PECOS DISTRICT DRILLING
CONDITIONS OF APPROVAL

OPERATOR'S NAME:	**Matador Production Company**
LEASE NO.:	**NMNM-086150**
WELL NAME & NO.:	**Brad Dyer Federal 206H**
SURFACE HOLE FOOTAGE:	**0329' FSL & 2219' FWL**
BOTTOM HOLE FOOTAGE	**0240' FNL & 2310' FWL**
LOCATION:	**Section 35, T. 22 S., R 32 E., NMPM**
COUNTY:	**County, New Mexico**

10M will need to be used for drilling below 9-5/8" shoe as the 7-5/8" X 7" will be in the Wolfcamp and average mud weight is 12 lb per e-mail exchange with Matador on 06/11/2018.

A. DRILLING OPERATIONS REQUIREMENTS

The BLM is to be notified in advance for a representative to witness:

a. Spudding well (minimum of 24 hours)
b. Setting and/or Cementing of all casing strings (minimum of 4 hours)
c. BOPE tests (minimum of 4 hours)

☐ **Lea County**
Call the Hobbs Field Station, 414 West Taylor, Hobbs NM 88240,
(575) 3933612

1. A Hydrogen Sulfide (H2S) Drilling Plan shall be activated 500 feet prior to drilling into the **Delaware** formation. **As a result, the Hydrogen Sulfide area must meet Onshore Order 6 requirements, which includes equipment and personnel/public protection items. If Hydrogen Sulfide is encountered, please provide measured values and formations to the BLM.**

2. Unless the production casing has been run and cemented or the well has been properly plugged, the drilling rig shall not be removed from over the hole without prior approval. **If the drilling rig is removed without approval – an Incident of Non-Compliance will be written and will be a "Major" violation.**

3. Floor controls are required for 3M or Greater systems. These controls will be on the rig floor, unobstructed, readily accessible to the driller and will be operational at all times during drilling and/or completion activities. Rig floor is defined as the area immediately around the rotary table; the area immediately above the substructure on which the draw works is located, this does not include the dog house or stairway area.

4. **The record of the drilling rate along with the GR/N well log run from TD to surface (horizontal well – vertical portion of hole) shall be submitted to the BLM office as well as all other logs run on the borehole 30 days from completion. If available, a digital copy of the logs is to be submitted in addition to the paper copies. The Rustler top and top and bottom of Salt are to be recorded on the Completion Report.**

B. CASING

Changes to the approved APD casing program need prior approval if the items substituted are of lesser grade or different casing size or are Non-API. The Operator can exchange the components of the proposal with that of superior strength (i.e. changing from J-55 to N-80, or from 36# to 40#). Changes to the approved cement program need prior approval if the altered cement plan has less volume or strength or if the changes are substantial (i.e. Multistage tool, ECP, etc.). The initial wellhead installed on the well will remain on the well with spools used as needed.

Centralizers required on surface casing per Onshore Order 2.III.B.1.f.

Wait on cement (WOC) for Water Basin:
After cementing but before commencing any tests, the casing string shall stand cemented under pressure until both of the following conditions have been met: 1) cement reaches a minimum compressive strength of 500 psi at the shoe, 2) until cement has been in place at least 8 hours. WOC time will be recorded in the driller's log. See individual casing strings for details regarding lead cement slurry requirements.

Provide compressive strengths including hours to reach required 500 pounds compressive strength prior to cementing each casing string. Have well specific cement details onsite prior to pumping the cement for each casing string.

No pea gravel permitted for remedial or fall back remedial without prior authorization from the BLM engineer.

Possibility of water flows in the Salado and Castile.
Possibility of lost circulation in the Red Beds, Rustler, and Delaware.
Abnormal pressures may be encountered when penetrating the 3rd Bone Spring Sandstone and all subsequent formations.

1. The **13-3/8** inch surface casing shall be set at approximately **1235** feet (a minimum of 25 feet into the Rustler Anhydrite and above the salt) and cemented to the surface. **If salt is encountered, set casing at least 25 feet above the salt.**

    a. If cement does not circulate to the surface, the appropriate BLM office shall be notified and a temperature survey utilizing an electronic type temperature survey with surface log readout will be used or a cement bond log shall be run to verify the top of the cement. Temperature survey will be run a minimum of six hours after pumping cement and ideally between 8-10 hours after completing the cement job.

    b. **Wait on cement (WOC) time for a primary cement job is to include the lead cement slurry.**

    c. Wait on cement (WOC) time for a remedial job will be a minimum of 4 hours after bringing cement to surface or 500 pounds compressive strength, whichever is greater.

    d. If cement falls back, remedial cementing will be done prior to drilling out that string.

Formation below the 13-3/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe and the mud weight for the bottom of the hole. Report results to BLM office.

9-5/8'' Intermediate casing shall be kept fluid filled while running into hole to meet BLM minimum collapse requirements.

2. The minimum required fill of cement behind the **9-5/8** inch 1st intermediate casing is:

    ☐ Cement to surface. If cement does not circulate see B.1.a, c-d above.

Formation below the 9-5/8" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe (not the mud weight required to prevent dissolving the salt formation) and the mud weight for the bottom of the hole. Report results to BLM office

3. The minimum required fill of cement behind the **7-5/8 X 7** inch intermediate casing is:

    ☐ Cement should tie-back at least 200 feet into previous casing string. Operator shall provide method of verification.

Formation below the 7" shoe to be tested according to Onshore Order 2.III.B.1.i. Test to be done as a mud equivalency test using the mud weight necessary for the pore pressure of the formation below the shoe and the mud weight for the bottom of the hole. Report results to BLM office.

Centralizers required on horizontal leg, must be type for horizontal service and a minimum of one every other joint.

4. The minimum required fill of cement behind the **5-1/2 X 4-1/2** inch production casing is:

   ☐ Cement as proposed by operator. Operator shall provide method of verification.

5. If hardband drill pipe is rotated inside casing, returns will be monitored for metal. If metal is found in samples, drill pipe will be pulled and rubber protectors which have a larger diameter than the tool joints of the drill pipe will be installed prior to continuing drilling operations.

C. PRESSURE CONTROL

1. All blowout preventer (BOP) and related equipment (BOPE) shall comply with well control requirements as described in Onshore Oil and Gas Order No. 2 and API 53.

2. Variance approved to use flex line from BOP to choke manifold. Check condition of flexible line from BOP to choke manifold, replace if exterior is damaged or if line fails test. Line to be as straight as possible with no hard bends and is to be anchored according to Manufacturer's requirements. The flexible hose can be exchanged with a hose of equal size and equal or greater pressure rating. **Anchor requirements, specification sheet and hydrostatic pressure test certification matching the hose in service, to be onsite for review. These documents shall be posted in the company man's trailer and on the rig floor.** If the BLM inspector questions the straightness of the hose, a BLM engineer will be contacted and will review in the field or via picture supplied by inspector to determine if changes are required (operator shall expect delays if this occurs).

3. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the surface casing shoe shall be psi. **5M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.**

4. Minimum working pressure of the blowout preventer (BOP) and related equipment (BOPE) required for drilling below the **9-5/8** intermediate casing shoe shall be psi.

10M system requires an HCR valve, remote kill line and annular to match. The remote kill line is to be installed prior to testing the system and tested to stack pressure.

Variance approved to use a 5M annular. The annular must be tested to full working pressure (5000 psi.)

5. **Operator has the option to utilize a multi-bowl wellhead assembly.**
    a. **Wellhead shall be installed by manufacturer's representatives, submit documentation with subsequent sundry.**
    b. **If the welding is performed by a third party, the manufacturer's representative shall monitor the temperature to verify that it does not exceed the maximum temperature of the seal.**
    c. **Manufacturer representative shall install the test plug for the initial BOP test.**
    d. **Operator shall perform the 9-5/8" and 7-5/8 X 7" casing integrity tests to 70% of the casing burst. This will test the multi-bowl seals.**
    e. **If the cement does not circulate and one inch operations would have been possible with a standard wellhead, the well head shall be cut off, cementing operations performed and another wellhead installed.**

6. The appropriate BLM office shall be notified a minimum of hours in advance for a representative to witness the tests.

    a. In a water basin, for all casing strings utilizing slips, these are to be set as soon as the crew and rig are ready and any fallback cement remediation has been done. The casing cut-off and BOP installation can be initiated four hours after installing the slips, which will be approximately six hours after bumping the plug. For those casing strings not using slips, the minimum wait time before cut-off is eight hours after bumping the plug. BOP/BOPE testing can begin after cut-off or once cement reaches 500 psi compressive strength (including lead when specified), whichever is greater. However, if the float does not hold, cut-off cannot be initiated until cement reaches 500 psi compressive strength (including lead when specified).

    a. The tests shall be done by an independent service company utilizing a test plug **not a cup or J-packer**.

    b. The test shall be run on a 5000 psi chart for a 2-3M BOP/BOP, on a 10000 psi chart for a 5M BOP/BOPE and on a 15000 psi chart for a 10M BOP/BOPE. If a linear chart is used, it shall be a one hour chart. A circular chart shall have a maximum 2 hour clock. If a twelve hour or twenty-four hour chart is used, tester shall make a notation that it is run with a two hour clock.

    c. The results of the test shall be reported to the appropriate BLM office.

d. All tests are required to be recorded on a calibrated test chart. **A copy of the BOP/BOPE test chart and a copy of independent service company test will be submitted to the appropriate BLM office.**

e. The BOP/BOPE test shall include a low pressure test from 250 to 300 psi. The test will be held for a minimum of 10 minutes if test is done with a test plug and 30 minutes without a test plug. This test shall be performed prior to the test at full stack pressure.

f. BOP/BOPE must be tested by an independent service company within 500 feet of the top of the **Wolfcamp** formation if the time between the setting of the intermediate casing and reaching this depth exceeds 20 days. This test does not exclude the test prior to drilling out the casing shoe as per Onshore Order No. 2.

D. DRILLING MUD

Mud system monitoring equipment, with derrick floor indicators and visual and audio alarms, shall be operating before drilling into the **Wolfcamp** formation, and shall be used until production casing is run and cemented.

E. DRILL STEM TEST

If drill stem tests are performed, Onshore Order 2.III.D shall be followed.

F. WASTE MATERIAL AND FLUIDS

All waste (i.e. drilling fluids, trash, salts, chemicals, sewage, gray water, etc.) created as a result of drilling operations and completion operations shall be safely contained and disposed of properly at a waste disposal facility. No waste material or fluid shall be disposed of on the well location or surrounding area.

Porto-johns and trash containers will be on-location during fracturing operations or any other crew-intensive operations.

JAM 082318

PECOS DISTRICT
SURFACE USE
CONDITIONS OF APPROVAL

OPERATOR'S NAME:	MATADOR PRODUCTION COMPANY
LEASE NO.:	NMNM 086150
WELL NAME & NO.:	206H:BRAD DYER FEDERAL
SURFACE HOLE FOOTAGE:	329'/S & 2219'/W
BOTTOM HOLE FOOTAGE	240'/N & 2310'/W
LOCATION:	T-22S, R-32E, S35. NMPM
COUNTY:	LEA, NM

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Standard Conditions of Approval (COA) apply to this APD. If any deviations to these standards exist or special COAs are required, the section with the deviation or requirement will be checked below.

I. GENERAL PROVISIONS

The approval of the Application For Permit To Drill (APD) is in compliance with all applicable laws and regulations: 43 Code of Federal Regulations 3160, the lease terms, Onshore Oil and Gas Orders, Notices To Lessees, New Mexico Oil Conservation Division (NMOCD) Rules, National Historical Preservation Act As Amended, and instructions and orders of the Authorized Officer. Any request for a variance shall be submitted to the Authorized Officer on Form 3160-5, Sundry Notices and Report on Wells.

II. PERMIT EXPIRATION

If the permit terminates prior to drilling and drilling cannot be commenced within 60 days after expiration, an operator is required to submit Form 3160-5, Sundry Notices and Reports on Wells, requesting surface reclamation requirements for any surface disturbance. However, if the operator will be able to initiate drilling within 60 days after the expiration of the permit, the operator must have set the conductor pipe in order to allow for an extension of 60 days beyond the expiration date of the APD. (Filing of a Sundry Notice is required for this 60 day extension.)

III. ARCHAEOLOGICAL, PALEONTOLOGY & HISTORICAL SITES

Any cultural and/or paleontological resource discovered by the operator or by any person working on the operator's behalf shall immediately report such findings to the Authorized Officer. The operator is fully accountable for the actions of their contractors and subcontractors. The operator shall suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Authorized Officer. An evaluation of the discovery shall be made by the Authorized Officer to determine the appropriate actions that shall be required to prevent the loss of significant cultural or scientific values of the discovery. The operator shall be held responsible for the cost of the proper mitigation measures that the Authorized Officer assesses after consultation with the operator on the evaluation and decisions of the discovery. Any unauthorized collection or disturbance of cultural or paleontological resources may result in a shutdown order by the Authorized Officer.

IV. NOXIOUS WEEDS

The operator shall be held responsible if noxious weeds become established within the areas of operations. Weed control shall be required on the disturbed land where noxious weeds exist, which includes the roads, pads, associated pipeline corridor, and adjacent land affected by the establishment of weeds due to this action. The operator shall consult with the Authorized Officer for acceptable weed control methods, which include following EPA and BLM requirements and policies.

V. SPECIAL REQUIREMENT(S)

Timing Limitation Stipulation / Condition of Approval for lesser prairie-chicken: Oil and gas activities including 3-D geophysical exploration, and drilling will not be allowed in lesser prairie-chicken habitat during the period from March 1st through June 15th annually. During that period, other activities that produce noise or involve human activity, such as the maintenance of oil and gas facilities, pipeline, road, and well pad construction, will be allowed except between 3:00 am and 9:00 am. The 3:00 am to 9:00 am restriction will not apply to normal, around-the-clock operations, such as venting, flaring, or pumping, which do not require a human presence during this period. Additionally, no new drilling will be allowed within up to 200 meters of leks known at the time of permitting. Normal vehicle use on existing roads will not be restricted. Exhaust noise from pump jack engines must be muffled or otherwise controlled so as not to exceed 75 db measured at 30 feet from the source of the noise.

Timing Limitation Exceptions:
The Carlsbad Field Office will publish an annual map of where the LPC timing and noise stipulations and conditions of approval (Limitations) will apply for the identified year (between March 1 and June 15) based on the latest survey information. The LPC Timing Area map will identify areas which are Habitat Areas (HA), Isolated Population Area (IPA), and Primary Population Area (PPA). The LPC Timing Area map will also have an area in red crosshatch. The red crosshatch area is the only area where an operator is required to submit a request for exception to the LPC Limitations. If an operator is operating outside the red crosshatch area, the LPC Limitations do not apply for that year and an exception to LPC Limitations is not required.

Ground-level Abandoned Well Marker to avoid raptor perching: Upon the plugging and subsequent abandonment of the well, the well marker will be installed at ground level on a plate containing the pertinent information for the plugged well. For more installation details, contact the Carlsbad Field Office at 575-234-5972.

Fence Requirement
Where entry granted across a fence line, the fence must be braced and tied off on both sides of the passageway prior to cutting. Once the work is completed, the fence will be restored to its prior condition, or better. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fence(s).

Cattle Guard Requirement
Any new or existing cattle guards on the access route shall be repaired or replaced if they are damaged or have deteriorated beyond practical use. The operator shall be responsible for the condition of the existing cattle guards that are in place and are utilized during lease operations. Once the road is abandoned, the fence would be restored to its prior condition, or better. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fences.

Livestock Watering Requirement
Structures that provide water to livestock, such as windmills, pipelines, drinking troughs, and earthen reservoirs, will be avoided by moving the proposed action.

