

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

APPLICATION FOR PERMIT TO DRILL OR REENTER

HOBBS, OGD
OCD Hobbs

MAY 26 2015

RECEIVED

ATS-15-115

FORM APPROVED
OMB No. 1004-0137
Expires October 31, 2014

1a. Type of work: ☒ DRILL ☐ REENTER		5. Lease Serial No. NMNM113964
1b. Type of Well: ☒ Oil Well ☐ Gas Well ☐ Other ☒ Single Zone ☐ Multiple Zone		6. If Indian, Allottee or Tribe Name (H)
2. Name of Operator Devon Energy Production Company, L.P. (6137)		7. If Unit or CA Agreement, Name and No.
3a. Address 333 W. Sheridan Oklahoma City, OK 73102-5010	3b. Phone No. (include area code) 405.228.7203	8. Lease Name and Well No. Paint 33 Fed 2H (314753)
4. Location of Well (Report location clearly and in accordance with any State requirements *) At surface 200 FSL & 1980 FWL, Unit N PP: 200 FSL & 1370 FWL At proposed prod. zone 330 FNL & 1980 FWL, Unit C		9. API Well No. 30-025-42591 (9789)
10. Field and Pool, or Exploratory WC-025 G-06 5253206M; BS		11. Sec., T. R. M. or Blk. and Survey or Area Sec. 33 T24S R32E
14. Distance in miles and direction from nearest town or post office* Approximately 23 miles SE of Malaga, NM		12. County or Parish Lea County
15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) See attached map		13. State NM
16. No. of acres in lease NMNM113964 - 360 ac		17. Spacing Unit dedicated to this well 160 ac
18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. See attached map		20. BLM/BIA Bond No. on file CO-1104; NBM-000801
21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3493.1' GL		22. Approximate date work will start* 04/20/2014
		23. Estimated duration 45 Days

24. Attachments

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, must be attached to this form:

1. Well plat certified by a registered surveyor.
2. A Drilling Plan.
3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO must be filed with the appropriate Forest Service Office).
4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).
5. Operator certification
6. Such other site specific information and/or plans as may be required by the BLM.

25. Signature <i>Trina C. Couch</i>	Name (Printed/Typed) Trina C. Couch	Date 10/17/2014
Title Regulatory Analyst		

Approved by (Signature) Steve Caffey	Name (Printed/Typed)	Date MAY 18 2015
Title FIELD MANAGER		
Office CARLSBAD FIELD OFFICE		

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Conditions of approval, if any, are attached.

APPROVAL FOR TWO YEARS

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 2)

*(Instructions on page 2)

Carlsbad Controlled Water Basin

KZ
05/26/15

Approval Subject to General Requirements
& Special Stipulations Attached

SEE ATTACHED FOR
CONDITIONS OF APPROVAL

MAY 26 2015

Devon Energy, Paint 33 Fed 2H

HOBBS OCD

MAY 26 2015

1. Geologic Formations

RECEIVED

TVD of target	10,602'	Pilot hole depth	N/A
MD at TD:	15,435'	Deepest expected fresh water:	

Basin

Formation	Depth (TVD) from KB	Water/Mineral Bearing/ Target Zone?	Hazards*
Rustler	965		
Top of Salt	1,125		
Base of Salt	4,490		
Lamar	4,520		
Bell Canyon	4,690		
Cherry Canyon	5,420		
Brushy Canyon	7,100		
Bone Spring	8,530		
1 st Bone Spring Sand	9,630		
2 nd Bone Spring Lime	9,850		
2 nd Bone Spring Sand	10,250		
Wolfcamp	11,750		

*H2S, water flows, loss of circulation, abnormal pressures, etc.

Devon Energy, Paint 33 Fed 2H

2. Casing Program

See COP

Hole Size	Casing Interval		Csg. Size	Weight (lbs)	Grade	Conn	SF Collapse	SF Burst	SF Tension
	From	To							
17.5"	0	1,000' 275'	13.375"	48	H40	STC	1.72	3.87	11.27
12.25"	0	4,000'	9.625"	40	J55	BTC	1.77	1.65	4.33
12.25"	4,000'	4,600'	9.625"	40	HCK-55	BTC	1.24	1.90	3.25
8.75"	0	15,435'	5.5"	17	HCP-110	BTC	1.66	2.06	3.10
BLM Minimum Safety Factor							1.10	1.10	1.6 Dry 1.8 Wet

All casing strings will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.h

Must have table for contingency casing

	Y or N
Is casing new? If used, attach certification as required in Onshore Order #1	Y
Does casing meet API specifications? If no, attach casing specification sheet.	Y
Is premium or uncommon casing planned? If yes attach casing specification sheet.	N
Does the above casing design meet or exceed BLM's minimum standards? If not provide justification (loading assumptions, casing design criteria).	Y
Will the intermediate pipe be kept at a minimum 1/3 fluid filled to avoid approaching the collapse pressure rating of the casing?	Y
Is well located within Capitan Reef?	N
If yes, does production casing cement tie back a minimum of 50' above the Reef?	
Is well within the designated 4 string boundary.	
Is well located in SOPA but not in R-111-P?	N
If yes, are the first 2 strings cemented to surface and 3 rd string cement tied back 500' into previous casing?	
Is well located in R-111-P and SOPA?	N
If yes, are the first three strings cemented to surface?	
Is 2 nd string set 100' to 600' below the base of salt?	
Is well located in high Cave/Karst?	N
If yes, are there two strings cemented to surface?	
(For 2 string wells) If yes, is there a contingency casing if lost circulation occurs?	
Is well located in critical Cave/Karst?	N
If yes, are there three strings cemented to surface?	

Devon Energy, Paint 33 Fed 2H

3. Cementing Program

Casing	# Sks	Wt. lb/gal	H ₂ O gal/sk	Yld ft ³ /sack	500# Comp. Strength (hours)	Slurry Description
Surf.	1080	14.8	6.32	1.33	7	Tail: Class C Cement + 0.125 lbs/sack Poly-E-Flake
Inter.	980	12.9	9.81	1.85	17	Lead: (65:35) Class C Cement: Poz (Fly Ash): 6% BWOC Bentonite + 5% BWOW Sodium Chloride + 0.125 lbs/sack Poly-E-Flake
	430	14.8	6.32	1.33	6	Tail: Class C Cement + 0.125 lbs/sack Poly-E-Flake
Prod.	890	12.5	10.86	1.96	30	1 st Lead: (65:35) Class H Cement: Poz (Fly Ash) + 6% BWOC Bentonite + 0.25% BWOC HR-601 + 0.125 lbs/sack Poly-E-Flake
	1380	14.5	5.31	1.2	25	1 st Tail: (50:50) Class H Cement: Poz (Fly Ash) + 0.5% bwoc HALAD-344 + 0.4% bwoc CFR-3 + 0.2% BWOC HR-601 + 2% bwoc Bentonite
	DV/ECP Tool 4700'					
	20	11	14.81	2.55	22	2 nd stage Lead: Tuned Light® Cement + 0.125 lb/sk Pol-E-Flake
	110	14.8	6.32	1.33	6	2 nd stage Tail: Class C Cement + 0.125 lbs/sack Poly-E-Flake

DV tool depth(s) will be adjusted based on hole conditions and cement volumes will be adjusted proportionally. DV tool will be set a minimum of 50 feet below previous casing and a minimum of 200 feet above current shoe. Lab reports with the 500 psi compressive strength time for the cement will be onsite for review.

Casing String	TOC	% Excess
Surface	0'	100%
Intermediate	0'	75%
Production	1 st Stage = 4700' / 2 nd Stage = 4100'	25%

Devon Energy, Paint 33 Fed 2H

4. Pressure Control Equipment

N	A variance is requested for the use of a diverter on the surface casing. See attached for schematic.
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BOP installed and tested before drilling which hole?	Size?	Min. Required WP	Type	✓	Tested to:
12-1/4"	13-5/8"	3M	Annular	x	50% of working pressure
			Blind Ram		3M
			Pipe Ram		
			Double Ram	x	
			Other*		
8-3/4"	13-5/8"	3M	Annular	x	50% testing pressure
			Blind Ram		3M
			Pipe Ram		
			Double Ram	x	
			Other*		
			Annular		
			Blind Ram		
			Pipe Ram		
			Double Ram		
			Other*		

*Specify if additional ram is utilized.

BOP/BOPE will be tested by an independent service company to 250 psi low and the high pressure indicated above per Onshore Order 2 requirements. The System may be upgraded to a higher pressure but still tested to the working pressure listed in the table above. If the system is upgraded all the components installed will be functional and tested.

Pipe rams will be operationally checked each 24 hour period. Blind rams will be operationally checked on each trip out of the hole. These checks will be noted on the daily tour sheets. Other accessories to the BOP equipment will include a Kelly cock and floor safety valve (inside BOP) and choke lines and choke manifold. See attached schematics.

Y	Formation integrity test will be performed per Onshore Order #2. On Exploratory wells or on that portion of any well approved for a 5M BOPE system or greater, a pressure integrity test of each casing shoe shall be performed. Will be tested in accordance with Onshore Oil and Gas Order #2 III.B.1.i.
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Devon Energy, Paint 33 Fed 2H

See Conf

Y	A variance is requested for the use of a flexible choke line from the BOP to Choke Manifold. See attached for specs and hydrostatic test chart.
Y	Are anchors required by manufacturer?
Y	A multibowl wellhead is being used. The BOP will be tested per Onshore Order #2 after installation on the surface casing which will cover testing requirements for a maximum of 30 days. If any seal subject to test pressure is broken the system must be tested. Devon proposes using a multi-bowl wellhead assembly (FMC Uni-head). This assembly will only be tested when installed on the surface casing. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be 3000 (3M) psi. - Wellhead will be installed by FMC's representatives. - If the welding is performed by a third party, the FMC's representative will monitor the temperature to verify that it does not exceed the maximum temperature of the seal. - FMC representative will install the test plug for the initial BOP test. - FMC will install a solid steel body pack-off to completely isolate the lower head after cementing intermediate casing. After installation of the pack-off, the pack-off and the lower flange will be tested to 5M, as shown on the attached schematic. Everything above the pack-off will not have been altered whatsoever from the initial nipple up. Therefore the BOP components will not be retested at that time. - If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head will be cut and top out operations will be conducted. - Devon will pressure test all seals above and below the mandrel (but still above the casing) to full working pressure rating. - Devon will test the casing to 0.22 psi/ft or 1500 psi, whichever is greater, as per Onshore Order #2. After running the 13-3/8" surface casing, a 13-5/8" BOP/BOPE system with a minimum rating of 3M will be installed on the FMC Uni-head wellhead system and will undergo a 250 psi low pressure test followed by a 3,000 psi high pressure test. The 3,000 psi high and 250 psi low test will cover testing requirements a maximum of 30 days, as per Onshore Order #2. If the well is not complete within 30 days of this BOP test, another full BOP test will be conducted, as per Onshore Order #2. After running the 9-5/8' intermediate casing with a mandrel hanger, the 13-5/8" BOP/BOPE system with a minimum rating of 3M will already be installed on the FMC Uni-head. The pipe rams will be operated and checked each 24 hour period and each time the drill pipe is out of the hole. These tests will be logged in the daily driller's log. A 2" kill line and 3" choke line will be incorporated into the drilling spool below the ram BOP. In addition to the rams and annular preventer, additional BOP accessories include a kelly cock, floor safety valve, choke lines, and choke manifold rated at 3,000 psi WP.

See Conf

Devon Energy, Paint 33 Fed 2H

	Devon requests a variance to use a flexible line with flanged ends between the BOP and the choke manifold (choke line). The line will be kept as straight as possible with minimal turns
	See attached schematic.

*See
COR*

5. Mud Program

Depth		Type	Weight (ppg)	Viscosity	Water Loss
From	To				
0	1,000' 275'	FW Gel	8.6-8.8	28-34	N/C
1,000'	4,600'	Saturated Brine	10.0-10.2	28-34	N/C
4,600'	15,435'	Cut Brine	8.5-9.3	28-34	N/C

Sufficient mud materials to maintain mud properties and meet minimum lost circulation and weight increase requirements will be kept on location at all times.

What will be used to monitor the loss or gain of fluid?	PVT/Pason/Visual Monitoring
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6. Logging and Testing Procedures

Logging, Coring and Testing	
x	Will run GR/CNL from TD to surface (horizontal well – vertical portion of hole). Stated logs run will be in the Completion Report and submitted to the BLM.
	No Logs are planned based on well control or offset log information.
	Drill stem test? If yes, explain
	Coring? If yes, explain

Additional logs planned	Interval
	Resistivity
	Density
X	CBL
X	Mud log
	PEX

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7. Drilling Conditions

Condition	Specify what type and where?
BH Pressure at deepest TVD	4771 psi
Abnormal Temperature	No

Mitigation measure for abnormal conditions. Describe. Lost circulation material/sweeps/mud scavengers.

