53	11723.95	269.56	55.06	24.12	1312.43	1202.80	11.97	
11900.00	9069.08	11823.95	269.56	56.77	24.76	1312.80	1199.81	11.62	
12000.00	9068.63	11923.95	269.56	58.49	25.40	1313.17	1196.80	11.28	
12100.00	9068.17	12023.95	269.56	60.21	26.04	1313.54	1193.77	10.97	
12200.00	9067.72	12123.95	269.56	61.94	26.68	1313.91	1190.69	10.66	
12300.00	9067.27	12223.95	269.56	63.68	27.33	1314.29	1187.60	10.37	
12400.00	9066.81	12323.95	269.56	65.42	27.98	1314.66	1184.50	10.10	
12500.00	9066.36	12423.94	269.56	67.16	28.63	1315.03	1181.38	9.84	
12600.00	9065.90	12523.94	269.56	68.91	29.29	1315.40	1178.26	9.59	
12700.00	9065.45	12623.94	269.56	70.66	29.95	1315.77	1175.14	9.36	
12800.00	9065.00	12723.94	269.56	72.42	30.62	1316.14	1172.00	9.13	
12900.00	9064.54	12823.94	269.56	74.17	31.29	1316.51	1168.86	8.92	
13000.00	9064.09	12923.94	269.56	75.94	31.96	1316.89	1165.71	8.71	
13100.00	9063.64	13023.94	269.56	77.70	32.63	1317.26	1162.56	8.52	
13200.00	9063.18	13123.94	269.56	79.47	33.31	1317.63	1159.40	8.33	
13300.00	9062.73	13223.94	269.56	81.24	33.98	1318.00	1156.24	8.15	
13400.00	9062.28	13323.94	269.56	83.01	34.67	1318.37	1153.07	7.98	
13500.00	9061.82	13423.94	269.57	84.78	35.35	1318.74	1149.90	7.81	
13600.00	9061.37	13523.94	269.57	86.56	36.03	1319.12	1146.73	7.65	
13700.00	9060.92	13623.94	269.57	88.34	36.72	1319.49	1143.55	7.50	
13800.00	9060.46	13723.94	269.57	90.12	37.41	1319.86	1140.36	7.35	
13900.00	9060.01	13823.93	269.57	91.89	38.10	1320.23	1137.18	7.21	
13904.15	9060.00	13825.74	269.57	91.93	38.11	1320.25	1137.11	7.21	

**Weatherford****Weatherford Drilling Services**

GeoDec4 v2.0.0.3

Report Date: April 29, 2014
Job Number: _____
Customer: Devon Energy
Well Name: Ragin, Cajun 12 Fed 2H
API Number: _____
Rig Name: _____
Location: Lea Co, NM Nad83: NME
Block: _____
Engineer: RWJ

NAD83 / New Mexico East (ftUS)	NAD83 (1986)
Projected Coordinate System	Geodetic Coordinate System
Datum: North American Datum 1983 (1986)	Datum: North American Datum 1983 (1986)
Ellipsoid: GRS 1980	Ellipsoid: GRS 1980
EPSG: 2257	EPSG: 4269
North: 383348.85 US Survey Foot	Latitude: 32.050677 Degree
East: 821674.21 US Survey Foot	Longitude: -103.428505 Degree
Convergence: 0.48°	
Declination: 7.24°	
Total Correction: 6.76°	
Datum Transformation: none	