Any damage to fences, cattle guards, and pipelines or structures that provide water to livestock during construction, throughout the life of the project, and caused by its operation, must be immediately corrected by Matador. Matador must notify the grazing allottee or the private surface landowner and the BLM-CFO (575-234-5972) if any damage occurs to pipelines or structures that provide water to livestock.

Production facilities on the well pads would be bermed to prevent oil, salt, and other chemical contaminants from leaving the pads. Topsoil shall not be used to construct the berm. No water flow from the uphill side(s) of the pad shall be allowed to enter the well pad. The berm shall be maintained through the life of the well and after interim reclamation has been completed.

Any water erosion that may occur due to the construction of the well pad during the life of the well will be quickly corrected and proper measures will be taken to prevent future erosion. Stockpiling of topsoil is required. The top soil shall be stockpiled in an appropriate location to prevent loss of soil due to water or wind erosion and not used for berming or erosion control.

VI. CONSTRUCTION

A. NOTIFICATION

The BLM shall administer compliance and monitor construction of the access road and well pad. Notify the Carlsbad Field Office at (575) 234-5909 at least 3 working days prior to commencing construction of the access road and/or well pad.

When construction operations are being conducted on this well, the operator shall have the approved APD and Conditions of Approval (COA) on the well site and they shall be made available upon request by the Authorized Officer.

B. TOPSOIL

The operator shall strip the top portion of the soil (root zone) from the entire well pad area and stockpile the topsoil along the edge of the well pad as depicted in the APD. The root zone is typically six (6) inches in depth. All the stockpiled topsoil will be redistributed over the interim reclamation areas. Topsoil shall not be used for berming the pad or facilities. For final reclamation, the topsoil shall be spread over the entire pad area for seeding preparation.

Other subsoil (below six inches) stockpiles must be completely segregated from the topsoil stockpile. Large rocks or subsoil clods (not evident in the surrounding terrain) must be buried within the approved area for interim and final reclamation.

C. CLOSED LOOP SYSTEM

Tanks are required for drilling operations: No Pits.

The operator shall properly dispose of drilling contents at an authorized disposal site.

D. FEDERAL MINERAL MATERIALS PIT

Payment shall be made to the BLM prior to removal of any federal mineral materials. Call the Carlsbad Field Office at (575) 234-5972.

E. WELL PAD SURFACING

Surfacing of the well pad is not required.

If the operator elects to surface the well pad, the surfacing material may be required to be removed at the time of reclamation. The well pad shall be constructed in a manner which creates the smallest possible surface disturbance, consistent with safety and operational needs.

F. EXCLOSURE FENCING (CELLARS & PITS)

Exclosure Fencing
The operator will install and maintain exclosure fencing for all open well cellars to prevent access to public, livestock, and large forms of wildlife before and after drilling operations until the pit is free of fluids and the operator initiates backfilling. (For examples of exclosure fencing design, refer to BLM's Oil and Gas Gold Book, Exclosure Fence Illustrations, Figure 1, Page 18.)

G. ON LEASE ACCESS ROADS

Road Width
The access road shall have a driving surface that creates the smallest possible surface disturbance and does not exceed fourteen (14) feet in width. The maximum width of surface disturbance, when constructing the access road, shall not exceed twenty-five (25) feet.

Surfacing
Surfacing material is not required on the new access road driving surface. If the operator elects to surface the new access road or pad, the surfacing material may be required to be removed at the time of reclamation.

Where possible, no improvements should be made on the unsurfaced access road other than to remove vegetation as necessary, road irregularities, safety issues, or to fill low areas that may sustain standing water.

The Authorized Officer reserves the right to require surfacing of any portion of the access road at any time deemed necessary. Surfacing may be required in the event the road deteriorates, erodes, road traffic increases, or it is determined to be beneficial for future field development. The surfacing depth and type of material will be determined at the time of notification.

Crowning
Crowning shall be done on the access road driving surface. The road crown shall have a grade of approximately 2% (i.e., a 1" crown on a 14' wide road). The road shall conform to Figure 1; cross section and plans for typical road construction.

Ditching
Ditching shall be required on both sides of the road.

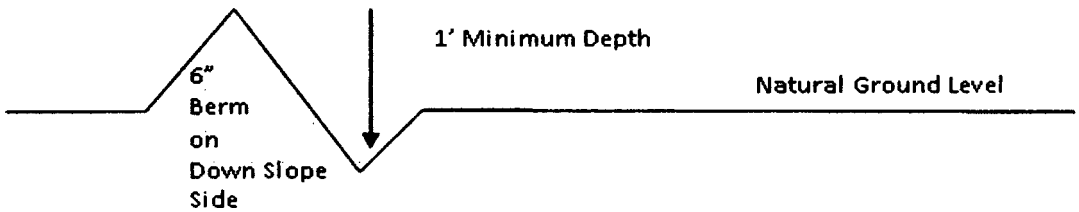
Turnouts
Vehicle turnouts shall be constructed on the road. Turnouts shall be intervisible with interval spacing distance less than 1000 feet. Turnouts shall conform to Figure 1; cross section and plans for typical road construction.

Drainage

Drainage control systems shall be constructed on the entire length of road (e.g. ditches, sidehill outsloping and insloping, lead-off ditches, culvert installation, and low water crossings).

A typical lead-off ditch has a minimum depth of 1 foot below and a berm of 6 inches above natural ground level. The berm shall be on the down-slope side of the lead-off ditch.

Cross Section of a Typical Lead-off Ditch



All lead-off ditches shall be graded to drain water with a 1 percent minimum to 3 percent maximum ditch slope. The spacing interval are variable for lead-off ditches and shall be determined according to the formula for spacing intervals of lead-off ditches, but may be amended depending upon existing soil types and centerline road slope (in %);

Formula for Spacing Interval of Lead-off Ditches

Example - On a 4% road slope that is 400 feet long, the water flow shall drain water into a lead-off ditch. Spacing interval shall be determined by the following formula:

400 foot road with 4% road slope: $\frac{400'}{4\%} + 100' = 200'$ lead-off ditch interval

Cattle guards

An appropriately sized cattle guard sufficient to carry out the project shall be installed and maintained at fence/road crossings. Any existing cattle guards on the access road route shall be repaired or replaced if they are damaged or have deteriorated beyond practical use. The operator shall be responsible for the condition of the existing cattle guards that are in place and are utilized during lease operations.

Fence Requirement

Where entry is granted across a fence line, the fence shall be braced and tied off on both sides of the passageway prior to cutting. The operator shall notify the private surface landowner or the grazing allotment holder prior to crossing any fences.

Public Access

Public access on this road shall not be restricted by the operator without specific written approval granted by the Authorized Officer.

Construction Steps

1. Salvage topsoil
2. Construct road
3. Redistribute topsoil
4. Revegetate slopes

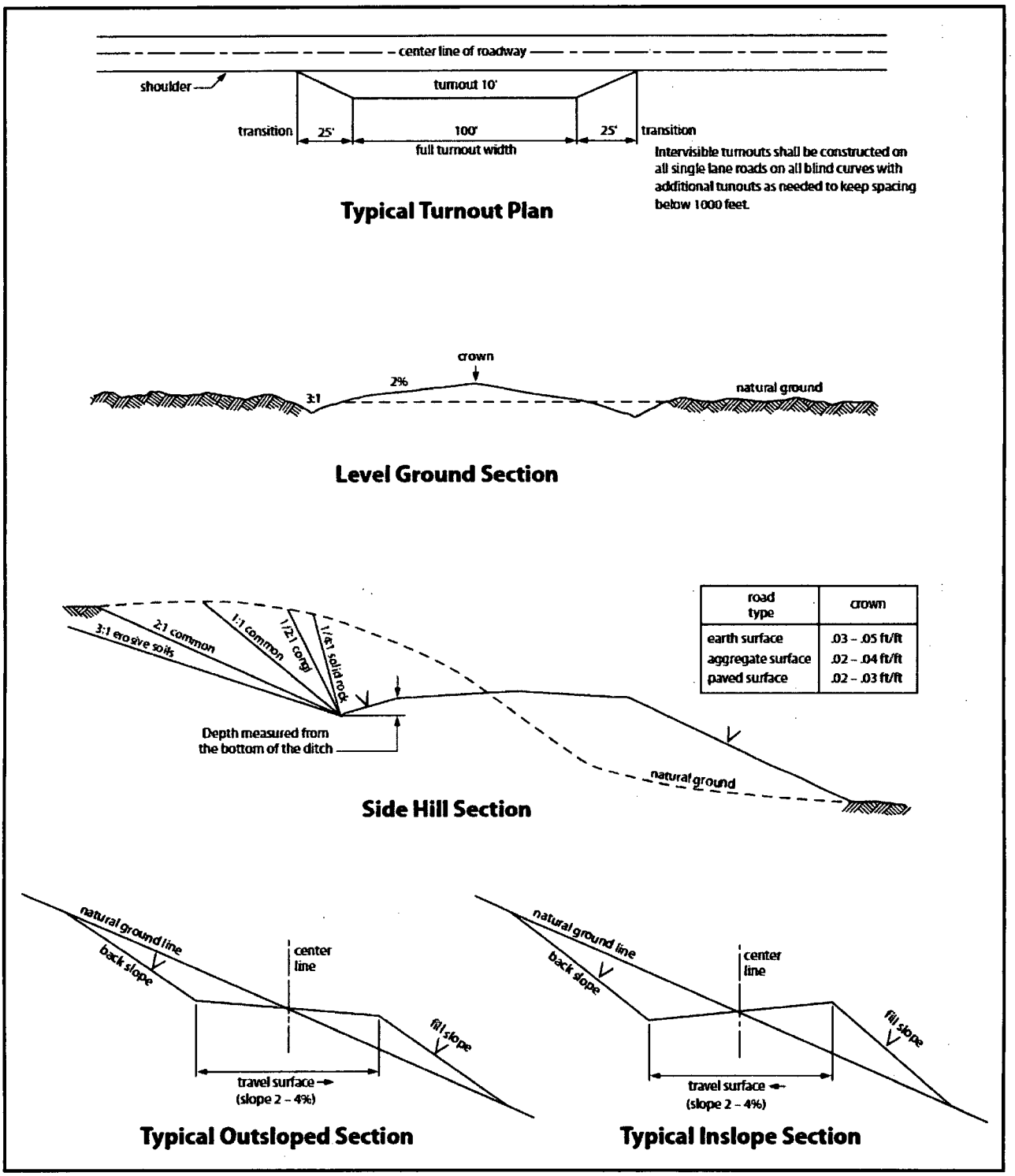


Figure 1. Cross-sections and plans for typical road sections representative of BLM resource or FS local and higher-class roads.

VII. PRODUCTION (POST DRILLING)

A. WELL STRUCTURES & FACILITIES

Placement of Production Facilities
Production facilities should be placed on the well pad to allow for maximum interim recontouring and revegetation of the well location.

Exclosure Netting (Open-top Tanks)
Immediately following active drilling or completion operations, the operator will take actions necessary to prevent wildlife and livestock access, including avian wildlife, to all open-topped tanks that contain or have the potential to contain salinity sufficient to cause harm to wildlife or livestock, hydrocarbons, or Resource Conservation and Recovery Act of 1976-exempt hazardous substances. At a minimum, the operator will net, screen, or cover open-topped tanks to exclude wildlife and livestock and prevent mortality. If the operator uses netting, the operator will cover and secure the open portion of the tank to prevent wildlife entry. The operator will net, screen, or cover the tanks until the operator removes the tanks from the location or the tanks no longer contain substances that could be harmful to wildlife or livestock. Use a maximum netting mesh size of 1 ½ inches. The netting must not be in contact with fluids and must not have holes or gaps.

Chemical and Fuel Secondary Containment and Exclosure Screening
The operator will prevent all hazardous, poisonous, flammable, and toxic substances from coming into contact with soil and water. At a minimum, the operator will install and maintain an impervious secondary containment system for any tank or barrel containing hazardous, poisonous, flammable, or toxic substances sufficient to contain the contents of the tank or barrel and any drips, leaks, and anticipated precipitation. The operator will dispose of fluids within the containment system that do not meet applicable state or U. S. Environmental Protection Agency livestock water standards in accordance with state law; the operator must not drain the fluids to the soil or ground. The operator will design, construct, and maintain all secondary containment systems to prevent wildlife and livestock exposure to harmful substances. At a minimum, the operator will install effective wildlife and livestock exclosure systems such as fencing, netting, expanded metal mesh, lids, and grate covers. Use a maximum netting mesh size of 1 ½ inches.

Open-Vent Exhaust Stack Exclosures
The operator will construct, modify, equip, and maintain all open-vent exhaust stacks on production equipment to prevent birds and bats from entering, and to discourage perching, roosting, and nesting. (*Recommended exclosure structures on open-vent exhaust stacks are in the shape of a cone.*) Production equipment includes, but may not be limited to, tanks, heater-treaters, separators, dehydrators, flare stacks, in-line units, and compressor mufflers.

Containment Structures

Proposed production facilities such as storage tanks and other vessels will have a secondary containment structure that is constructed to hold the capacity of 1.5 times the largest tank, plus freeboard to account for precipitation, unless more stringent protective requirements are deemed necessary.

Painting Requirement
All above-ground structures including meter housing that are not subject to safety requirements shall be painted a flat non-reflective paint color, **Shale Green** from the BLM Standard Environmental Color Chart (CC-001: June 2008).

B. ELECTRIC LINES

STANDARD STIPULATIONS FOR OVERHEAD ELECTRIC DISTRIBUTION LINES

A copy of the grant and attachments, including stipulations, survey plat and/or map, will be on location during construction. BLM personnel may request to you a copy of your permit during construction to ensure compliance with all stipulations.

Holder agrees to comply with the following stipulations to the satisfaction of the Authorized Officer:

1. The holder shall indemnify the United States against any liability for damage to life or property arising from the occupancy or use of public lands under this grant.

2. The holder shall comply with all applicable Federal laws and regulations existing or hereafter enacted or promulgated. In any event, the holder shall comply with the Toxic Substances Control Act of 1976 as amended, 15 USC 2601 et seq. (1982) with regards to any toxic substances that are used, generated by or stored on the right-of-way or on facilities authorized under this right-of-way grant. (See 40 CFR, Part 702-799 and especially, provisions on polychlorinated biphenyls, 40 CFR 761.1-761.193.) Additionally, any release of toxic substances (leaks, spills, etc.) in excess of the reportable quantity established by 40 CFR, Part 117 shall be reported as required by the Comprehensive Environmental Response, Compensation, and Liability Act, section 102b. A copy of any report required or requested by any Federal agency or State government as a result of a reportable release or spill of any toxic substances shall be furnished to the authorized officer concurrent with the filing of the reports to the involved Federal agency or State government.

3. The holder agrees to indemnify the United States against any liability arising from the release of any hazardous substance or hazardous waste (as these terms are defined in the Comprehensive Environmental Response, Compensation and Liability Act of 1980, 42 U.S.C. 9601, et seq. or the Resource Conservation and Recovery Act, 42 U.S.C. 6901, et seq.) on the Right-of-Way (unless the release or threatened release is wholly unrelated to the Right-of-Way holder's activity on the Right-of-Way), or resulting from the activity of the Right-of-Way holder on the Right-of-Way. This agreement applies without regard to whether a release is caused by the holder, its agent, or unrelated third parties.

4. There will be no clearing or blading of the right-of-way unless otherwise agreed to in writing by the Authorized Officer.

5. Power lines shall be constructed and designed in accordance to standards outlined in "Suggested Practices for Avian Protection on Power lines: The State of the Art in 2006" Edison Electric Institute, APLIC, and the California Energy Commission 2006 . The holder shall assume the burden and expense of proving that pole designs not shown in the above publication deter raptor perching, roosting, and nesting. Such proof shall be provided by a raptor expert approved by the Authorized Officer. The BLM reserves the right to require modification or additions to all powerline structures placed on this right-of-way, should they be necessary to ensure the safety of large perching birds. Such modifications and/or additions shall be made by the holder without liability or expense to the United States.

