

Submit 1 Copy To Appropriate District
Office
District I
1625 N. French Dr., Hobbs, NM 88240
District II
1301 W. Grand Ave., Artesia, NM 88210
District III
1000 Rio Brazos Rd., Aztec, NM 87410
District IV
1220 S. St. Francis Dr., Santa Fe, NM
87505

State of New Mexico

Energy, Minerals and Natural Resources

Form C-103

October 13, 2009

HOBBS OFFICE

DEC 15 2014

RECEIVED

OIL CONSERVATION DIVISION

1220 South St. Francis Dr.
Santa Fe, NM 87505

WELL API NO.
30-025-42139

5. Indicate Type of Lease

STATE ☒ FEE ☐

6. State Oil & Gas Lease No.
V07530-0001

7. Lease Name or Unit Agreement Name

Linam AGI

8. Well Number #2

9. OGRID Number
36785

10. Pool name or Wildcat
AGI: Wolfcamp

SUNDRY NOTICES AND REPORTS ON WELLS

(DO NOT USE THIS FORM FOR PROPOSALS TO DRILL OR TO DEEPEN OR PLUG BACK TO A DIFFERENT RESERVOIR. USE "APPLICATION FOR PERMIT" (FORM C-101) FOR SUCH PROPOSALS.)

1. Type of Well: Oil Well ☐ Gas Well ☐ Other Acid Gas Injection ☒

2. Name of Operator

DCP Midstream LP

3. Address of Operator

370 17th Street, Suite 2500, Denver, CO 80202

4. Well Location

Unit Letter K : 1600 feet from the South line and 1750 feet from the West line

Section 30 Township 18S Range 37E NMPM County Lea

11. Elevation (Show whether DR, RKB, RT, GR, etc.)
3736 GR

12. Check Appropriate Box to Indicate Nature of Notice, Report or Other Data

NOTICE OF INTENTION TO:

PERFORM REMEDIAL WORK ☐ PLUG AND ABANDON ☐

TEMPORARILY ABANDON ☐ CHANGE PLANS ☐

PULL OR ALTER CASING ☐ MULTIPLE COMPL ☐

DOWNHOLE COMMINGLE ☐

OTHER.

SUBSEQUENT REPORT OF:

REMEDIAL WORK ☐ ALTERING CASING

COMMENCE DRILLING OPNS. ☐ P AND A

CASING/CEMENT JOB ☒

Production Casing to 9,204'

OTHER:

13. Describe proposed or completed operations. (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion.

The Linam AGI #2 production borehole reached TD (9,234') at 06:16 on December 9, 2014. The caliper log for the production (8 1/2-inch) borehole indicates a clean hole with no significant washouts from 8,630' to TD. A ledge is present between the bottom of the 9 5/8-inch lower intermediate casing and the total depth of the 12 1/4-borehole (8,600 to 8,630'). The caliper log from 8,594' to 9,234' is attached to this C-103. The production borehole log runs (three) were completed at 06:36 on December 10, 2014.

The Top of the Lower Leonard Formation was determined to be 8,811' and the Wolfcamp Formation was determined to be 9,041' based on open-hole geophysical logs and the mud log. Geophysical logs are attached. Several small isolated H₂S detections were encountered during drilling of the production borehole from 8,696' to 9,028', as the drill bit cut through the injection zone in the Linam AGI #1 well. None of the H₂S concentrations exceeded 1.3 ppm, which is below mud loggers bloodhound detector limit (+/- 5.0 ppm). Monitoring continued until the 7-inch production casing was set on Friday, December 12, 2014.

The Linam AGI #2 production casing was run starting at 18:30 December 11, 2014, after completing the logging of the open borehole and laying down the drill string. Casing was set at 9,204' in the Wolfcamp Formation (100% Dolomite - Low Porosity). The Linam AGI #2 production casing is constructed with 184 joints of 7.0", 26#, HCL 80 casing from the surface to 8,414.42' and 24 joints of 7.0", 26#, 28 Cr (nickel-plated, corrosion-resistant) casing from 8,414.42' to 9,155.21'. A schematic of the Linam AGI #2 well design and the as built casing tally is attached.

The production casing for the Linam AGI #2 was cemented in two stages. A Differential Valve (DV) Tool is located at a depth of 8,092.05' (see casing tally sheet). The 1st Stage (Bottom 9,234' - Top 8,092') utilized 207 sx of 16.0 ppg EverCRETE™ cement with a yield of 1.12 cuft/sk (approx. 41 bbls). WOC time for the 1st Stage was more than 24 hrs while circulating through DV Tool to surface to clean out 2nd stage annulus space. The 2nd Stage (Bottom 8,092' - Top surface) utilized 870 sx of 13.2 ppg TXI with a yield of 1.34 cuft/sx (207.4 bbls) for Tail. WOC time for the 2nd Stage is 24 hrs (minimum). Thirty bbls of cement were returned on the 2nd Stage. The cement returns were not witnessed by the NMOCD but were photographed (photos attached). Cement did not fall back and the production casing remained cemented to surface. The cement report is attached.

After completing the 2nd Stage cement Precision Rig #107 was released for removal. The DV Tool will be drilled out and a circumferential cement bond log (CBL) will run with the completion rig.

FEB 23 2015

I hereby certify that the information above is true and complete to the best of my knowledge and belief.



SIGNATURE

TITLE: Consultant to DCP Midstream LP

DATE: 12/15/14

Type or print name

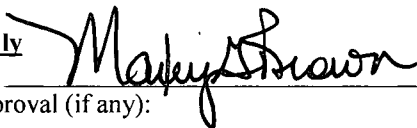
Michael W. Selke, RG

E-mail address: mselke@geolex.com

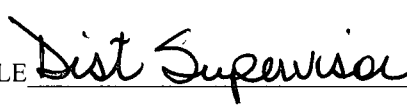
PHONE: 505-842-8000

For State Use Only

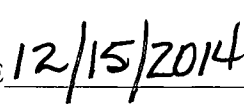
APPROVED BY:



TITLE



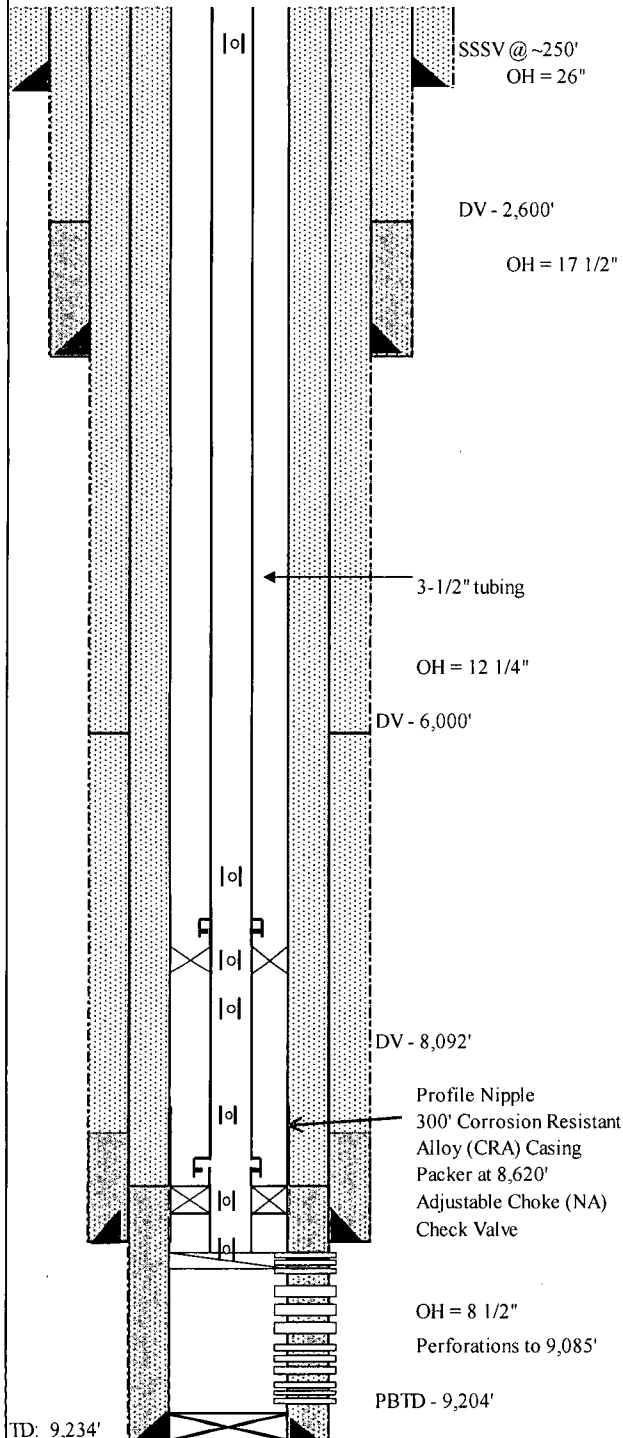
DATE



Conditions of Approval (if any):

FEB 23 2015

Location: 2120 FSL & 2120' FWL
 STR S30-T18S-R37E
 County, St.: LEA COUNTY, NEW MEXICO



CONDUCTOR CASING

30" Conductor at 120'

SURFACE CASING

20", 106.5#, J55, BTC from 0' to 1650'
 Cement to surface (10/23/14)