Hydrogen Sulfide (H2S) monitors will be installed prior to drilling out the surface shoe. If H2S is detected in concentrations greater than 100 ppm, the operator will comply with the provisions of Onshore Oil and Gas Order #6. If Hydrogen Sulfide is encountered, measured values and formations will be provided to the BLM.

N	H2S is present
Y	H2S Plan attached

8. Other facets of operation

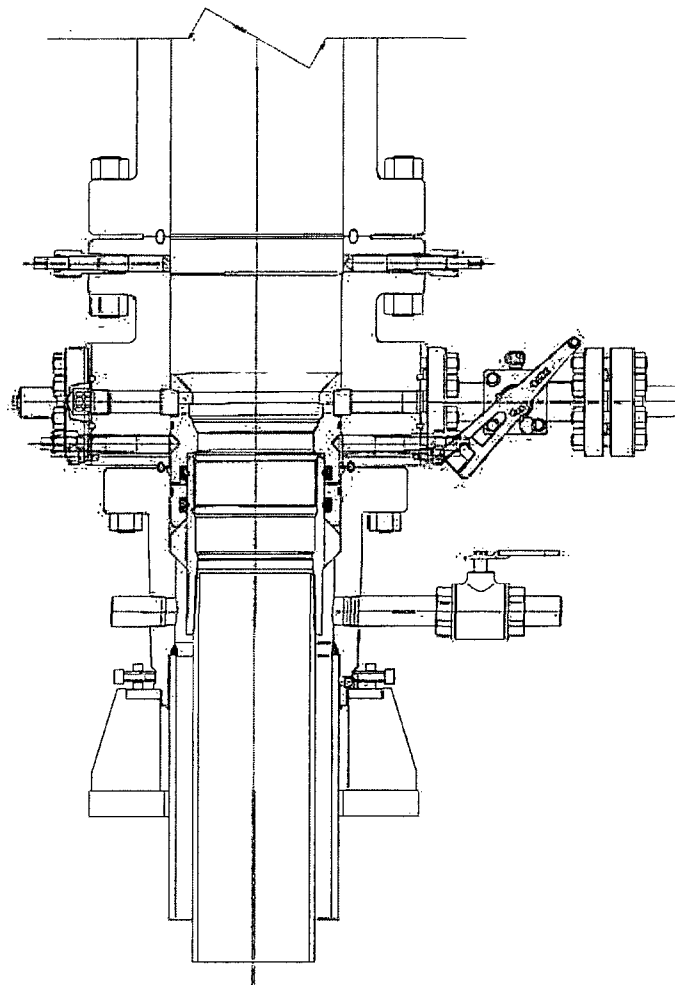
Is this a walking operation? No.

Will be pre-setting casing? No.

Attachments

☒ Directional Plan

☐ Other, describe



PRIMARY MODE

DEVON ENERGY

ARTESIA

S.E.N.M

13 3/8 X 9 5/8

QUOTE LAYOUT
F18648
REF: DM100161737
DM100151315

PRIVATE AND CONFIDENTIAL

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REVISIONS

A	05-08-13
B	1-22-14
C	5-13-14

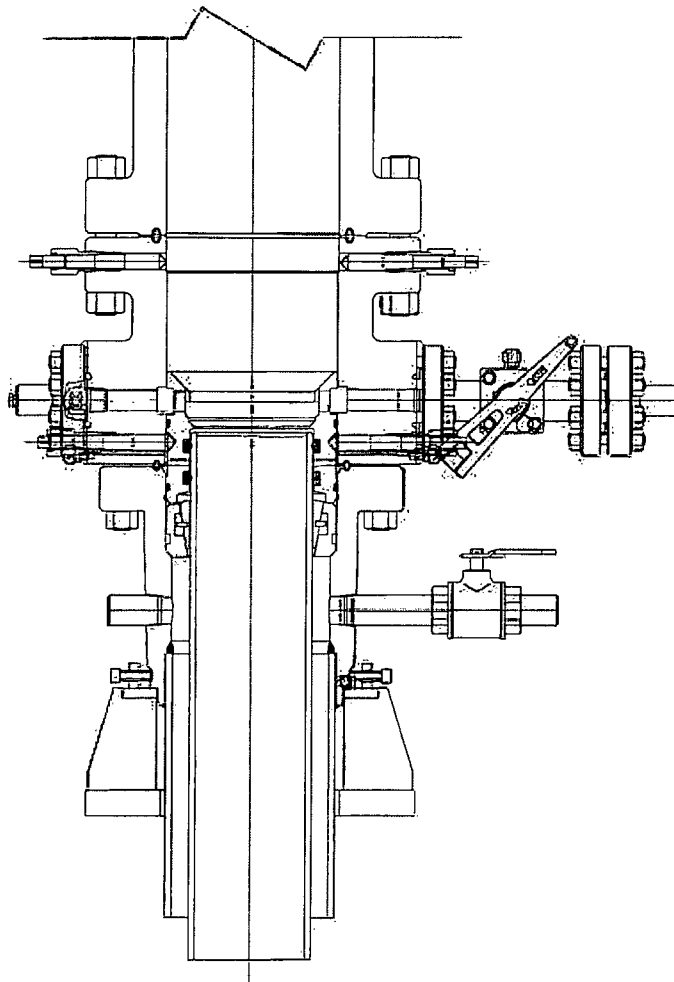
DESCRIPTION

SURFACE WELLHEAD LAYOUT
UNIHEAD, UH-1, SOW,
DEVON ENERGY, ODESSA

DRAWN BY	K. VU	05-08-13
DRAFTING REVIEW	Z. MARQUEZ	05-08-13
DESIGN REVIEW	K. TAHA	05-08-13
APPROVED BY	R. HAMILTON	05-08-13

FMC Technologies

DRAWING NUMBER
DM100161771-2A



CONTINGENCY MODE

DEVON ENERGY
ARTESIA
S.E.N.M
13 3/8 X 9 5/8

QUOTE LAYOUT
F18648
REF: DM100161737
DM100151315

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	A 05-08-13	SURFACE WELLHEAD LAYOUT UNIHEAD, UH-1, SOW, DEVON ENERGY, ODESSA	DESIGNED BY	K. VU 05-08-13	
	B 1-22-14		DRAFTING REVIEW	Z. MARQUEZ 05-08-13	
	C 5-13-14		DESIGN REVIEW	K. TAHA 05-08-13	
			APPROVED BY	R. HAMILTON 05-08-13	

5D Plan Report**Devon Energy****Field Name:** *Lea Co, NM Nad 83 NMEZ***Site Name:** *Paint 33 Fed 2H***Well Name:** *Paint 33 Fed 2H***Plan:** *P1:V1*

04 September 2014

**Weatherford®**

Paint 33 Fed 2H

Field Name Lea Co NM Nad 83 NMEZ	Map Units : US ft		Company Name : Devon Energy	
	Vertical Reference Datum (VRD) : Mean Sea Level			
	Projected Coordinate System : NAD83 / New Mexico East (ftUS)			
Comment :				
Site Name Paint 33 Fed 2H	Units : US ft	North Reference : Grid	Convergence Angle : 0.35	
	Position	Northing : 425194.55 US ft	Latitude : 32° 10' 2.14"	
		Easting : 742962.07 US ft	Longitude : -103° 40' 54.22"	
	Elevation above Mean Sea Level : 3493.00 US ft			
Comment :				
Slot Name Paint 33 Fed 2H	Position (Offsets relative to Site Centre)			
	+N / -S : 0.00 US ft	Northing : 425194.55 US ft	Latitude : 32°10'2.14"	
	+E / -W : 0.00 US ft	Easting : 742962.07 US ft	Longitude : -103°40'54.22"	
	Slot TVD Reference : Ground Elevation			
	Elevation above Mean Sea Level : 3493.00 US ft			
Comment :				
Well Name Paint 33 Fed 2H	Type : Main well		UWI :	Plan : P1:V1
	Rig Height Kelly Bushing : 25.00 US ft		Comment :	
	Relative to Mean Sea Level : 3518.00 US ft			
	Closure Distance : 4755.9 US ft		Closure Azimuth : 359.557°	
	Vertical Section (Position of Origin Relative to Slot)			
	+N / -S : 0.00 US ft		+E / -W : 0.00 US ft	Az : 359.56°
	Magnetic Parameters			
	Model : BGGM	Field Strength :	Dec : 7.38°	Dip : 60.02° Date : 30/Nov/2014
	48204.3nT			

Target Set				
Name : Paint 33 Fed 2H		Number of Targets : 2		
Comment :				
Target Name S Tgt Shape: Gulboid	Position (Relative to Slot centre)			
	+N / -S : -150.00US ft	Northing : 425044.55 US ft	Latitude : 32°10'0.65"	
	+E / -W : 1.15 US ft	Easting : 742963.22US ft	Longitude : -103°40'54.21"	
	TVD (Kelly Bushing) : 10195.50 US ft			
	Orientation Azimuth : 0.00° Inclination : 0.00°			
Dimensions Length : 20.00 US ft		Breadth : 20.00 US ft		Height : 20.00 US ft

SD Plan Report

Target Name: PBHL 2H Shape: Cuboid	Position (Relative to Slot centre)			
	+N / -S : 4755.76US ft	Northing : 429950.31 US ft	Latitude : 32°10'49.20"	
	+E / -W : -36.78 US ft	Easting : 742925.29US ft	Longitude : -103°40'54.31"	
	TVD (Kelly Bushing) : 10783.00 US ft			
	Orientation	Azimuth : 0.00°	Inclination : 0.00°	
	Dimensions	Length : 20.00 US ft	Breadth : 20.00 US ft	Height : 20.00 US ft

Well path created using minimum curvature

Salient Points (Relative to Slot centre, TVD relative to Kelly Bushing)											Comment
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	VS (US ft)	DLS (°/100 US ft)	B. Rate (°/100 US ft)	T. Rate (°/100 US ft)	T. Face (°)	
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
8073.00	0.00	0.00	8073.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Nudge
8773.03	7.00	179.56	8771.29	-42.71	0.33	-42.71	1.00	1.00	0.00	179.56	Hold
9302.92	7.00	179.56	9297.23	-107.29	0.82	-107.29	0.00	0.00	0.00	0.00	Drop
10002.95	0.00	0.00	9995.52	-150.00	1.15	-150.00	1.00	-1.00	0.00	180.00	Hold
10202.45	0.00	0.00	10195.02	-150.00	1.15	-150.00	0.00	0.00	0.00	0.00	KOP
11100.46	89.80	359.56	10767.97	420.96	-3.26	420.97	10.00	10.00	0.00	359.56	LP
15435.42	89.80	359.56	10783.00	4755.76	-36.78	4755.90	0.00	0.00	0.00	0.00	PBHL 2H