Geodetic Location WGS84

MSL Elevation = 0 m
Latitude = 32° 03' 02.44" N
Longitude = 103° 25' 42.62" W

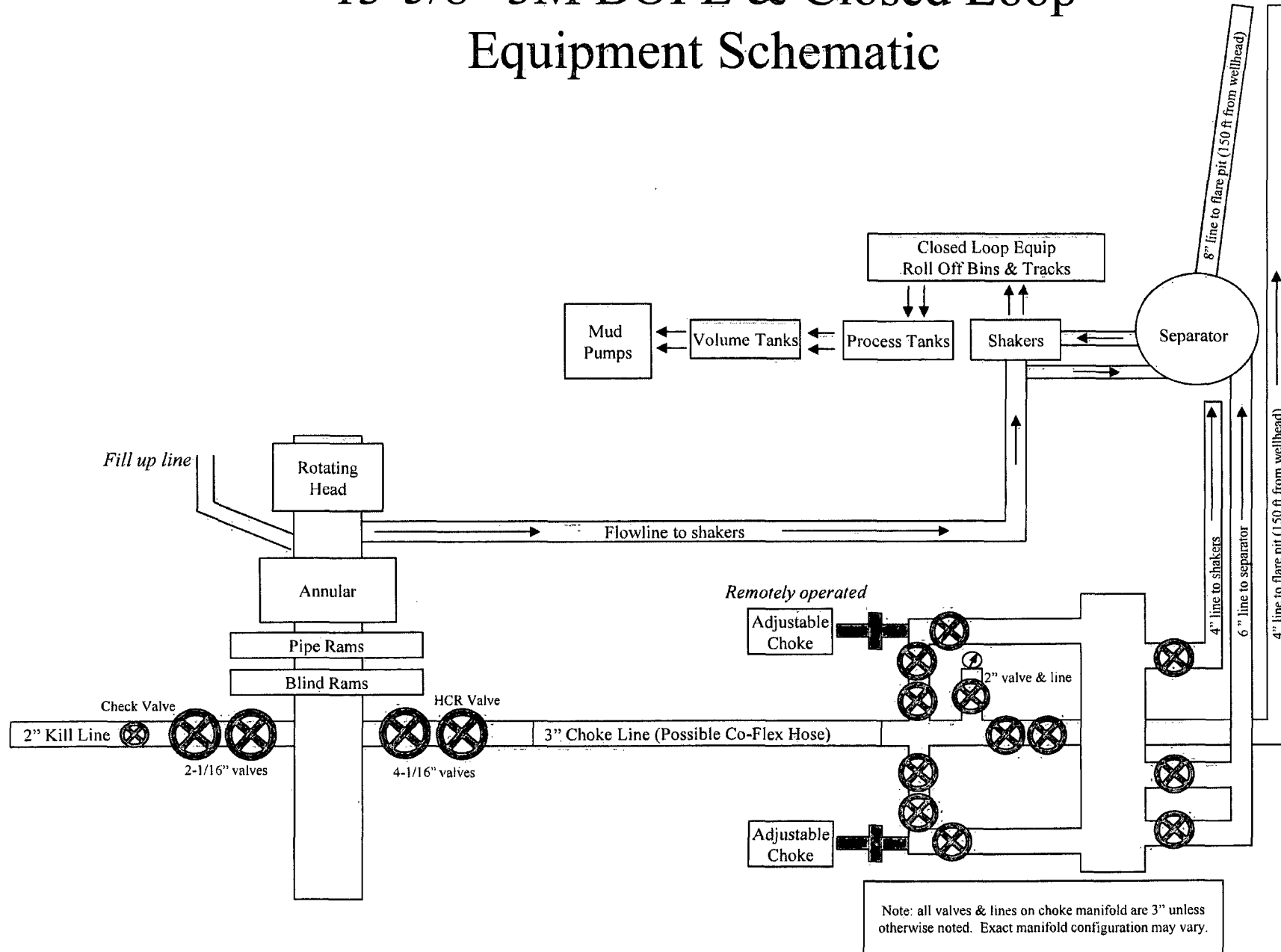
Magnetic Declination = 7.24 deg	[True North Offset]
Local Gravity = .9988 g	Checksum = 6819
Local Field Strength = 48220 nT	Magnetic Vector X = 23950 nT
Magnetic Dip = 59.96 deg	Magnetic Vector Y = 3042 nT
Magnetic Model = bggm2013.bgs	Magnetic Vector Z = 41742 nT
Run Date = July 15, 2014	Magnetic Vector H = 24142 nT

Signed: _____ Date: _____

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Warning: This information is controlled, and any printed version is deemed as uncontrolled unless suitably endorsed by a controlling authority or accompanied by a controlled table of contents in order to ensure adequate revision control.