UPPER INTERMEDIATE CASING:

13 3/8", 68 #/ft, J55, STC at 3,200'
 Cement to surface (11/2/14)

LOWER INTERMEDIATE CASING:

9 5/8", 47 #/ft, HCL-80, LTC at 8,600'
 Cement to surface (12/4/14)

PRODUCTION CASING:

7", 26 #/ft, HCL-80, LTC to 8,414'
 7", 26 #/ft, 28Cr, VAM TOP from 8,414' to 9,155'
 7", 26 #/ft, HCL-80, LTC from 9,155' to 9,204'
 Cement to surface (12/14/14)

TUBING:

Subsurface Safety Valve at 250'
 3 1/2", 9.3#/ft, L80 from surface to 8,530'
 3 1/2", 9.3#/ft, SM2550 from 8,530' to 8,620'
 Premium thread utilizing metal to metal sealing in collars

ANNULAR FLUID:

Diesel Fuel from top of packer to surface

PACKER:

Permanent injection packer with Incaloy components set in Corrosion Resistant Alloy (CRA) csg at 8,620'

PERFORATIONS:

Primary Targets:

Cherry Canyon

8,710'-9,085' Will select upon logging

Linam AGI #2 Well Schematic

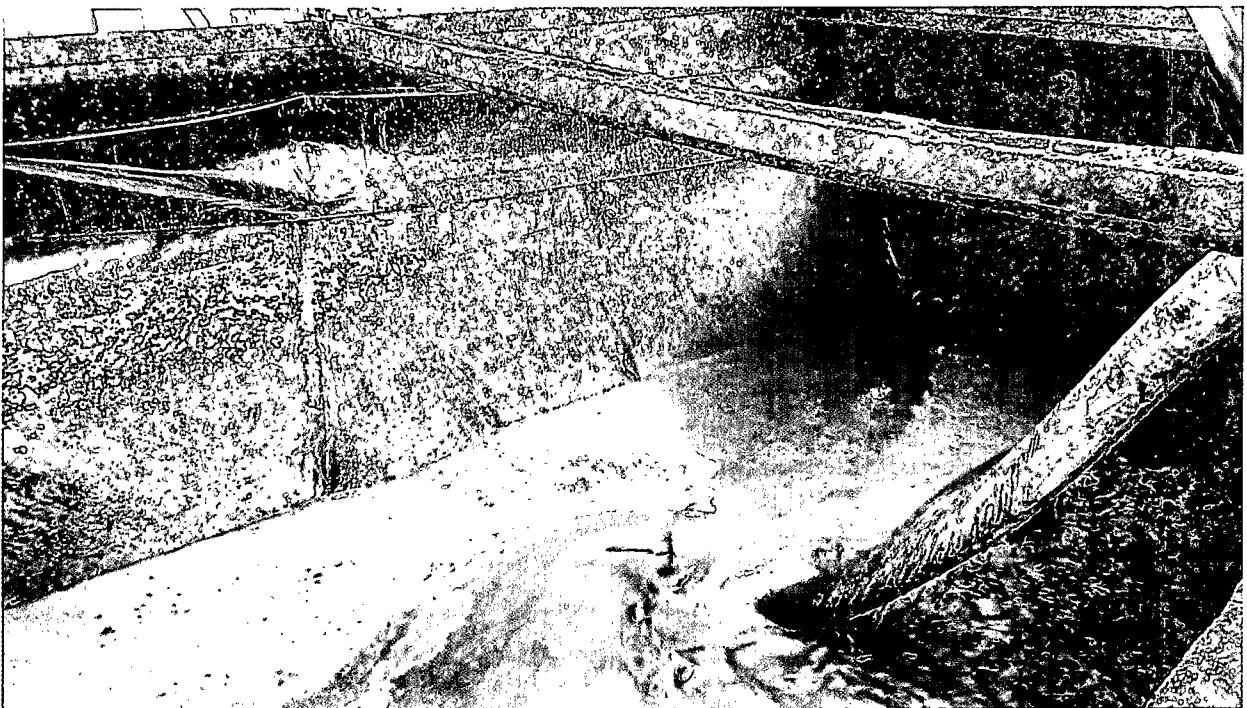
							Well	Linam AGI #2	
							Date	10-Dec-14	
							Total Depth	9,234	
							Shoe Depth	9,204	
							Rathole	30	
							Total		Collar
Run Jt #	Unit #	Length	O.D.	Weight	Grade	Thread	Remarks	Length	Depth
1	F/S	1.60	7	26	HCL-80	LTC		1.60	9,202.40
2	1	45.78	7	26	HCL-80	LTC	(2) Cent 1 & 2	47.38	9,156.62
3	F/C	1.41	7	26	HCL-80	LTC		48.79	9,155.21
4	2	32.15	7	26	28 Cr	Vam Top	Cent #3	80.94	9,123.06
5	3	32.90	7	26	28 Cr	Vam Top		113.84	9,090.16
6	4	32.01	7	26	28 Cr	Vam Top	Cent #4	145.85	9,058.15
7	5	33.11	7	26	28 Cr	Vam Top		178.96	9,025.04
8	6	30.63	7	26	28 Cr	Vam Top	Cent #5	209.59	8,994.41
9	7	31.71	7	26	28 Cr	Vam Top		241.30	8,962.70
10	8	29.70	7	26	28 Cr	Vam Top	Cent #6	271.00	8,933.00
11	9	29.83	7	26	28 Cr	Vam Top		300.83	8,903.17
12	10	32.16	7	26	28 Cr	Vam Top	Cent #7	332.99	8,871.01
13	11	31.28	7	26	28 Cr	Vam Top		364.27	8,839.73
14	12	28.72	7	26	28 Cr	Vam Top		392.99	8,811.01
15	13	32.35	7	26	28 Cr	Vam Top	Cent #8	425.34	8,778.66
16	14	28.83	7	26	28 Cr	Vam Top		454.17	8,749.83
17	15	31.39	7	26	28 Cr	Vam Top		485.56	8,718.44
18	16	31.78	7	26	28 Cr	Vam Top	Cent #9	517.34	8,686.66
19	17	30.10	7	26	28 Cr	Vam Top		547.44	8,656.56
20	18	31.68	7	26	28 Cr	Vam Top		579.12	8,624.88
21	19	31.48	7	26	28 Cr	Vam Top		610.60	8,593.40
22	20	30.85	7	26	28 Cr	Vam Top	Cent #10	641.45	8,562.55
23	21	32.18	7	26	28 Cr	Vam Top		673.63	8,530.37
24	22	26.03	7	26	28 Cr	Vam Top		699.66	8,504.34
25	23	25.78	7	26	28 Cr	Vam Top		725.44	8,478.56
26	24	31.80	7	26	28 Cr	Vam Top	Cent #11	757.24	8,446.76
27	25	32.34	7	26	28 Cr	Vam Top		789.58	8,414.42
28	26	45.58	7	26	HCL-80	LTC		835.16	8,368.84
29	27	45.55	7	26	HCL-80	LTC		880.71	8,323.29
30	28	45.78	7	26	HCL-80	LTC	Cent #12	926.49	8,277.51
31	29	45.58	7	26	HCL-80	LTC		972.07	8,231.93
32	30	45.57	7	26	HCL-80	LTC		1,017.64	8,186.36
33	31	45.80	7	26	HCL-80	LTC		1,063.44	8,140.56
34	32	45.81	7	26	HCL-80	LTC	Cent #13	1,109.25	8,094.75
	DVT	2.70	7	26	HCL-80	LTC		1,111.95	8,092.05
35	33	45.57	7	26	HCL-80	LTC		1,157.52	8,046.48
36	34	45.57	7	26	HCL-80	LTC		1,203.09	8,000.91
37	35	45.60	7	26	HCL-80	LTC		1,248.69	7,955.31
38	36	45.79	7	26	HCL-80	LTC	Cent #14	1,294.48	7,909.52
39	37	45.57	7	26	HCL-80	LTC		1,340.05	7,863.95
40	38	45.63	7	26	HCL-80	LTC		1,385.68	7,818.32
41	39	45.60	7	26	HCL-80	LTC		1,431.28	7,772.72
42	40	45.60	7	26	HCL-80	LTC	Cent #15	1,476.88	7,727.12
43	41	45.60	7	26	HCL-80	LTC		1,522.48	7,681.52
44	42	45.61	7	26	HCL-80	LTC		1,568.09	7,635.91
45	43	45.64	7	26	HCL-80	LTC		1,613.73	7,590.27
46	44	45.61	7	26	HCL-80	LTC	Cent #16	1,659.34	7,544.66
47	45	45.59	7	26	HCL-80	LTC		1,704.93	7,499.07
48	46	45.58	7	26	HCL-80	LTC		1,750.51	7,453.49
49	47	45.59	7	26	HCL-80	LTC		1,796.10	7,407.90
50	48	45.57	7	26	HCL-80	LTC	Cent #17	1,841.67	7,362.33
51	49	45.62	7	26	HCL-80	LTC		1,887.29	7,316.71
52	50	45.63	7	26	HCL-80	LTC		1,932.92	7,271.08
53	51	45.29	7	26	HCL-80	LTC		1,978.21	7,225.79
54	52	45.79	7	26	HCL-80	LTC	Cent #18	2,024.00	7,180.00
55	53	45.58	7	26	HCL-80	LTC		2,069.58	7,134.42
56	54	45.58	7	26	HCL-80	LTC		2,115.16	7,088.84
57	55	45.28	7	26	HCL-80	LTC		2,160.44	7,043.56
58	56	45.61	7	26	HCL-80	LTC	Cent #19	2,206.05	6,997.95
59	57	44.99	7	26	HCL-80	LTC		2,251.04	6,952.96
60	58	45.28	7	26	HCL-80	LTC		2,296.32	6,907.68
61	59	45.59	7	26	HCL-80	LTC		2,341.91	6,862.09
62	60	44.37	7	26	HCL-80	LTC	Cent #20	2,386.28	6,817.72
63	61	44.57	7	26	HCL-80	LTC		2,430.85	6,773.15
64	62	44.58	7	26	HCL-80	LTC		2,475.43	6,728.57
65	63	44.58	7	26	HCL-80	LTC		2,520.01	6,683.99
66	64	45.80	7	26	HCL-80	LTC	Cent #21	2,565.81	6,638.19
67	65	45.61	7	26	HCL-80	LTC		2,611.42	6,592.58
68	66	45.62	7	26	HCL-80	LTC		2,657.04	6,546.96
69	67	45.61	7	26	HCL-80	LTC		2,702.65	6,501.35
70	68	45.60	7	26	HCL-80	LTC	Cent #22	2,748.25	6,455.75
71	69	45.60	7	26	HCL-80	LTC		2,793.85	6,410.15
72	70	45.62	7	26	HCL-80	LTC		2,839.47	6,364.53
73	71	45.62	7	26	HCL-80	LTC		2,885.09	6,318.91