Interpolated Points (Relative to Slot centre, TVD relative to Kelly Bushing)											Comment
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	VS (US ft)	DLS (°/100 US ft)	Northing (US ft)	Easting (US ft)		
8000.00	0.00	0.00	8000.00	0.00	0.00	0.00	0.00	425194.55	742962.07		
8073.00	0.00	0.00	8073.00	0.00	0.00	0.00	0.00	425194.55	742962.07		Nudge
8100.00	0.27	179.56	8100.00	-0.06	0.00	-0.06	1.00	425194.49	742962.07		
8200.00	1.27	179.56	8199.99	-1.41	0.01	-1.41	1.00	425193.14	742962.08		
8300.00	2.27	179.56	8299.94	-4.50	0.03	-4.50	1.00	425190.05	742962.10		
8400.00	3.27	179.56	8399.82	-9.33	0.07	-9.33	1.00	425185.22	742962.14		
8500.00	4.27	179.56	8499.60	-15.90	0.12	-15.90	1.00	425178.65	742962.19		
8600.00	5.27	179.56	8599.26	-24.22	0.19	-24.22	1.00	425170.33	742962.26		
8700.00	6.27	179.56	8698.75	-34.27	0.26	-34.27	1.00	425160.28	742962.33		
8773.03	7.00	179.56	8771.29	-42.71	0.33	-42.71	1.00	425151.84	742962.40		Hold
8800.00	7.00	179.56	8798.06	-46.00	0.35	-46.00	0.00	425148.55	742962.42		
8900.00	7.00	179.56	8897.31	-58.18	0.45	-58.19	0.00	425136.37	742962.52		
9000.00	7.00	179.56	8996.57	-70.37	0.54	-70.37	0.00	425124.18	742962.61		
9100.00	7.00	179.56	9095.82	-82.56	0.63	-82.56	0.00	425111.99	742962.70		
9200.00	7.00	179.56	9195.08	-94.74	0.73	-94.75	0.00	425099.81	742962.80		
9300.00	7.00	179.56	9294.33	-106.93	0.82	-106.94	0.00	425087.62	742962.89		
9302.92	7.00	179.56	9297.23	-107.29	0.82	-107.29	0.00	425087.26	742962.89		Drop
9400.00	6.03	179.56	9393.68	-118.30	0.91	-118.31	1.00	425076.25	742962.98		
9500.00	5.03	179.56	9493.21	-127.94	0.98	-127.94	1.00	425066.61	742963.05		
9600.00	4.03	179.56	9592.90	-135.83	1.04	-135.84	1.00	425058.72	742963.11		
9700.00	3.03	179.56	9692.71	-141.99	1.09	-141.99	1.00	425052.56	742963.16		
9800.00	2.03	179.56	9792.61	-146.40	1.12	-146.41	1.00	425048.15	742963.19		
9900.00	1.03	179.56	9892.57	-149.07	1.14	-149.08	1.00	425045.48	742963.21		
10000.00	0.03	179.56	9992.57	-150.00	1.15	-150.00	1.00	425044.55	742963.22		
10002.95	0.00	0.00	9995.52	-150.00	1.15	-150.00	1.00	425044.55	742963.22		Hold
10100.00	0.00	0.00	10092.57	-150.00	1.15	-150.00	0.00	425044.55	742963.22		
10200.00	0.00	0.00	10192.57	-150.00	1.15	-150.00	0.00	425044.55	742963.22		
10202.45	0.00	0.00	10195.02	-150.00	1.15	-150.00	0.00	425044.55	742963.22		KOP
10300.00	9.76	359.56	10292.10	-141.71	1.09	-141.72	10.00	425052.84	742963.16		
10400.00	19.76	359.56	10388.68	-116.28	0.89	-116.28	10.00	425078.27	742962.96		
10500.00	29.76	359.56	10479.37	-74.46	0.57	-74.46	10.00	425120.09	742962.64		
10600.00	39.76	359.56	10561.43	-17.52	0.13	-17.52	10.00	425177.03	742962.20		

5D Plan Report

Interpolated Points (Relative to Slot centre, TVD relative to Kelly Bushing)										
MD (US ft)	Inc (°)	Az (°)	TVD (US ft)	N. Offset (US ft)	E. Offset (US ft)	VS (US ft)	DLS (%/100 US ft)	Northing (US ft)	Easting (US ft)	Comment
10700.00	49.76	359.56	10632.35	52.79	-0.42	52.80	10.00	425247.34	742961.65	
10800.00	59.76	359.56	10689.98	134.36	-1.05	134.36	10.00	425328.91	742961.02	
10900.00	69.76	359.56	10732.58	224.69	-1.75	224.70	10.00	425419.24	742960.32	
11000.00	79.76	359.56	10758.84	321.05	-2.49	321.05	10.00	425515.60	742959.58	
11100.00	89.76	359.56	10767.97	420.50	-3.26	420.51	10.00	425615.05	742958.81	
11100.46	89.80	359.56	10767.97	420.96	-3.26	420.97	10.00	425615.51	742958.81	LP
11200.00	89.80	359.56	10768.32	520.49	-4.03	520.51	0.00	425715.04	742958.04	
11300.00	89.80	359.56	10768.66	620.49	-4.81	620.51	0.00	425815.04	742957.26	
11400.00	89.80	359.56	10769.01	720.49	-5.58	720.51	0.00	425915.04	742956.49	
11500.00	89.80	359.56	10769.36	820.48	-6.35	820.51	0.00	426015.03	742955.72	
11600.00	89.80	359.56	10769.70	920.48	-7.13	920.51	0.00	426115.03	742954.94	
11700.00	89.80	359.56	10770.05	1020.48	-7.90	1020.51	0.00	426215.03	742954.17	
11800.00	89.80	359.56	10770.40	1120.47	-8.67	1120.51	0.00	426315.02	742953.40	
11900.00	89.80	359.56	10770.74	1220.47	-9.44	1220.50	0.00	426415.02	742952.63	
12000.00	89.80	359.56	10771.09	1320.46	-10.22	1320.50	0.00	426515.01	742951.85	
12100.00	89.80	359.56	10771.44	1420.46	-10.99	1420.50	0.00	426615.01	742951.08	
12200.00	89.80	359.56	10771.78	1520.46	-11.76	1520.50	0.00	426715.01	742950.31	
12300.00	89.80	359.56	10772.13	1620.45	-12.54	1620.50	0.00	426815.00	742949.53	
12400.00	89.80	359.56	10772.48	1720.45	-13.31	1720.50	0.00	426915.00	742948.76	
12500.00	89.80	359.56	10772.82	1820.45	-14.08	1820.50	0.00	427015.00	742947.99	
12600.00	89.80	359.56	10773.17	1920.44	-14.86	1920.50	0.00	427114.99	742947.21	
12700.00	89.80	359.56	10773.52	2020.44	-15.63	2020.50	0.00	427214.99	742946.44	
12800.00	89.80	359.56	10773.86	2120.44	-16.40	2120.50	0.00	427314.99	742945.67	
12900.00	89.80	359.56	10774.21	2220.43	-17.18	2220.50	0.00	427414.98	742944.89	
13000.00	89.80	359.56	10774.56	2320.43	-17.95	2320.50	0.00	427514.98	742944.12	
13100.00	89.80	359.56	10774.90	2420.43	-18.72	2420.50	0.00	427614.98	742943.35	
13200.00	89.80	359.56	10775.25	2520.42	-19.50	2520.50	0.00	427714.97	742942.57	
13300.00	89.80	359.56	10775.60	2620.42	-20.27	2620.50	0.00	427814.97	742941.80	
13400.00	89.80	359.56	10775.94	2720.41	-21.04	2720.50	0.00	427914.96	742941.03	
13500.00	89.80	359.56	10776.29	2820.41	-21.82	2820.50	0.00	428014.96	742940.25	
13600.00	89.80	359.56	10776.64	2920.41	-22.59	2920.49	0.00	428114.96	742939.48	
13700.00	89.80	359.56	10776.98	3020.40	-23.36	3020.49	0.00	428214.95	742938.71	
13800.00	89.80	359.56	10777.33	3120.40	-24.14	3120.49	0.00	428314.95	742937.93	
13900.00	89.80	359.56	10777.68	3220.40	-24.91	3220.49	0.00	428414.95	742937.16	
14000.00	89.80	359.56	10778.02	3320.39	-25.68	3320.49	0.00	428514.94	742936.39	
14100.00	89.80	359.56	10778.37	3420.39	-26.45	3420.49	0.00	428614.94	742935.62	
14200.00	89.80	359.56	10778.72	3520.39	-27.23	3520.49	0.00	428714.94	742934.84	
14300.00	89.80	359.56	10779.06	3620.38	-28.00	3620.49	0.00	428814.93	742934.07	
14400.00	89.80	359.56	10779.41	3720.38	-28.77	3720.49	0.00	428914.93	742933.30	
14500.00	89.80	359.56	10779.76	3820.38	-29.55	3820.49	0.00	429014.93	742932.52	
14600.00	89.80	359.56	10780.10	3920.37	-30.32	3920.49	0.00	429114.92	742931.75	
14700.00	89.80	359.56	10780.45	4020.37	-31.09	4020.49	0.00	429214.92	742930.98	
14800.00	89.80	359.56	10780.80	4120.36	-31.87	4120.49	0.00	429314.91	742930.20	
14900.00	89.80	359.56	10781.14	4220.36	-32.64	4220.49	0.00	429414.91	742929.43	
15000.00	89.80	359.56	10781.49	4320.36	-33.41	4320.49	0.00	429514.91	742928.66	
15100.00	89.80	359.56	10781.84	4420.35	-34.19	4420.49	0.00	429614.90	742927.88	
15200.00	89.80	359.56	10782.18	4520.35	-34.96	4520.49	0.00	429714.90	742927.11	
15300.00	89.80	359.56	10782.53	4620.35	-35.73	4620.48	0.00	429814.90	742926.34	
15400.00	89.80	359.56	10782.88	4720.34	-36.51	4720.48	0.00	429914.89	742925.56	
15435.42	89.80	359.56	10783.00	4755.76	-36.78	4755.90	0.00	429950.31	742925.29	PBHL 2H

5D Anti-Collision Report**Devon Energy****Field Name:** *Lea Co, NM Nad 83 NMEZ***Site Name:** *Paint 33 Fed 2H***Well Name:** *Paint 33 Fed 2H*

04 September 2014

**Weatherford®**


Weatherford
Paint 33 Fed 2H

Field Name Lea Co. NM Nad 83 NMEZ	Map Units : US ft		Company Name : Devon Energy	
	Vertical Reference Datum (VRD) : Mean Sea Level			
	Projected Coordinate System : NAD83 / New Mexico East (ftUS)			
Comment :				
Site Name Paint 33 Fed 2H	Units : US ft	North Reference : Grid	Convergence Angle : 0.35	
	Position	Northing : 425194.55 US ft	Latitude : 32° 10' 2.14"	
		Easting : 742962.07 US ft	Longitude : -103° 40' 54.22"	
Elevation above Mean Sea Level : 3493.00 US ft				
Comment :				
Slot Name Paint 33 Fed 2H	Position (Offsets relative to Site Centre)			
	+N / -S : 0.00 US ft	Northing : 425194.55 US ft	Latitude : 32° 10' 2.14"	
	+E / -W : 0.00 US ft	Easting : 742962.07 US ft	Longitude : -103° 40' 54.22"	
	Slot TVD Reference : Ground Elevation			
	Elevation above Mean Sea Level : 3493.00 US ft			
Comment :				
Well Name Paint 33 Fed 2H	Type : Main well		UWI :	Plan : Working Plan
	Rig Height <i>Kelly Bushing</i> : 25.00 US ft		Comment :	
	Relative to Mean Sea Level : 3518.00 US ft			
	Closure Distance : 4755.9 US ft		Closure Azimuth : 359.557°	
	Vertical Section (Position of Origin Relative to Slot)			
	+N / -S : 0.00 US ft		+E / -W : 0.00 US ft	Az : 359.56°
	Magnetic Parameters			
	Model : BGGM	Field Strength : 48204.3nT	Dec : 7.38°	Dip : 60.02°
				Date : 30/Nov/2014

Collision / Uncertainty Analysis				
Primary Well	Start MD (US ft)	End MD (US ft)	Collision Risk Interval	No. of Std Deviations in Error Computation
Paint 33 Fed 2H (p)	0.00	15435.42	100.00	2

Secondary Well Names
Cotton Draw 33 Fed 2H (p)

Anti-Collision Report Terminology
S.Minor, S.Major : Radii of the ellipse of uncertainty at the current location as seen in the along hole direction.
PHI : Angle between high-side vector and semi-minor axis
TVD Spread : Total TVD range of the ellipsoid of uncertainty at the current location
ES : Distance between the extremities of the primary and secondary uncertainty ellipsoids in the direction Cr-Cr
T.Face to Sec : Angle between the Hi-Side vector of the primary well at the current location and line of closest approach between the two wells

Separation factors calculated using Pedal Curve (Independent Uncertainty) Well path created using minimum curvature.