13-5/8" 3M BOPE & Closed Loop Equipment Schematic



NOTES REGARDING BLOWOUT PREVENTERS

Devon Energy Production Company, L.P.
Ragin Cajun 12 Fed 2H

1. Drilling Nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
2. Wear ring will be properly installed in head.
3. Blowout preventer and all associated filings will be in operable condition to withstand a minimum of 3000psi working pressure.
4. All fittings will be flanged.
5. A full bore safety valve tested to a minimum of 3000psi WP with proper thread connections will be available on the rotary rig floor at all times.
6. All choke lines will be anchored to prevent movement.
7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
8. Will maintain a kelly cock attached to the kelly.
9. Hand wheels and wrenches will be properly installed and tested for safe operation.
10. Hydraulic floor control for blowout preventer will be located as near in proximity to driller's controls as possible.
11. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.



Fluid Technology

ContiTech Beattie Corp.
Website: www.contitechbeattie.com

Monday, June 14, 2010

RE: Drilling & Production Hoses
Lifting & Safety Equipment

To Helmerich & Payne,

A Continental Contitech hose assembly can perform as intended and suitable for the application regardless of whether the hose is secured or unsecured in its configuration. As a manufacturer of High Pressure Hose Assemblies for use in Drilling & Production, we do offer the corresponding lifting and safety equipment, this has the added benefit of easing the lifting and handling of each hose assembly whilst affording hose longevity by ensuring correct handling methods and procedures as well as securing the hose in the unlikely event of a failure; but in no way does the lifting and safety equipment affect the performance of the hoses providing the hoses have been handled and installed correctly. It is good practice to use lifting & safety equipment but not mandatory.

Should you have any questions or require any additional information/clarifications then please do not hesitate to contact us.

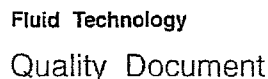
ContiTech Beattie is part of the Continental AG Corporation and can offer the full support resources associated with a global organization.

Best regards,

Robin Hodgson
Sales Manager
ContiTech Beattie Corp

ContiTech Beattie Corp,
11535 Brittmoore Park Drive,
Houston, TX 77041
Phone: +1 (832) 327-0141
Fax: +1 (832) 327-0148
www.contitechbeattie.com





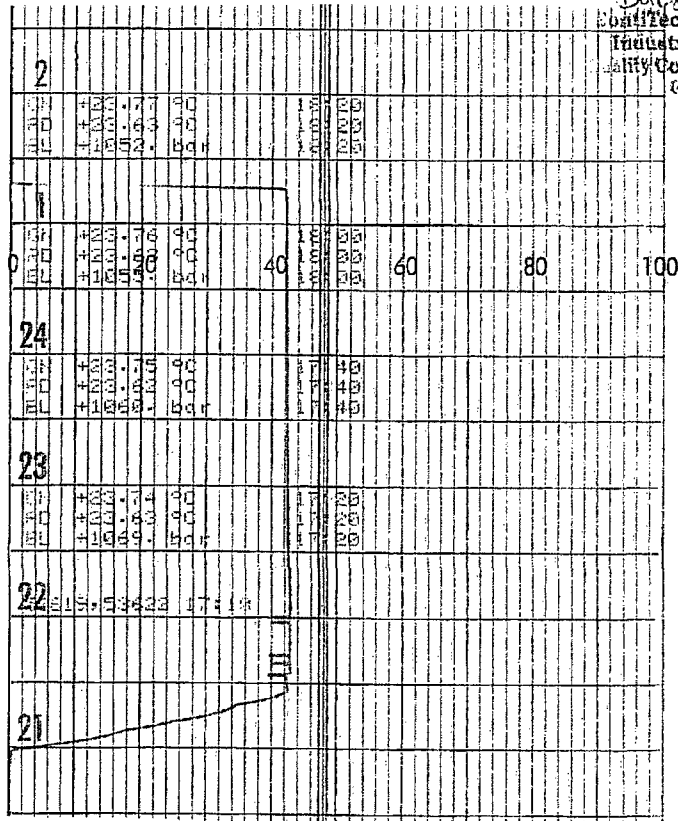
ContiTech Rubber Industrial Kft.
Budapesti út 10., Szeged H-6728
P.O.Box 152 Szeged H-6701
Hungary