74	72	45.80	7	26	HCL-80	LTC	Cent #23	2,930.89	6,273.11
75	73	45.80	7	26	HCL-80	LTC		2,976.69	6,227.31
76	74	45.75	7	26	HCL-80	LTC		3,022.44	6,181.56
77	75	45.81	7	26	HCL-80	LTC		3,068.25	6,135.75
78	76	45.82	7	26	HCL-80	LTC	Cent #24	3,114.07	6,089.93
79	77	45.68	7	26	HCL-80	LTC		3,159.75	6,044.25
80	78	45.63	7	26	HCL-80	LTC		3,205.38	5,998.62
81	79	45.61	7	26	HCL-80	LTC		3,250.99	5,953.01
82	80	45.83	7	26	HCL-80	LTC	Cent #25	3,296.82	5,907.18
83	81	45.64	7	26	HCL-80	LTC		3,342.46	5,861.54
84	82	45.63	7	26	HCL-80	LTC		3,388.09	5,815.91
85	83	45.61	7	26	HCL-80	LTC		3,433.70	5,770.30
86	84	45.82	7	26	HCL-80	LTC	Cent #26	3,479.52	5,724.48
87	85	45.63	7	26	HCL-80	LTC		3,525.15	5,678.85
88	86	45.59	7	26	HCL-80	LTC		3,570.74	5,633.26
89	87	45.65	7	26	HCL-80	LTC		3,616.39	5,587.61
90	88	45.63	7	26	HCL-80	LTC	Cent #27	3,662.02	5,541.98
91	89	45.62	7	26	HCL-80	LTC		3,707.64	5,496.36
92	90	45.62	7	26	HCL-80	LTC		3,753.26	5,450.74
93	91	45.60	7	26	HCL-80	LTC		3,798.86	5,405.14
94	92	45.59	7	26	HCL-80	LTC	Cent #28	3,844.45	5,359.55
95	93	45.60	7	26	HCL-80	LTC		3,890.05	5,313.95
96	94	45.63	7	26	HCL-80	LTC		3,935.68	5,268.32
97	95	45.84	7	26	HCL-80	LTC		3,981.52	5,222.48
98	96	45.62	7	26	HCL-80	LTC	Cent #29	4,027.14	5,176.86
99	97	45.65	7	26	HCL-80	LTC		4,072.79	5,131.21
100	98	45.83	7	26	HCL-80	LTC		4,118.62	5,085.38
101	99	45.84	7	26	HCL-80	LTC		4,164.46	5,039.54
102	100	45.88	7	26	HCL-80	LTC	Cent #30	4,210.34	4,993.66
103	101	45.82	7	26	HCL-80	LTC		4,256.16	4,947.84
104	102	45.62	7	26	HCL-80	LTC		4,301.78	4,902.22
105	103	45.60	7	26	HCL-80	LTC		4,347.38	4,856.62
106	104	45.82	7	26	HCL-80	LTC	Cent #31	4,393.20	4,810.80
107	105	45.61	7	26	HCL-80	LTC		4,438.81	4,765.19
108	106	45.58	7	26	HCL-80	LTC		4,484.39	4,719.61
109	107	45.55	7	26	HCL-80	LTC		4,529.94	4,674.06
110	108	45.28	7	26	HCL-80	LTC	Cent #32	4,575.22	4,628.78
111	109	45.28	7	26	HCL-80	LTC		4,620.50	4,583.50
112	110	45.29	7	26	HCL-80	LTC		4,665.79	4,538.21
113	111	45.57	7	26	HCL-80	LTC		4,711.36	4,492.64
114	112	45.57	7	26	HCL-80	LTC	Cent #33	4,756.93	4,447.07
115	113	45.56	7	26	HCL-80	LTC		4,802.49	4,401.51
116	114	45.56	7	26	HCL-80	LTC		4,848.05	4,355.95
117	115	45.28	7	26	HCL-80	LTC		4,893.33	4,310.67
118	116	45.25	7	26	HCL-80	LTC	Cent #34	4,938.58	4,265.42
119	117	45.22	7	26	HCL-80	LTC		4,983.80	4,220.20
120	118	44.90	7	26	HCL-80	LTC		5,028.70	4,175.30
121	119	44.92	7	26	HCL-80	LTC		5,073.62	4,130.38
122	120	44.89	7	26	HCL-80	LTC	Cent #35	5,118.51	4,085.49
123	121	44.95	7	26	HCL-80	LTC		5,163.46	4,040.54
124	122	44.95	7	26	HCL-80	LTC		5,208.41	3,995.59
125	123	44.93	7	26	HCL-80	LTC		5,253.34	3,950.66
126	124	45.23	7	26	HCL-80	LTC	Cent #36	5,298.57	3,905.43
127	125	45.18	7	26	HCL-80	LTC		5,343.75	3,860.25
128	126	45.21	7	26	HCL-80	LTC		5,388.96	3,815.04
129	127	45.20	7	26	HCL-80	LTC		5,434.16	3,769.84
130	128	45.22	7	26	HCL-80	LTC	Cent #37	5,479.38	3,724.62
131	129	45.21	7	26	HCL-80	LTC		5,524.59	3,679.41
132	130	45.46	7	26	HCL-80	LTC		5,570.05	3,633.95
133	131	45.21	7	26	HCL-80	LTC		5,615.26	3,588.74
134	132	45.34	7	26	HCL-80	LTC	Cent #38	5,660.60	3,543.40
135	133	45.16	7	26	HCL-80	LTC		5,705.76	3,498.24
136	134	45.21	7	26	HCL-80	LTC		5,750.97	3,453.03
137	135	45.20	7	26	HCL-80	LTC		5,796.17	3,407.83
138	136	45.18	7	26	HCL-80	LTC	Cent #39	5,841.35	3,362.65
139	137	44.90	7	26	HCL-80	LTC		5,886.25	3,317.75
140	138	45.19	7	26	HCL-80	LTC		5,931.44	3,272.56
141	139	45.23	7	26	HCL-80	LTC		5,976.67	3,227.33
142	140	45.28	7	26	HCL-80	LTC	Cent #40	6,021.95	3,182.05
143	141	45.23	7	26	HCL-80	LTC		6,067.18	3,136.82
144	142	45.45	7	26	HCL-80	LTC		6,112.63	3,091.37
145	143	45.81	7	26	HCL-80	LTC		6,158.44	3,045.56
146	144	45.83	7	26	HCL-80	LTC	Cent #41	6,204.27	2,999.73
147	145	45.60	7	26	HCL-80	LTC		6,249.87	2,954.13
148	146	45.70	7	26	HCL-80	LTC		6,295.57	2,908.43
149	147	45.60	7	26	HCL-80	LTC		6,341.17	2,862.83
150	148	45.61	7	26	HCL-80	LTC	Cent #42	6,386.78	2,817.22
151	149	45.82	7	26	HCL-80	LTC		6,432.60	2,771.40
152	150	45.63	7	26	HCL-80	LTC		6,478.23	2,725.77
153	151	45.68	7	26	HCL-80	LTC		6,523.91	2,680.09
154	152	45.62	7	26	HCL-80	LTC	Cent #43	6,569.53	2,634.47
155	153	45.61	7	26	HCL-80	LTC		6,615.14	2,588.86
156	154	45.59	7	26	HCL-80	LTC		6,660.73	2,543.27