5D Anti-Collision Report

Anti-Collision Proximity Summary (TVD relative to Kelly Bushing)

Secondary Well Name	Pri MD (US ft)	Sec MD (US ft)	TVD (US ft)	CC (US ft)	ES (US ft)	SF	Risk
Cotton Draw 33 Fed 2H (p)	8696.48	13208.84	8695.25	164.54	122.34	3.90	

Primary Well: Paint 33 Fed 2H (p) (TVD Relative to Kelly Bushing) All Azimuth Relative to GRID NORTH									
MD (US ft)	TVD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	Nearest Well	CC (US ft)	ES (US ft)	SF	Risk
0.00	0.00	351.95	0.00	0.00	Cotton Draw 33 Fed 2H (p)	4798.77	4798.05	6638.28	
100.00	100.00	351.95	0.11	0.11	Cotton Draw 33 Fed 2H (p)	4796.10	4795.26	5715.39	
200.00	200.00	351.95	0.34	0.34	Cotton Draw 33 Fed 2H (p)	4795.47	4794.36	4326.28	
300.00	300.00	351.95	0.56	0.56	Cotton Draw 33 Fed 2H (p)	4795.47	4794.00	3268.89	
400.00	400.00	351.95	0.79	0.79	Cotton Draw 33 Fed 2H (p)	4795.47	4793.56	2520.61	
500.00	500.00	351.95	1.01	1.01	Cotton Draw 33 Fed 2H (p)	4795.47	4793.12	2042.53	
600.00	600.00	351.95	1.24	1.24	Cotton Draw 33 Fed 2H (p)	4795.47	4792.67	1715.58	
700.00	700.00	351.95	1.46	1.46	Cotton Draw 33 Fed 2H (p)	4795.47	4792.22	1478.50	
800.00	800.00	351.95	1.69	1.69	Cotton Draw 33 Fed 2H (p)	4795.47	4791.77	1298.86	
900.00	900.00	351.95	1.91	1.91	Cotton Draw 33 Fed 2H (p)	4795.47	4791.32	1158.08	
1000.00	1000.00	351.95	2.14	2.14	Cotton Draw 33 Fed 2H (p)	4795.47	4790.88	1044.80	
1100.00	1100.00	351.95	2.36	2.36	Cotton Draw 33 Fed 2H (p)	4795.47	4790.43	951.70	
1200.00	1200.00	351.95	2.59	2.59	Cotton Draw 33 Fed 2H (p)	4795.47	4789.98	873.82	
1300.00	1300.00	351.95	2.81	2.81	Cotton Draw 33 Fed 2H (p)	4795.47	4789.53	807.72	
1400.00	1400.00	351.95	3.03	3.03	Cotton Draw 33 Fed 2H (p)	4795.47	4789.08	750.91	
1500.00	1500.00	351.95	3.26	3.26	Cotton Draw 33 Fed 2H (p)	4795.47	4788.63	701.56	
1600.00	1600.00	351.95	3.48	3.48	Cotton Draw 33 Fed 2H (p)	4795.47	4788.18	658.30	
1700.00	1700.00	351.95	3.71	3.71	Cotton Draw 33 Fed 2H (p)	4795.47	4787.73	620.06	
1800.00	1800.00	351.95	3.93	3.93	Cotton Draw 33 Fed 2H (p)	4795.47	4787.28	586.02	
1900.00	1900.00	351.95	4.16	4.16	Cotton Draw 33 Fed 2H (p)	4795.47	4786.83	555.53	
2000.00	2000.00	351.95	4.38	4.38	Cotton Draw 33 Fed 2H (p)	4795.47	4786.38	528.05	
2100.00	2100.00	351.95	4.61	4.61	Cotton Draw 33 Fed 2H (p)	4795.47	4785.93	503.16	
2200.00	2200.00	351.95	4.83	4.83	Cotton Draw 33 Fed 2H (p)	4795.47	4785.49	480.51	
2300.00	2300.00	351.95	5.06	5.06	Cotton Draw 33 Fed 2H (p)	4795.47	4785.04	459.81	
2400.00	2400.00	351.95	5.28	5.28	Cotton Draw 33 Fed 2H (p)	4795.47	4784.59	440.82	
2500.00	2500.00	351.95	5.51	5.51	Cotton Draw 33 Fed 2H (p)	4795.47	4784.14	423.33	
2600.00	2600.00	351.95	5.73	5.73	Cotton Draw 33 Fed 2H (p)	4795.47	4783.69	407.18	
2700.00	2700.00	351.95	5.96	5.96	Cotton Draw 33 Fed 2H (p)	4795.47	4783.24	392.22	
2800.00	2800.00	351.95	6.18	6.18	Cotton Draw 33 Fed 2H (p)	4795.47	4782.79	378.32	
2900.00	2900.00	351.95	6.41	6.41	Cotton Draw 33 Fed 2H (p)	4795.47	4782.34	365.37	
3000.00	3000.00	351.95	6.63	6.63	Cotton Draw 33 Fed 2H (p)	4795.47	4781.89	353.28	
3100.00	3100.00	351.95	6.86	6.86	Cotton Draw 33 Fed 2H (p)	4795.47	4781.44	341.96	

5D Anti-Collision Report

Primary Well : Paint 33 Fed 2H (p) (TVD Relative to Kelly Bushing, All Azimuth Relative to GRID NORTH)									
MD (US ft)	TVD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	Nearest Well	CC (US ft)	ES (US ft)	SF	Risk
3200.00	3200.00	351.95	7.08	7.08	Cotton Draw 33 Fed 2H (p)	4795.47	4780.99	331.34	
3300.00	3300.00	351.95	7.31	7.31	Cotton Draw 33 Fed 2H (p)	4795.47	4780.54	321.37	
3400.00	3400.00	351.95	7.53	7.53	Cotton Draw 33 Fed 2H (p)	4795.47	4780.09	311.97	
3500.00	3500.00	351.95	7.76	7.76	Cotton Draw 33 Fed 2H (p)	4795.47	4779.64	303.11	
3600.00	3600.00	351.95	7.98	7.98	Cotton Draw 33 Fed 2H (p)	4795.47	4779.20	294.74	
3700.00	3700.00	351.95	8.20	8.20	Cotton Draw 33 Fed 2H (p)	4795.47	4778.75	286.82	
3800.00	3800.00	351.95	8.43	8.43	Cotton Draw 33 Fed 2H (p)	4795.47	4778.30	279.32	
3900.00	3900.00	351.95	8.65	8.65	Cotton Draw 33 Fed 2H (p)	4795.47	4777.85	272.19	
4000.00	4000.00	359.69	8.88	8.88	Cotton Draw 33 Fed 2H (p)	4704.81	4661.84	109.50	
4100.00	4100.00	359.69	9.10	9.10	Cotton Draw 33 Fed 2H (p)	4604.85	4561.78	106.92	
4200.00	4200.00	359.69	9.33	9.33	Cotton Draw 33 Fed 2H (p)	4504.89	4461.72	104.35	
4300.00	4300.00	359.69	9.55	9.55	Cotton Draw 33 Fed 2H (p)	4404.93	4361.66	101.78	
4400.00	4400.00	359.69	9.78	9.78	Cotton Draw 33 Fed 2H (p)	4304.98	4261.59	99.23	
4500.00	4500.00	359.69	10.00	10.00	Cotton Draw 33 Fed 2H (p)	4205.02	4161.53	96.69	
4600.00	4600.00	359.69	10.23	10.23	Cotton Draw 33 Fed 2H (p)	4105.07	4061.47	94.15	
4700.00	4700.00	359.69	10.45	10.45	Cotton Draw 33 Fed 2H (p)	4005.13	3961.41	91.62	
4800.00	4800.00	359.69	10.68	10.68	Cotton Draw 33 Fed 2H (p)	3905.18	3861.35	89.11	
4900.00	4900.00	359.69	10.90	10.90	Cotton Draw 33 Fed 2H (p)	3805.24	3761.30	86.60	
5000.00	5000.00	359.69	11.13	11.13	Cotton Draw 33 Fed 2H (p)	3705.30	3661.24	84.11	
5100.00	5100.00	359.69	11.35	11.35	Cotton Draw 33 Fed 2H (p)	3605.36	3561.19	81.62	
5200.00	5200.00	359.69	11.58	11.58	Cotton Draw 33 Fed 2H (p)	3505.43	3461.14	79.14	
5300.00	5300.00	359.69	11.80	11.80	Cotton Draw 33 Fed 2H (p)	3405.50	3361.09	76.68	
5400.00	5400.00	359.69	12.03	12.03	Cotton Draw 33 Fed 2H (p)	3305.58	3261.04	74.22	
5500.00	5500.00	359.69	12.25	12.25	Cotton Draw 33 Fed 2H (p)	3205.66	3161.00	71.78	
5600.00	5600.00	359.69	12.48	12.48	Cotton Draw 33 Fed 2H (p)	3105.74	3060.96	69.35	
5700.00	5700.00	359.69	12.70	12.70	Cotton Draw 33 Fed 2H (p)	3005.83	2960.92	66.93	
5800.00	5800.00	359.69	12.93	12.93	Cotton Draw 33 Fed 2H (p)	2905.93	2860.89	64.52	
5900.00	5900.00	359.69	13.15	13.15	Cotton Draw 33 Fed 2H (p)	2806.03	2760.86	62.12	
6000.00	6000.00	359.69	13.37	13.37	Cotton Draw 33 Fed 2H (p)	2706.15	2660.84	59.73	
6100.00	6100.00	359.69	13.60	13.60	Cotton Draw 33 Fed 2H (p)	2606.27	2560.83	57.35	
6200.00	6200.00	359.69	13.82	13.82	Cotton Draw 33 Fed 2H (p)	2506.40	2460.82	54.99	
6300.00	6300.00	359.69	14.05	14.05	Cotton Draw 33 Fed 2H (p)	2406.54	2360.82	52.63	
6400.00	6400.00	359.69	14.27	14.27	Cotton Draw 33 Fed 2H (p)	2306.69	2260.83	50.29	
6500.00	6500.00	359.69	14.50	14.50	Cotton Draw 33 Fed 2H (p)	2206.86	2160.85	47.96	
6600.00	6600.00	359.69	14.72	14.72	Cotton Draw 33 Fed 2H (p)	2107.04	2060.88	45.65	
6700.00	6700.00	359.69	14.95	14.95	Cotton Draw 33 Fed 2H (p)	2007.24	1960.94	43.34	

5D Anti-Collision Report

Primary Well	Paint 33 Fed 2H (p)	(TVD Relative to Kelly Bushing)	All Azimuth Relative to GRID NORTH						
MD (US ft)	TVD (US ft)	T.Face to Sec (°)	S. Major (US ft)	S. Minor (US ft)	Nearest Well	CC (US ft)	ES (US ft)	SF	Risk
6800.00	6800.00	359.69	15.17	15.17	Cotton Draw 33 Fed 2H (p)	1907.47	1861.01	41.06	
6900.00	6900.00	359.69	15.40	15.40	Cotton Draw 33 Fed 2H (p)	1807.71	1761.10	38.78	
7000.00	7000.00	359.69	15.62	15.62	Cotton Draw 33 Fed 2H (p)	1707.99	1661.23	36.53	
7100.00	7100.00	359.69	15.85	15.85	Cotton Draw 33 Fed 2H (p)	1608.30	1561.39	34.28	
7200.00	7200.00	359.69	16.07	16.07	Cotton Draw 33 Fed 2H (p)	1508.65	1461.59	32.05	
7300.00	7300.00	359.69	16.30	16.30	Cotton Draw 33 Fed 2H (p)	1409.05	1361.84	29.84	
7400.00	7400.00	359.69	16.52	16.52	Cotton Draw 33 Fed 2H (p)	1309.52	1262.15	27.65	
7500.00	7500.00	359.69	16.75	16.75	Cotton Draw 33 Fed 2H (p)	1210.05	1162.54	25.47	
7600.00	7600.00	359.69	16.97	16.97	Cotton Draw 33 Fed 2H (p)	1110.69	1063.01	23.29	
7700.00	7700.00	359.69	17.20	17.20	Cotton Draw 33 Fed 2H (p)	1011.45	963.60	21.14	
7800.00	7800.00	359.69	17.42	17.42	Cotton Draw 33 Fed 2H (p)	912.38	864.37	19.00	
7900.00	7900.00	359.69	17.65	17.65	Cotton Draw 33 Fed 2H (p)	813.53	765.37	16.89	
8000.00	8000.00	359.69	17.87	17.87	Cotton Draw 33 Fed 2H (p)	715.00	666.67	14.79	
8100.00	8100.00	180.13	18.09	18.09	Cotton Draw 33 Fed 2H (p)	616.97	568.49	12.73	
8200.00	8199.99	180.12	18.25	18.25	Cotton Draw 33 Fed 2H (p)	520.01	471.48	10.72	
8300.00	8299.94	180.11	18.42	18.41	Cotton Draw 33 Fed 2H (p)	425.06	376.60	8.77	
8400.00	8399.82	180.11	18.59	18.56	Cotton Draw 33 Fed 2H (p)	333.86	285.84	6.95	
8500.00	8499.60	180.10	18.75	18.71	Cotton Draw 33 Fed 2H (p)	250.59	203.42	5.31	
8600.00	8599.26	180.10	18.92	18.85	Cotton Draw 33 Fed 2H (p)	186.26	141.71	4.18	
8700.00	8698.75	180.10	19.10	18.99	Cotton Draw 33 Fed 2H (p)	164.80	122.55	3.90	
8800.00	8798.06	180.10	19.27	19.13	Cotton Draw 33 Fed 2H (p)	200.44	154.14	4.33	
8900.00	8897.31	180.10	19.45	19.30	Cotton Draw 33 Fed 2H (p)	270.83	221.82	5.53	
9000.00	8996.57	180.10	19.63	19.48	Cotton Draw 33 Fed 2H (p)	355.70	305.48	7.08	
9100.00	9095.82	180.10	19.82	19.65	Cotton Draw 33 Fed 2H (p)	446.87	396.06	8.79	
9200.00	9195.08	180.10	20.01	19.83	Cotton Draw 33 Fed 2H (p)	541.17	489.94	10.56	
9300.00	9294.33	180.10	20.20	20.01	Cotton Draw 33 Fed 2H (p)	637.21	585.60	12.35	
9400.00	9393.68	180.10	20.42	20.25	Cotton Draw 33 Fed 2H (p)	734.12	682.25	14.15	
9500.00	9493.21	180.09	20.66	20.51	Cotton Draw 33 Fed 2H (p)	831.39	779.32	15.97	
9600.00	9592.90	180.08	20.89	20.76	Cotton Draw 33 Fed 2H (p)	928.89	876.59	17.76	
9700.00	9692.71	180.08	21.13	21.01	Cotton Draw 33 Fed 2H (p)	1026.53	973.99	19.54	
9800.00	9792.61	180.07	21.36	21.25	Cotton Draw 33 Fed 2H (p)	1124.24	1071.48	21.31	
9900.00	9892.57	180.06	21.59	21.48	Cotton Draw 33 Fed 2H (p)	1221.98	1169.02	23.07	
10000.00	9992.57	180.06	21.81	21.71	Cotton Draw 33 Fed 2H (p)	1319.72	1266.56	24.83	
10100.00	10092.57	359.62	22.04	21.93	Cotton Draw 33 Fed 2H (p)	1417.59	1364.20	26.55	
10200.00	10192.57	359.62	22.26	22.15	Cotton Draw 33 Fed 2H (p)	1515.74	1462.10	28.26	
10300.00	10292.10	0.03	22.46	22.17	Cotton Draw 33 Fed 2H (p)	1612.24	1558.32	29.90	