Raptor deterrence will consist of but not limited to the following: triangle perch discouragers shall be placed on each side of the cross arms and a nonconductive perching deterrence shall be placed on all vertical poles that extend past the cross arms.

6. The holder shall minimize disturbance to existing fences and other improvements on public lands. The holder is required to promptly repair improvements to at least their former state. Functional use of these improvements will be maintained at all times. The holder will contact the owner of any improvements prior to disturbing them. When necessary to pass through a fence line, the fence shall be braced on both sides of the passageway prior to cutting the fence. No permanent gates will be allowed unless approved by the Authorized Officer.

7. The BLM serial number assigned to this authorization shall be posted in a permanent, conspicuous manner where the power line crosses roads and at all serviced facilities. Numbers will be at least two inches high and will be affixed to the pole nearest the road crossing and at the facilities served.

8. Upon cancellation, relinquishment, or expiration of this grant, the holder shall comply with those abandonment procedures as prescribed by the Authorized Officer.

9. All surface structures (poles, lines, transformers, etc.) shall be removed within 180 days of abandonment, relinquishment, or termination of use of the serviced facility or facilities or within 180 days of abandonment, relinquishment, cancellation, or expiration of this grant, whichever comes first. This will not apply where the power line extends service to an active, adjoining facility or facilities.

10. Any cultural and/or paleontological resource (historic or prehistoric site or object) discovered by the holder, or any person working on his behalf, on public or Federal land shall be immediately reported to the Authorized Officer. Holder shall suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Authorized Officer. An evaluation of the discovery will be made by the

Authorized Officer to determine appropriate actions to prevent the loss of significant cultural or scientific values. The holder will be responsible for the cost of evaluation and any decision as to proper mitigation measures will be made by the Authorized Officer after consulting with the holder.

11. Special Stipulations:
    - For reclamation remove poles, lines, transformer, etc. and dispose of properly.
    - Fill in any holes from the poles removed.

Timing Limitation Stipulation/Condition of Approval for Lesser Prairie-Chicken: Oil and gas activities including 3-D geophysical exploration, and drilling will not be allowed in lesser prairie-chicken habitat during the period from March 1st through June 15th annually. During that period, other activities that produce noise or involve human activity, such as the maintenance of oil and gas facilities, geophysical exploration other than 3-D operations, and pipeline, road, and well pad construction, will be allowed except between 3:00 am and 9:00 am. The 3:00 am to 9:00 am restriction will not apply to normal, around-the-clock operations, such as venting, flaring, or pumping, which do not require a human presence during this period. Additionally, no new drilling will be allowed within up to 200 meters of leks known at the time of permitting. Normal vehicle use on existing roads will not be restricted. Exhaust noise from pump jack engines must be muffled or otherwise controlled so as not to exceed 75 db measured at 30 ft. from the source of the noise.

VIII. INTERIM RECLAMATION

During the life of the development, all disturbed areas not needed for active support of production operations should undergo interim reclamation in order to minimize the environmental impacts of development on other resources and uses.

Within six (6) months of well completion, operators should work with BLM surface management specialists (Jim Amos: 575-234-5909) to devise the best strategies to reduce the size of the location. Interim reclamation should allow for remedial well operations, as well as safe and efficient removal of oil and gas.

During reclamation, the removal of caliche is important to increasing the success of revegetating the site. Removed caliche that is free of contaminants may be used for road repairs, fire walls or for building other roads and locations. In order to operate the well or complete workover operations, it may be necessary to drive, park and operate on restored interim vegetation within the previously disturbed area. Disturbing revegetated areas for production or workover operations will be allowed. If there is significant disturbance and loss of vegetation, the area will need to be revegetated. Communicate with the appropriate BLM office for any exceptions/exemptions if needed.

All disturbed areas after they have been satisfactorily prepared need to be reseeded with the seed mixture provided below.

Upon completion of interim reclamation, the operator shall submit a Sundry Notices and Reports on Wells, Subsequent Report of Reclamation (Form 3160-5).

IX. FINAL ABANDONMENT & RECLAMATION

At final abandonment, well locations, production facilities, and access roads must undergo "final" reclamation so that the character and productivity of the land are restored.

Earthwork for final reclamation must be completed within six (6) months of well plugging. All pads, pits, facility locations and roads must be reclaimed to a satisfactory revegetated, safe, and stable condition, unless an agreement is made with the landowner or BLM to keep the road and/or pad intact.

After all disturbed areas have been satisfactorily prepared, these areas need to be revegetated with the seed mixture provided below. Seeding should be accomplished by drilling on the contour whenever practical or by other approved methods. Seeding may need to be repeated until revegetation is successful, as determined by the BLM.

Operators shall contact a BLM surface protection specialist prior to surface abandonment operations for site specific objectives (Jim Amos: 575-234-5909).

Ground-level Abandoned Well Marker to avoid raptor perching: Upon the plugging and subsequent abandonment of the well, the well marker will be installed at ground level on a plate containing the pertinent information for the plugged well.

Seed Mixture for LPC Sand/Shinnery Sites

Holder shall seed all disturbed areas with the seed mixture listed below. The seed mixture shall be planted in the amounts specified in pounds of pure live seed (PLS)* per acre. There shall be no primary or secondary noxious weeds in the seed mixture. Seed will be tested and the viability testing of seed shall be done in accordance with State law(s) and within nine (9) months prior to purchase. Commercial seed shall be either certified or registered seed. The seed container shall be tagged in accordance with State law(s) and available for inspection by the Authorized Officer.

Seed will be planted using a drill equipped with a depth regulator to ensure proper depth of planting where drilling is possible. The seed mixture will be evenly and uniformly planted over the disturbed area (smaller/heavier seeds have a tendency to drop the bottom of the drill and are planted first). Holder shall take appropriate measures to ensure this does not occur. Where drilling is not possible, seed will be broadcast and the area shall be raked or chained to cover the seed. When broadcasting the seed, the pounds per acre are to be doubled. Seeding shall be repeated until a satisfactory stand is established as determined by the Authorized Officer. Evaluation of growth may not be made before completion of at least one full growing season after seeding.

Species to be planted in pounds of pure live seed* per acre:

Species	lb/acre
Plains Bristlegrass	5lbs/A
Sand Bluestem	5lbs/A
Little Bluestem	3lbs/A
Big Bluestem	6lbs/A
Plains Coreopsis	2lbs/A
Sand Dropseed	1lbs/A

*Pounds of pure live seed:

Pounds of seed **x** percent purity **x** percent germination = pounds pure live seed

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 50 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.47 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.52 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
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Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Casing Design Criteria and Load Case Assumptions

Surface Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.43 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.52 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.43 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (8.3 ppg).

Intermediate #1 Casing

Collapse: DF_C=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.52 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.52 psi/ft), which is a more conservative backup force than pore pressure.
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Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (10.0 ppg).

Intermediate #2 Casing

Collapse: DF_C=1.125

- Partial Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.47 psi/ft). The effects of axial load on collapse will be considered. Internal force equal to gas gradient over half of setting depth and mud gradient with which the next hole section will be run below that (0.65 psi/ft).

- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.47 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: Casing test per Onshore Oil and Gas Order No. 2 with an external force equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Gas Kick Profile: Internal burst force at the shoe will be Fracture Pressure at that depth. Surface burst pressure will be fracture gradient at setting depth less a gas gradient to equivalent height of 100 bbl kick with Drill Pipe inside casing and mud gradient with which the next hole section will be run above that (0.65 psi/ft). External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft), which is a more conservative backup force than pore pressure.
- Fracture at Shoe with 1/3 BHP at Surface: Internal burst force at the shoe will be Fracture Pressure at setting depth. Internal burst force at surface will be 1/3 of pore pressure at setting depth. External force will be equal to the mud gradient in which the casing will be run (0.47 psi/ft) which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (9.0 ppg).

Production Casing

Collapse: DF_c=1.125

- Full Internal Evacuation: Collapse force equal to the mud gradient in which the casing will be run (0.65 psi/ft). The effects of axial load on collapse will be considered.
- Cementing: Collapse force equal to the gradient of planned cement slurries to planned depths and mud gradient in which the casing will be run above that (0.65 psi/ft) and an internal force equal to mud gradient of displacement fluid (0.43 psi/ft).

Burst: DF_b=1.125

- Pressure Test: 8000 psi casing test with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.
- Injection Down Casing: 9500 psi surface injection pressure plus an internal pressure gradient of 0.65 psi/ft with an external force equal to the mud gradient in which the casing will be run (0.65 psi/ft), which is a more conservative backup force than pore pressure.

Tensile: DF_t=1.8

- Overpull: A downward force of 100,000 lbs is applied at the shoe along with the weight of the casing string utilizing the effects of buoyancy (12.5 ppg).

Hydrogen Sulfide Drilling

Operations Plan

1 H2S Safety Instructions:

- Characteristics of H2S
- Physical effects and hazards
- Principal and operation of H2S detectors, warning system, and briefing areas
- Evacuation procedures, routes, and first aid
- Proper use of safety equipment & life support systems
- Essential personnel meeting medical evaluation criteria will receive additional training on the proper use of 30-minute pressure demand air packs

2 H2S Detection and Alarm Systems:

- H2S sensor/detectors will be located on the drill rig floor, in the base of the sub structure / cellar area, and on the mud pits in the shale shaker area. Additional H2S detectors may be placed as deemed necessary.
- An audio alarm system will be installed on the derrick floor and in the doghouse.

3 Windsocks and / Wind Streamers:

- Windsocks at mud tank area will be high enough to be visible.
- Windsock on the rig floor and / top of doghouse will be high enough to be visible.

4 Condition Flags and Signs:

- Warning sign on access road to location
- Flags to be displayed on sign at entrance to location
    - Green Flag – Normal Safe Operation Condition
    - Yellow Flag – Potential Pressure and Danger
    - Red Flag – Danger (H2S present in dangerous concentrations) Only H2S trained personnel admitted on location

5 Well Control Equipment:

- Attached

6 Communication:

- While working under masks, chalkboards will be used for communications.
- Hand signals will be used where chalk board is inappropriate.
- Two-way radio will be used to communicate off location in case of emergency help is required. In most cases cellular telephones will be available at most drilling foreman's trailer or living quarters.

7 Drilling Stem Testing:

- No DST or cores are planned at this time.

8 Drilling contractor supervisor will be required to be familiar with the effects H2S has on tubulars good and other mechanical equipment.

9 If H2S is encountered, then mud system will be altered if necessary to maintain control of formation. A mud gas separator will be brought into service along with H2S scavengers if necessary.

11 Emergency Contacts

- See next page.

H2S Contingency Plan Emergency Contacts
Brad Dyer Federal wells
Matador Production Company
Sec. 35, T22S, R32E Lea County, NM

Company Office			
Matador Production Company	(972)-371-5200		
Key Personnel			
Name	**Title**	**Office**	**Mobile**
Billy Goodwin	Vice President Drilling	972-371-5210	817-522-2928
Dee Smith	Drilling Superintendent	972-371-5447	972-822-1010
Adam Lange	Drilling Engineer	972-371-5292	214-458-0788
Lea County			
Ambulance		911	
Nor Lea General Hospital (Hobbs)		575-397-0560	
State Police (Hobbs)		575-392-5580	
City Police (Hobbs)		575-397-9625	
Sheriff's Office (Lovington)		575-396-3611	
Fire Marshall (Lovington)		575-391-2983	
Volunteer Fire Dept. (Eunice)		575-394-3258	
Emergency Management (Lovington)		575-391-2983	
New Mexico Oil Conservation Division (Hobbs)		575-393-6161	575-390-3186
BLM (Hobbs)		575-393-3612	
Hobbs Animal Clinic		575-392-5563	
Dal Paso Animal Hospital (Hobbs)		575-397-2286	
Mountain States Equine (Hobbs)		575-392-7488	
Carlsbad			
BLM		575-234-5972	
Santa Fe			
New Mexico Emergency Response Commission (Santa Fe)		505-476-9600	
New Mexico Emergency Response Commission (Santa Fe) 24 hours		505-827-9126	
New Mexico State Emergency Operations Center		505-476-9635	
National			
National Emergency Response Center (Washington, D.C.)		800-424-8802	
Medical			
Flight for Life- 4000 24th St.; Lubbock, TX		806-743-9911	
Aerocare- R3, Box 49F; Lubbock, TX		806-747-8923	
Med Flight Air Amb- 2301 Yale Blvd SE, D3; Albuquerque, NM		505-842-4433	
SB Air Med Service- 2505 Clark Carr Loop SE; Albuquerque, NM		505-842-4949	
Other			
Boots & Coots IWC		800-256-9688	or 281-931-8884
Cudd Pressure Control		432-699-0139	or 432-563-3356
Halliburton		575-746-2757	
B.J. Services		575-746-3569	
NM Dept. of Transportation (Roswell)		575-637-7200	

Rig Diagram

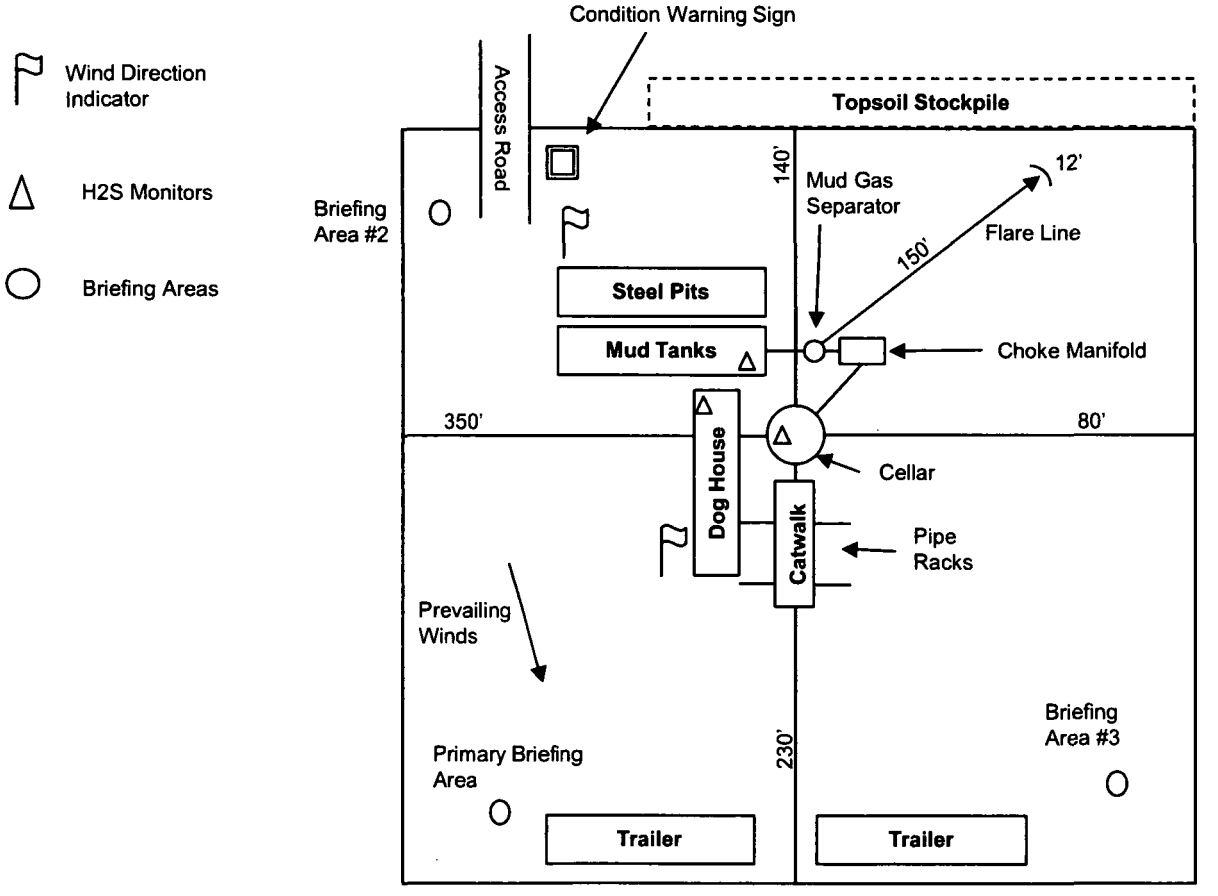


Exhibit E-3: Rig Diagram
Brad Dyer #206H
Matador Resources Company
35-22S-32E
SHL 329' FSL & 2219' FWL
BHL 240' FNL & 2310' FWL
Lea County, NM

