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State of New Mexico
 Energy, Minerals and Natural Resources
HOBBBS OCD
 OIL CONSERVATION DIVISION
 220 South St. Francis Dr.
 Santa Fe, NM 87505

Form C-103
 Revised August 1, 2011

MAR 19 2018
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WELL API NO. 30-025-38576 AND 30-025-42139
5. Indicate Type of Lease STATE <input checked="" type="checkbox"/> FEE <input type="checkbox"/>
6. State Oil & Gas Lease No. V07530-0001
7. Lease Name or Unit Agreement Name Linam AGI
8. Wells Number 1 and 2
9. OGRID Number 36785
10. Pool name or Wildcat Wildcat
11. Elevation (Show whether DR, RKB, RT, GR, etc.) 3736 GR

SUNDRY NOTICES AND REPORTS ON WELLS
 (DO NOT USE THIS FORM FOR PROPOSALS TO DRILL OR TO DEEPEN OR PLUG BACK TO A DIFFERENT RESERVOIR. USE "APPLICATION FOR PERMIT" (FORM C-101) FOR SUCH PROPOSALS.)

1. Type of Well: Oil Well Gas Well Other

2. Name of Operator
DCP Midstream LP

3. Address of Operator
370 17th Street, Suite 2500, Denver CO 80202

4. Well Location
Unit Letter K; 1980 feet from the South line and 1980 feet from the West line
Section 30 Township 18S Range 37E NMPM County Lea

12. Check Appropriate Box to Indicate Nature of Notice, Report or Other Data

NOTICE OF INTENTION TO:		SUBSEQUENT REPORT OF:	
PERFORM REMEDIAL WORK <input type="checkbox"/>	PLUG AND ABANDON <input type="checkbox"/>	REMEDIAL WORK <input type="checkbox"/>	ALTERING CASING <input type="checkbox"/>
TEMPORARILY ABANDON <input type="checkbox"/>	CHANGE PLANS <input type="checkbox"/>	COMMENCE DRILLING OPNS. <input type="checkbox"/>	P AND A <input type="checkbox"/>
PULL OR ALTER CASING <input type="checkbox"/>	MULTIPLE COMPL <input type="checkbox"/>	CASING/CEMENT JOB <input type="checkbox"/>	
DOWNHOLE COMMINGLE <input type="checkbox"/>			
OTHER: <input type="checkbox"/>		OTHER: Annual Summary Report and Notification parameter review pursuant to NMOCC R12546-K <input checked="" type="checkbox"/>	

13. Describe proposed or completed operations. (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work). SEE RULE 19.15.7.14 NMAC. For Multiple Completions: Attach wellbore diagram of proposed completion or recompletion.

Annual Summary for 2017 Pursuant to NMOCC R-12546-K and ACO-275 C-103 for Linam AGI#1 and AGI#2 and Request to Continue with Approved Immediate Notification Parameters for Operation of Both Wells

This is annual summary submittal of data as agreed to between DCP and OCD relative to injection pressure, TAG temperature and casing annulus pressure for Linam AGI#1 until the well is worked over, which occurred in June 2017 and for Linam AGI#2 (API #30-025-42139) which was brought online in October 2015.

The analyses of data from both wells has been submitted monthly as required until the workover of the AGI#1 well and has also been submitted monthly for the AGI#2 well. The AGI#1 well was successfully worked over as planned in June 2017 we will request that the reporting be changed to quarterly for both wells as detailed in NMOCC R-12546-K once independent volume measurement for each well is available. The summary of data for the 2017 calendar year for the operation of the Linam Ranch AGI Facility and request to keep the approved immediate notification parameters for both wells is the purpose of this submittal.

The summary of the data and supporting tables and figures are attached.

SIGNATURE  TITLE Consultant to DCP Midstream/ Geolex, Inc. DATE 2/27/2017
 Type or print name Alberto A. Gutierrez, RG E-mail address: aag@geolex.com PHONE: 505-842-8000

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 Conditions of Approval (if any): msbrown 3/19/2018

ANALYSIS OF ANNUAL TRENDS AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS FOR OPERATION OF LINAM AGI #1 AND LINAM AGI #2 (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all

This document presents the results from the analyses of the injection parameter data collected from the Linam AGI #1 and #2 Wells which serve the Linam Ranch Gas Processing Facility near Hobbs, NM. Data from the Linam AGI #1 have been collected continuously and have been analyzed on a monthly basis by Geolex and transmitted to DCP for reporting to NMOCD as required by ACO 275 and the approved post-workover C-103. In addition, the Linam AGI #2 well was completed and brought on line in October 2015. The AGI #2 well was completed in the same injection zone as the AGI#1 approximately 450 feet to the southwest of AGI #1. From the time that AGI #2 was brought on line, injection has sometimes been solely into one of the two wells or into both wells simultaneously. AGI#2 was operated in conjunction with AGI #1 from October 2015 to January 2016 when a switch was made to operate only AGI#1 for the remainder of 2016. In May 2017, DCP switched over to injecting into AGI#2 to allow for the workover of AGI#1. The workover was completed on June 8, 2017 and AGI #1 was brought back on line in July 2017 with bottom hole sensors installed. These sensors are now serving to monitor downhole and reservoir conditions since the downhole sensors in AGI #2 failed due to a lightning strike shortly after installation 2015 and will not be able to be repaired until sometime in the future when AGI #2 is worked over. The system has been operating with only AGI #1 active while waiting for independent flow meters to be installed/repared in both wells so that reliable flow information will be available for each well independently. This operational mode (utilizing only AGI #1) will continue until the volume meters are installed/repared. In the meantime, in order to obtain reservoir data which would have been provided by the downhole PT sensors in AGI #2, a slick line with a pressure recorder was placed into AGI #2 and downhole pressure data were collected under both injection and non-injection conditions for the AGI #2 and AGI #1. Presently surface data from both wells is being collected relative to the following parameters:

- Treated Acid Gas (TAG) surface injection pressure (both wells),
- TAG injection temperature (both wells),
- Annular pressure (both wells)
- Bottom Hole pressure and temperature (AGI#1 beginning 7/2017)
- Overall total TAG flow rate from compressors

These above are the key parameters which are currently being measured in both wells in order to monitor the operations of the wells, prevent hydrate formation, reduce corrosion potential following the workover of AGI#1. While improvements have been implemented in the placement of temperature controls, dehydration of TAG during compression and other systems improvements at the AGI facility, there continue to be variations in the desired and normal operating levels of the above-referenced parameters. Since these parameters are useful indicators and predictors of potential operational or mechanical problems in the well, various levels of alarms have been established for each of these parameters. These parameters include three which are measured directly (TAG injection pressure, TAG injection

temperature and annular pressure) and one (differential pressure) which is a calculated value (the difference between the two measured parameters of injection and annular pressure). The analyses of the long-term trends in these values have been useful in smoothing out shorter-term variations which can be observed from detailed inspection of hourly data and in the development of appropriate alarm bands for each parameter.

The Linam AGI #1 experienced a tubing leak in late 2011 which was partially addressed in a workover conducted in April/May 2012. The leak was detected in the end of 2011 and beginning of 2012, until the workover, the injection parameters were reviewed, analyzed and reported weekly to the NMOCD. Following the workover in which the tubing leak was repaired, some compromised production casing was detected immediately above the packer depth. At that time, we recommended keeping only approximately 250 psig on the annular space between the tubing and casing in AGI #1 since with annular pressure at this level, under normal operating conditions, this parameter can serve as a useful indicator of when activity should be initiated to prevent damage to the well or trigger a NMOCD shutdown and/or immediate notification requirements. Concern about this compromised casing was eliminated by stacking packers when the well was worked over again in June 2017. All of the data from January 2012 through December 2015 are included in our analysis, but only the post-workover data have been used to develop the recommended alarm and emergency shutdown (ESD) levels in conjunction with the requirements of NMOCD Order 12546-all, ACO-275 and the post-workover C-103.

Furthermore, a similar process has been employed on the Linam AGI#2 since it was brought online in October 2015. As described above, this well is equipped with bottom hole (just at top of packer) P/T measurement capability both inside and outside the tubing. When the current sensor/communication issues are resolved in AGI #2, the monitoring of these four additional parameters will also aid significantly in determining the appropriate immediate notification parameters which are required by the NMOCC order for AGI #2. In general, the immediate notification parameters for both wells were developed from this long-term analysis of the injection data. Initial testing of the Linam AGI#2 indicates that the pressure variations induced by flow rate and temperature fluctuations in the Linam AGI#1 are influencing the reservoir as measured in the AGI #2 location. This is to be expected as the new well is completed in the same zone at a distance away from the initial well which we predicted would see the edge of the plume in about 7 years. The Linam AGI #1 has been injecting for approximately 12 years.

Data from AGI #1 were continuously collected and analyzed weekly prior to the original workover in April/May 2012 and then monthly after the workover from June 2012 through December 2017 (see Figure 1). These data collection, analysis and reporting functions continue as required by NMOCD on a monthly basis. Furthermore, since it is necessary to evaluate the data from both wells to know how the system is operating overall, the surface data from AGI #2 area also being collected, analyzed and reported monthly. The reporting requirement for the AGI #2 is only quarterly and now that AGI #1 has been successfully worked over, the reporting for both wells will shift to quarterly as soon as independent reliable volume measurement is available for each well.

The NMOCD also requires that immediate notification parameters and levels be discussed and agreed upon with the agency, and that these be periodically reviewed and updated as needed based on operational

or regulatory changes. The immediate notification parameters for both wells have been approved by NMOCD and DCP requests no changes in these approved values. With this requirement in mind and for the purpose of protecting the mechanical integrity and safety of both wells and the overall AGI facility, Geolex monitors these data under contract to DCP to prevent damage to the wells or violation of regulatory requirements or permit constraints.