5D Anti-Collision Report

Primary Well: Paint 93 Fed 2H (p) (TVD Relative to Kelly Bushing) All Azimuth Relative to GRID (North)									
MD (US ft)	TVD (US ft)	T Face to Sec (°)	S Major (US ft)	S Minor (US ft)	Nearest Well	CC (US ft)	ES (US ft)	SF	Risk
10400.00	10388.68	0.02	22.62	21.84	Cotton Draw 33 Fed 2H (p)	1703.64	1649.47	31.45	
10500.00	10479.37	0.02	22.76	21.29	Cotton Draw 33 Fed 2H (p)	1788.16	1733.80	32.90	
10600.00	10561.43	0.01	22.90	20.47	Cotton Draw 33 Fed 2H (p)	1864.31	1809.85	34.23	
10700.00	10632.35	0.01	23.06	19.51	Cotton Draw 33 Fed 2H (p)	1930.91	1876.27	35.34	
10800.00	10689.98	0.01	23.30	18.53	Cotton Draw 33 Fed 2H (p)	1986.98	1932.26	36.31	
10900.00	10732.58	359.99	23.64	17.69	Cotton Draw 33 Fed 2H (p)	2029.58	1975.36	37.43	
11000.00	10758.84	359.97	24.06	17.20	Cotton Draw 33 Fed 2H (p)	2055.84	2002.16	38.30	
11100.00	10767.97	359.95	24.58	17.16	Cotton Draw 33 Fed 2H (p)	2064.97	2011.84	38.87	
11200.00	10768.32	359.93	25.21	17.31	Cotton Draw 33 Fed 2H (p)	2065.32	2012.73	39.27	
11300.00	10768.66	359.91	25.95	17.50	Cotton Draw 33 Fed 2H (p)	2065.66	2013.58	39.66	
11400.00	10769.01	359.89	26.79	17.71	Cotton Draw 33 Fed 2H (p)	2066.01	2014.41	40.04	
11500.00	10769.36	359.87	27.73	17.94	Cotton Draw 33 Fed 2H (p)	2066.36	2015.22	40.40	
11600.00	10769.70	359.85	28.76	18.20	Cotton Draw 33 Fed 2H (p)	2066.71	2016.00	40.75	
11700.00	10770.05	359.83	29.86	18.48	Cotton Draw 33 Fed 2H (p)	2067.06	2016.76	41.09	
11800.00	10770.40	359.81	31.03	18.80	Cotton Draw 33 Fed 2H (p)	2067.41	2017.45	41.38	
11900.00	10770.74	359.79	32.27	19.17	Cotton Draw 33 Fed 2H (p)	2067.76	2018.12	41.65	
12000.00	10771.09	359.77	33.55	19.55	Cotton Draw 33 Fed 2H (p)	2068.11	2018.76	41.91	
12100.00	10771.44	359.75	34.89	19.95	Cotton Draw 33 Fed 2H (p)	2068.46	2019.39	42.16	
12200.00	10771.78	359.73	36.27	20.35	Cotton Draw 33 Fed 2H (p)	2068.81	2020.01	42.40	
12300.00	10772.13	359.71	37.69	20.75	Cotton Draw 33 Fed 2H (p)	2069.16	2020.64	42.65	
12400.00	10772.48	359.70	39.14	21.15	Cotton Draw 33 Fed 2H (p)	2069.51	2021.25	42.89	
12500.00	10772.82	359.68	40.62	21.67	Cotton Draw 33 Fed 2H (p)	2069.86	2021.76	43.03	
12600.00	10773.17	359.66	42.13	22.09	Cotton Draw 33 Fed 2H (p)	2070.21	2022.35	43.26	
12700.00	10773.52	359.64	43.66	22.62	Cotton Draw 33 Fed 2H (p)	2070.56	2022.82	43.38	
12800.00	10773.86	359.62	45.22	23.11	Cotton Draw 33 Fed 2H (p)	2070.91	2023.33	43.52	
12900.00	10774.21	359.60	46.79	23.61	Cotton Draw 33 Fed 2H (p)	2071.26	2023.79	43.63	
13000.00	10774.56	359.58	48.38	24.10	Cotton Draw 33 Fed 2H (p)	2071.61	2024.25	43.74	
13100.00	10774.90	359.56	49.99	24.65	Cotton Draw 33 Fed 2H (p)	2071.97	2024.66	43.80	
13200.00	10775.25	359.54	51.62	25.21	Cotton Draw 33 Fed 2H (p)	2072.32	2025.04	43.83	
13300.00	10775.60	359.52	53.25	25.76	Cotton Draw 33 Fed 2H (p)	2072.67	2025.47	43.91	
13400.00	10775.94	359.50	54.90	26.25	Cotton Draw 33 Fed 2H (p)	2073.02	2025.90	43.99	
13500.00	10776.29	359.48	56.56	26.85	Cotton Draw 33 Fed 2H (p)	2073.38	2026.22	43.97	
13600.00	10776.64	359.46	58.23	27.47	Cotton Draw 33 Fed 2H (p)	2073.73	2026.53	43.94	
13700.00	10776.98	359.44	59.91	28.06	Cotton Draw 33 Fed 2H (p)	2074.09	2026.87	43.93	
13800.00	10777.33	359.42	61.60	28.65	Cotton Draw 33 Fed 2H (p)	2074.44	2027.20	43.91	
13900.00	10777.68	359.40	63.30	29.24	Cotton Draw 33 Fed 2H (p)	2074.79	2027.52	43.89	

5D Anti-Collision Report

Primary Well: Paint 33 Fed 2H (p) (TVD Relative to Kelly Bushing); All Azimuth Relative to GRID NORTH									
MD (US ft)	TVD (US ft)	T. Face to Sec (°)	S. Major (US ft)	S. Minor (US ft)	Nearest Well	CC (US ft)	ES (US ft)	SF	Risk
14000.00	10778.02	359.38	65.00	29.83	Cotton Draw 33 Fed 2H (p)	2075.15	2027.82	43.85	
14100.00	10778.37	359.36	66.71	30.43	Cotton Draw 33 Fed 2H (p)	2075.50	2028.10	43.78	
14200.00	10778.72	359.34	68.43	31.02	Cotton Draw 33 Fed 2H (p)	2075.86	2028.36	43.70	
14300.00	10779.06	359.32	70.15	31.62	Cotton Draw 33 Fed 2H (p)	2076.21	2028.59	43.60	
14400.00	10779.41	359.30	71.88	32.23	Cotton Draw 33 Fed 2H (p)	2076.57	2028.80	43.47	
14500.00	10779.76	359.28	73.61	32.84	Cotton Draw 33 Fed 2H (p)	2076.92	2028.99	43.33	
14600.00	10780.10	359.26	75.34	33.46	Cotton Draw 33 Fed 2H (p)	2077.28	2029.13	43.15	
14700.00	10780.45	359.24	77.09	34.10	Cotton Draw 33 Fed 2H (p)	2077.63	2029.23	42.92	
14800.00	10780.80	359.23	78.83	34.75	Cotton Draw 33 Fed 2H (p)	2077.99	2029.29	42.67	
14900.00	10781.14	359.21	80.58	35.40	Cotton Draw 33 Fed 2H (p)	2078.35	2029.32	42.39	
15000.00	10781.49	359.19	82.33	36.06	Cotton Draw 33 Fed 2H (p)	2078.70	2029.32	42.09	
15100.00	10781.84	359.17	84.09	36.72	Cotton Draw 33 Fed 2H (p)	2079.06	2029.27	41.76	
15200.00	10782.18	359.15	85.84	37.38	Cotton Draw 33 Fed 2H (p)	2079.63	2029.31	41.33	
15300.00	10782.53	359.15	87.61	38.04	Cotton Draw 33 Fed 2H (p)	2083.22	2032.18	40.81	
15400.00	10782.88	359.14	89.37	38.71	Cotton Draw 33 Fed 2H (p)	2090.70	2038.95	40.40	
15435.42	10783.00	359.13	90.00	38.94	Cotton Draw 33 Fed 2H (p)	2094.28	2042.29	40.28	

Secondary Well: Cotton Draw 33 Fed 2H (p) (TVD Relative to Kelly Bushing (Primary)); All Azimuth Relative to GRID NORTH									
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T. Face to Sec (°)	S. Major (US ft)	S. Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
0.00	178.00	0.00	351.95	0.00	0.00	4798.77	4798.05	6638.28	
100.00	178.00	0.00	351.95	0.00	0.00	4796.10	4795.26	5715.39	
200.00	200.00	22.00	351.95	0.05	0.05	4795.47	4794.36	4326.28	
300.00	300.00	122.00	351.95	0.19	0.19	4795.47	4794.00	3268.89	
400.00	400.00	222.00	351.95	0.40	0.40	4795.47	4793.56	2520.61	
500.00	500.00	322.00	351.95	0.62	0.62	4795.47	4793.12	2042.53	
600.00	600.00	422.00	351.95	0.84	0.84	4795.47	4792.67	1715.58	
700.00	700.00	522.00	351.95	1.07	1.07	4795.47	4792.22	1478.50	
800.00	800.00	622.00	351.95	1.29	1.29	4795.47	4791.77	1298.86	
900.00	900.00	722.00	351.95	1.51	1.51	4795.47	4791.32	1158.08	
1000.00	1000.00	822.00	351.95	1.74	1.74	4795.47	4790.88	1044.80	
1100.00	1100.00	922.00	351.95	1.96	1.96	4795.47	4790.43	951.70	
1200.00	1200.00	1022.00	351.95	2.19	2.19	4795.47	4789.98	873.82	
1300.00	1300.00	1122.00	351.95	2.41	2.41	4795.47	4789.53	807.72	
1400.00	1400.00	1222.00	351.95	2.64	2.64	4795.47	4789.08	750.91	
1500.00	1500.00	1322.00	351.95	2.86	2.86	4795.47	4788.63	701.56	
1600.00	1600.00	1422.00	351.95	3.09	3.09	4795.47	4788.18	658.30	
1700.00	1700.00	1522.00	351.95	3.31	3.31	4795.47	4787.73	620.06	
1800.00	1800.00	1622.00	351.95	3.53	3.53	4795.47	4787.28	586.02	
1900.00	1900.00	1722.00	351.95	3.76	3.76	4795.47	4786.83	555.53	
2000.00	2000.00	1822.00	351.95	3.98	3.98	4795.47	4786.38	528.05	
2100.00	2100.00	1922.00	351.95	4.21	4.21	4795.47	4785.93	503.16	
2200.00	2200.00	2022.00	351.95	4.43	4.43	4795.47	4785.49	480.51	
2300.00	2300.00	2122.00	351.95	4.66	4.66	4795.47	4785.04	459.81	
2400.00	2400.00	2222.00	351.95	4.88	4.88	4795.47	4784.59	440.82	
2500.00	2500.00	2322.00	351.95	5.11	5.11	4795.47	4784.14	423.33	
2600.00	2600.00	2422.00	351.95	5.33	5.33	4795.47	4783.69	407.18	
2700.00	2700.00	2522.00	351.95	5.56	5.56	4795.47	4783.24	392.22	
2800.00	2800.00	2622.00	351.95	5.78	5.78	4795.47	4782.79	378.32	