Company: Matador Resources
Site: Brad Dyer 35-22S-32E AR
Well: #206H
Project: Lea County, New Mexico (NAD 27)
Rig: Patterson 282

MS Directional

ANNOTATIONS

MD	Inc	Azi	TVD	+N/-S	+E/-W	VSect	Departure	Annotation
1000.00	0.00	0.00	1000.00	0.00	0.00	0.00	0.00	KOP, 1.00°/100' Build
1399.91	4.00	161.46	1399.58	-13.23	4.44	-13.26	13.95	Begin 4.00° Tangent
5205.01	4.00	161.46	5195.42	-264.82	88.81	-265.42	279.32	Begin 1.00°/100' Drop
5604.91	0.00	0.00	5595.00	-278.05	93.25	-278.68	293.27	Begin Vertical Hold
11824.15	0.00	0.00	11814.24	-278.05	93.25	-278.68	293.27	Begin 10.00°/100' Build
12624.15	80.00	359.61	12378.49	195.40	90.03	194.79	766.73	Begin 6.00°/100' Build
12790.82	90.00	359.61	12393.00	361.22	88.89	360.61	932.56	Begin 90.00° Lateral
17143.70	90.00	359.61	12393.00	4714.00	59.00	4713.49	5285.44	PBHL

Azimuths to Grid North
True North: -0.37°
Magnetic North: 6.62°

Magnetic Field
Strength: 47983.2snT
Dip Angle: 60.13°
Date: 2/12/2018
Model: BGGM2017

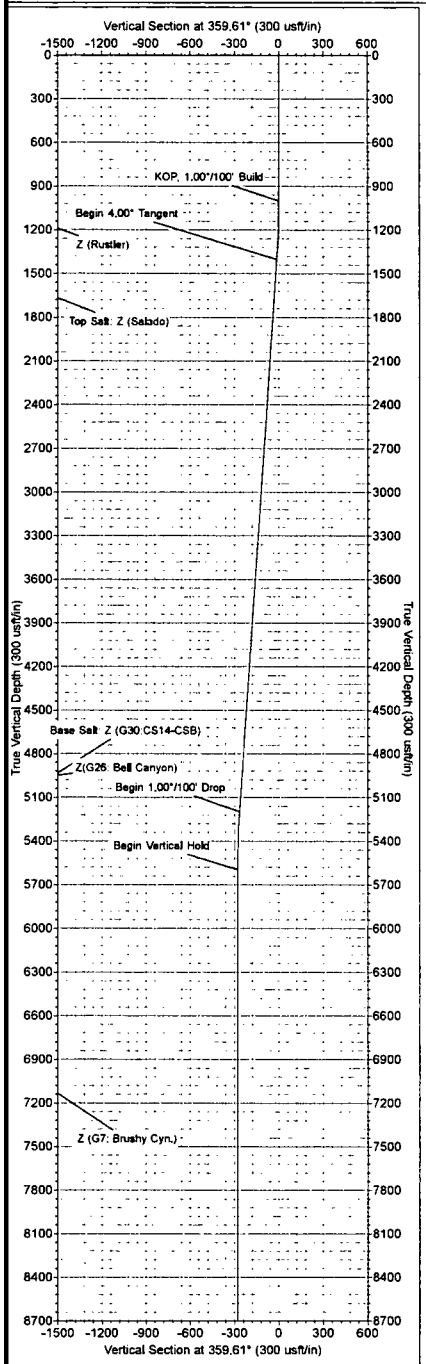
WELL DETAILS: #206H

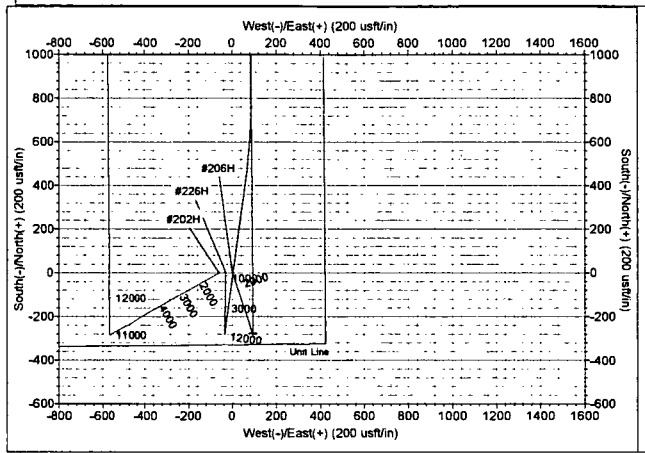
+N/-S	+E/-W	Northing	Easting	Latitude	Longitude
0.00	0.00	488723.00	712181.00	32° 20' 30.280 N	103° 38' 46.729 W

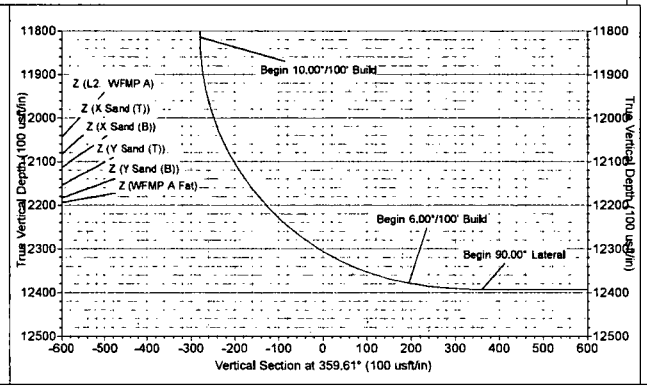
3732.00

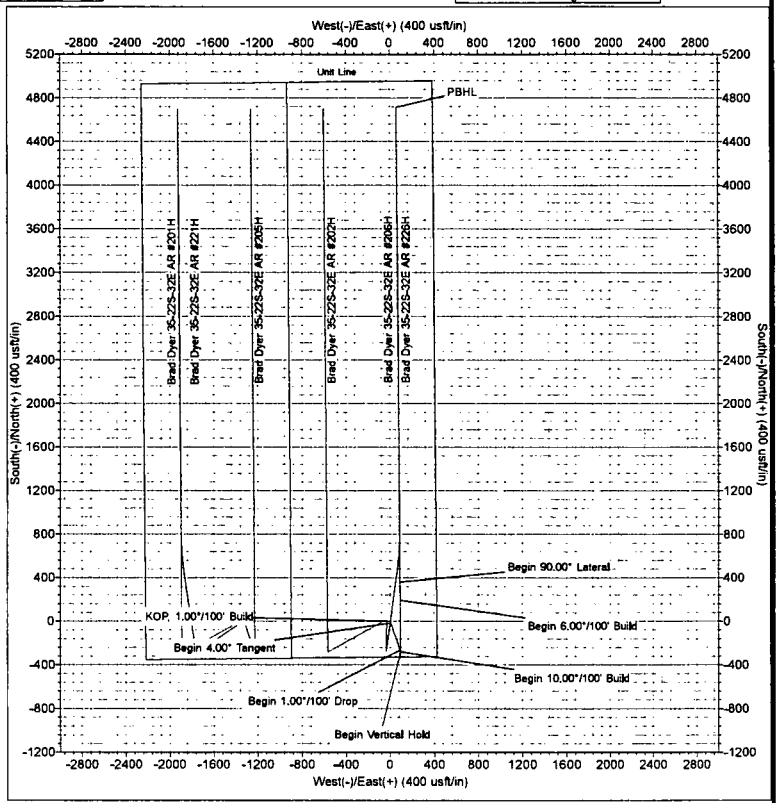
US State Plane 1927 (Exact solution)
New Mexico East 3001

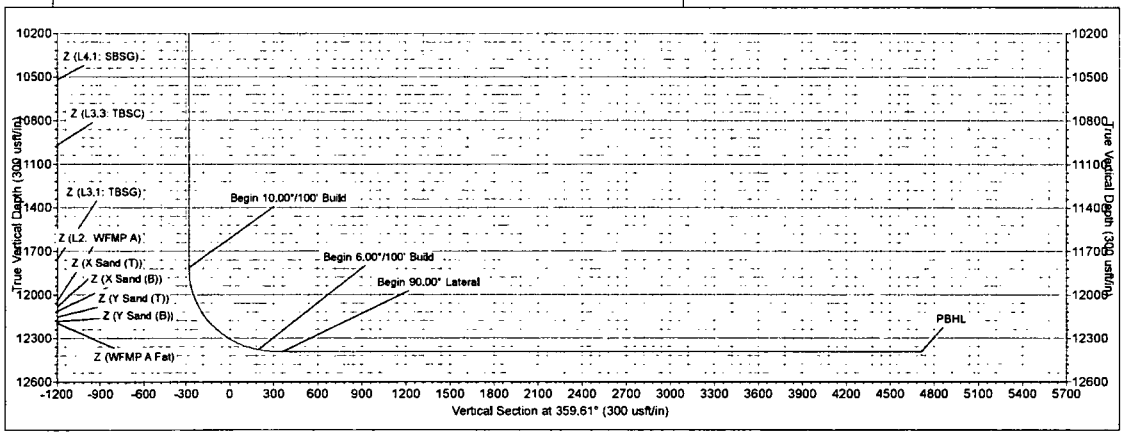
Created By: HLH
Date: 14:47, February 15 2018
Plan: Design #2











Matador Resources

Lea County, New Mexico (NAD 27)
Brad Dyer 35-22S-32E AR
#206H

Wellbore #1

Plan: Design #2

Standard Planning Report

15 February, 2018

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Project	Lea County, New Mexico (NAD 27)		
Map System:	US State Plane 1927 (Exact solution)	**System Datum:**	Mean Sea Level
Geo Datum:	NAD 1927 (NADCON CONUS)		
Map Zone:	New Mexico East 3001		

Well	#206H					
Well Position	**+N/-S**	488,723.00 usft	**Northing:**	488,723.00 usft	**Latitude:**	32° 20' 30.280 N
	+E/-W	712,181.00 usft	**Easting:**	712,181.00 usft	**Longitude:**	103° 38' 46.729 W
Position Uncertainty		0.00 usft	**Wellhead Elevation:**		**Ground Level:**	3,732.00 usft

Wellbore	Wellbore #1			
Magnetics	**Model Name**	**Sample Date**	**Declination (°)**	**Dip Angle (°)**	**Field Strength (nT)**
	BGGM2017	2/12/2018	6.99	60.13	47,983

Design	Design #2				
Audit Notes:					
Version:		**Phase:**	PROTOTYPE	**Tie On Depth:**	0.00
Vertical Section:	**Depth From (TVD) (usft)**	**+N/-S (usft)**	**+E/-W (usft)**	**Direction (°)**	
	0.00	0.00	0.00	359.61	

Plan Survey Tool Program **Date** 2/15/2018

	Depth From (usft)	Depth To (usft)	Survey (Wellbore)	Tool Name	Remarks
1	0.00	17,143.70	Design #2 (Wellbore #1)	MWD OWSG MWD - Standard	

Plan Sections

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00	
1,399.91	4.00	161.46	1,399.58	-13.23	4.44	1.00	1.00	0.00	161.46	
5,205.01	4.00	161.46	5,195.42	-264.82	88.81	0.00	0.00	0.00	0.00	
5,604.91	0.00	0.00	5,595.00	-278.05	93.25	1.00	-1.00	0.00	180.00	VP v2 - Brad Dyer #
11,824.15	0.00	0.00	11,814.24	-278.05	93.25	0.00	0.00	0.00	0.00	
12,624.15	80.00	359.61	12,378.49	195.40	90.03	10.00	10.00	0.00	359.61	
12,790.82	90.00	359.61	12,393.00	361.22	88.89	6.00	6.00	0.00	-0.02	
17,143.70	90.00	359.61	12,393.00	4,714.00	59.00	0.00	0.00	0.00	0.00	PBHL v2 - Brad Dy

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
KOP, 1.00°/100' Build									
1,100.00	1.00	161.46	1,099.99	-0.83	0.28	-0.83	1.00	1.00	0.00
1,200.00	2.00	161.46	1,199.96	-3.31	1.11	-3.32	1.00	1.00	0.00
1,300.00	3.00	161.46	1,299.86	-7.44	2.50	-7.46	1.00	1.00	0.00
1,399.91	4.00	161.46	1,399.58	-13.23	4.44	-13.26	1.00	1.00	0.00
Begin 4.00° Tangent									
1,500.00	4.00	161.46	1,499.43	-19.84	6.66	-19.89	0.00	0.00	0.00
1,600.00	4.00	161.46	1,599.19	-26.46	8.87	-26.52	0.00	0.00	0.00
1,700.00	4.00	161.46	1,698.94	-33.07	11.09	-33.14	0.00	0.00	0.00
1,800.00	4.00	161.46	1,798.70	-39.68	13.31	-39.77	0.00	0.00	0.00
1,900.00	4.00	161.46	1,898.46	-46.29	15.53	-46.40	0.00	0.00	0.00
2,000.00	4.00	161.46	1,998.21	-52.91	17.74	-53.02	0.00	0.00	0.00
2,100.00	4.00	161.46	2,097.97	-59.52	19.96	-59.65	0.00	0.00	0.00
2,200.00	4.00	161.46	2,197.73	-66.13	22.18	-66.28	0.00	0.00	0.00
2,300.00	4.00	161.46	2,297.48	-72.74	24.40	-72.91	0.00	0.00	0.00
2,400.00	4.00	161.46	2,397.24	-79.35	26.61	-79.53	0.00	0.00	0.00
2,500.00	4.00	161.46	2,497.00	-85.97	28.83	-86.16	0.00	0.00	0.00
2,600.00	4.00	161.46	2,596.75	-92.58	31.05	-92.79	0.00	0.00	0.00
2,700.00	4.00	161.46	2,696.51	-99.19	33.27	-99.41	0.00	0.00	0.00
2,800.00	4.00	161.46	2,796.27	-105.80	35.48	-106.04	0.00	0.00	0.00
2,900.00	4.00	161.46	2,896.02	-112.41	37.70	-112.67	0.00	0.00	0.00
3,000.00	4.00	161.46	2,995.78	-119.03	39.92	-119.30	0.00	0.00	0.00
3,100.00	4.00	161.46	3,095.54	-125.64	42.14	-125.92	0.00	0.00	0.00
3,200.00	4.00	161.46	3,195.29	-132.25	44.35	-132.55	0.00	0.00	0.00
3,300.00	4.00	161.46	3,295.05	-138.86	46.57	-139.18	0.00	0.00	0.00
3,400.00	4.00	161.46	3,394.81	-145.47	48.79	-145.80	0.00	0.00	0.00
3,500.00	4.00	161.46	3,494.56	-152.09	51.01	-152.43	0.00	0.00	0.00
3,600.00	4.00	161.46	3,594.32	-158.70	53.22	-159.06	0.00	0.00	0.00
3,700.00	4.00	161.46	3,694.08	-165.31	55.44	-165.68	0.00	0.00	0.00
3,800.00	4.00	161.46	3,793.83	-171.92	57.66	-172.31	0.00	0.00	0.00
3,900.00	4.00	161.46	3,893.59	-178.54	59.88	-178.94	0.00	0.00	0.00
4,000.00	4.00	161.46	3,993.34	-185.15	62.09	-185.57	0.00	0.00	0.00
4,100.00	4.00	161.46	4,093.10	-191.76	64.31	-192.19	0.00	0.00	0.00
4,200.00	4.00	161.46	4,192.86	-198.37	66.53	-198.82	0.00	0.00	0.00
4,300.00	4.00	161.46	4,292.61	-204.98	68.75	-205.45	0.00	0.00	0.00
4,400.00	4.00	161.46	4,392.37	-211.60	70.96	-212.07	0.00	0.00	0.00
4,500.00	4.00	161.46	4,492.13	-218.21	73.18	-218.70	0.00	0.00	0.00
4,600.00	4.00	161.46	4,591.88	-224.82	75.40	-225.33	0.00	0.00	0.00
4,700.00	4.00	161.46	4,691.64	-231.43	77.62	-231.95	0.00	0.00	0.00
4,800.00	4.00	161.46	4,791.40	-238.04	79.83	-238.58	0.00	0.00	0.00
4,900.00	4.00	161.46	4,891.15	-244.66	82.05	-245.21	0.00	0.00	0.00
5,000.00	4.00	161.46	4,990.91	-251.27	84.27	-251.84	0.00	0.00	0.00
5,100.00	4.00	161.46	5,090.67	-257.88	86.49	-258.46	0.00	0.00	0.00