After 5.5 years (65 months) of carefully analyzing the performance of AGI #1 on a continuous basis, Geolex has assembled the data and has analyzed observed trends for the post-workover period of June 2012 – December 2017 as can be seen on Figure 2. Several important observations can be made from analyzing these data and taking into consideration important system modifications that have occurred during this time period. These include the following:

1. AGI #1 Post-Workover MIT completed in May 2012
2. AGI #1 MIT test completed November 14, 2012
3. Bleeding of diesel from casing annular space immediately after the November 2012 AGI #1 MIT test.
4. AGI #1 MIT test completed April 30, 2013
5. Addition of diesel in annular space after April 2013 AGI #1 MIT and May 2013 plant shutdown
6. AGI #1 MIT test completed October 30, 2013
7. Failure of the VFD for the cooler on the AGI compressor from February 4 through 9, 2014.
8. AGI #1 MIT test completed April 30, 2014
9. Addition of diesel in annular space after April 2014 AGI #1 MIT
10. AGI #1 MIT test completed September 19, 2014
11. AGI #1 MIT test completed March 19, 2015
12. AGI #1 MIT test completed September 15, 2015
13. AGI #2 brought online with startup in October-November 2015 and operated until January 2016
14. AGI #1 MIT test completed March 22, 2016
15. AGI #2 MIT test completed April 1, 2016
16. AGI #2 TAG lines bled to flare on June 13, 2016 to remove static TAG in line when well is not operating.
17. AGI #1 MIT test completed September 14, 2016
18. AGI #1 Workover completed June 8, 2017 including stacked packer, bottom hole PT gauges
19. AGI #1 MIT test completed June 7, 2017 after workover completion
20. AGI #2 MIT test completed February 16, 2017
21. AGI #2 MIT test completed February 15, 2018

The following trends have been observed in the AGI #1 data and are reflected on Figure 2:

1. TAG injection pressure which was on a slight increasing trend due to slightly increasing average temperature of injected TAG has leveled off due to temperature decreases in 2017. The TAG injection pressure and rate was more variable since AGI #2 was also operated part of the time but AGI #1 has been used exclusively since the workover in June 2017 through end of 2017.

2. The TAG injection temperature decreased slightly from 2016 with an arithmetic mean of 106°F, in 2017 from 113°F in 2016.
3. The TAG injection temperature is significantly lower during periods of low flow into AGI#1 when AGI #2 was used for a short time and similarly for AGI #2 when AGI#1 is used primarily or exclusively.
4. Pressure in the casing annulus has been consistently tracked the correlative nature of variable injection temperature, pressure and flowrate, and its arithmetic mean for the period has been approximately 348 psig.
5. The pressure differential between the casing annulus and the TAG injection pressure clearly indicates that no communication currently exists between the tubing and casing annulus.
6. The generally low annular pressures observed indicate that the production casing/cement still has good integrity.
7. TAG injection temperatures can now be lower due to the improvement of water reduction in compression which reduces the potential for hydrate formation at lower temperatures

Given the observations of the trends in the graphs and the competing influence of average injection temperature decrease and injection volumes increased over the 2017 period, the observed TAG injection pressure increase is predictable and normal. There is no current indication of the reservoir being pressured up to any significant degree by the injection from Linam AGI #1. This was confirmed during the drilling and testing of AGI #2. Upon startup from any shutdown that lasts more than 6-8 hours it is critical to inject methanol along with the TAG for the initial startup period to prevent the formation of hydrates. While this may no longer be necessary due to the changes which were made in the water removal efficiency of the AGI compressor system, it is a good preventative measure. Prior to the increased water removal efficiency, this effect was observed in the period of March 2013 when hydrate formation during one of these events caused a spike in TAG injection pressure of approximately 35% over normal pressures due to partial blockage of the injection line and tubing created by the hydrate formation. This persisted for several hours until the situation was alleviated by the stabilization of the compressor and the simultaneous injection of methanol to cause the hydrates to be reabsorbed into the TAG. Injection pressures and temperatures then returned to normal.

It is also critical to maintain the temperature control on the injected TAG and to avoid rapid temperature or pressure fluctuations during periods when power failures or other mechanical failures may occur. The extensive and wide variation in TAG injection temperatures observed prior to the failure of the tubing in late 2011, resulted in the formation of free water within the tubing and corrosion resulting in a tubing leak which had to be repaired in April/May 2012. Temperature control changes were implemented and helped to significantly control downward swings in temperature and prevent the formation of hydrates. However, in February 2014, there was a failure in the VFD for the cooler on the AGI compressor which persisted for five days. During this period of time, the TAG temperature increased to at least 150 °F, and the annular pressure increased dramatically due to the heating of the diesel fluid in the annular space as a result of the elevated TAG injection temperature. TAG temperature as well as annular pressure returned to the normal range once the VFD on the cooler was repaired. The significant spread between TAG injection pressure and the annular pressure maintained even during this heating episode proves the continued integrity of the well, packer, casing and tubing. However, the rise in annular pressure has a



potential to damage the integrity of the compromised casing in the well and should be avoided during all subsequent operations. In response to these issues, DCP undertook and successfully completed a project in 2015 to address the temperature fluctuations resulting from compression controls and to increase the efficiency of water removal to the point where all free water is removed from the TAG prior to injection. This significantly reduces hydrate formation potential in the entire system regardless of temperature variations.