5D Anti-Collision Report

Secondary Wellbore Cotton Draw 33 (Fed 2H (B)) (TVD Relative to Kelly Bushing (Primary)) / All Azimuth Relative to GRID NORTH									
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T.Face to Sec (°)	S.Major (US ft)	S.Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
2900.00	2900.00	2722.00	351.95	6.01	6.01	4795.47	4782.34	365.37	
3000.00	3000.00	2822.00	351.95	6.23	6.23	4795.47	4781.89	353.28	
3100.00	3100.00	2922.00	351.95	6.46	6.46	4795.47	4781.44	341.96	
3200.00	3200.00	3022.00	351.95	6.68	6.68	4795.47	4780.99	331.34	
3300.00	3300.00	3122.00	351.95	6.91	6.91	4795.47	4780.54	321.37	
3400.00	3400.00	3222.00	351.95	7.13	7.13	4795.47	4780.09	311.97	
3500.00	3500.00	3322.00	351.95	7.36	7.36	4795.47	4779.64	303.11	
3600.00	3600.00	3422.00	351.95	7.58	7.58	4795.47	4779.20	294.74	
3700.00	3700.00	3522.00	351.95	7.81	7.81	4795.47	4778.75	286.82	
3800.00	3800.00	3622.00	351.95	8.03	8.03	4795.47	4778.30	279.32	
3900.00	3900.00	3722.00	351.95	8.25	8.25	4795.47	4777.85	272.19	
4000.00	8703.00	13208.84	359.69	87.14	37.29	4704.81	4661.84	109.50	
4100.00	8703.00	13208.84	359.69	87.14	37.29	4604.85	4561.78	106.92	
4200.00	8703.00	13208.84	359.69	87.14	37.29	4504.89	4461.72	104.35	
4300.00	8703.00	13208.84	359.69	87.14	37.29	4404.93	4361.66	101.78	
4400.00	8703.00	13208.84	359.69	87.14	37.29	4304.98	4261.59	99.23	
4500.00	8703.00	13208.84	359.69	87.14	37.29	4205.02	4161.53	96.69	
4600.00	8703.00	13208.84	359.69	87.14	37.29	4105.07	4061.47	94.15	
4700.00	8703.00	13208.84	359.69	87.14	37.29	4005.13	3961.41	91.62	
4800.00	8703.00	13208.84	359.69	87.14	37.29	3905.18	3861.35	89.11	
4900.00	8703.00	13208.84	359.69	87.14	37.29	3805.24	3761.30	86.60	
5000.00	8703.00	13208.84	359.69	87.14	37.29	3705.30	3661.24	84.11	
5100.00	8703.00	13208.84	359.69	87.14	37.29	3605.36	3561.19	81.62	
5200.00	8703.00	13208.84	359.69	87.14	37.29	3505.43	3461.14	79.14	
5300.00	8703.00	13208.84	359.69	87.14	37.29	3405.50	3361.09	76.68	
5400.00	8703.00	13208.84	359.69	87.14	37.29	3305.58	3261.04	74.22	
5500.00	8703.00	13208.84	359.69	87.14	37.29	3205.66	3161.00	71.78	
5600.00	8703.00	13208.84	359.69	87.14	37.29	3105.74	3060.96	69.35	
5700.00	8703.00	13208.84	359.69	87.14	37.29	3005.83	2960.92	66.93	
5800.00	8703.00	13208.84	359.69	87.14	37.29	2905.93	2860.89	64.52	
5900.00	8703.00	13208.84	359.69	87.14	37.29	2806.03	2760.86	62.12	
6000.00	8703.00	13208.84	359.69	87.14	37.29	2706.15	2660.84	59.73	
6100.00	8703.00	13208.84	359.69	87.14	37.29	2606.27	2560.83	57.35	
6200.00	8703.00	13208.84	359.69	87.14	37.29	2506.40	2460.82	54.99	
6300.00	8703.00	13208.84	359.69	87.14	37.29	2406.54	2360.82	52.63	
6400.00	8703.00	13208.84	359.69	87.14	37.29	2306.69	2260.83	50.29	
6500.00	8703.00	13208.84	359.69	87.14	37.29	2206.86	2160.85	47.96	
6600.00	8703.00	13208.84	359.69	87.14	37.29	2107.04	2060.88	45.65	
6700.00	8703.00	13208.84	359.69	87.14	37.29	2007.24	1960.94	43.34	
6800.00	8703.00	13208.84	359.69	87.14	37.29	1907.47	1861.01	41.06	
6900.00	8703.00	13208.84	359.69	87.14	37.29	1807.71	1761.10	38.78	
7000.00	8703.00	13208.84	359.69	87.14	37.29	1707.99	1661.23	36.53	
7100.00	8703.00	13208.84	359.69	87.14	37.29	1608.30	1561.39	34.28	
7200.00	8703.00	13208.84	359.69	87.14	37.29	1508.65	1461.59	32.05	
7300.00	8703.00	13208.84	359.69	87.14	37.29	1409.05	1361.84	29.84	
7400.00	8703.00	13208.84	359.69	87.14	37.29	1309.52	1262.15	27.65	
7500.00	8703.00	13208.84	359.69	87.14	37.29	1210.05	1162.54	25.47	
7600.00	8703.00	13208.84	359.69	87.14	37.29	1110.69	1063.01	23.29	
7700.00	8703.00	13208.84	359.69	87.14	37.29	1011.45	963.60	21.14	
7800.00	8703.00	13208.84	359.69	87.14	37.29	912.38	864.37	19.00	
7900.00	8703.00	13208.84	359.69	87.14	37.29	813.53	765.37	16.89	
8000.00	8703.00	13208.84	359.69	87.14	37.29	715.00	666.67	14.79	
8100.00	8703.00	13208.84	180.13	87.14	37.29	616.97	568.49	12.73	
8200.00	8703.00	13208.84	180.12	87.14	37.29	520.01	471.48	10.72	
8300.00	8703.00	13208.84	180.11	87.14	37.29	425.06	376.60	8.77	
8400.00	8703.00	13208.84	180.11	87.14	37.29	333.86	285.84	6.95	
8500.00	8703.00	13208.84	180.10	87.14	37.29	250.59	203.42	5.31	
8600.00	8703.00	13208.84	180.10	87.14	37.29	186.26	141.71	4.18	

SD Anti-Collision Report

Secondary Wellbore Cotton Draw 83 Fed 2H (P) (TVD Relative to Kelly Bushing (Primary)); All Azimuth Relative to GRID NORTH									Risk
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T Face to Sec (°)	S Major (US ft)	S Minor (US ft)	CC (US ft)	ES (US ft)	SF	
8700.00	8703.00	13208.84	180.10	87.14	37.29	164.80	122.55	3.90	
8800.00	8703.00	13208.84	180.10	87.14	37.29	200.44	154.14	4.33	
8900.00	8703.00	13208.84	180.10	87.14	37.29	270.83	221.82	5.53	
9000.00	8703.00	13208.84	180.10	87.14	37.29	355.70	305.48	7.08	
9100.00	8703.00	13208.84	180.10	87.14	37.29	446.87	396.06	8.79	
9200.00	8703.00	13208.84	180.10	87.14	37.29	541.17	489.94	10.56	
9300.00	8703.00	13208.84	180.10	87.14	37.29	637.21	585.60	12.35	
9400.00	8703.00	13208.84	180.10	87.14	37.29	734.12	682.25	14.15	
9500.00	8703.00	13208.84	180.09	87.14	37.29	831.39	779.32	15.97	
9600.00	8703.00	13208.84	180.08	87.14	37.29	928.89	876.59	17.76	
9700.00	8703.00	13208.84	180.08	87.14	37.29	1026.53	973.99	19.54	
9800.00	8703.00	13208.84	180.07	87.14	37.29	1124.24	1071.48	21.31	
9900.00	8703.00	13208.84	180.06	87.14	37.29	1221.98	1169.02	23.07	
10000.00	8703.00	13208.84	180.06	87.14	37.29	1319.72	1266.56	24.83	
10100.00	8703.00	13208.84	359.62	87.14	37.29	1417.59	1364.20	26.55	
10200.00	8703.00	13208.84	359.62	87.14	37.29	1515.74	1462.10	28.26	
10300.00	8703.00	13208.84	0.03	87.14	37.29	1612.24	1558.32	29.90	
10400.00	8703.00	13208.84	0.02	87.14	37.29	1703.64	1649.47	31.45	
10500.00	8703.00	13208.84	0.02	87.14	37.29	1788.16	1733.80	32.90	
10600.00	8703.00	13208.84	0.01	87.14	37.29	1864.31	1809.85	34.23	
10700.00	8703.00	13208.84	0.01	87.14	37.29	1930.91	1876.27	35.34	
10800.00	8703.00	13204.95	0.01	87.07	37.26	1986.98	1932.26	36.31	
10900.00	8703.00	13114.62	359.99	85.46	36.63	2029.58	1975.36	37.43	
11000.00	8703.00	13018.26	359.97	83.74	35.96	2055.84	2002.16	38.30	
11100.00	8703.00	12918.81	359.95	81.96	35.27	2064.97	2011.84	38.87	
11200.00	8703.00	12818.81	359.93	80.18	34.58	2065.32	2012.73	39.27	
11300.00	8703.00	12718.82	359.91	78.40	33.88	2065.66	2013.58	39.66	
11400.00	8703.00	12618.82	359.89	76.62	33.19	2066.01	2014.41	40.04	
11500.00	8703.00	12518.82	359.87	74.85	32.51	2066.36	2015.22	40.40	
11600.00	8703.00	12418.83	359.85	73.08	31.82	2066.71	2016.00	40.75	
11700.00	8703.00	12318.83	359.83	71.31	31.14	2067.06	2016.76	41.09	
11800.00	8703.00	12218.83	359.81	69.54	30.45	2067.41	2017.45	41.38	
11900.00	8703.00	12118.84	359.79	67.78	29.77	2067.76	2018.12	41.65	
12000.00	8703.00	12018.84	359.77	66.02	29.09	2068.11	2018.76	41.91	
12100.00	8703.00	11918.84	359.75	64.26	28.42	2068.46	2019.39	42.16	
12200.00	8703.00	11818.85	359.73	62.51	27.75	2068.81	2020.01	42.40	
12300.00	8703.00	11718.85	359.71	60.76	27.08	2069.16	2020.64	42.65	
12400.00	8703.00	11618.85	359.70	59.02	26.41	2069.51	2021.25	42.89	
12500.00	8703.00	11518.86	359.68	57.28	25.74	2069.86	2021.76	43.03	
12600.00	8703.00	11418.86	359.66	55.54	25.08	2070.21	2022.35	43.26	
12700.00	8703.00	11318.86	359.64	53.81	24.42	2070.56	2022.82	43.38	
12800.00	8703.00	11218.86	359.62	52.09	23.76	2070.91	2023.33	43.52	
12900.00	8703.00	11118.87	359.60	50.38	23.13	2071.26	2023.79	43.63	
13000.00	8703.00	11018.87	359.58	48.67	22.52	2071.61	2024.25	43.74	
13100.00	8703.00	10918.87	359.56	46.97	21.92	2071.97	2024.66	43.80	
13200.00	8703.00	10818.88	359.54	45.33	21.32	2072.32	2025.04	43.83	
13300.00	8703.00	10718.88	359.52	43.70	20.69	2072.67	2025.47	43.91	
13400.00	8703.00	10618.88	359.50	42.06	20.09	2073.02	2025.90	43.99	
13500.00	8703.00	10518.89	359.48	40.33	19.61	2073.38	2026.22	43.97	
13600.00	8703.00	10418.89	359.46	38.89	18.94	2073.73	2026.53	43.94	
13700.00	8703.00	10318.89	359.44	37.35	18.34	2074.09	2026.87	43.93	
13800.00	8703.00	10218.90	359.42	35.80	17.72	2074.44	2027.20	43.91	
13900.00	8703.00	10118.90	359.40	34.27	17.18	2074.79	2027.52	43.89	
14000.00	8703.00	10018.90	359.38	32.75	16.67	2075.15	2027.82	43.85	
14100.00	8703.00	9918.91	359.36	31.25	16.15	2075.50	2028.10	43.78	
14200.00	8703.00	9818.91	359.34	29.77	15.65	2075.86	2028.36	43.70	
14300.00	8703.00	9718.91	359.32	28.41	15.16	2076.21	2028.59	43.60	
14400.00	8703.00	9618.91	359.30	27.12	14.70	2076.57	2028.80	43.47	