157	155	45.56	7	26	HCL-80	LTC		6,706.29	2,497.71
158	156	45.78	7	26	HCL-80	LTC	Cent #44	6,752.07	2,451.93
159	157	45.87	7	26	HCL-80	LTC		6,797.94	2,406.06
160	158	45.58	7	26	HCL-80	LTC		6,843.52	2,360.48
161	159	45.59	7	26	HCL-80	LTC		6,889.11	2,314.89
162	160	45.58	7	26	HCL-80	LTC	Cent #45	6,934.69	2,269.31
163	161	45.57	7	26	HCL-80	LTC		6,980.26	2,223.74
164	162	45.56	7	26	HCL-80	LTC		7,025.82	2,178.18
165	163	45.63	7	26	HCL-80	LTC		7,071.45	2,132.55
166	164	45.57	7	26	HCL-80	LTC	Cent #46	7,117.02	2,086.98
167	165	45.58	7	26	HCL-80	LTC		7,162.60	2,041.40
168	166	45.59	7	26	HCL-80	LTC		7,208.19	1,995.81
169	167	45.57	7	26	HCL-80	LTC		7,253.76	1,950.24
170	168	45.58	7	26	HCL-80	LTC	Cent #47	7,299.34	1,904.66
171	169	45.58	7	26	HCL-80	LTC		7,344.92	1,859.08
172	170	45.59	7	26	HCL-80	LTC		7,390.51	1,813.49
173	171	45.63	7	26	HCL-80	LTC		7,436.14	1,767.86
174	172	45.62	7	26	HCL-80	LTC	Cent #48	7,481.76	1,722.24
175	173	45.59	7	26	HCL-80	LTC		7,527.35	1,676.65
176	174	45.64	7	26	HCL-80	LTC		7,572.99	1,631.01
177	175	45.30	7	26	HCL-80	LTC		7,618.29	1,585.71
178	176	45.29	7	26	HCL-80	LTC	Cent #49	7,663.58	1,540.42
179	177	45.28	7	26	HCL-80	LTC		7,708.86	1,495.14
180	178	45.58	7	26	HCL-80	LTC		7,754.44	1,449.56
181	179	45.59	7	26	HCL-80	LTC		7,800.03	1,403.97
182	180	45.60	7	26	HCL-80	LTC	Cent #50	7,845.63	1,358.37
183	181	45.62	7	26	HCL-80	LTC		7,891.25	1,312.75
184	182	45.61	7	26	HCL-80	LTC		7,936.86	1,267.14
185	183	45.68	7	26	HCL-80	LTC		7,982.54	1,221.46
186	184	45.62	7	26	HCL-80	LTC	Cent #51	8,028.16	1,175.84
187	185	45.59	7	26	HCL-80	LTC		8,073.75	1,130.25
188	186	45.59	7	26	HCL-80	LTC		8,119.34	1,084.66
189	187	45.61	7	26	HCL-80	LTC		8,164.95	1,039.05
190	188	45.62	7	26	HCL-80	LTC	Cent #52	8,210.57	993.43
191	189	45.83	7	26	HCL-80	LTC		8,256.4	947.60
192	190	45.64	7	26	HCL-80	LTC		8,302.04	901.96
193	191	45.60	7	26	HCL-80	LTC		8,347.64	856.36
194	192	45.68	7	26	HCL-80	LTC	Cent #53	8,393.32	810.68
195	193	45.58	7	26	HCL-80	LTC		8,438.9	765.10
196	194	45.57	7	26	HCL-80	LTC		8,484.47	719.53
198	195	45.56	7	26	HCL-80	LTC		8,530.03	673.97
199	196	45.55	7	26	HCL-80	LTC	Cent #54	8,575.58	628.42
200	197	45.56	7	26	HCL-80	LTC		8,621.14	582.86
201	198	45.78	7	26	HCL-80	LTC		8,666.92	537.08
202	199	45.60	7	26	HCL-80	LTC		8,712.52	491.48
203	200	45.57	7	26	HCL-80	LTC	Cent #55	8,758.09	445.91
204	201	45.55	7	26	HCL-80	LTC		8,803.64	400.36
205	202	45.79	7	26	HCL-80	LTC		8,849.43	354.57
206	203	45.82	7	26	HCL-80	LTC		8,895.25	308.75
207	204	45.78	7	26	HCL-80	LTC	Cent #56	8,941.03	262.97
208	205	45.58	7	26	HCL-80	LTC		8,986.61	217.39
209	206	45.59	7	26	HCL-80	LTC		9,032.2	171.80
210	207	45.80	7	26	HCL-80	LTC		9,078	126.00
211	208	45.57	7	26	HCL-80	LTC	Cent #57	9,123.57	80.43
212	209	45.70	7	26	HCL-80	LTC		9,169.27	34.73
	Hanger	10.50	7	26	HCL-80	LTC		9,179.77	24.23
	LD Joint	25.00	7	26	HCL-80	LTC		9,204.77	-0.77
		Out							
213	1	45.57							
214	2	45.58							
215	3	45.28							
216	4	45.58							
217	5	45.58							
218	6	45.57							
219	7	45.57							
220	8	45.55							
221	9	45.58							



Linam AGI #2 production casing cementing



Linam AGI #2 production casing cementing



Dispatch Report for i-District Job: 2030595

Customer Name: Parsons Brinckerhoff	Person Taking Call: Lorena/Selena	Location: Hobbs, NM WS	Province: Not Applicable	Order Date: 9/25/2014	Job Number: 2030595
Service Order Number: D3RM-00245	Service Line: Cement	Supervisor:		Legal Location:	
Well Name and Number: Linam #2 -	Pad/Platform:	Field: Red Hills West	County:	State/Prov:	
Well Master Number:	API/UWI:	Rig Name: PRECISION #107	Well Age:	Sales Engineer: Perono, Fred	
Job Type: Cement - 7" Production Casing	Time Well Ready: 12/12/2014 12:00 AM	Deviation: 0 deg	Hole Size: 8.5 in	Well MD: 9100 ft	
Well TVD: 9100 ft	BHP: 3900 psi	BHST: 154 °F	BHCT: 136 °F	Treat Down: Casing	
Packer Type:	Packer Depth: 0 in	Well Head Connection: Conventional	HHP on Location: 197.04 hhp	Max Allowed Pressure: 5000 psi	
Max Allowed Ann Pressure: 5500 psi		No of Stages/SubJobs:	FTL Ticket/Quote Number :		
Expected on Location:	Ready to Pump:	Job Start Date: 12/12/2014 3:30 AM	Job End Date: 12/13/2014 3:30 AM		
Rig Up Time:		Rig Down Time:			
Client Contact					
Name	Voice	Fax	Email	Title	Company
Roger Ramos					
Resources					
Personnel	Equipment 1	Equipment 2	Assignment	Note	
		2CSS14883 - 2CSS14883	12/12/2014 3:30 AM - 12/13/2014 3:30 AM	#1-435SX 2ND STG TAIL (LT07) HAULED BY LAZARUS 12/11/14RK.	
	2TRAL35371 - 2TRAL35371	2CTF26189 - 2CTF26189	12/12/2014 3:30 AM - 12/13/2014 3:30 AM	LOADED WITH 175SX EVERCRETE 12/10/14RK.	
	2TRAL51623 - 2TRAL51623	2CTF50320 - 2CTF50320	12/12/2014 3:30 AM - 12/13/2014 3:30 AM	LOADED WITH (F)- 1ST STG MPE (B)- 2ND STG MPE. 12-11-14ATR	
	2TRAL27690 - 2TRAL27690	2CTF27182 HYD - 2CTF27182	12/12/2014 3:30 AM - 12/13/2014 3:30 AM	LOADED WITH 290SXS 2ND STG TAIL. 12-11-14ATR	
	2TRAL51627 - 2TRAL51627	2CTF50319 - 2CTF50319	12/12/2014 3:30 AM - 12/13/2014 3:30 AM	LOADED WITH 145SXS 2ND STG TAIL. 12-11-14ATR	
Casing/Tubing					
String Type	Depth	Size	Weight	Grade	Thread
Casing	9100 ft	7 in	26 lb/ft	P-110 - Specs to be confirmed by FC	Specs to be confirmed by FC
Service Instructions: Cement 7" Production casing as per design and company rep.					