In October 2015, AGI #2 was started up and operated in a startup mode switching back and forth from AGI #1. This effect is reflected in the trend data shown in Figure 2. Due to a volume meter sensor failure and configuration issues which are currently being addressed, only total flow to the AGI system can be reliably measured through 2017. For this reason, only the total flow rate is plotted on Figure 3. Once flow metering for each well is engineered and constructed in 2018 only total flow is being reported and wells are being used only one at a time to allow for accurate measurement of flow into each well.

REVIEW OF STATISTICAL ANALYSIS OF INJECTION PARAMETERS, DEVELOPMENT OF AND REQUEST TO CONTINUE WITH APPROVED IMMEDIATE NOTIFICATION PARAMETERS (API #s 30-025-38576 AND 30-025-42139) UNDER R-12546-all

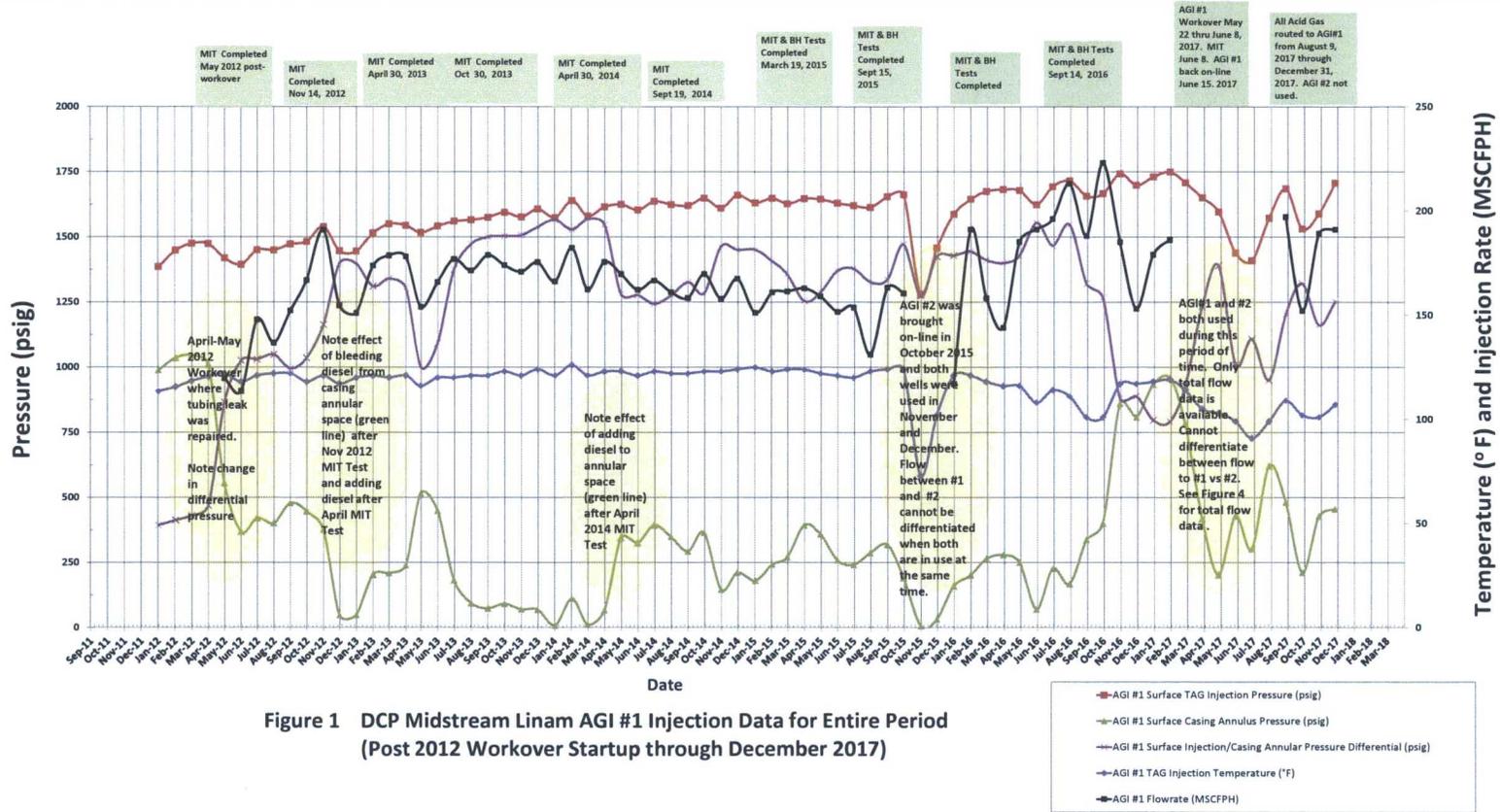
The statistical analyses of the injection parameter data were initially conducted for the purpose of establishing normal operating levels for these parameters which are automatically monitored. Several data filtering steps were accomplished to take the hourly data which forms the basis of the analysis in order to smooth out variability and to account for the physical changes in the well and its operation after the repair of the tubing leak in the workover completed in May 2012. Because the configuration of the well changed dramatically after the workover, only data after the well had stabilized post-workover were used in this analysis. Furthermore, the subsequent stacked packer workover of the AGI#1 in June 2017 was completed and essentially only the AGI #1 has been used since then. The bottom hole PT sensors installed during the 2017 workover of AGI #1 have been providing excellent data and these data are shown on the graph attached here as Figure 4.