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,205.01	4.00	161.46	5,195.42	-264.82	88.81	-265.42	0.00	0.00	0.00
Begin 1.00°/100' Drop									
5,300.00	3.05	161.46	5,290.23	-270.36	90.67	-270.97	1.00	-1.00	0.00
5,400.00	2.05	161.46	5,390.13	-274.58	92.09	-275.20	1.00	-1.00	0.00
5,500.00	1.05	161.46	5,490.09	-277.14	92.94	-277.77	1.00	-1.00	0.00
5,604.91	0.00	0.00	5,595.00	-278.05	93.25	-278.68	1.00	-1.00	0.00
Begin Vertical Hold									
5,700.00	0.00	0.00	5,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
5,800.00	0.00	0.00	5,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
5,900.00	0.00	0.00	5,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,000.00	0.00	0.00	5,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,100.00	0.00	0.00	6,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,200.00	0.00	0.00	6,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,300.00	0.00	0.00	6,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,400.00	0.00	0.00	6,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,500.00	0.00	0.00	6,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,600.00	0.00	0.00	6,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,700.00	0.00	0.00	6,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,800.00	0.00	0.00	6,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
6,900.00	0.00	0.00	6,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,000.00	0.00	0.00	6,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,100.00	0.00	0.00	7,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,200.00	0.00	0.00	7,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,300.00	0.00	0.00	7,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,400.00	0.00	0.00	7,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,500.00	0.00	0.00	7,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,600.00	0.00	0.00	7,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,700.00	0.00	0.00	7,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,800.00	0.00	0.00	7,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
7,900.00	0.00	0.00	7,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,000.00	0.00	0.00	7,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,100.00	0.00	0.00	8,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,200.00	0.00	0.00	8,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,300.00	0.00	0.00	8,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,400.00	0.00	0.00	8,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,500.00	0.00	0.00	8,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,600.00	0.00	0.00	8,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,700.00	0.00	0.00	8,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,800.00	0.00	0.00	8,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
8,900.00	0.00	0.00	8,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,000.00	0.00	0.00	8,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,100.00	0.00	0.00	9,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,200.00	0.00	0.00	9,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,300.00	0.00	0.00	9,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,400.00	0.00	0.00	9,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,500.00	0.00	0.00	9,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,600.00	0.00	0.00	9,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,700.00	0.00	0.00	9,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,800.00	0.00	0.00	9,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
9,900.00	0.00	0.00	9,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,000.00	0.00	0.00	9,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,100.00	0.00	0.00	10,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,200.00	0.00	0.00	10,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,300.00	0.00	0.00	10,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
10,400.00	0.00	0.00	10,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,500.00	0.00	0.00	10,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,600.00	0.00	0.00	10,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,700.00	0.00	0.00	10,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,800.00	0.00	0.00	10,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
10,900.00	0.00	0.00	10,890.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,000.00	0.00	0.00	10,990.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,100.00	0.00	0.00	11,090.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,200.00	0.00	0.00	11,190.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,300.00	0.00	0.00	11,290.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,400.00	0.00	0.00	11,390.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,500.00	0.00	0.00	11,490.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,600.00	0.00	0.00	11,590.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,700.00	0.00	0.00	11,690.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,800.00	0.00	0.00	11,790.09	-278.05	93.25	-278.68	0.00	0.00	0.00
11,824.15	0.00	0.00	11,814.24	-278.05	93.25	-278.68	0.00	0.00	0.00
Begin 10.00°/100' Build									
11,850.00	2.58	359.61	11,840.08	-277.47	93.25	-278.10	10.00	10.00	0.00
11,900.00	7.58	359.61	11,889.86	-273.04	93.22	-273.67	10.00	10.00	0.00
11,950.00	12.58	359.61	11,939.08	-264.29	93.16	-264.91	10.00	10.00	0.00
12,000.00	17.58	359.61	11,987.34	-251.28	93.07	-251.91	10.00	10.00	0.00
12,050.00	22.58	359.61	12,034.28	-234.11	92.95	-234.74	10.00	10.00	0.00
12,100.00	27.58	359.61	12,079.55	-212.92	92.81	-213.55	10.00	10.00	0.00
12,150.00	32.58	359.61	12,122.80	-187.87	92.64	-188.49	10.00	10.00	0.00
12,200.00	37.58	359.61	12,163.71	-159.14	92.44	-159.76	10.00	10.00	0.00
12,250.00	42.58	359.61	12,201.95	-126.95	92.22	-127.58	10.00	10.00	0.00
12,300.00	47.58	359.61	12,237.24	-91.56	91.98	-92.18	10.00	10.00	0.00
12,350.00	52.58	359.61	12,269.31	-53.22	91.72	-53.84	10.00	10.00	0.00
12,400.00	57.58	359.61	12,297.92	-12.23	91.44	-12.86	10.00	10.00	0.00
12,450.00	62.58	359.61	12,322.85	31.09	91.15	30.47	10.00	10.00	0.00
12,500.00	67.58	359.61	12,343.91	76.42	90.84	75.80	10.00	10.00	0.00
12,550.00	72.58	359.61	12,360.93	123.41	90.52	122.79	10.00	10.00	0.00
12,600.00	77.58	359.61	12,373.80	171.71	90.19	171.09	10.00	10.00	0.00
12,624.15	80.00	359.61	12,378.49	195.40	90.03	194.79	10.00	10.00	0.00
Begin 6.00°/100' Build									
12,650.00	81.55	359.61	12,382.64	220.91	89.85	220.30	6.00	6.00	0.00
12,700.00	84.55	359.61	12,388.69	270.54	89.51	269.92	6.00	6.00	0.00
12,750.00	87.55	359.61	12,392.13	320.41	89.17	319.80	6.00	6.00	0.00
12,790.82	90.00	359.61	12,393.00	361.22	88.89	360.61	6.00	6.00	0.00
Begin 90.00° Lateral									
12,800.00	90.00	359.61	12,393.00	370.40	88.83	369.79	0.00	0.00	0.00
12,900.00	90.00	359.61	12,393.00	470.40	88.14	469.79	0.00	0.00	0.00
13,000.00	90.00	359.61	12,393.00	570.40	87.46	569.79	0.00	0.00	0.00
13,100.00	90.00	359.61	12,393.00	670.39	86.77	669.79	0.00	0.00	0.00
13,200.00	90.00	359.61	12,393.00	770.39	86.08	769.79	0.00	0.00	0.00
13,300.00	90.00	359.61	12,393.00	870.39	85.40	869.79	0.00	0.00	0.00
13,400.00	90.00	359.61	12,393.00	970.39	84.71	969.79	0.00	0.00	0.00
13,500.00	90.00	359.61	12,393.00	1,070.38	84.02	1,069.79	0.00	0.00	0.00
13,600.00	90.00	359.61	12,393.00	1,170.38	83.34	1,169.79	0.00	0.00	0.00
13,700.00	90.00	359.61	12,393.00	1,270.38	82.65	1,269.79	0.00	0.00	0.00
13,800.00	90.00	359.61	12,393.00	1,370.38	81.96	1,369.79	0.00	0.00	0.00
13,900.00	90.00	359.61	12,393.00	1,470.37	81.28	1,469.79	0.00	0.00	0.00
14,000.00	90.00	359.61	12,393.00	1,570.37	80.59	1,569.79	0.00	0.00	0.00

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Planned Survey

Measured Depth (usft)	Inclination (°)	Azimuth (°)	Vertical Depth (usft)	+N/-S (usft)	+E/-W (usft)	Vertical Section (usft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
14,100.00	90.00	359.61	12,393.00	1,670.37	79.90	1,669.79	0.00	0.00	0.00
14,200.00	90.00	359.61	12,393.00	1,770.37	79.22	1,769.79	0.00	0.00	0.00
14,300.00	90.00	359.61	12,393.00	1,870.37	78.53	1,869.79	0.00	0.00	0.00
14,400.00	90.00	359.61	12,393.00	1,970.36	77.84	1,969.79	0.00	0.00	0.00
14,500.00	90.00	359.61	12,393.00	2,070.36	77.16	2,069.79	0.00	0.00	0.00
14,600.00	90.00	359.61	12,393.00	2,170.36	76.47	2,169.79	0.00	0.00	0.00
14,700.00	90.00	359.61	12,393.00	2,270.36	75.78	2,269.79	0.00	0.00	0.00
14,800.00	90.00	359.61	12,393.00	2,370.35	75.10	2,369.79	0.00	0.00	0.00
14,900.00	90.00	359.61	12,393.00	2,470.35	74.41	2,469.79	0.00	0.00	0.00
15,000.00	90.00	359.61	12,393.00	2,570.35	73.72	2,569.79	0.00	0.00	0.00
15,100.00	90.00	359.61	12,393.00	2,670.35	73.04	2,669.79	0.00	0.00	0.00
15,200.00	90.00	359.61	12,393.00	2,770.34	72.35	2,769.79	0.00	0.00	0.00
15,300.00	90.00	359.61	12,393.00	2,870.34	71.66	2,869.79	0.00	0.00	0.00
15,400.00	90.00	359.61	12,393.00	2,970.34	70.97	2,969.79	0.00	0.00	0.00
15,500.00	90.00	359.61	12,393.00	3,070.34	70.29	3,069.79	0.00	0.00	0.00
15,600.00	90.00	359.61	12,393.00	3,170.33	69.60	3,169.79	0.00	0.00	0.00
15,700.00	90.00	359.61	12,393.00	3,270.33	68.91	3,269.79	0.00	0.00	0.00
15,800.00	90.00	359.61	12,393.00	3,370.33	68.23	3,369.79	0.00	0.00	0.00
15,900.00	90.00	359.61	12,393.00	3,470.33	67.54	3,469.79	0.00	0.00	0.00
16,000.00	90.00	359.61	12,393.00	3,570.33	66.85	3,569.79	0.00	0.00	0.00
16,100.00	90.00	359.61	12,393.00	3,670.32	66.17	3,669.79	0.00	0.00	0.00
16,200.00	90.00	359.61	12,393.00	3,770.32	65.48	3,769.79	0.00	0.00	0.00
16,300.00	90.00	359.61	12,393.00	3,870.32	64.79	3,869.79	0.00	0.00	0.00
16,400.00	90.00	359.61	12,393.00	3,970.32	64.11	3,969.79	0.00	0.00	0.00
16,500.00	90.00	359.61	12,393.00	4,070.31	63.42	4,069.79	0.00	0.00	0.00
16,600.00	90.00	359.61	12,393.00	4,170.31	62.73	4,169.79	0.00	0.00	0.00
16,700.00	90.00	359.61	12,393.00	4,270.31	62.05	4,269.79	0.00	0.00	0.00
16,800.00	90.00	359.61	12,393.00	4,370.31	61.36	4,369.79	0.00	0.00	0.00
16,900.00	90.00	359.61	12,393.00	4,470.30	60.67	4,469.79	0.00	0.00	0.00
17,000.00	90.00	359.61	12,393.00	4,570.30	59.99	4,569.79	0.00	0.00	0.00
17,100.00	90.00	359.61	12,393.00	4,670.30	59.30	4,669.79	0.00	0.00	0.00
17,143.70	90.00	359.61	12,393.00	4,714.00	59.00	4,713.49	0.00	0.00	0.00
PBHL									

Design Targets

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (usft)	+N/-S (usft)	+E/-W (usft)	Northing (usft)	Easting (usft)	Latitude	Longitude
VP v2 - Brad Dyer #2(- plan hits target center - Point	0.00	0.00	5,595.00	-278.05	93.25	488,444.95	712,274.25	32° 20' 27.523 N	103° 38' 45.663 W
PBHL v2 - Brad Dyer : - plan hits target center - Point	0.00	0.00	12,393.00	4,714.00	59.00	493,437.00	712,240.00	32° 21' 16.924 N	103° 38' 45.688 W

Database:	EDM Conroe	**Local Co-ordinate Reference:**	Well #206H
Company:	Matador Resources	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Project:	Lea County, New Mexico (NAD 27)	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site:	Brad Dyer 35-22S-32E AR	**North Reference:**	Grid
Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	Wellbore #1		
Design:	Design #2		

Formations

Measured Depth (usft)	Vertical Depth (usft)	Name	Lithology	Dip (°)	Dip Direction (°)
1,189.91	1,189.88	Z (Rustler)		0.00	
1,667.40	1,666.42	Top Salt: Z (Salado)		0.00	
4,941.91	4,932.96	Base Salt: Z (G30:CS14-CSB)		0.00	
4,956.24	4,947.26	Z(G26: Bell Canyon)		0.00	
7,142.96	7,133.05	Z (G7: Brushy Cyn.)		0.00	
8,714.75	8,704.84	Z(G4: BSGL (CS9))		0.00	
9,817.76	9,807.85	Z(L5.3: FBSC)		0.00	
9,839.00	9,829.09	Z (L5.1: FBSG)		0.00	
10,172.94	10,163.03	Z (L4.3: SBSC)		0.00	
10,530.49	10,520.58	Z (L4.1: SBSG)		0.00	
10,978.91	10,969.00	Z (L3.3: TBSC)		0.00	
11,764.32	11,754.41	Z (L3.1: TBSG)		0.00	
12,059.87	12,043.36	Z (L2: WFMP A)		0.00	
12,102.83	12,082.06	Z (X Sand (T))		0.00	
12,138.97	12,113.45	Z (X Sand (B))		0.00	
12,187.99	12,154.11	Z (Y Sand (T))		0.00	
12,224.91	12,183.11	Z (Y Sand (B))		0.00	
12,239.27	12,193.98	Z (WFMP A Fat)		0.00	

Plan Annotations

Measured Depth (usft)	Vertical Depth (usft)	Local Coordinates +N/-S (usft)	Local Coordinates +E/-W (usft)	Comment
1,000.00	1,000.00	0.00	0.00	KOP, 1.00°/100' Build
1,399.91	1,399.58	-13.23	4.44	Begin 4.00° Tangent
5,205.01	5,195.42	-264.82	88.81	Begin 1.00°/100' Drop
5,604.91	5,595.00	-278.05	93.25	Begin Vertical Hold
11,824.15	11,814.24	-278.05	93.25	Begin 10.00°/100' Build
12,624.15	12,378.49	195.40	90.03	Begin 6.00°/100' Build
12,790.82	12,393.00	361.22	88.89	Begin 90.00° Lateral
17,143.70	12,393.00	4,714.00	59.00	PBHL