Phone: +36 62 566 737
Fax: +36 62 566 738
e-mail: info@fluid.contitech.hu
Internet: www.contitech-rubber.hu

The Court of Csongrád County as
Registry Court
Registry Court No: HU 06-09-002502
EU VAT No: HU11087209

Bank data
Commerzbank Zrt.
Szeged
14220108-26830003-00000000

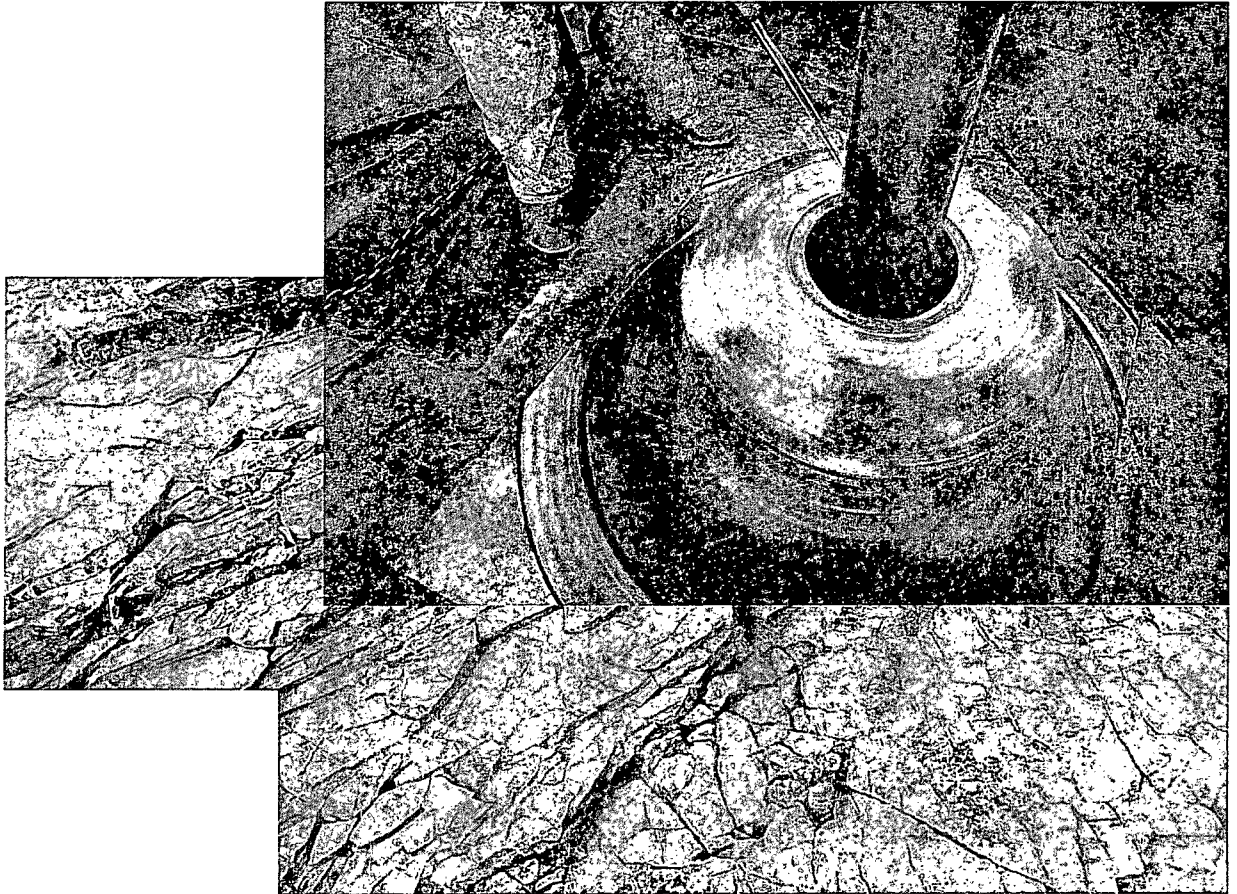
HARTMANN &



Daech
Contitech Rubber
Industrial Kft.
Quality Control Dept.
(2)



Commitment Runs Deep



Design Plan
Operation and Maintenance Plan
Closure Plan

SENM - Closed Loop Systems
February 2014

I. Design Plan

Devon uses MI SWACO closed loop system (CLS). The MI SWACO CLS is designed to maintain drill solids at or below 5%. The equipment is arranged to progressively remove solids from the largest to the smallest size. Drilling fluids can thus be reused and savings is realized on mud and disposal costs. Dewatering may be required with the centrifuges to insure removal of ultra fine solids.