All the data are summarized in Table 1, and the calculated statistical parameters of arithmetic mean and standard deviation were used to establish base levels and variability for each parameter. The results of these analyses resulted in the immediate notification parameters which were approved both for AGI #2 and the parameters required under ACO 275 for AGI#1. These approved parameters are presented at the bottom of Table 1 and DCP requests that these parameters remain the same until the workover for the AGI#1 is completed in 2017. At this time the parameters will be reevaluated and operations and reporting requirements should be as they currently are for AGI #2.

TABLE 1 SUMMARY DATA ANALYSIS OF LINAM AGI #1 TRENDS FOR JANUARY 2012 THROUGH DECEMBER 2017 (2 PAGES)

DCP MIDSTREAM LINAM RANCH AGI #1 AND #2 CUMULATIVE INJECTION DATA														
Month Ended	AGI #1 TAG Injection Temperature (°F)	AGI #1 Surface TAG Injection Pressure (psig)	AGI #1 Surface Casing Annulus Pressure (psig)	Injection/Casing Annular Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig)	AGI #1 Average Bottom Hole Temperature (°F)	Total Flowrate (MSCFPH)	AGI #1 Flowrate (MSCFPH)	AGI #2 Flowrate (MSCFPH)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	Injection/Casing Annular Pressure Differential (psig)	Notes
January 2012	Jan-12	Jan-12	Jan-12	114	1385	389								
February 2012	Feb-12	Feb-12	Feb-12	116	1448	1036								
March 2012	Mar-12	Mar-12	Mar-12	118	1475	1046								
April 2012	Apr-12	Apr-12	Apr-12	121	1474	1010								
May 2012	May-12	May-12	May-12	122	1419	555	864	120	120					Plant Workover and Shutdown
June 2012	Jun-12	Jun-12	Jun-12	118	1394	368	1025	113	113					Plant Workover and Shutdown
July 2012	Jul-12	Jul-12	Jul-12	121	1450	420	1030	148	148					
August 2012	Aug-12	Aug-12	Aug-12	122	1449	401	1048	137	137					
September 2012	Sep-12	Sep-12	Sep-12	122	1472	479	995	152	152					
October 2012	Oct-12	Oct-12	Oct-12	118	1482	442	1035	187	187					
November 2012	Nov-12	Nov-12	Nov-12	121	1539	376	1163	191	191					November 14, 2012 MIT Test
December 2012	Dec-12	Dec-12	Dec-12	117	1446	48	1398	155	155					
January 2013	Jan-13	Jan-13	Jan-13	120	1445	49	1397	151	151					
February 2013	Feb-13	Feb-13	Feb-13	121	1515	203	1311	174	174					
March 2013	Mar-13	Mar-13	Mar-13	120	1550	209	1340	179	179					
April 2013	Apr-13	Apr-13	Apr-13	121	1544	240	1304	178	178					April 30, 2013 MIT Test
May 2013	May-13	May-13	May-13	116	1514	515	1001	154	154					
June 2013	Jun-13	Jun-13	Jun-13	120	1541	449	1092	166	166					
July 2013	Jul-13	Jul-13	Jul-13	120	1560	182	1375	177	177					
August 2013	Aug-13	Aug-13	Aug-13	121	1565	94	1472	171	171					
September 2013	Sep-13	Sep-13	Sep-13	121	1575	74	1500	179	179					
October 2013	Oct-13	Oct-13	Oct-13	123	1594	91	1503	174	174					October 30, 2013 MIT Test
November 2013	Nov-13	Nov-13	Nov-13	121	1576	70	1506	171	171					
December 2013	Dec-13	Dec-13	Dec-13	124	1607	69	1538	175	175					
January 2014	Jan-14	Jan-14	Jan-14	121	1574	8	1566	164	164					
February 2014	Feb-14	Feb-14	Feb-14	126	1639	111	1528	187	187					
March 2014	Mar-14	Mar-14	Mar-14	121	1579	11	1568	182	182					
April 2014	Apr-14	Apr-14	Apr-14	123	1615	87	1547	175	175					April 30, 2014 MIT Test
May 2014	May-14	May-14	May-14	123	1625	344	1280	170	170					
June 2014	Jun-14	Jun-14	Jun-14	121	1603	325	1277	162	162					
July 2014	Jul-14	Jul-14	Jul-14	123	1636	393	1243	167	167					
August 2014	Aug-14	Aug-14	Aug-14	122	1624	348	1275	161	161					
September 2014	Sep-14	Sep-14	Sep-14	122	1620	293	1327	158	158					September 15, 2014 MIT Test
October 2014	Oct-14	Oct-14	Oct-14	123	1648	364	1284	170	170					
November 2014	Nov-14	Nov-14	Nov-14	123	1610	146	1464	158	158					
December 2014	Dec-14	Dec-14	Dec-14	124	1640	211	1450	168	168					
January 2015	Jan-15	Jan-15	Jan-15	125	1631	180	1451	151	151					
February 2015	Feb-15	Feb-15	Feb-15	123	1649	242	1407	161	161					
March 2015	Mar-15	Mar-15	Mar-15	124	1627	270	1357	161	161					March 19, 2015 MIT Test
April 2015	Apr-15	Apr-15	Apr-15	124	1647	393	1254	163	163					
May 2015	May-15	May-15	May-15	122	1645	358	1287	159	159					
June 2015	Jun-15	Jun-15	Jun-15	121	1629	259	1375	152	152					
July 2015	Jul-15	Jul-15	Jul-15	120	1620	241	1378	154	154					
August 2015	Aug-15	Aug-15	Aug-15	123	1613	287	1327	131	131					
September 2015	Sep-15	Sep-15	Sep-15	124	1654	318	1336	163	163					September 15, 2015 MIT Test
October 2015	Oct-15	Oct-15	Oct-15	124	1662	191	1471	160	160					AGI #2 Operations Began October 2015
November 2015	Nov-15	Nov-15	Nov-15	79	1280	7	1273	164	164	109	1430	394	1035	AGI #1 & #2 both in use
December 2015	Dec-15	Dec-15	Dec-15	102	1457	32	1425	151	151	111	1498	494	1004	AGI #1 & #2 both in use
January 2016	Jan-16	Jan-16	Jan-16	121	1587	139	1428	117	117	77	1094	0	1094	AGI #2 not in use
February 2016	Feb-16	Feb-16	Feb-16	121	1645	203	1444	191	191	40	1609	0	1609	AGI #2 not in use
March 2016	Mar-16	Mar-16	Mar-16	118	1679	264	1411	158	158	58	1679	1	1678	AGI #2 not in use
April 2016	Apr-16	Apr-16	Apr-16	116	1682	279	1400	144	144	63	1688	1	1687	AGI #2 not in use
May 2016	May-16	May-16	May-16	116	1678	250	1428	185	185	70	1685	1	1684	AGI #2 not in use