Perforations				
Top	Bottom	SPF	No of Shots	Formation Name
Total Interval:		Diameter:		
Notes: Take Batchmixer				
Directions:				
Materials				
Name	Code	Description	Quantity	Note
D206	D206	Antifoaming Agent D206	25 gal	For Spacer, to be determine by Lab

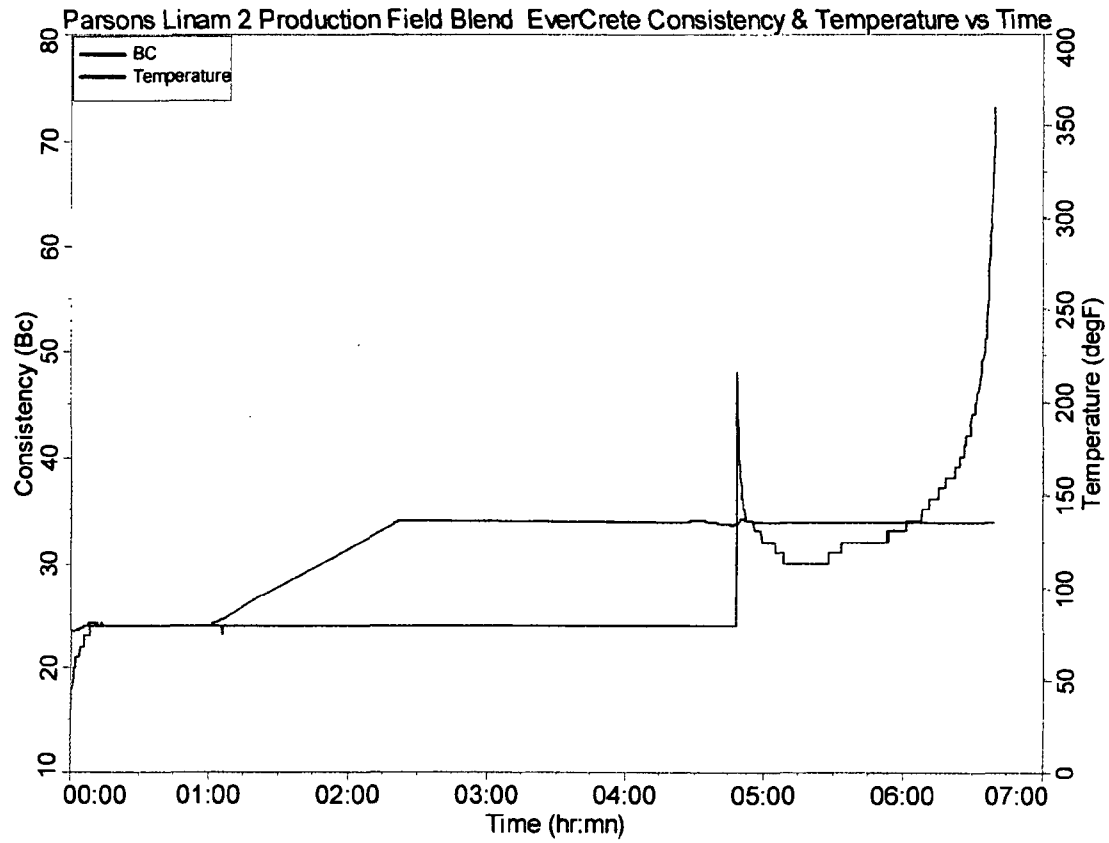
Fluid Systems:

MPE Stg1 AND STG 2				
Load with highlighted excess For Both stgs 25 for each stg				
Sacks Of:	Cement	Total Blend/Cem:		
Sack Weight:		Dry Blend Code:		
Yield:		Final Fluid Density:	12 lb/gal	
Mix Water:		Base Fluid Den:	8.33 lb/mgal	
Mix Fluid:		Volume:	50 bbl	
Mix Water Den:		Base Fluid Vol:	1000 gal	
Sacks Blend/Cem:		Acid Volume:		
Total Mix Water:		Acid Conc:		
Total Mix Fluid:				
Load out Excess				
Code	Conc	Design	Total by design	Load out with excess
B389	1 lb/bbl	BWOSpacerV O	50 lb	75 lb
D206	0.2 gal/bbl	BVOSpacerV O	10 gal	15 gal
D031	199.89 lb/bbl	BWOSpacerV O	9994.5 lb	15000 lb

2CTF 50320 was already loaded with 75lbs B389 and 1536 lb of D031, Have the Bulk Plant add Barite to meet the above volumes.

16 ppg EverCRETE STG 1				
207 sks EverCRETE STG 1				
LOADED 157 SKS				
LACKING 50 SKS				
Sacks Of:	Cement	Total Blend/Cem:	20700 lb	
Sack Weight:	100 lb	Dry Blend Code:		
Yield:	1.12 ft3/sk	Final Fluid Density:	16 lb/gal	
Mix Water:	3.48 ft3/sk	Base Fluid Den:		
Mix Fluid:	3.54 ft3/sk	Volume:	31.3 bbl	
Mix Water Den:	8.33 lb/gal	Base Fluid Vol:		
Sacks Blend/Cem:	207 sks	Acid Volume:		
Total Mix Water:	720.36 ft3	Acid Conc:		
Total Mix Fluid:	732.78 ft3			
		Load out Excess		
Code	Conc	Design	Total by design	Load out with excess
D189A	29 lb/sk	WTSK	6003 lb	6003 lb
S100	59 lb/sk	WTSK	12213 lb	12213 lb
D195	2 lb/sk	WTSK	414 lb	414 lb
D178	10 lb/sk	WTSK	2070 lb	2070 lb
D065	0.2 %	BWOB	41.4 lb	41.4 lb
D167	0.3 %	BWOB	62.1 lb	62.1 lb
D174	4.35 %	BWOB	900.45 lb	900.45 lb
D206	0.02 gal/sk	VOLSACK	4.14 gal	4.14 gal
D177	0.04 gal/sk	VOLSACK	8.28 gal	8.28 gal

13.2 ppg Tail STG 2				
870 sks STG 2				
LOADED 870 SKS				
Sacks Of:	Cement	Total Blend/Cem:	65250 lb	
Sack Weight:	75 lb	Dry Blend Code:		
Yield:	1.34 ft3/sk	Final Fluid Density:	13.2 lb/gal	
Mix Water:	6.76 ft3/sk	Base Fluid Den:		
Mix Fluid:	6.76 ft3/sk	Volume:	207.4 bbl	
Mix Water Den:	8.33 lb/gal	Base Fluid Vol:		
Sacks Blend/Cem:	870 sks	Acid Volume:		
Total Mix Water:	5881.2 gal	Acid Conc:		
Total Mix Fluid:				
		Load out Excess		
Code	Conc	Design	Total by design	Load out with excess
D049	75 lb/sk	WTSK	65250 lb	65250 lb
D046	0.2 %	BWOC	130.5 lb	130.5 lb
D013	0.4 %	BWOC	261 lb	261 lb
D065	0.2 %	BWOC	130.5 lb	130.5 lb
D020	0.5 %	BWOC	326.25 lb	326.25 lb



*Location water = 0 mg/L of Chloride

Parsons Linam 2 Production Field Blend Tail

Fluid No : HNM14C677004	Client : Parsons	Location / Rig : Lea	Signatures
Date : Dec-11-2014	Well Name : Linam #2	Field :	P. Quintana, LT1 K. Hamburg

Job Type	Production	Depth	8100.0 ft	TVD	8100.0 ft
BHST	146 degF	BHCT	125 degF	BHP	4970 psi
Starting Temp.	80 degF	Time to Temp.	00:46 hr:mn	Heating Rate	0.98 degF/min
Starting Pressure	555 psi	Time to Pressure	00:46 hr:mn	Schedule	9.6-1

Composition

Slurry Density	13.20 lb/gal	Yield	1.34 ft ³ /sk	Mix Fluid	6.757 gal/sk
Solid Vol. Fraction	32.5 %	Porosity	67.5 %	Slurry type	Conventional
Code	Concentration	Sack Reference	Component	Blend Density	Lot Number
D049		75 lb of BLEND	Blend	176.05 lb/ft ³	FB3088
Fresh water	6.757 gal/sk		Base Fluid		Tap
D046	0.200 %BWOC		Antifoam		CW4J0265A1
D013	0.400 %BWOC		Retarder		KB08E155296
D065	0.200 %BWOC		Dispersant		BA17DP22
D020	0.500 %BWOC		Extender		Bulk

Rheology

Temperature	80 degF			125 degF		
(rpm)	Up (deg)	Down (deg)	Average (deg)	Up (deg)	Down (deg)	Average (deg)
300	17.0	17.0	17.0	63.0	63.0	63.0
200	14.0	13.0	13.5	56.0	51.0	53.5
100	11.0	10.0	10.5	47.0	42.0	44.5
60	8.0	7.0	7.5	40.0	39.0	39.5
30	6.0	6.0	6.0	36.0	34.0	35.0
6	5.0	5.0	5.0	20.0	19.0	19.5
3	4.0	3.0	3.5	16.0	15.0	15.5
10 sec Gel	4 deg - 4.27 lb/100ft ²			18 deg - 19.21 lb/100ft ²		
10 min Gel	9 deg - 9.61 lb/100ft ²			18 deg - 19.21 lb/100ft ²		
Rheo. computed	Viscosity : 12.322 cP Yield Point : 5.25 lb/100ft ²			Viscosity : 30.465 cP Yield Point : 33.10 lb/100ft ²		

Thickening Time

Consistency	Time
POD :	02:58 hr:mn
30 Bc	03:45 hr:mn
50 Bc	04:34 hr:mn
70 Bc	04:43 hr:mn