5D Anti-Collision Report

Secondary Well: Cotton Draw 33 FSD 2H (P) (TVD Relative to Kelly Bushing (Primary)) (All Azimuth Relative to GRID NORTH)									
Pri MD (US ft)	TVD (US ft)	Sec MD (US ft)	T Face to Sec (°)	S Major (US ft)	S Minor (US ft)	CC (US ft)	ES (US ft)	SF	Risk
14500.00	8703.00	9518.92	359.28	25.85	14.26	2076.92	2028.99	43.33	
14600.00	8703.00	9418.92	359.26	24.58	13.84	2077.28	2029.13	43.15	
14700.00	8703.00	9318.92	359.24	23.51	13.45	2077.63	2029.23	42.92	
14800.00	8703.00	9218.93	359.23	22.46	13.10	2077.99	2029.29	42.67	
14900.00	8703.00	9118.93	359.21	21.56	12.78	2078.35	2029.32	42.39	
15000.00	8703.00	9018.93	359.19	20.70	12.50	2078.70	2029.32	42.09	
15100.00	8703.00	8918.94	359.17	20.00	12.25	2079.06	2029.27	41.76	
15200.00	8702.96	8845.70	359.15	19.64	12.10	2079.63	2029.31	41.33	
15300.00	8702.35	8826.89	359.15	19.53	12.05	2083.22	2032.18	40.81	
15400.00	8701.02	8808.16	359.14	19.43	12.11	2090.70	2038.95	40.40	
15435.42	8700.38	8801.56	359.13	19.42	12.14	2094.28	2042.29	40.28	

**Weatherford**

Weatherford Drilling Services

GeoDec4 v2.0.0.3

Report Date: September 04, 2014
Job Number: _____
Customer: Devon Energy
Well Name: Paint 33 Fed 2H
API Number: _____
Rig Name: _____
Location: Lea Co, NM Nad83 NME
Block: _____
Engineer: RWJ

NAD83 / New Mexico East (ftUS)	NAD83 (1986)
Projected Coordinate System	Geodetic Coordinate System
Datum: North American Datum 1983 (1986)	Datum: North American Datum 1983 (1986)
Ellipsoid: GRS 1980	Ellipsoid: GRS 1980
EPSG: 2257	EPSG: 4269
North: 425194.55 US Survey Foot	Latitude: 32.16726 Degree
East: 742962.07 US Survey Foot	Longitude: -103.681727 Degree
Convergence: 0.35°	
Declination: 7.38°	
Total Correction: 7.03°	
Datum Transformation: none	

Geodetic Location WGS84

MSL Elevation = 0 m
Latitude = 32° 10' 02.14" N
Longitude = 103° 40' 54.22" W

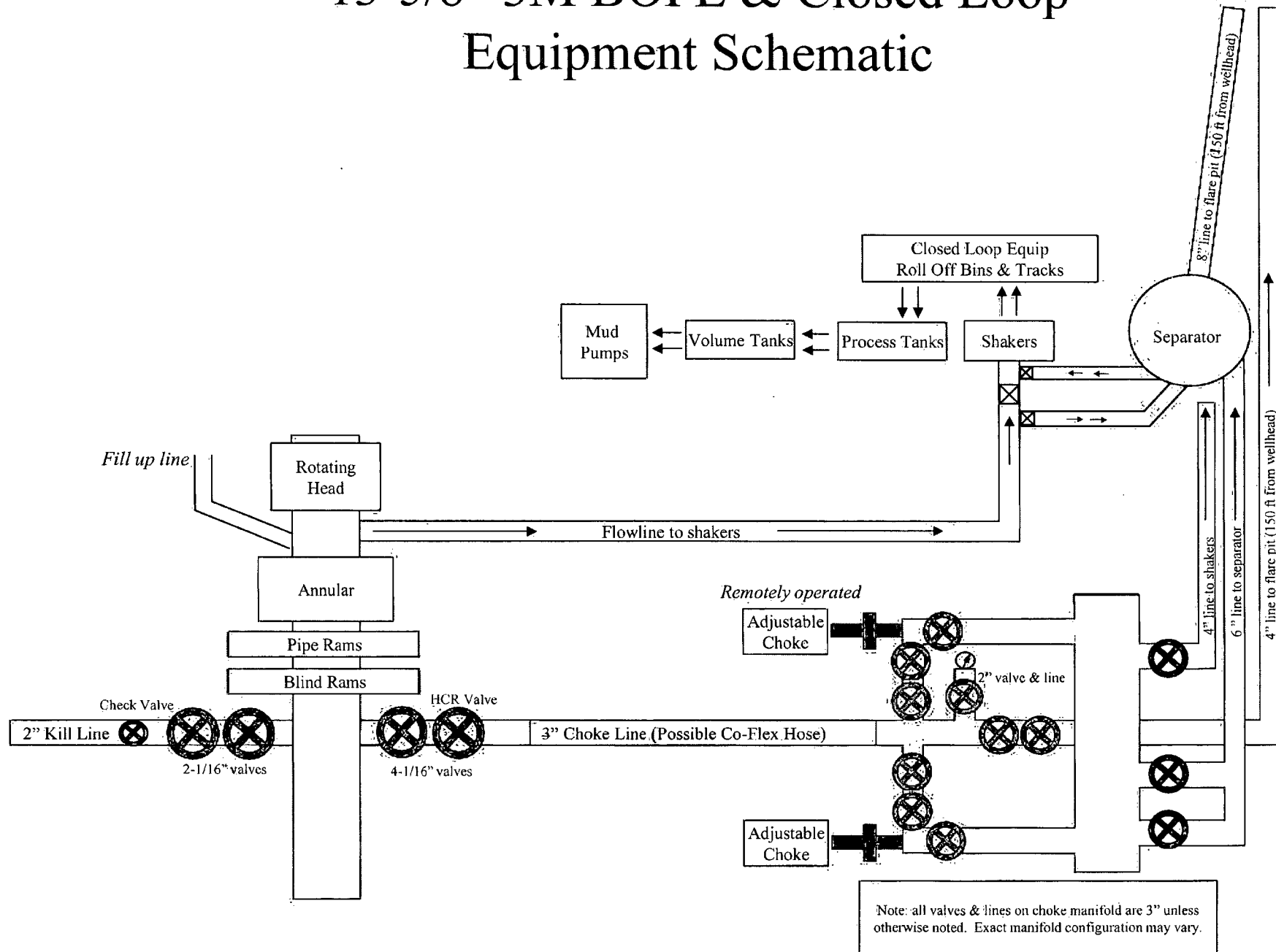
Magnetic Declination = 7.38 deg	[True North Offset]
Local Gravity = .9988 g	Checksum = 6441
Local Field Strength = 48204 nT	Magnetic Vector X = 23888 nT
Magnetic Dip = 60.02 deg	Magnetic Vector Y = 3092 nT
Magnetic Model = bggm2014.dat	Magnetic Vector Z = 41755 nT
Run Date = November 30, 2014	Magnetic Vector H = 24087 nT

Signed: _____ Date: _____

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Warning: This information is controlled, and any printed version is deemed as uncontrolled unless suitably endorsed by a controlling authority or accompanied by a controlled table of contents in order to ensure adequate revision control.

13-5/8" 3M BOPE & Closed Loop Equipment Schematic



NOTES REGARDING BLOWOUT PREVENTERS

Devon Energy Production Company, L.P.
Paint 33 Fed 2H

1. Drilling Nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
2. Wear ring will be properly installed in head.
3. Blowout preventer and all associated filings will be in operable condition to withstand a minimum of 3000psi working pressure.
4. All fittings will be flanged.
5. A fill bore safety valve tested to a minimum of 3000psi WP with proper thread connections will be available on the rotary rig floor at all times.
6. All choke lines will be anchored to prevent movement.
7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
8. Will maintain a kelly cock attached to the kelly.
9. Hand wheels and wrenches will be properly installed and tested for safe operation.
10. Hydraulic floor control for blowout preventer will be located as near in proximity to driller's controls as possible.
11. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.



Fluid Technology

ContiTech Beattie Corp.
Website: www.contitechbeattie.com

Monday, June 14, 2010

RE: Drilling & Production Hoses
Lifting & Safety Equipment

To Helmerich & Payne,

A Continental ContiTech hose assembly can perform as intended and suitable for the application regardless of whether the hose is secured or unsecured in its configuration. As a manufacturer of High Pressure Hose Assemblies for use in Drilling & Production, we do offer the corresponding lifting and safety equipment, this has the added benefit of easing the lifting and handling of each hose assembly whilst affording hose longevity by ensuring correct handling methods and procedures as well as securing the hose in the unlikely event of a failure; but in no way does the lifting and safety equipment affect the performance of the hoses providing the hoses have been handled and installed correctly. It is good practice to use lifting & safety equipment but not mandatory.

Should you have any questions or require any additional information/clarifications then please do not hesitate to contact us.

ContiTech Beattie is part of the Continental AG Corporation and can offer the full support resources associated with a global organization.

Best regards,

Robin Hodgson
Sales Manager
ContiTech Beattie Corp

ContiTech Beattie Corp,
11535 Brittmoore Park Drive,
Houston, TX 77041
Phone: +1 (832) 327-0141
Fax: +1 (832) 327-0148
www.contitechbeattie.com





QUALITY DOCUMENT

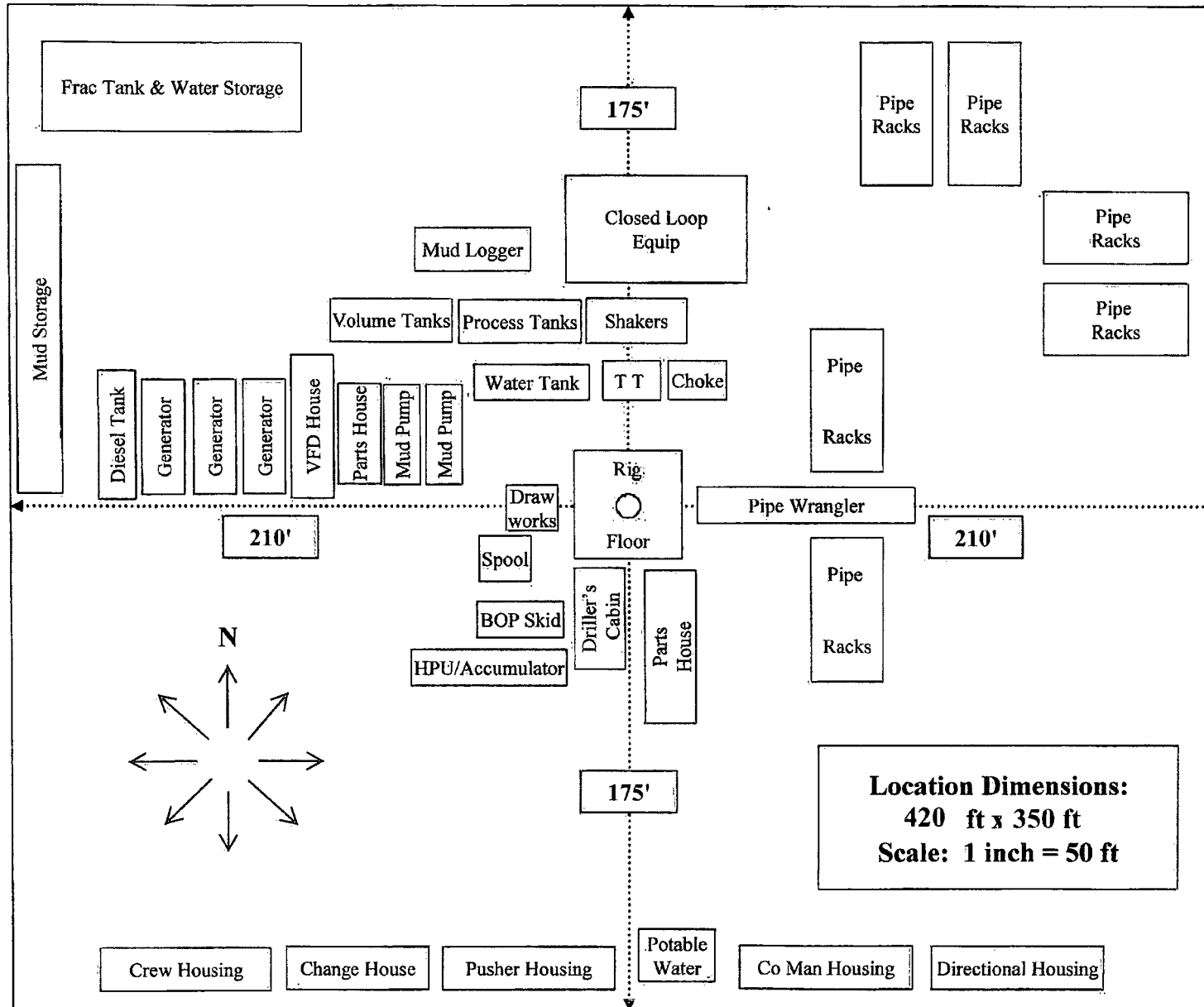
**PHOENIX RUBBER
INDUSTRIAL LTD.**

H-6728 Szeged, Budapesti út 10. Hungary • H-6701 Szeged, P. O. Box 152
Phone: (3662) 506-737 • Fax (3662) 506-738

SALES & MARKETING: H-1092 Budapest, Ráday u. 42-44. Hungary • H-1440 Budapest, P. O. Box 26
Phone: (361) 456-4200 • Fax (361) 217-2972, 456-4273 • www.taronsemtarg.hu