Month Ended				AGI #1 TAG Injection Temperature (°F)	AGI #1 Surface TAG Injection Pressure (psig)	AGI #1 Surface Casing Annulus Pressure (psig)	Injection/Casing Annulus Pressure Differential (psig)	AGI #1 Average Bottom Hole Pressure (psig)	AGI #1 Average Bottom Hole Temperature (°F)	Total Flowrate (MSCFPH)	AGI #1 Flowrate (MSCFPH)	AGI #2 Flowrate (MSCFPH)	AGI #2 Surface TAG Injection Temperature (°F)	AGI #2 Surface TAG Injection Pressure (psig)	AGI #2 Surface Casing Annulus Pressure (psig)	Injection/Casing Annulus Pressure Differential (psig)	Notes
June	2016	Jun-16	Jun-16	108	1624	70	1554	191	191	191	191	81	2	1	1	AGI #2 not in use. TAG trapped in blocked off section of AGI #2 pipe blown down	
July	2016	Jul-16	Jul-16	114	1693	226	1467	196	196	196	196	88	2	1	1	AGI #2 not in use	
August	2016	Aug-16	Aug-16	111	1715	168	1547	213	213	213	213	78	3	1	2	AGI #2 not in use	
September	2016	Sep-16	Sep-16	105	1657	337	1320	188	188	188	188	73	3	1	2	AGI #2 not in use	
October	2016	Oct-16	Oct-16	101	1644	400	1264	223	223	223	223	68	2	0	2	AGI #2 not in use	
November	2016	Nov-16	Nov-16	117	1743	862	881	185	185	185	185	54	1	0	1	AGI #2 not in use	
December	2016	Dec-16	Dec-16	117	1688	809	889	153	153	153	153	43	1	0	1	AGI #1 not in use	
January	2017	Jan-17	Jan-17	118	1780	934	796	179	179	179	179	45	8	0	8	AGI #2 not in use	
February	2017	Feb-17	Feb-17	119	1750	998	791	186	186	186	186	0	54	10	278	267 Both wells used. #2 flow meter not functioning. AGI #1 for entire month and AGI #2 only from 3-13 to 3-16 and 3-21 to 3-31	
March	2017	Mar-17	Mar-17	114	1708	782	927	186	186	186	186	104	1705	373	1323	Both wells used. Flow meter for #2 not working. TAG routed to #1 well exclusively, both wells simultaneously and #2 well exclusively. All TAG routed to #2 from 4-26 onward in anticipation of workover of #1 well.	
April	2017	Apr-17	Apr-17	105	1651	418	1234	194	194	194	194	100	1862	296	1566	Both wells used. #2 Flow Meter not working. TAG Routed to AGI #2 save for 19 hour period from 5-17 to 5-18 when it was routed to AGI #1. AGI #1 workover 5-22 thru 6-8. AGI #2 experienced mechanical blockage resulting in both wells being shut down from 5-29 to 5-31.	
May	2017	May-17	May-17	103	1596	203	1390	155	155	155	155	104	1842	66	1772	Both wells used. #2 used from 6-2 through 6-15. Workover of #1 completed 6-8 and successful MIT performed 6-8. #1 back online 6-15. #1 and #2 used simultaneously from 6-15 to 6-30. Mechanical Problem with flow meter for #2 well. Only total flow can be measured; no way to differentiate between #1 and #2 when they are used together.	
June	2017	Jun-17	Jun-17	99	1489	429	1010	147	147	147	147	113	1838	1	1837	Both wells used. Annular Pressure Meter for AGI #2 malfunctioning for month of July. Mechanical problem with flow meter for #2 well persists. Bottomhole sensor added to #1 Well as part of workover completed in June and began recording data on 7-20-17	
July	2017	Jul-17	Jul-17	91	1409	302	1108	492	137	171	171	102	1810	sensor error	n/a	Both wells used. Mechanical problem with flow meter for #1 well persists. Only total flow data available. Annular Pressure meter for AGI #2 back in service 8-11-17. Annular Pressure and differential pressure readings are for period 8-11-17 through 8-31-17.	
August	2017	Aug-17	Aug-17	99	1572	621	950	454	134	187	187	83	1400	192	1064	Only AGI #1 used. Entire plant shut down from Sept 19 to Sept 30th for a scheduled turnaround. Data available only for first 19 days of September	
September	2017	Sep-17	Sep-17	109	1685	482	1203	458	135	197	197	77	1267	134	1132	Plant shutdown 9-19 through 10-3 for a turnaround. Only AGI #1 used during remainder of month. Major software upgrade in DCS. BH sensors not yet integrated into DCS.	
October	2017	Oct-17	Oct-17	102	1591	211	1321	476	136	152	152	63	872	97	778	Only AGI #1 in use in November. BH sensors not reconnected to DCS until 11-29	
November	2017	Nov-17	Nov-17	101	1589	428	1161	408	136	189	189	56	1015	82	931	Only AGI #1 in use in December.	
December	2017	Dec-17	Dec-17	107	1707	456	1252	408	136	191	191	44	1102	84	1017	Only AGI #1 in use in December.	
Average for 2017				106	1614	519	1095	431.6	146	179	182	0	79	1227	146	1015	
Standard Deviation 2017				9	107	245	191	1	17	15	0		24	639	138	632	
Average for Entire Period				116.4	1593.3	348.1	1235.0	431.7	135.9	167.3	167.0	0.0	75.7	977.5	99.9	918.3	
Standard Deviation Entire Period				9.3	97.4	264.5	279.8	195.3	0.9	20.2	20.6	0.0	22.1	751.7	146.4	706.8	
OPERATING CONSTRAINTS BASED ON NMOCC ORDER AND ACO 275																	
MADP in NMOCC Order is 2664 psig																	
Immediate Notification Parameters of ACO 275 and NMOCC Order																	
1. Injection/Annulus Differential Pressure 100 psig																	
2. Annulus Pressure > 1200psig																	