Matador Resources

Lea County, New Mexico (NAD 27)
Brad Dyer 35-22S-32E AR
#206H

Wellbore #1
Design #2

Anticollision Report

15 February, 2018

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Reference	Design #2		
Filter type:	NO GLOBAL FILTER: Using user defined selection & filtering criteria		
Interpolation Method:	MD + Stations Interval 100.00usft	**Error Model:**	ISCWSA
Depth Range:	Unlimited	**Scan Method:**	Closest Approach 3D
Results Limited by:	Maximum center-center distance of 10,000.00 u	**Error Surface:**	Pedal Curve
Warning Levels Evaluated at:	2.00 **Sigma**	**Casing Method:**	Not applied

Survey Tool Program **Date** 2/15/2018

From (usft)	To (usft)	Survey (Wellbore)	Tool Name	Description
0.00	17,143.70	Design #2 (Wellbore #1)	MWD	OWSG MWD - Standard

Summary

Site Name Offset Well - Wellbore - Design	Reference Measured Depth (usft)	Offset Measured Depth (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Separation Factor	Warning
Brad Dyer 35-22S-32E AR						
#201H - Wellbore #1 - Design #1	600.00	602.00	1,380.06	1,376.21	358.626	CC, ES
#201H - Wellbore #1 - Design #1	17,144.46	16,919.32	1,994.96	1,815.51	11.117	SF
#202H - Wellbore #1 - Design #2	1,000.00	999.00	60.00	53.29	8.948	CC, ES
#202H - Wellbore #1 - Design #2	17,144.46	16,943.30	696.37	522.43	4.004	SF
#205H - Wellbore #1 - Design #2	1,399.14	1,429.49	1,319.73	1,310.24	139.067	CC
#205H - Wellbore #1 - Design #2	17,144.46	17,119.49	1,320.31	1,139.67	7.309	ES, SF
#221H - Wellbore #1 - Design #2	1,000.00	1,001.00	1,350.06	1,343.35	201.130	CC, ES
#221H - Wellbore #1 - Design #2	17,141.78	17,353.71	1,990.27	1,809.99	11.040	SF
#226H - Wellbore #1 - Design #2	600.00	600.00	30.00	26.16	7.810	CC
#226H - Wellbore #1 - Design #2	800.00	799.90	30.26	25.03	5.787	ES
#226H - Wellbore #1 - Design #2	11,900.00	11,900.71	128.37	45.17	1.543	SF

Offset Design Brad Dyer 35-22S-32E AR - #201H - Wellbore #1 - Design #1 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
0.00	0.00	2.00	2.00	0.00	0.00	-90.54	-13.00	-1,380.00	1,380.06				
100.00	100.00	102.00	102.00	0.13	0.14	-90.54	-13.00	-1,380.00	1,380.06	1,379.80	0.26	5,237.883	
200.00	200.00	202.00	202.00	0.49	0.49	-90.54	-13.00	-1,380.00	1,380.06	1,379.08	0.98	1,407.623	
300.00	300.00	302.00	302.00	0.85	0.85	-90.54	-13.00	-1,380.00	1,380.06	1,378.36	1.70	813.062	
400.00	400.00	402.00	402.00	1.20	1.21	-90.54	-13.00	-1,380.00	1,380.06	1,377.65	2.41	571.618	
500.00	500.00	502.00	502.00	1.56	1.57	-90.54	-13.00	-1,380.00	1,380.06	1,376.93	3.13	440.738	
600.00	600.00	602.00	602.00	1.92	1.93	-90.54	-13.00	-1,380.00	1,380.06	1,376.21	3.85	358.626	CC, ES
700.00	700.00	684.18	684.18	2.28	2.21	-90.55	-13.30	-1,380.54	1,380.72	1,376.23	4.49	307.476	
800.00	800.00	766.68	766.66	2.64	2.49	-90.59	-14.18	-1,382.12	1,382.64	1,377.51	5.13	269.590	
900.00	900.00	849.11	849.03	3.00	2.78	-90.65	-15.63	-1,384.73	1,385.83	1,380.06	5.77	240.294	
1,000.00	1,000.00	931.43	931.25	3.35	3.06	-90.73	-17.66	-1,388.37	1,390.29	1,383.88	6.41	216.976	
1,100.00	1,099.99	1,013.63	1,013.27	3.70	3.35	-90.80	-20.26	-1,393.04	1,396.27	1,389.24	7.03	198.569	
1,200.00	1,199.96	1,095.65	1,095.04	4.02	3.65	-90.82	-23.42	-1,398.72	1,404.05	1,396.41	7.64	183.684	
1,300.00	1,299.86	1,177.46	1,176.49	4.36	3.94	-90.80	-27.14	-1,405.41	1,413.61	1,405.35	8.26	171.096	
1,399.91	1,399.58	1,271.85	1,270.36	4.70	4.29	-90.75	-31.92	-1,413.99	1,424.60	1,415.67	8.94	159.427	
1,500.00	1,499.43	1,371.29	1,369.25	5.04	4.67	-90.69	-36.97	-1,423.07	1,435.92	1,426.29	9.64	149.008	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #201H - Wellbore #1 - Design #1 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
1,600.00	1,599.19	1,470.63	1,468.05	5.39	5.04	-90.62	-42.02	-1,432.14	1,447.24	1,436.89	10.34	139.920	
1,700.00	1,698.94	1,569.98	1,566.85	5.74	5.42	-90.55	-47.07	-1,441.22	1,458.55	1,447.50	11.06	131.936	
1,800.00	1,798.70	1,669.32	1,665.65	6.10	5.80	-90.49	-52.12	-1,450.29	1,469.87	1,458.10	11.77	124.873	
1,900.00	1,898.46	1,768.66	1,764.45	6.46	6.19	-90.42	-57.17	-1,459.36	1,481.19	1,468.70	12.49	118.587	
2,000.00	1,998.21	1,868.01	1,863.25	6.82	6.57	-90.36	-62.22	-1,468.44	1,492.51	1,479.29	13.21	112.961	
2,100.00	2,097.97	1,967.35	1,962.05	7.18	6.95	-90.30	-67.27	-1,477.51	1,503.83	1,489.89	13.94	107.898	
2,200.00	2,197.73	2,066.69	2,060.85	7.54	7.34	-90.24	-72.32	-1,486.58	1,515.15	1,500.49	14.66	103.322	
2,300.00	2,297.48	2,166.04	2,159.65	7.91	7.73	-90.17	-77.37	-1,495.66	1,526.48	1,511.09	15.39	99.166	
2,400.00	2,397.24	2,265.38	2,258.45	8.27	8.12	-90.11	-82.42	-1,504.73	1,537.81	1,521.68	16.12	95.376	
2,500.00	2,497.00	2,364.73	2,357.25	8.64	8.50	-90.06	-87.47	-1,513.80	1,549.13	1,532.28	16.86	91.907	
2,600.00	2,596.75	2,464.07	2,456.05	9.01	8.89	-90.00	-92.52	-1,522.88	1,560.46	1,542.88	17.59	88.721	
2,700.00	2,696.51	2,563.41	2,554.85	9.38	9.28	-89.94	-97.58	-1,531.95	1,571.80	1,553.47	18.32	85.784	
2,800.00	2,796.27	2,662.76	2,653.65	9.75	9.67	-89.88	-102.63	-1,541.02	1,583.13	1,564.07	19.06	83.070	
2,900.00	2,896.02	2,762.10	2,752.45	10.12	10.06	-89.83	-107.68	-1,550.10	1,594.47	1,574.67	19.79	80.554	
3,000.00	2,995.78	2,861.44	2,851.25	10.49	10.45	-89.77	-112.73	-1,559.17	1,605.80	1,585.27	20.53	78.215	
3,100.00	3,095.54	2,960.79	2,950.05	10.86	10.84	-89.72	-117.78	-1,568.25	1,617.14	1,595.87	21.27	76.036	
3,200.00	3,195.29	3,060.13	3,048.84	11.23	11.23	-89.67	-122.83	-1,577.32	1,628.48	1,606.47	22.01	74.001	
3,300.00	3,295.05	3,159.47	3,147.64	11.60	11.63	-89.61	-127.88	-1,586.39	1,639.82	1,617.08	22.74	72.096	
3,400.00	3,394.81	3,258.82	3,246.44	11.97	12.02	-89.56	-132.93	-1,595.47	1,651.16	1,627.68	23.48	70.310	
3,500.00	3,494.56	3,358.16	3,345.24	12.34	12.41	-89.51	-137.98	-1,604.54	1,662.51	1,638.28	24.22	68.631	
3,600.00	3,594.32	3,457.51	3,444.04	12.71	12.80	-89.46	-143.03	-1,613.61	1,673.85	1,648.89	24.96	67.051	
3,700.00	3,694.08	3,556.85	3,542.84	13.09	13.19	-89.41	-148.08	-1,622.69	1,685.20	1,659.49	25.70	65.561	
3,800.00	3,793.83	3,656.19	3,641.64	13.46	13.58	-89.36	-153.13	-1,631.76	1,696.54	1,670.10	26.45	64.153	
3,900.00	3,893.59	3,755.54	3,740.44	13.83	13.98	-89.31	-158.18	-1,640.83	1,707.89	1,680.71	27.19	62.821	
4,000.00	3,993.34	3,854.88	3,839.24	14.21	14.37	-89.27	-163.23	-1,649.91	1,719.24	1,691.31	27.93	61.559	
4,100.00	4,093.10	3,954.22	3,938.04	14.58	14.76	-89.22	-168.28	-1,658.98	1,730.59	1,701.92	28.67	60.362	
4,200.00	4,192.86	4,053.57	4,036.84	14.95	15.15	-89.17	-173.33	-1,668.05	1,741.94	1,712.53	29.41	59.225	
4,300.00	4,292.61	4,152.91	4,135.64	15.33	15.55	-89.13	-178.38	-1,677.13	1,753.30	1,723.14	30.15	58.143	
4,400.00	4,392.37	4,252.25	4,234.44	15.70	15.94	-89.08	-183.43	-1,686.20	1,764.65	1,733.75	30.90	57.113	
4,500.00	4,492.13	4,351.60	4,333.24	16.08	16.33	-89.04	-188.48	-1,695.27	1,776.01	1,744.37	31.64	56.131	
4,600.00	4,591.88	4,450.94	4,432.04	16.45	16.73	-88.99	-193.53	-1,704.35	1,787.36	1,754.98	32.38	55.194	
4,700.00	4,691.64	4,550.29	4,530.84	16.82	17.12	-88.95	-198.58	-1,713.42	1,798.72	1,765.59	33.13	54.298	
4,800.00	4,791.40	4,649.63	4,629.64	17.20	17.51	-88.91	-203.63	-1,722.49	1,810.08	1,776.21	33.87	53.441	
4,900.00	4,891.15	4,748.97	4,728.43	17.57	17.90	-88.86	-208.68	-1,731.57	1,821.44	1,786.82	34.61	52.621	
5,000.00	4,990.91	4,848.32	4,827.23	17.95	18.30	-88.82	-213.73	-1,740.64	1,832.80	1,797.44	35.36	51.835	
5,100.00	5,090.67	4,947.66	4,926.03	18.32	18.69	-88.78	-218.78	-1,749.71	1,844.16	1,808.06	36.10	51.082	
5,200.00	5,190.42	5,047.00	5,024.83	18.70	19.08	-88.74	-223.83	-1,758.79	1,855.52	1,818.68	36.85	50.358	
5,205.01	5,195.42	5,051.98	5,029.78	18.72	19.10	-88.74	-224.08	-1,759.24	1,856.09	1,819.21	36.88	50.323	
5,300.00	5,290.23	5,146.38	5,123.67	19.07	19.48	-88.72	-228.88	-1,767.86	1,866.62	1,829.04	37.59	49.661	
5,400.00	5,390.13	5,245.82	5,222.56	19.43	19.87	-88.75	-233.94	-1,776.95	1,877.15	1,838.83	38.32	48.983	
5,500.00	5,490.09	5,345.29	5,321.48	19.79	20.27	-88.84	-238.99	-1,786.03	1,887.09	1,848.04	39.05	48.324	
5,600.00	5,590.09	5,444.75	5,420.40	20.13	20.66	-88.97	-244.05	-1,795.12	1,896.46	1,856.70	39.76	47.699	
5,604.91	5,595.00	5,449.64	5,425.26	20.15	20.68	-88.98	-244.30	-1,795.56	1,896.90	1,857.11	39.79	47.668	
5,700.00	5,690.09	5,544.20	5,519.31	20.46	21.05	-89.13	-249.11	-1,804.20	1,905.52	1,865.07	40.45	47.105	
5,800.00	5,790.09	5,643.66	5,618.22	20.78	21.45	-89.28	-254.16	-1,813.28	1,914.59	1,873.45	41.15	46.531	
5,900.00	5,890.09	5,743.11	5,717.12	21.11	21.84	-89.44	-259.22	-1,822.37	1,923.68	1,881.84	41.84	45.976	
6,000.00	5,990.09	5,842.56	5,816.03	21.43	22.24	-89.59	-264.27	-1,831.45	1,932.78	1,890.25	42.54	45.438	
6,100.00	6,090.09	5,942.01	5,914.94	21.76	22.63	-89.74	-269.33	-1,840.53	1,941.90	1,898.67	43.23	44.916	
6,200.00	6,190.09	6,041.46	6,013.85	22.09	23.02	-89.89	-274.39	-1,849.62	1,951.03	1,907.10	43.93	44.411	
6,300.00	6,290.09	6,140.92	6,112.75	22.42	23.42	-90.04	-279.44	-1,858.70	1,960.17	1,915.54	44.63	43.921	
6,400.00	6,390.09	6,278.45	6,249.67	22.75	23.95	-90.22	-285.76	-1,870.05	1,968.47	1,922.97	45.50	43.261	
6,500.00	6,490.09	6,421.30	6,392.17	23.08	24.49	-90.37	-290.63	-1,878.80	1,974.62	1,928.24	46.38	42.577	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #201H - Wellbore #1 - Design #1