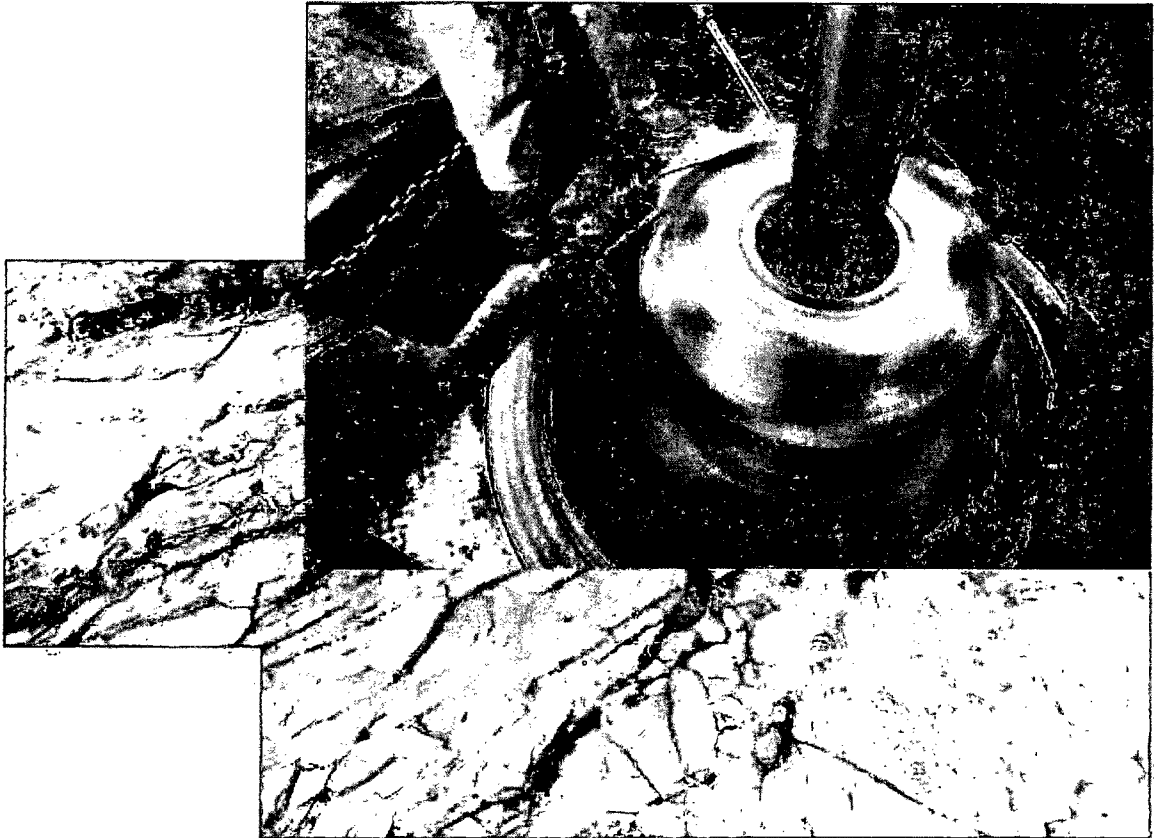
QUALITY CONTROL INSPECTION AND TEST CERTIFICATE				CERT. N°: 555	
PURCHASER: Phoenix Beattie Co.				P.O. N°: 1519FA-871	
PHOENIX RUBBER order N°: 170466		HOSE TYPE: 3" ID Choke and Kill Hose			
HOSE SERIAL N°: 34137		NOMINAL / ACTUAL LENGTH: 11,43 m			
W.P. 68,96 MPa 10000 psi		T.P. 103,4 MPa 15000 psi		Duration: 60 min.	
Pressure test with water at ambient temperature See attachment. (1 page)					
↑ 10 mm = 10 Min. → 10 mm = 16 MPa					
COUPLINGS					
Type	Serial N°		Quality	Heat N°	
3" coupling with 4 1/16" Flange end	714 715		AISI 4130	C7626	
			AISI 4130	47357	
API Spec 16 C Temperature rate: "B"					
All metal parts are flawless					
WE CERTIFY THAT THE ABOVE HOSE HAS BEEN MANUFACTURED IN ACCORDANCE WITH THE TERMS OF THE ORDER AND PRESSURE TESTED AS ABOVE WITH SATISFACTORY RESULT.					
Date:	Inspector		Quality Control		
30. April. 2002.			PHOENIX RUBBER Industrial Ltd. Hose Inspection and Pressure Testing Department 		

H&P Flex Rig Location Layout





Commitment Runs Deep



Design Plan
Operation and Maintenance Plan
Closure Plan

SENM - Closed Loop Systems
June 2010

I. Design Plan

Devon uses MI SWACO closed loop system (CLS). The MI SWACO CLS is designed to maintain drill solids at or below 5%. The equipment is arranged to progressively remove solids from the largest to the smallest size. Drilling fluids can thus be reused and savings is realized on mud and disposal costs. Dewatering may be required with the centrifuges to insure removal of ultra fine solids.

The drilling location is constructed to allow storm water to flow to a central sump normally the cellar. This insures no contamination leaves the drilling pad in the event of a spill. Storm water is reused in the mud system or stored in a reserve fluid tank farm until it can be reused. All lubricants, oils, or chemicals are removed immediately from the ground to prevent the contamination of storm water. An oil trap is normally installed on the sump if an oil spill occurs during a storm.

A tank farm is utilized to store drilling fluids including fresh water and brine fluids. The tank farm is constructed on a 20 ml plastic lined, bermed pad to prevent the contamination of the drilling site during a spill. Fluids from other sites may be stored in these tanks for processing by the solids control equipment and reused in the mud system. At the end of the well the fluids are transported from the tank farm to an adjoining well or to the next well for the rig.

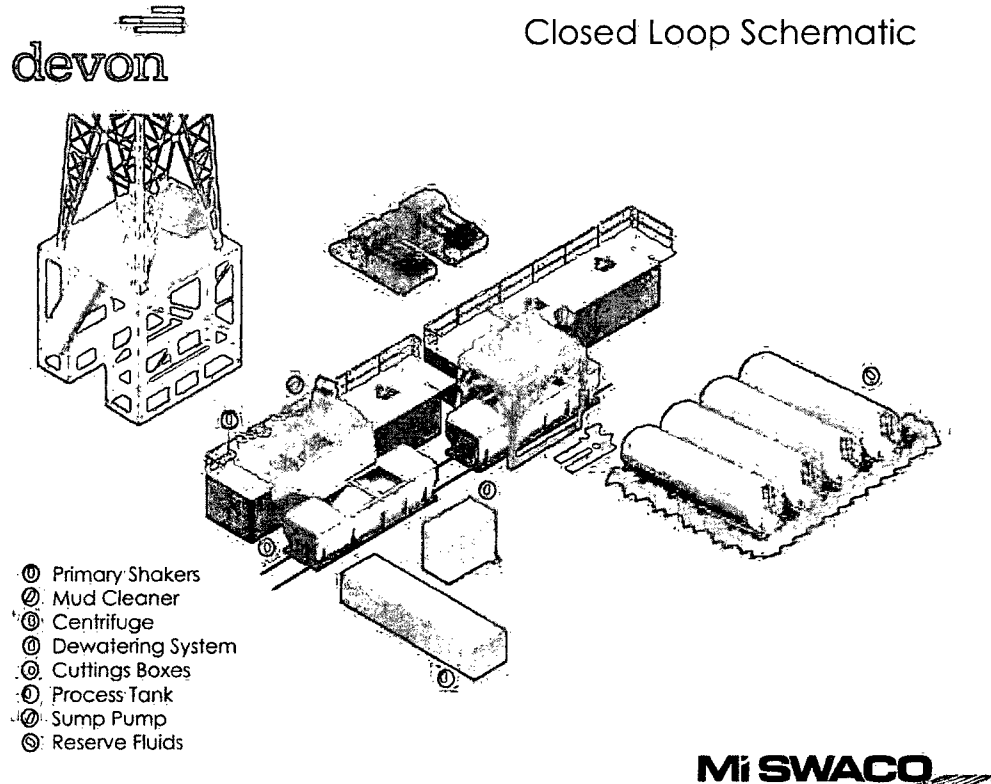
Prior to installing a closed-loop system on site, the topsoil, if present, will be stripped and stockpiled for use as the final cover or fill at the time of closure.

Signs will be posted on the fence surrounding the closed-loop system unless the closed-loop system is located on a site where there is an existing well, that is operated by Devon.

II. Operations and Maintenance Plan

Primary Shakers: The primary shakers make the first removal of drill solids from the drilling mud as it leaves the well bore. The shakers are sized to handle maximum drilling rate at optimal screen size. The shakers normally remove solids down to 74 microns.

Mud Cleaner: The Mud Cleaner cleans the fluid after it leaves the shakers. A set of hydrocyclones are sized to handle 1.25 to 1.5 times the maximum circulating rate. This ensures all the fluid is being processed to an average cut point of 25 microns. The wet discharged is dewatered on a shaker equipped with ultra fine mesh screens and generally cut at 40 microns.



Centrifuges: The centrifuges can be one or two in number depending on the well geometry or depth of well. The centrifuges are sized to maintain low gravity solids at 5% or below. They may or may not need a dewatering system to enhance the removal rates. The centrifuges can make a cut point of 8-10 microns depending on bowl speed, feed rate, solids loading and other factors.

The centrifuge system is designed to work on the active system and be flexible to process incoming fluids from other locations. This set-up is also dependant on well factors.

Dewatering System: The dewatering system is a chemical mixing and dosing system designed to enhance the solids removal of the centrifuge. Not commonly used in shallow wells. It may contain pH adjustment, coagulant mixing and dosing, and polymer mixing and dosing. Chemical flocculation binds ultra fine solids into a mass that is within the centrifuge operating design. The

dewatering system improves the centrifuge cut point to infinity or allows for the return of clear water or brine fluid. This ability allows for the ultimate control of low gravity solids.

Cuttings Boxes: Cuttings boxes are utilized to capture drill solids that are discarded from the solids control equipment. These boxes are set upon a rail system that allows for the removal and replacement of a full box of cuttings with an empty one. They are equipped with a cover that insures no product is spilled into the environment during the transportation phase.

Process Tank: (Optional) The process tank allows for the holding and process of fluids that are being transferred into the mud system. Additionally, during times of lost circulation the process tank may hold active fluids that are removed for additional treatment. It can further be used as a mixing tank during well control conditions.

Sump and Sump Pump: The sump is used to collect storm water and the pump is used to transfer this fluid to the active system or to the tank for to hold in reserve. It can also be used to collect fluids that may escape during spills. The location contains drainage ditches that allow the location fluids to drain to the sump.

Reserve Fluids (Tank Farm): A series of frac tanks are used to replace the reserve pit. These are steel tanks that are equipped with a manifold system and a transfer pump. These tanks can contain any number of fluids used during the drilling process. These can include fresh water, cut brine, and saturated salt fluid. The fluid can be from the active well or reclaimed fluid from other locations. A 20 ml liner and berm system is employed to ensure the fluids do not migrate to the environment during a spill.

If a leak develops, the appropriate division district office will be notified within 48 hours of the discovery and the leak will be addressed. Spill prevention is accomplished by maintaining pump packing, hoses, and pipe fittings to insure no leaks are occurring. During an upset condition the source of the spill is isolated and repaired as soon as it is discovered. Free liquid is removed by a diaphragm pump and returned to the mud system. Loose topsoil may be used to stabilize the spill and the contaminated soil is excavated and placed in the cuttings boxes. After the well is finished and the rig has moved, the entire location is scrapped and testing will be performed to determine if a release has occurred.

All trash is kept in a wire mesh enclosure and removed to an approved landfill when full. All spent motor oils are kept in separate containers and they are removed and sent to an approved recycling center. Any spilled lubricants, pipe

dope, or regulated chemicals are removed from soil and sent to landfills approved for these products.

These operations are monitored by Mi Swaco service technicians. Daily logs are maintained to ensure optimal equipment operation and maintenance. Screen and chemical use is logged to maintain inventory control. Fluid properties are monitored and recorded and drilling mud volumes are accounted for in the mud storage farm. This data is kept for end of well review to insure performance goals are met. Lessons learned are logged and used to help with continuous improvement.

A MI SWACO field supervisor manages from 3-5 wells. They are responsible for training personnel, supervising installations, and inspecting sites for compliance of MI SWACO safety and operational policy.

III. Closure Plan

A maximum 340' X 340' caliche pad is built per well. All of the trucks and steel tanks fit on this pad. All fluid cuttings go to the steel tanks to be hauled by various trucking companies to an agency approved disposal.