UCA Compressive Strength

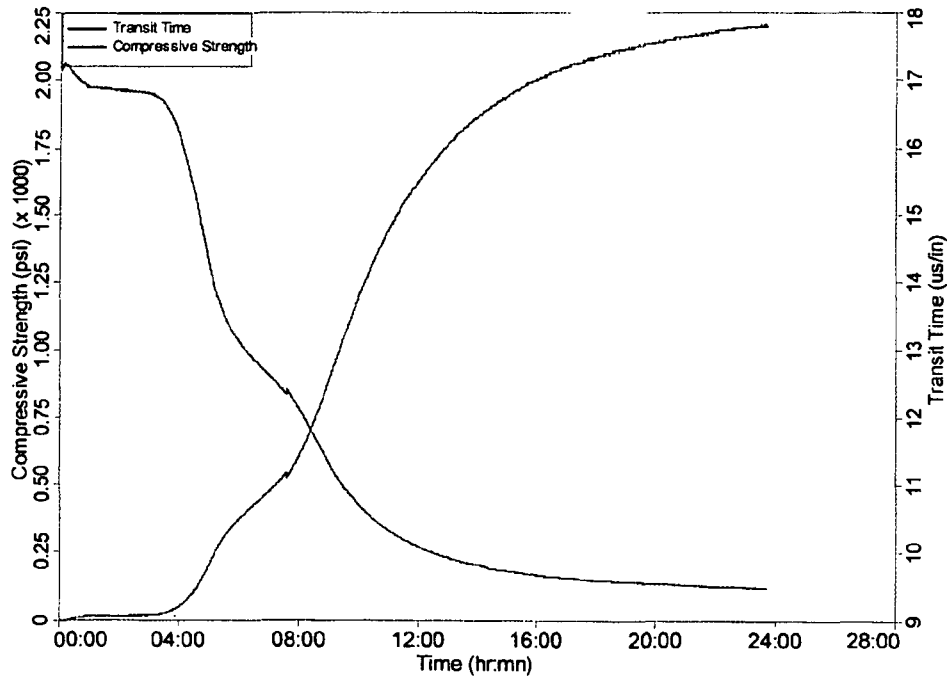
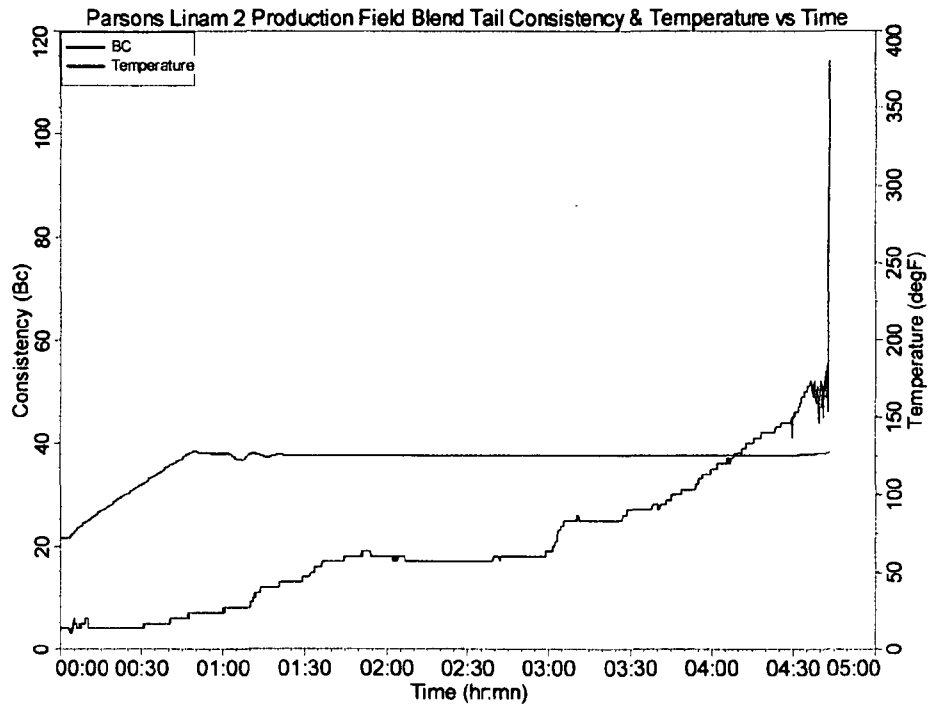
Time	CS
04:03 hr:mn	50 psi
07:15 hr:mn	500 psi
12:00 hr:mn	1626 psi
23:00 hr:mn	2191 psi

Free Fluid

0.0 mL/250mL in 2 hrs
At 125 degF and 0 deg incl
Sedimentation : None

Comments

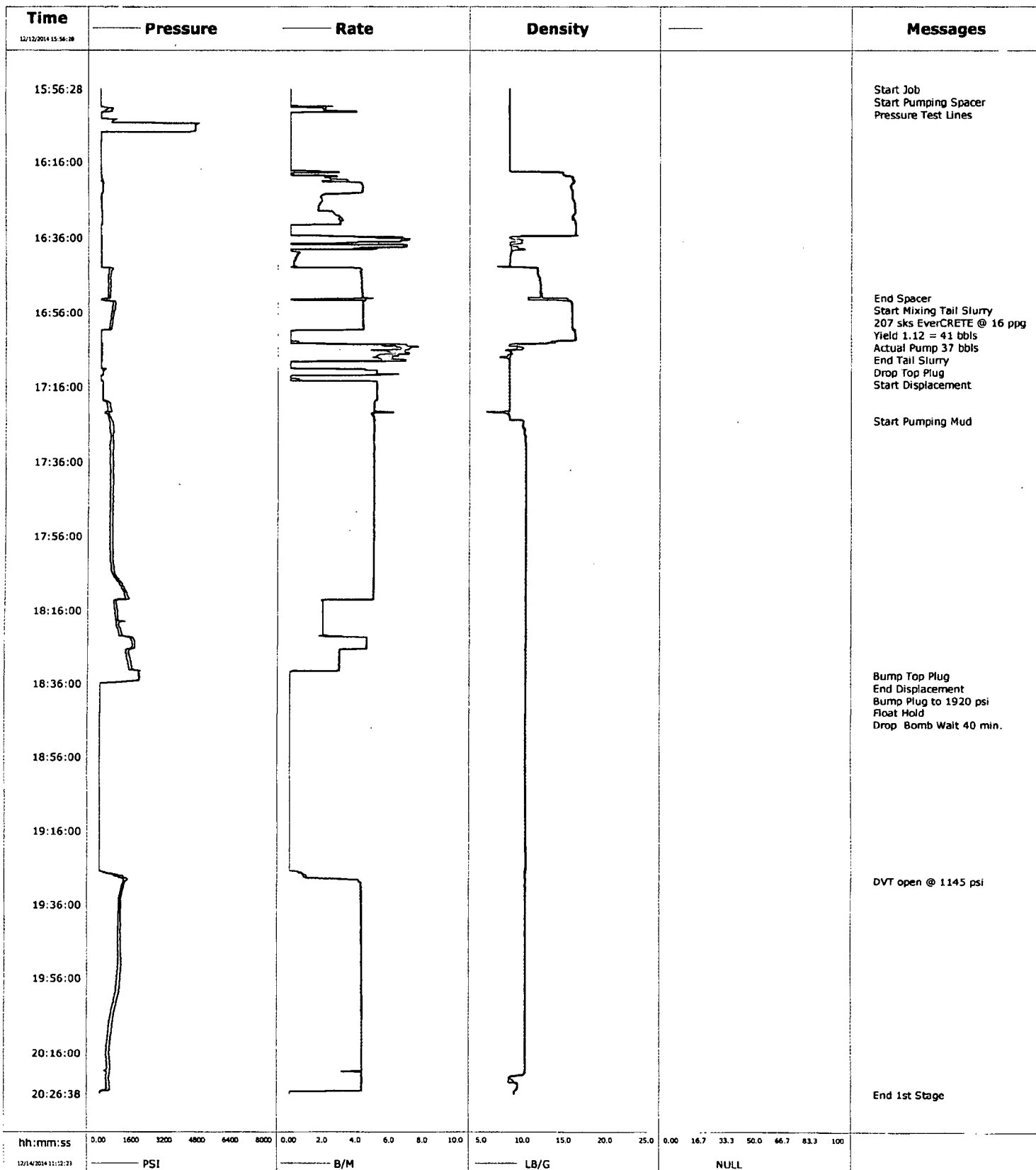
Thickening Time Comment : Go/NoGo: 10min@51min
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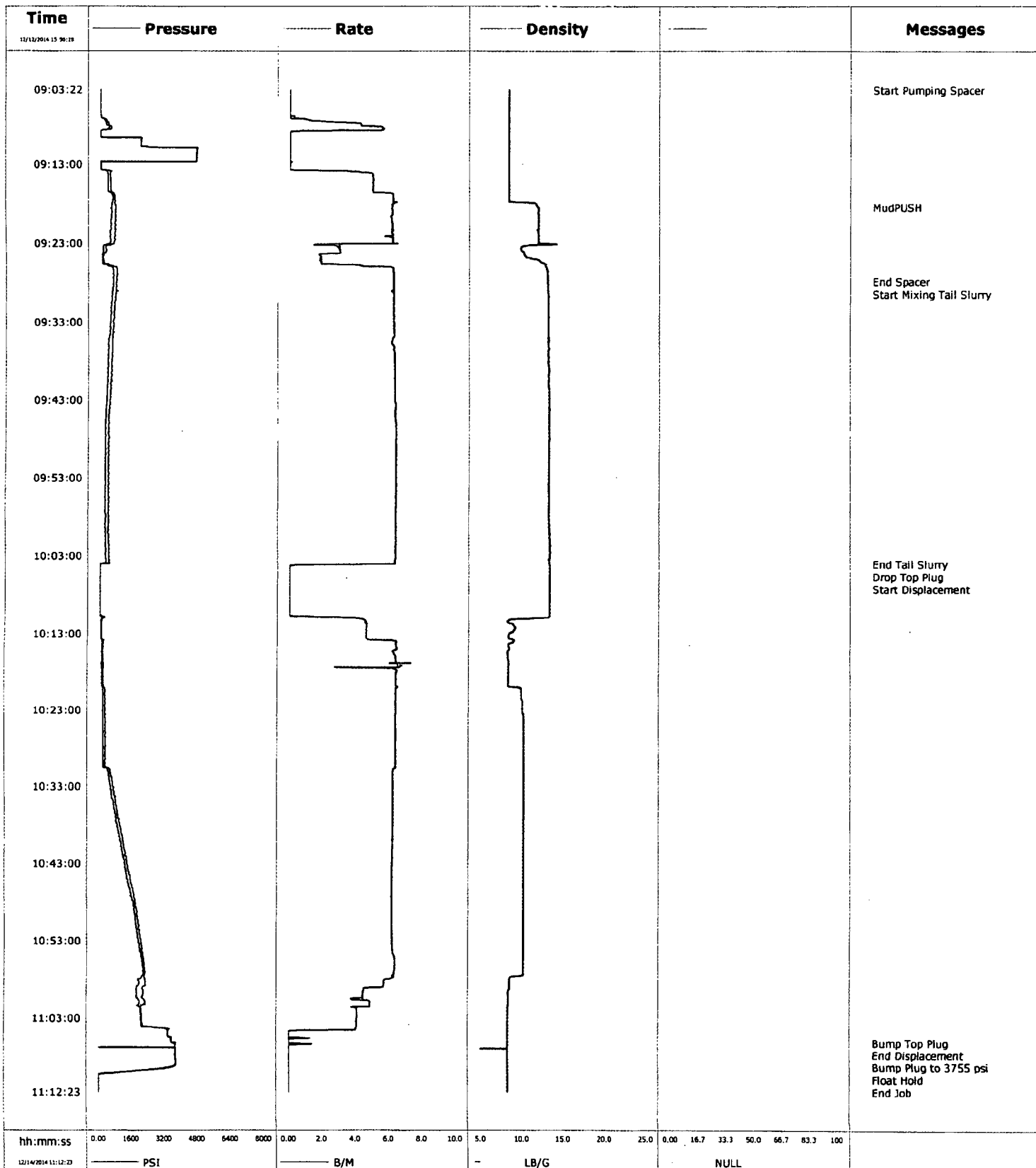
Well	Linam	Client	Parsons Brinkerhoff
Field	Red Hills West	SIR No.	D3RM-00245
Engineer	Jose Carmona	Job Type	7" Production
Country	United States	Job Date	12-12-2014