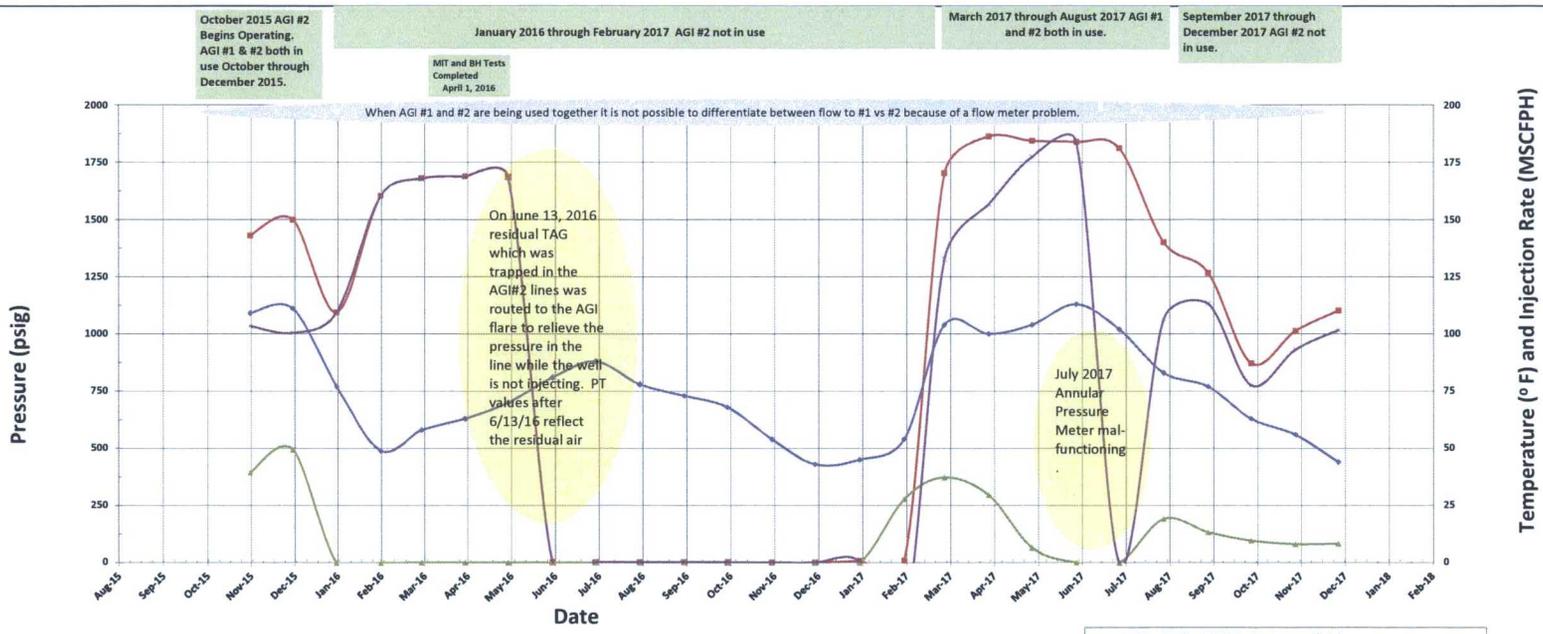


Figure 2 DCP Midstream Linam AGI #2 All Injection Data

Figure 3 DCP Midstream Linam AGI #1 and #2 Combined Total Flowrate (MSCFPH)
(May 2012 through January 2017)