The drilling location is constructed to allow storm water to flow to a central sump normally the cellar. This insures no contamination leaves the drilling pad in the event of a spill. Storm water is reused in the mud system or stored in a reserve fluid tank farm until it can be reused. All lubricants, oils, or chemicals are removed immediately from the ground to prevent the contamination of storm water. An oil trap is normally installed on the sump if an oil spill occurs during a storm.

A tank farm is utilized to store drilling fluids including fresh water and brine fluids. The tank farm is constructed on a 20 ml plastic lined, bermed pad to prevent the contamination of the drilling site during a spill. Fluids from other sites may be stored in these tanks for processing by the solids control equipment and reused in the mud system. At the end of the well the fluids are transported from the tank farm to an adjoining well or to the next well for the rig.

Prior to installing a closed-loop system on site, the topsoil, if present, will be stripped and stockpiled for use as the final cover or fill at the time of closure.

Signs will be posted on the fence surrounding the closed-loop system unless the closed-loop system is located on a site where there is an existing well, that is operated by Devon.

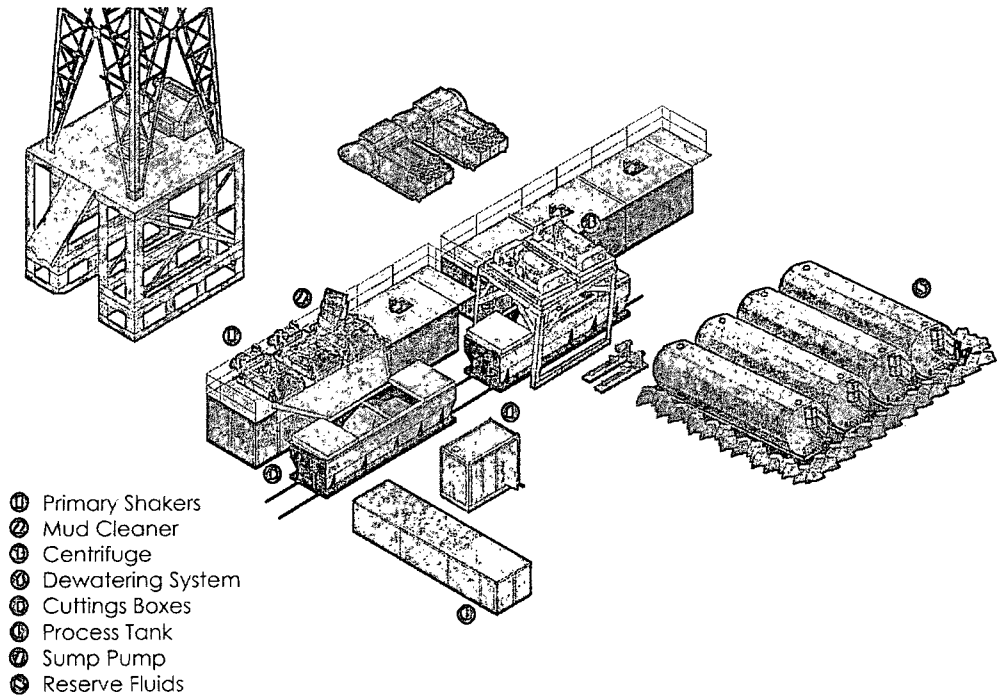
II. Operations and Maintenance Plan

Primary Shakers: The primary shakers make the first removal of drill solids from the drilling mud as it leaves the well bore. The shakers are sized to handle maximum drilling rate at optimal screen size. The shakers normally remove solids down to 74 microns.