Time	Pressure	Rate	Density		Messages
12/12/2014 15:56:28					
15:56:28					Start Job Start Pumping Spacer Pressure Test Lines
16:26:00					
16:56:00					End Spacer Start Mixing Tail Slurry 207 sks EverCRETE @ 16 ppq Yield 1.12 = 41 bbls Actual Pump 37 bbls End Tail Slurry Drop Top Plug Start Displacement Start Pumping Mud
17:26:00					
17:56:00					
18:26:00					Bump Top Plug End Displacement Bump Plug to 1920 psi Float Hold Drop Bomb Wait 40 min.
18:56:00					
19:26:00					DVT open @ 1145 psi
19:56:00					
20:27:18					End 1st Stage Stopped Acquisition
09:00:46					Start Pumping Spacer
09:36:00					MudPUSH End Spacer Start Mixing Tail Slurry
10:11:00					End Tail Slurry Drop Top Plug Start Displacement
10:46:00					
11:12:23					Bump Top Plug End Displacement Bump Plug to 3755 psi Float Hold
hh:mm:ss	0.00 1600 3200 4800 6400 8000	0.00 2.0 4.0 6.0 8.0 10.0	5.0 10.0 15.0 20.0 25.0	0.00 16.7 33.3 50.0 66.7 83.3 100	
12/14/2014 13:12:23	PSI	B/M	LB/G	NULL	

Well	Linam	Client	Parsons Brinkerhoff
Field	Red Hills West	SIR No.	D3RM-00245
Engineer	Jose Carmona	Job Type	1st Stage
Country	United States	Job Date	12-12-2014



Well	Linam	Client	Parsons Brinkerhoff
Field	Red Hills West	SIR No.	D3RM-00245
Engineer	Jose Carmona	Job Type	2nd Stage
Country	United States	Job Date	12-12-2014



				Customer Parsons Brinkerhoff		Job Number D3RM-00245	
Well Unam 2		Location (legal)		Schlumberger Location Hobbs NM.		Job Start Dec/12/2014	
Field Red Hills West		Formation Name/Type		Deviation deg		Well MD 9204.0 ft	
County Lead		State/Province New Mexico		BHP psi		Well TVD 9204.0 ft	
Well Master 0631589525		API/UWI 30-025-42139		BHST 154 degF		BHCT 136 degF	
Rig Name Precision #107		Drilled For Oil & Gas		Service Via Land		Casing/Liner	
Offshore Zone		Well Class New		Well Type Development		Pore Press. Gradient lb/gal	
Drilling Fluid Type		Max. Density lb/gal		Plastic Viscosity CP		T/D	
Service Line Cementing		Job Type 7" Production		Depth, ft 9204.0		Size, in 7.0	
Max. Allowed Tub. Press psi		Max. Allowed Ann. Press psi		WH Connection Single Cement head		Weight, lb/ft 26.0	
Service Instructions Cement 7" Production Casing 1st Tail 207 sks @ 16 ppg Yield 1.12 = 41 bbls 2nd Tail 970 sks @ 13.2 ppg Yield 1.34 = 231 bbls 1st Stage Got MudPUSH Spacer back to surface 2nd Stage 30 bbls back to surface = 125 sks		Perforations/Open Hole		Grade N80		Thread 8RD	
		Top, ft		Bottom, ft		shot/ft	
		ft		ft		No. of Shots	
		ft		ft		Total Interval ft	
		ft		ft		Diameter in	
Treat Down Casing		Displacement 351.0 bbl		Packer Type		Packer Depth ft	
Tubing Vol. bbl		Casing Vol. 353.0 bbl		Annular Vol. bbl		Openhole Vol. bbl	
Casing/Tubing Secured ☒		1 Hole Vol. Circulated prior to Cement ☒		Casing Tools		Squeeze Job	
Lift Pressure psi		Shoe Type Guide		Squeeze Type			
Pipe Rotated ☐		Pipe Reciprocated ☐		Shoe Depth 9204.0 ft		Tool Type	
No. Centralizers		Top Plugs		Bottom Plugs		Tool Depth ft	
Cement Head Type Single		Stage Tool Type DVT		Stage Tool Depth 8092.0 ft		Tail Pipe Size in	
Job Scheduled For Dec/12/2014		Arrived on Location Dec/12/2014		Leave Location Dec/12/2014		Tail Pipe Depth ft	
				Collar Type Float		Sqz. Total Vol. bbl	
				Collar Depth 9156.0 ft			
Date	Time 24-hr clock	Treating Pressure PSI	Flow Rate B/M	Density LB/G	Volume BBL	Message	
12/12/2014	15:56:28	13	0.0	8.33	0.0	Started Acquisition	
12/12/2014	15:56:33	13	0.0	8.33	0.0	Start Job	
12/12/2014	15:56:34	13	0.0	8.33	0.0	Start Pumping Spacer	
12/12/2014	15:56:37	14	0.0	8.33	0.0	Pressure Test Lines	
12/12/2014	15:59:48	10	0.0	8.33	0.0		
12/12/2014	16:03:08	64	0.0	8.33	3.3		
12/12/2014	16:06:28	4619	0.0	8.33	3.3		
12/12/2014	16:09:48	57	0.0	8.33	3.3		
12/12/2014	16:13:08	7	0.0	8.33	3.3		
12/12/2014	16:16:28	4	0.0	8.33	3.3		
12/12/2014	16:19:48	56	2.5	15.26	4.7		
12/12/2014	16:23:08	130	4.3	15.80	16.4		
12/12/2014	16:26:28	51	1.9	16.08	26.0		
12/12/2014	16:29:48	88	2.6	16.24	32.4		
12/12/2014	16:33:08	2	0.0	16.37	41.0		
12/12/2014	16:36:28	67	7.1	9.05	45.4		
12/12/2014	16:39:48	8	0.3	8.71	60.5		
12/12/2014	16:43:08	55	0.2	8.44	61.6		
12/12/2014	16:46:28	424	4.3	11.85	71.4		
12/12/2014	16:49:48	457	4.3	12.08	85.7		
12/12/2014	16:52:27	127	4.4	13.92	97.1	End Spacer	