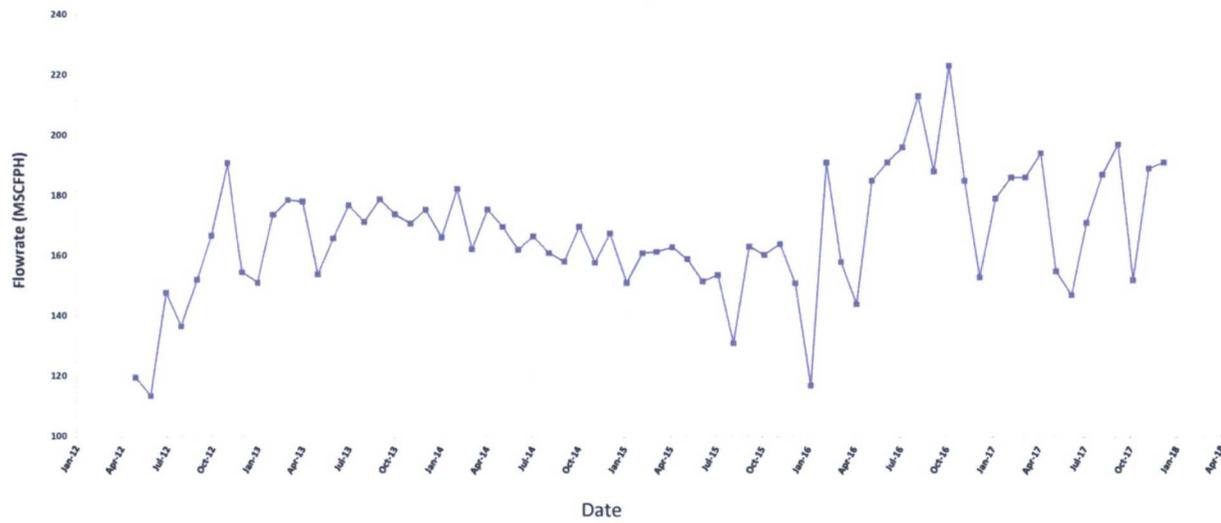
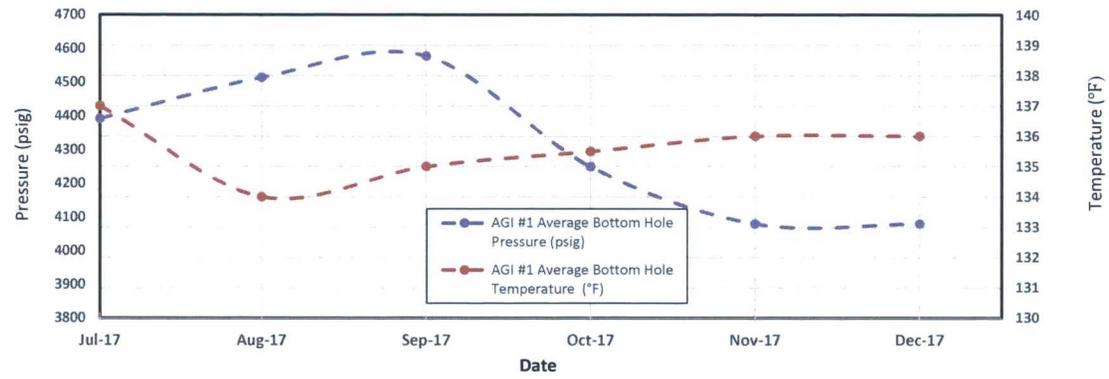


FIGURE 4 BOTTOM HOLE PRESSURE AND TEMPERATURE - AGI #1



Note: Bottom Hole Sensors Installed During Workover Completed June 2017 in AGI#1