Mud Cleaner: The Mud Cleaner cleans the fluid after it leaves the shakers. A set of hydrocyclones are sized to handle 1.25 to 1.5 times the maximum circulating rate. This ensures all the fluid is being processed to an average cut point of 25 microns. The wet discharged is dewatered on a shaker equipped with ultra fine mesh screens and generally cut at 40 microns.



Closed Loop Schematic



Centrifuges: The centrifuges can be one or two in number depending on the well geometry or depth of well. The centrifuges are sized to maintain low gravity solids at 5% or below. They may or may not need a dewatering system to enhance the removal rates. The centrifuges can make a cut point of 8-10 microns depending on bowl speed, feed rate, solids loading and other factors.

The centrifuge system is designed to work on the active system and be flexible to process incoming fluids from other locations. This set-up is also dependant on well factors.

Dewatering System: The dewatering system is a chemical mixing and dosing system designed to enhance the solids removal of the centrifuge. Not commonly used in shallow wells. It may contain pH adjustment, coagulant mixing and dosing, and polymer mixing and dosing. Chemical flocculation binds ultra fine solids into a mass that is within the centrifuge operating design. The

dewatering system improves the centrifuge cut point to infinity or allows for the return of clear water or brine fluid. This ability allows for the ultimate control of low gravity solids.

Cuttings Boxes: Cuttings boxes are utilized to capture drill solids that are discarded from the solids control equipment. These boxes are set upon a rail system that allows for the removal and replacement of a full box of cuttings with an empty one. They are equipped with a cover that insures no product is spilled into the environment during the transportation phase.

Process Tank: (Optional) The process tank allows for the holding and process of fluids that are being transferred into the mud system. Additionally, during times of lost circulation the process tank may hold active fluids that are removed for additional treatment. It can further be used as a mixing tank during well control conditions.

Sump and Sump Pump: The sump is used to collect storm water and the pump is used to transfer this fluid to the active system or to the tank for to hold in reserve. It can also be used to collect fluids that may escape during spills. The location contains drainage ditches that allow the location fluids to drain to the sump.

Reserve Fluids (Tank Farm): A series of frac tanks are used to replace the reserve pit. These are steel tanks that are equipped with a manifold system and a transfer pump. These tanks can contain any number of fluids used during the drilling process. These can include fresh water, cut brine, and saturated salt fluid. The fluid can be from the active well or reclaimed fluid from other locations. A 20 ml liner and berm system is employed to ensure the fluids do not migrate to the environment during a spill.

If a leak develops, the appropriate division district office will be notified within 48 hours of the discovery and the leak will be addressed. Spill prevention is accomplished by maintaining pump packing, hoses, and pipe fittings to insure no leaks are occurring. During an upset condition the source of the spill is isolated and repaired as soon as it is discovered. Free liquid is removed by a diaphragm pump and returned to the mud system. Loose topsoil may be used to stabilize the spill and the contaminated soil is excavated and placed in the cuttings boxes. After the well is finished and the rig has moved, the entire location is scrapped and testing will be performed to determine if a release has occurred.

All trash is kept in a wire mesh enclosure and removed to an approved landfill when full. All spent motor oils are kept in separate containers and they are removed and sent to an approved recycling center. Any spilled lubricants, pipe

dope, or regulated chemicals are removed from soil and sent to landfills approved for these products.

These operations are monitored by Mi Swaco service technicians. Daily logs are maintained to ensure optimal equipment operation and maintenance. Screen and chemical use is logged to maintain inventory control. Fluid properties are monitored and recorded and drilling mud volumes are accounted for in the mud storage farm. This data is kept for end of well review to insure performance goals are met. Lessons learned are logged and used to help with continuous improvement.

A MI SWACO field supervisor manages from 3-5 wells. They are responsible for training personnel, supervising installations, and inspecting sites for compliance of MI SWACO safety and operational policy.

III. Closure Plan

A maximum 340' X 340' caliche pad is built per well. All of the trucks and steel tanks fit on this pad. All fluid cuttings go to the steel tanks to be hauled by various trucking companies to an agency approved disposal.

H&P Flex Rig Location Layout

2 Well Pad