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
6,600.00	6,590.09	6,564.57	6,535.29	23.41	25.00	-90.46	-293.78	-1,884.46	1,978.59	1,931.36	47.23	41.894	
6,700.00	6,690.09	6,708.08	6,678.76	23.74	25.50	-90.50	-295.19	-1,886.99	1,980.36	1,932.31	48.05	41.212	
6,800.00	6,790.09	6,821.41	6,792.09	24.08	25.86	-90.50	-295.27	-1,887.14	1,980.46	1,931.71	48.75	40.623	
6,900.00	6,890.09	6,921.41	6,892.09	24.41	26.17	-90.50	-295.27	-1,887.14	1,980.46	1,931.05	49.41	40.082	
7,000.00	6,990.09	7,021.41	6,992.09	24.75	26.48	-90.50	-295.27	-1,887.14	1,980.46	1,930.39	50.07	39.553	
7,100.00	7,090.09	7,121.41	7,092.09	25.08	26.80	-90.50	-295.27	-1,887.14	1,980.46	1,929.73	50.73	39.037	
7,200.00	7,190.09	7,221.41	7,192.09	25.42	27.12	-90.50	-295.27	-1,887.14	1,980.46	1,929.07	51.40	38.534	
7,300.00	7,290.09	7,321.41	7,292.09	25.75	27.43	-90.50	-295.27	-1,887.14	1,980.46	1,928.40	52.06	38.042	
7,400.00	7,390.09	7,421.41	7,392.09	26.09	27.75	-90.50	-295.27	-1,887.14	1,980.46	1,927.74	52.73	37.561	
7,500.00	7,490.09	7,521.41	7,492.09	26.43	28.07	-90.50	-295.27	-1,887.14	1,980.46	1,927.07	53.39	37.092	
7,600.00	7,590.09	7,621.41	7,592.09	26.77	28.39	-90.50	-295.27	-1,887.14	1,980.46	1,926.40	54.06	36.633	
7,700.00	7,690.09	7,721.41	7,692.09	27.11	28.71	-90.50	-295.27	-1,887.14	1,980.46	1,925.73	54.73	36.185	
7,800.00	7,790.09	7,821.41	7,792.09	27.45	29.03	-90.50	-295.27	-1,887.14	1,980.46	1,925.06	55.40	35.747	
7,900.00	7,890.09	7,921.41	7,892.09	27.79	29.36	-90.50	-295.27	-1,887.14	1,980.46	1,924.39	56.08	35.318	
8,000.00	7,990.09	8,021.41	7,992.09	28.13	29.68	-90.50	-295.27	-1,887.14	1,980.46	1,923.71	56.75	34.899	
8,100.00	8,090.09	8,121.41	8,092.09	28.47	30.00	-90.50	-295.27	-1,887.14	1,980.46	1,923.04	57.42	34.489	
8,200.00	8,190.09	8,221.41	8,192.09	28.81	30.33	-90.50	-295.27	-1,887.14	1,980.46	1,922.36	58.10	34.088	
8,300.00	8,290.09	8,321.41	8,292.09	29.15	30.65	-90.50	-295.27	-1,887.14	1,980.46	1,921.69	58.77	33.696	
8,400.00	8,390.09	8,421.41	8,392.09	29.49	30.98	-90.50	-295.27	-1,887.14	1,980.46	1,921.01	59.45	33.312	
8,500.00	8,490.09	8,521.41	8,492.09	29.83	31.31	-90.50	-295.27	-1,887.14	1,980.46	1,920.33	60.13	32.937	
8,600.00	8,590.09	8,621.41	8,592.09	30.18	31.64	-90.50	-295.27	-1,887.14	1,980.46	1,919.65	60.81	32.569	
8,700.00	8,690.09	8,721.41	8,692.09	30.52	31.97	-90.50	-295.27	-1,887.14	1,980.46	1,918.97	61.49	32.209	
8,800.00	8,790.09	8,821.41	8,792.09	30.86	32.29	-90.50	-295.27	-1,887.14	1,980.46	1,918.29	62.17	31.856	
8,900.00	8,890.09	8,921.41	8,892.09	31.21	32.62	-90.50	-295.27	-1,887.14	1,980.46	1,917.61	62.85	31.511	
9,000.00	8,990.09	9,021.41	8,992.09	31.55	32.95	-90.50	-295.27	-1,887.14	1,980.46	1,916.93	63.53	31.172	
9,100.00	9,090.09	9,121.41	9,092.09	31.90	33.29	-90.50	-295.27	-1,887.14	1,980.46	1,916.25	64.22	30.841	
9,200.00	9,190.09	9,221.41	9,192.09	32.24	33.62	-90.50	-295.27	-1,887.14	1,980.46	1,915.56	64.90	30.516	
9,300.00	9,290.09	9,321.41	9,292.09	32.59	33.95	-90.50	-295.27	-1,887.14	1,980.46	1,914.88	65.58	30.197	
9,400.00	9,390.09	9,421.41	9,392.09	32.93	34.28	-90.50	-295.27	-1,887.14	1,980.46	1,914.19	66.27	29.885	
9,500.00	9,490.09	9,521.41	9,492.09	33.28	34.62	-90.50	-295.27	-1,887.14	1,980.46	1,913.51	66.96	29.579	
9,600.00	9,590.09	9,621.41	9,592.09	33.62	34.95	-90.50	-295.27	-1,887.14	1,980.46	1,912.82	67.64	29.279	
9,700.00	9,690.09	9,721.41	9,692.09	33.97	35.28	-90.50	-295.27	-1,887.14	1,980.46	1,912.13	68.33	28.984	
9,800.00	9,790.09	9,821.41	9,792.09	34.31	35.62	-90.50	-295.27	-1,887.14	1,980.46	1,911.45	69.02	28.695	
9,900.00	9,890.09	9,921.41	9,892.09	34.66	35.95	-90.50	-295.27	-1,887.14	1,980.46	1,910.76	69.70	28.412	
10,000.00	9,990.09	10,021.41	9,992.09	35.01	36.29	-90.50	-295.27	-1,887.14	1,980.46	1,910.07	70.39	28.134	
10,100.00	10,090.09	10,121.41	10,092.09	35.36	36.62	-90.50	-295.27	-1,887.14	1,980.46	1,909.38	71.08	27.861	
10,200.00	10,190.09	10,221.41	10,192.09	35.70	36.96	-90.50	-295.27	-1,887.14	1,980.46	1,908.69	71.77	27.593	
10,300.00	10,290.09	10,321.41	10,292.09	36.05	37.30	-90.50	-295.27	-1,887.14	1,980.46	1,908.00	72.46	27.330	
10,400.00	10,390.09	10,421.41	10,392.09	36.40	37.64	-90.50	-295.27	-1,887.14	1,980.46	1,907.31	73.15	27.072	
10,500.00	10,490.09	10,521.41	10,492.09	36.75	37.97	-90.50	-295.27	-1,887.14	1,980.46	1,906.62	73.85	26.819	
10,600.00	10,590.09	10,621.41	10,592.09	37.09	38.31	-90.50	-295.27	-1,887.14	1,980.46	1,905.92	74.54	26.570	
10,700.00	10,690.09	10,721.41	10,692.09	37.44	38.65	-90.50	-295.27	-1,887.14	1,980.46	1,905.23	75.23	26.325	
10,800.00	10,790.09	10,821.41	10,792.09	37.79	38.99	-90.50	-295.27	-1,887.14	1,980.46	1,904.54	75.92	26.085	
10,900.00	10,890.09	10,921.41	10,892.09	38.14	39.33	-90.50	-295.27	-1,887.14	1,980.46	1,903.85	76.62	25.849	
11,000.00	10,990.09	11,021.41	10,992.09	38.49	39.67	-90.50	-295.27	-1,887.14	1,980.46	1,903.15	77.31	25.617	
11,100.00	11,090.09	11,121.41	11,092.09	38.84	40.01	-90.50	-295.27	-1,887.14	1,980.46	1,902.46	78.00	25.389	
11,200.00	11,190.09	11,221.41	11,192.09	39.19	40.35	-90.50	-295.27	-1,887.14	1,980.46	1,901.76	78.70	25.165	
11,300.00	11,290.09	11,321.41	11,292.09	39.54	40.69	-90.50	-295.27	-1,887.14	1,980.46	1,901.07	79.39	24.945	
11,400.00	11,390.09	11,421.41	11,392.09	39.89	41.03	-90.50	-295.27	-1,887.14	1,980.46	1,900.37	80.09	24.728	
11,500.00	11,490.09	11,521.41	11,492.09	40.24	41.37	-90.50	-295.27	-1,887.14	1,980.46	1,899.68	80.79	24.515	
11,600.00	11,590.09	11,621.52	11,592.20	40.59	41.71	-90.49	-294.96	-1,887.14	1,980.46	1,898.98	81.48	24.306	
11,646.84	11,636.93	11,668.39	11,638.93	40.75	41.86	-90.39	-291.49	-1,887.16	1,980.46	1,898.66	81.80	24.210	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #201H - Wellbore #1 - Design #1

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
11,700.00	11,690.09	11,720.50	11,690.35	40.94	42.03	-90.15	-283.17	-1,887.22	1,980.48	1,898.32	82.16	24.106	
11,800.00	11,790.09	11,812.87	11,778.86	41.29	42.29	-89.39	-257.10	-1,887.40	1,980.80	1,898.01	82.79	23.924	
11,824.15	11,814.24	11,833.75	11,798.21	41.37	42.35	-89.17	-249.26	-1,887.45	1,980.99	1,898.05	82.94	23.884	
11,850.00	11,840.08	11,855.61	11,818.14	41.46	42.40	-88.92	-240.29	-1,887.51	1,981.25	1,898.16	83.09	23.844	
11,900.00	11,889.86	11,897.12	11,855.00	41.63	42.50	-88.50	-221.20	-1,887.64	1,981.88	1,898.50	83.37	23.771	
11,950.00	11,939.08	11,937.71	11,889.61	41.79	42.59	-88.14	-200.01	-1,887.78	1,982.65	1,899.01	83.64	23.705	
12,000.00	11,987.34	11,977.49	11,921.98	41.94	42.66	-87.85	-176.91	-1,887.94	1,983.55	1,899.66	83.88	23.647	
12,050.00	12,034.28	12,016.55	11,952.13	42.09	42.73	-87.63	-152.10	-1,888.11	1,984.54	1,900.43	84.11	23.595	
12,100.00	12,079.55	12,054.97	11,980.08	42.23	42.78	-87.48	-125.75	-1,888.29	1,985.61	1,901.29	84.32	23.548	
12,150.00	12,122.80	12,092.84	12,005.84	42.36	42.83	-87.40	-98.00	-1,888.48	1,986.71	1,902.20	84.51	23.507	
12,200.00	12,163.71	12,130.22	12,029.41	42.48	42.87	-87.39	-69.00	-1,888.67	1,987.84	1,903.14	84.70	23.470	
12,250.00	12,201.95	12,167.17	12,050.80	42.59	42.90	-87.45	-38.88	-1,888.88	1,988.96	1,904.09	84.87	23.436	
12,300.00	12,237.24	12,203.74	12,070.03	42.70	42.92	-87.58	-7.77	-1,889.09	1,990.05	1,905.02	85.03	23.404	
12,350.00	12,269.31	12,240.00	12,087.08	42.81	42.94	-87.76	24.21	-1,889.31	1,991.08	1,905.89	85.19	23.373	
12,400.00	12,297.92	12,275.98	12,101.98	42.91	42.95	-88.00	56.96	-1,889.53	1,992.04	1,906.69	85.34	23.342	
12,450.00	12,322.85	12,311.72	12,114.71	43.02	42.96	-88.29	90.35	-1,889.75	1,992.90	1,907.40	85.50	23.309	
12,500.00	12,343.91	12,350.00	12,126.01	43.13	42.96	-88.54	126.92	-1,890.00	1,993.65	1,907.98	85.66	23.273	
12,550.00	12,360.93	12,382.66	12,133.70	43.24	42.97	-88.98	158.65	-1,890.22	1,994.27	1,908.45	85.82	23.237	
12,600.00	12,373.80	12,419.98	12,140.36	43.35	43.00	-89.32	195.37	-1,890.47	1,994.74	1,908.74	86.00	23.195	
12,624.15	12,378.49	12,439.28	12,143.17	43.40	43.02	-89.45	214.46	-1,890.60	1,994.88	1,908.79	86.09	23.172	
12,650.00	12,382.64	12,459.92	12,145.75	43.46	43.06	-89.59	234.94	-1,890.74	1,994.99	1,908.80	86.19	23.146	
12,700.00	12,388.69	12,500.00	12,149.49	43.58	43.16	-89.88	274.84	-1,891.01	1,995.16	1,908.76	86.40	23.092	
12,750.00	12,392.13	12,539.70	12,151.54	43.70	43.27	-90.17	314.48	-1,891.28	1,995.26	1,908.64	86.62	23.034	
12,790.82	12,393.00	12,573.00	12,152.00	43.81	43.36	-90.39	347.78	-1,891.50	1,995.29	1,908.48	86.82	22.983	
12,800.00	12,393.00	12,582.18	12,152.00	43.83	43.39	-90.39	356.96	-1,891.56	1,995.29	1,908.43	86.87	22.969	
12,900.00	12,393.00	12,682.18	12,152.00	44.14	43.72	-90.39	456.96	-1,892.24	1,995.28	1,907.81	87.48	22.809	
13,000.00	12,393.00	12,782.18	12,152.00	44.51	44.10	-90.39	556.95	-1,892.92	1,995.28	1,907.07	88.21	22.620	
13,100.00	12,393.00	12,882.18	12,152.00	44.93	44.54	-90.39	656.95	-1,893.60	1,995.27	1,906.22	89.05	22.406	
13,200.00	12,393.00	12,982.18	12,152.00	45.41	45.04	-90.39	756.95	-1,894.28	1,995.26	1,905.25	90.01	22.168	
13,300.00	12,393.00	13,082.18	12,152.00	45.95	45.58	-90.39	856.95	-1,894.96	1,995.25	1,904.18	91.08	21.908	
13,400.00	12,393.00	13,182.18	12,152.00	46.54	46.18	-90.39	956.95	-1,895.64	1,995.24	1,903.00	92.25	21.629	
13,500.00	12,393.00	13,282.18	12,152.00	47.18	46.83	-90.39	1,056.94	-1,896.31	1,995.24	1,901.71	93.52	21.334	
13,600.00	12,393.00	13,382.18	12,152.00	47.87	47.52	-90.39	1,156.94	-1,896.99	1,995.23	1,900.33	94.89	21.026	
13,700.00	12,393.00	13,482.18	12,152.00	48.60	48.26	-90.39	1,256.94	-1,897.67	1,995.22	1,898.86	96.36	20.706	
13,800.00	12,393.00	13,582.18	12,152.00	49.38	49.04	-90.39	1,356.94	-1,898.35	1,995.21	1,897.30	97.91	20.377	
13,900.00	12,393.00	13,682.18	12,152.00	50.21	49.87	-90.39	1,456.93	-1,899.03	1,995.20	1,895.65	99.55	20.041	
14,000.00	12,393.00	13,782.18	12,152.00	51.07	50.74	-90.39	1,556.93	-1,899.71	1,995.20	1,893.92	101.28	19.701	
14,100.00	12,393.00	13,882.18	12,152.00	51.97	51.64	-90.39	1,656.93	-1,900.39	1,995.19	1,892.11	103.07	19.357	
14,200.00	12,393.00	13,982.18	12,152.00	52.91	52.58	-90.39	1,756.93	-1,901.07	1,995.18	1,890.24	104.94	19.012	
14,300.00	12,393.00	14,082.18	12,152.00	53.89	53.56	-90.39	1,856.92	-1,901.74	1,995.17	1,888.29	106.88	18.667	
14,400.00	12,393.00	14,182.18	12,152.00	54.89	54.57	-90.39	1,956.92	-1,902.42	1,995.16	1,886.27	108.89	18.323	
14,500.00	12,393.00	14,282.18	12,152.00	55.93	55.61	-90.39	2,056.92	-1,903.10	1,995.16	1,884.20	110.96	17.981	
14,600.00	12,393.00	14,382.18	12,152.00	57.00	56.68	-90.39	2,156.92	-1,903.78	1,995.15	1,882.06	113.08	17.643	
14,700.00	12,393.00	14,482.18	12,152.00	58.10	57.77	-90.39	2,256.92	-1,904.46	1,995.14	1,879.88	115.27	17.309	
14,800.00	12,393.00	14,582.18	12,152.00	59.22	58.90	-90.39	2,356.91	-1,905.14	1,995.13	1,877.63	117.50	16.980	
14,900.00	12,393.00	14,682.18	12,152.00	60.36	60.05	-90.39	2,456.91	-1,905.82	1,995.12	1,875.34	119.78	16.656	
15,000.00	12,393.00	14,782.18	12,152.00	61.53	61.22	-90.39	2,556.91	-1,906.50	1,995.12	1,873.01	122.11	16.339	
15,100.00	12,393.00	14,882.18	12,152.00	62.73	62.41	-90.39	2,656.91	-1,907.17	1,995.11	1,870.63	124.48	16.027	
15,200.00	12,393.00	14,982.18	12,152.00	63.94	63.62	-90.39	2,756.90	-1,907.85	1,995.10	1,868.20	126.90	15.722	
15,300.00	12,393.00	15,082.18	12,152.00	65.17	64.86	-90.39	2,856.90	-1,908.53	1,995.09	1,865.74	129.35	15.424	
15,400.00	12,393.00	15,182.18	12,152.00	66.42	66.11	-90.39	2,956.90	-1,909.21	1,995.08	1,863.24	131.84	15.132	
15,500.00	12,393.00	15,282.18	12,152.00	67.69	67.38	-90.39	3,056.90	-1,909.89	1,995.08	1,860.71	134.37	14.848	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #201H - Wellbore #1 - Design #1