Well	Field	Job Start	Customer	Job Number	Message
12/12/2014	Unam 2	Red Hills West	Parsons Brinkerhoff	D3RM-00245	
Date	Time 24-hr clock	Flow Rate B/M	Density LB/G	Volume BBL	
12/12/2014	16:52:40	44	1.3	97.7	207 SKS EVERCRETE @ 16 PPG
12/12/2014	16:53:08	485	4.4	98.4	
12/12/2014	16:53:11	601	4.4	98.6	Yield 1.12 = 41 bbls
12/12/2014	16:56:28	595	4.4	112.9	
12/12/2014	16:59:48	552	4.4	127.4	
12/12/2014	17:00:27	514	4.4	130.3	Actual Pump 37 bbls
12/12/2014	17:01:07	28	0.1	132.6	End Tail Slurry
12/12/2014	17:01:09	26	0.0	132.6	Drop Top Plug
12/12/2014	17:01:10	26	0.0	132.6	Start Displacement
12/12/2014	17:03:08	23	0.0	132.6	
12/12/2014	17:06:28	24	6.8	145.2	
12/12/2014	17:09:48	9	0.0	162.6	
12/12/2014	17:13:08	11	3.1	171.9	
12/12/2014	17:16:28	119	5.2	181.6	
12/12/2014	17:19:48	205	5.1	198.9	
12/12/2014	17:23:08	340	5.0	215.9	
12/12/2014	17:25:16	480	5.0	226.6	Start Pumping Mud
12/12/2014	17:26:28	593	5.0	232.6	
12/12/2014	17:29:48	550	5.0	249.4	
12/12/2014	17:33:08	551	5.0	266.1	
12/12/2014	17:36:28	500	5.0	282.9	
12/12/2014	17:39:48	507	5.0	299.7	
12/12/2014	17:43:08	500	5.0	316.5	
12/12/2014	17:46:28	490	5.0	333.3	
12/12/2014	17:49:48	500	5.0	350.0	
12/12/2014	17:53:08	502	5.0	366.8	
12/12/2014	17:56:28	494	5.0	383.6	
12/12/2014	17:59:48	520	5.0	400.4	
12/12/2014	18:03:08	514	5.0	417.2	
12/12/2014	18:06:28	655	5.0	433.9	
12/12/2014	18:09:48	1102	5.0	450.7	
12/12/2014	18:13:08	927	2.2	467.2	
12/12/2014	18:16:28	791	2.0	473.8	
12/12/2014	18:19:48	791	2.0	480.5	
12/12/2014	18:23:08	1127	2.7	487.1	
12/12/2014	18:26:28	1661	4.6	502.2	
12/12/2014	18:29:48	1455	3.0	512.9	
12/12/2014	18:33:08	1916	0.0	521.6	
12/12/2014	18:33:36	1919	0.0	521.6	Bump Top Plug
12/12/2014	18:33:37	1919	0.0	521.6	End Displacement
12/12/2014	18:33:53	1919	0.0	521.6	Bump Plug to 1920 psi
12/12/2014	18:36:15	11	0.0	521.6	Float Hold
12/12/2014	18:36:28	10	0.0	521.6	
12/12/2014	18:38:05	7	0.0	521.6	Drop Bomb Wait 40 min.
12/12/2014	18:39:48	9	0.0	521.6	
12/12/2014	18:43:08	9	0.0	521.6	
12/12/2014	18:46:28	8	0.0	521.6	
12/12/2014	18:49:48	8	0.0	521.6	
12/12/2014	18:53:08	9	0.0	521.6	
12/12/2014	18:56:28	8	0.0	521.6	
12/12/2014	18:59:48	8	0.0	521.6	
12/12/2014	19:03:08	8	0.0	521.6	
12/12/2014	19:06:28	8	0.0	521.6	
12/12/2014	19:09:48	9	0.0	521.6	

Well	Field	Job Start	Customer	Job Number	Message
Lnarm 2	Red Hills West	Dec/12/2014	Parsons Brinkerhoff	D3RM-00245	
Date	Time 24-hr clock	Treating Pressure PSI	Flow Rate B/M	Density LB/G	Volume BBL
12/12/2014	19:16:28	9	0.0	10.41	521.6
12/12/2014	19:19:48	9	0.0	10.41	521.6
12/12/2014	19:23:08	9	0.0	10.42	521.6
12/12/2014	19:26:28	7	0.0	10.42	521.6
12/12/2014	19:29:04	1307	3.8	10.40	524.1
12/12/2014	19:29:48	1226	4.2	10.36	527.1
12/12/2014	19:33:08	1043	4.3	10.37	541.5
12/12/2014	19:36:28	1035	4.3	10.37	555.8
12/12/2014	19:39:48	959	4.3	10.36	570.2
12/12/2014	19:43:08	994	4.3	10.36	584.6
12/12/2014	19:46:28	993	4.3	10.36	599.0
12/12/2014	19:49:48	999	4.3	10.36	613.4
12/12/2014	19:53:08	970	4.3	10.36	627.8
12/12/2014	19:56:28	1036	4.3	10.36	642.2
12/12/2014	19:59:48	906	4.3	10.36	656.7
12/12/2014	20:03:08	669	4.3	10.36	671.1
12/12/2014	20:06:28	588	4.3	10.36	685.6
12/12/2014	20:09:48	490	4.4	10.36	700.1
12/12/2014	20:13:08	535	4.4	10.36	714.6
12/12/2014	20:16:28	450	4.4	10.36	729.1
12/12/2014	20:19:48	512	4.4	10.36	743.6
12/12/2014	20:23:08	415	4.3	8.50	758.0
12/12/2014	20:26:28	70	0.0	9.05	770.2
12/12/2014	20:26:35	71	0.0	9.06	770.2
12/12/2014	09:03:24	3	0.0	8.36	0.0
12/14/2014	09:06:28	19	0.0	8.36	0.0
12/14/2014	09:09:48	2007	0.0	8.36	0.0
12/14/2014	09:13:08	27	0.0	8.35	5.8
12/14/2014	09:16:28	404	5.0	8.34	18.3
12/14/2014	09:18:31	576	6.1	11.79	30.8
12/14/2014	09:19:48	518	6.1	11.90	38.6
12/14/2014	09:23:08	585	6.2	11.92	59.0
12/14/2014	09:26:28	646	6.2	12.95	69.0
12/14/2014	09:28:02	751	6.2	13.05	78.7
12/14/2014	09:28:04	742	6.2	13.05	78.9
12/14/2014	09:29:48	550	6.2	13.13	89.7
12/14/2014	09:33:08	530	6.2	13.17	110.5
12/14/2014	09:36:28	418	6.3	13.23	131.2
12/14/2014	09:39:48	413	6.3	13.20	152.1
12/14/2014	09:43:08	396	6.3	13.21	173.1
12/14/2014	09:46:28	350	6.3	13.22	194.1
12/14/2014	09:49:48	371	6.4	13.23	215.3
12/14/2014	09:53:08	375	6.4	13.21	236.5
12/14/2014	09:56:28	347	6.4	13.21	257.7
12/14/2014	09:59:48	411	6.4	13.30	278.9
12/14/2014	10:03:08	425	6.3	13.36	300.1
12/14/2014	10:04:05	429	6.3	13.26	306.1
12/14/2014	10:04:06	231	6.3	13.26	306.2
12/14/2014	10:06:28	12	0.0	13.34	306.7
12/14/2014	10:09:48	13	0.0	13.36	306.7
12/14/2014	10:13:08	108	4.6	8.38	316.9
12/14/2014	10:16:28	142	6.4	8.33	336.6
12/14/2014	10:19:48	159	6.4	8.37	357.8
12/14/2014	10:23:08	262	6.4	10.10	379.1

Well		Field		Job Start		Customer		Job Number	
Linam 2		Red Hills West		Dec/12/2014		Parsons Brinkerhoff		D3RM-00245	
Date	Time 24-hr clock	Treating Pressure PSI	Flow Rate B/M	Density LB/G	Volume BBL	Message			
12/14/2014	10:29:48	263	6.4	10.25	421.5				
12/14/2014	10:33:08	691	6.2	10.25	442.4				
12/14/2014	10:36:28	873	6.2	10.25	463.1				
12/14/2014	10:39:48	1148	6.2	10.25	483.8				
12/14/2014	10:43:08	1372	6.2	10.25	504.5				
12/14/2014	10:46:28	1673	6.2	10.25	525.0				
12/14/2014	10:49:48	1855	6.2	10.25	545.6				
12/14/2014	10:53:08	2028	6.2	10.24	566.2				
12/14/2014	10:56:28	2222	6.3	10.24	587.1				
12/14/2014	10:59:48	2176	4.4	8.39	606.0				
12/14/2014	11:03:08	2089	4.1	8.36	620.4				
12/14/2014	11:05:58	3556	0.0	8.34	626.2	Bump Top Plug			
12/14/2014	11:06:28	3755	0.0	8.34	626.3				
12/14/2014	11:06:36	3756	0.0	8.34	626.3	Bump Plug to 3755 psi			
12/14/2014	11:09:48	1984	0.0	8.34	626.3				
12/14/2014	11:10:18	3	0.0	8.34	626.3	Float Hold			

Post Job Summary

Average Pump Rates, bbl/min					Volume of Fluid Injected, bbl			
Slurry	N2	Mud	Maximum Rate	Total Slurry	Mud	Spacer	N2	
5.8			7.3	626.3	0.0	78.7		
Treating Pressure Summary, psi					Breakdown Fluid			
Maximum	Final	Average	Bump Plug to	Breakdown	Type	Volume	Density	
4749	1	856	3755		FreshWater	20.0 bbl	8.34 lb/gal	
Avg. N2 Percent	Designed Slurry Volume	Displacement	Mix Water Temp	Cement Circulated to Surface?	☒	Volume	30.0 bbl	
%	272.0 bbl	320.1 bbl	degF	Washed Thru Perfs	☐	To	ft	
Customer or Authorized Representative		Schlumberger Supervisor		Circulation Lost	☐	Job Completed ☒		
		Jose Carmona						