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
15,600.00	12,393.00	15,382.18	12,152.00	68.97	68.66	-90.39	3,156.90	-1,910.57	1,995.07	1,858.14	136.93	14.570	
15,700.00	12,393.00	15,482.18	12,152.00	70.28	69.97	-90.39	3,256.89	-1,911.25	1,995.06	1,855.54	139.52	14.300	
15,800.00	12,393.00	15,582.18	12,152.00	71.59	71.28	-90.39	3,356.89	-1,911.92	1,995.05	1,852.92	142.13	14.036	
15,900.00	12,393.00	15,682.18	12,152.00	72.92	72.61	-90.39	3,456.89	-1,912.60	1,995.04	1,850.26	144.78	13.780	
16,000.00	12,393.00	15,782.18	12,152.00	74.26	73.96	-90.39	3,556.89	-1,913.28	1,995.04	1,847.58	147.45	13.530	
16,100.00	12,393.00	15,882.18	12,152.00	75.62	75.31	-90.39	3,656.88	-1,913.96	1,995.03	1,844.88	150.15	13.287	
16,200.00	12,393.00	15,982.18	12,152.00	76.99	76.68	-90.39	3,756.88	-1,914.64	1,995.02	1,842.15	152.87	13.050	
16,300.00	12,393.00	16,082.18	12,152.00	78.37	78.06	-90.39	3,856.88	-1,915.32	1,995.01	1,839.39	155.62	12.820	
16,400.00	12,393.00	16,182.18	12,152.00	79.75	79.45	-90.39	3,956.88	-1,916.00	1,995.00	1,836.62	158.38	12.596	
16,500.00	12,393.00	16,282.18	12,152.00	81.15	80.85	-90.39	4,056.87	-1,916.68	1,995.00	1,833.83	161.17	12.378	
16,600.00	12,393.00	16,382.18	12,152.00	82.56	82.26	-90.39	4,156.87	-1,917.35	1,994.99	1,831.01	163.97	12.167	
16,700.00	12,393.00	16,482.18	12,152.00	83.98	83.68	-90.39	4,256.87	-1,918.03	1,994.98	1,828.18	166.80	11.961	
16,800.00	12,393.00	16,582.18	12,152.00	85.41	85.11	-90.39	4,356.87	-1,918.71	1,994.97	1,825.34	169.64	11.760	
16,900.00	12,393.00	16,682.18	12,152.00	86.84	86.55	-90.39	4,456.87	-1,919.39	1,994.96	1,822.47	172.49	11.566	
17,000.00	12,393.00	16,782.18	12,152.00	88.29	87.99	-90.39	4,556.86	-1,920.07	1,994.96	1,819.59	175.36	11.376	
17,100.00	12,393.00	16,882.18	12,152.00	89.74	89.44	-90.39	4,656.86	-1,920.75	1,994.95	1,816.70	178.25	11.192	
17,137.74	12,393.00	16,919.92	12,152.00	90.29	89.99	-90.39	4,694.59	-1,921.00	1,994.95	1,815.60	179.34	11.124	
17,143.70	12,393.00	16,919.32	12,152.00	90.37	89.98	-90.58	4,694.00	-1,921.00	1,994.96	1,815.52	179.44	11.118	
17,144.46	12,393.00	16,919.32	12,152.00	90.38	89.98	-90.60	4,694.00	-1,921.00	1,994.96	1,815.51	179.45	11.117	SF

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #202H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
0.00	0.00	1.00	-1.00	0.00	0.00	-90.00	0.00	-60.00	60.00				
100.00	100.00	101.00	99.00	0.13	0.13	-90.00	0.00	-60.00	60.00	59.74	0.26	230.865	
200.00	200.00	201.00	199.00	0.49	0.49	-90.00	0.00	-60.00	60.00	59.02	0.98	61.423	
300.00	300.00	301.00	299.00	0.85	0.85	-90.00	0.00	-60.00	60.00	58.31	1.69	35.424	
400.00	400.00	401.00	399.00	1.20	1.21	-90.00	0.00	-60.00	60.00	57.59	2.41	24.889	
500.00	500.00	501.00	499.00	1.56	1.57	-90.00	0.00	-60.00	60.00	56.87	3.13	19.184	
600.00	600.00	601.00	599.00	1.92	1.92	-90.00	0.00	-60.00	60.00	56.16	3.84	15.606	
700.00	700.00	701.00	699.00	2.28	2.28	-90.00	0.00	-60.00	60.00	55.44	4.56	13.153	
800.00	800.00	801.00	799.00	2.64	2.64	-90.00	0.00	-60.00	60.00	54.72	5.28	11.367	
900.00	900.00	901.00	899.00	3.00	3.00	-90.00	0.00	-60.00	60.00	54.00	6.00	10.008	
1,000.00	1,000.00	999.00	999.00	3.35	3.35	-90.00	0.00	-60.00	60.00	53.29	6.71	8.948	CC, ES
1,100.00	1,099.99	1,098.09	1,098.09	3.70	3.69	-89.61	-0.41	-60.73	61.02	53.63	7.39	8.259	
1,200.00	1,199.96	1,197.10	1,197.07	4.02	4.03	-88.53	-1.66	-62.96	64.11	56.07	8.05	7.968	
1,300.00	1,299.86	1,295.97	1,295.84	4.36	4.36	-86.94	-3.74	-66.66	69.32	60.61	8.71	7.956	
1,399.91	1,399.58	1,394.53	1,394.22	4.70	4.70	-85.07	-6.65	-71.84	76.68	67.29	9.39	8.170	
1,500.00	1,499.43	1,493.04	1,492.43	5.04	5.05	-83.66	-10.39	-78.48	85.87	75.81	10.06	8.532	
1,600.00	1,599.19	1,609.83	1,590.03	5.39	5.47	-83.11	-14.92	-86.55	96.46	85.65	10.81	8.922	
1,700.00	1,698.94	1,690.43	1,688.83	5.74	5.76	-83.02	-20.01	-95.61	107.88	96.44	11.45	9.425	
1,800.00	1,798.70	1,789.77	1,787.63	6.10	6.13	-82.95	-25.10	-104.67	119.30	107.15	12.15	9.817	
1,900.00	1,898.46	1,889.12	1,886.44	6.46	6.49	-82.90	-30.19	-113.73	130.72	117.85	12.86	10.162	
2,000.00	1,998.21	1,988.46	1,985.24	6.82	6.87	-82.85	-35.28	-122.79	142.14	128.56	13.58	10.467	
2,100.00	2,097.97	2,087.81	2,084.04	7.18	7.24	-82.81	-40.37	-131.85	153.56	139.26	14.30	10.740	
2,200.00	2,197.73	2,187.15	2,182.84	7.54	7.62	-82.78	-45.47	-140.91	164.98	149.96	15.02	10.984	
2,300.00	2,297.48	2,286.50	2,281.64	7.91	7.99	-82.75	-50.56	-149.97	176.40	160.65	15.74	11.204	
2,400.00	2,397.24	2,385.85	2,380.44	8.27	8.37	-82.72	-55.65	-159.03	187.81	171.34	16.47	11.403	
2,500.00	2,497.00	2,485.19	2,479.24	8.64	8.75	-82.70	-60.74	-168.09	199.23	182.04	17.20	11.584	
2,600.00	2,596.75	2,584.54	2,578.04	9.01	9.14	-82.68	-65.83	-177.15	210.65	192.72	17.93	11.749	
2,700.00	2,696.51	2,683.88	2,676.84	9.38	9.52	-82.66	-70.92	-186.21	222.07	203.41	18.66	11.901	
2,800.00	2,796.27	2,783.23	2,775.64	9.75	9.90	-82.64	-76.01	-195.27	233.49	214.10	19.39	12.040	
2,900.00	2,896.02	2,882.58	2,874.44	10.12	10.29	-82.63	-81.10	-204.33	244.91	224.78	20.13	12.168	
3,000.00	2,995.78	2,981.92	2,973.24	10.49	10.67	-82.61	-86.19	-213.39	256.33	235.47	20.86	12.287	
3,100.00	3,095.54	3,081.27	3,072.04	10.86	11.06	-82.60	-91.28	-222.45	267.75	246.15	21.60	12.397	
3,200.00	3,195.29	3,180.61	3,170.85	11.23	11.44	-82.59	-96.38	-231.51	279.17	256.83	22.33	12.499	
3,300.00	3,295.05	3,279.96	3,269.65	11.60	11.83	-82.58	-101.47	-240.57	290.59	267.52	23.07	12.595	
3,400.00	3,394.81	3,379.30	3,368.45	11.97	12.22	-82.57	-106.56	-249.63	302.01	278.20	23.81	12.684	
3,500.00	3,494.56	3,478.65	3,467.25	12.34	12.61	-82.56	-111.65	-258.69	313.43	288.88	24.55	12.767	
3,600.00	3,594.32	3,578.00	3,566.05	12.71	13.00	-82.55	-116.74	-267.75	324.85	299.56	25.29	12.845	
3,700.00	3,694.08	3,677.34	3,664.85	13.09	13.38	-82.54	-121.83	-276.81	336.27	310.24	26.03	12.919	
3,800.00	3,793.83	3,776.69	3,763.65	13.46	13.77	-82.54	-126.92	-285.87	347.69	320.92	26.77	12.988	
3,900.00	3,893.59	3,876.03	3,862.45	13.83	14.16	-82.53	-132.01	-294.93	359.11	331.59	27.51	13.053	
4,000.00	3,993.34	3,975.38	3,961.25	14.21	14.55	-82.52	-137.10	-303.99	370.53	342.27	28.25	13.115	
4,100.00	4,093.10	4,074.73	4,060.05	14.58	14.94	-82.52	-142.20	-313.05	381.94	352.95	28.99	13.173	
4,200.00	4,192.86	4,174.07	4,158.85	14.95	15.33	-82.51	-147.29	-322.11	393.36	363.63	29.74	13.228	
4,300.00	4,292.61	4,273.42	4,257.65	15.33	15.72	-82.51	-152.38	-331.17	404.78	374.30	30.48	13.281	
4,400.00	4,392.37	4,372.76	4,356.45	15.70	16.11	-82.50	-157.47	-340.23	416.20	384.98	31.22	13.330	
4,500.00	4,492.13	4,472.11	4,455.26	16.08	16.50	-82.50	-162.56	-349.29	427.62	395.66	31.97	13.378	
4,600.00	4,591.88	4,571.45	4,554.06	16.45	16.89	-82.49	-167.65	-358.35	439.04	406.33	32.71	13.423	
4,700.00	4,691.64	4,670.80	4,652.86	16.82	17.29	-82.49	-172.74	-367.41	450.46	417.01	33.45	13.466	
4,800.00	4,791.40	4,770.15	4,751.66	17.20	17.68	-82.48	-177.83	-376.47	461.88	427.69	34.20	13.507	
4,900.00	4,891.15	4,869.49	4,850.46	17.57	18.07	-82.48	-182.92	-385.53	473.30	438.36	34.94	13.546	
5,000.00	4,990.91	4,968.84	4,949.26	17.95	18.46	-82.48	-188.01	-394.59	484.72	449.04	35.68	13.583	
5,100.00	5,090.67	5,068.18	5,048.06	18.32	18.85	-82.47	-193.11	-403.65	496.14	459.71	36.43	13.619	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #202H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
5,200.00	5,190.42	5,167.53	5,146.86	18.70	19.24	-82.47	-198.20	-412.70	507.56	470.39	37.17	13.654	
5,205.01	5,195.42	5,172.50	5,151.81	18.72	19.26	-82.47	-198.45	-413.16	508.13	470.92	37.21	13.655	
5,300.00	5,290.23	5,266.91	5,245.70	19.07	19.64	-82.54	-203.29	-421.77	518.64	480.72	37.92	13.679	
5,400.00	5,390.13	5,366.35	5,344.59	19.43	20.03	-82.79	-208.39	-430.84	528.97	490.32	38.65	13.686	
5,500.00	5,490.09	5,465.82	5,443.51	19.79	20.42	-83.19	-213.48	-439.91	538.57	499.20	39.38	13.678	
5,600.00	5,590.09	5,565.28	5,542.43	20.13	20.81	-83.74	-218.58	-448.98	547.47	507.39	40.08	13.659	
5,604.91	5,595.00	5,570.17	5,547.29	20.15	20.83	-83.77	-218.83	-449.42	547.89	507.77	40.12	13.658	
5,700.00	5,690.09	5,664.73	5,641.33	20.46	21.21	-84.37	-223.68	-458.05	556.03	515.25	40.77	13.638	
5,800.00	5,790.09	5,764.18	5,740.24	20.78	21.60	-84.97	-228.77	-467.12	564.65	523.18	41.46	13.619	
5,900.00	5,890.09	5,863.63	5,839.15	21.11	21.99	-85.56	-233.87	-476.19	573.33	531.17	42.15	13.601	
6,000.00	5,990.09	5,963.09	5,938.05	21.43	22.38	-86.13	-238.97	-485.26	582.07	539.22	42.84	13.586	
6,100.00	6,090.09	6,062.54	6,036.96	21.76	22.78	-86.69	-244.06	-494.33	590.86	547.33	43.54	13.572	
6,200.00	6,190.09	6,161.99	6,135.86	22.09	23.17	-87.23	-249.16	-503.39	599.71	555.48	44.23	13.560	
6,300.00	6,290.09	6,261.44	6,234.77	22.42	23.56	-87.75	-254.25	-512.46	608.61	563.69	44.92	13.548	
6,400.00	6,390.09	6,360.89	6,333.67	22.75	23.96	-88.26	-259.35	-521.53	617.56	571.94	45.61	13.539	
6,500.00	6,490.09	6,460.34	6,432.58	23.08	24.35	-88.75	-264.45	-530.60	626.55	580.25	46.31	13.530	
6,600.00	6,590.09	6,559.88	6,531.58	23.41	24.74	-89.23	-269.55	-539.68	635.60	588.59	47.01	13.522	
6,700.00	6,690.09	6,670.12	6,641.31	23.74	25.17	-89.70	-274.67	-548.80	643.83	596.06	47.77	13.477	
6,800.00	6,790.09	6,780.72	6,751.59	24.08	25.59	-90.06	-278.77	-556.09	650.43	601.90	48.53	13.403	
6,900.00	6,890.09	6,891.60	6,862.30	24.41	26.00	-90.33	-281.83	-561.55	655.35	606.08	49.27	13.301	
7,000.00	6,990.09	7,002.69	6,973.31	24.75	26.39	-90.50	-283.85	-565.13	658.60	608.59	50.00	13.171	
7,100.00	7,090.09	7,113.89	7,084.49	25.08	26.78	-90.59	-284.81	-566.84	660.14	609.43	50.72	13.016	
7,200.00	7,190.09	7,218.49	7,189.09	25.42	27.11	-90.59	-284.90	-567.00	660.29	608.89	51.39	12.848	
7,300.00	7,290.09	7,318.49	7,289.09	25.75	27.43	-90.59	-284.90	-567.00	660.29	608.23	52.06	12.684	
7,400.00	7,390.09	7,418.49	7,389.09	26.09	27.75	-90.59	-284.90	-567.00	660.29	607.56	52.72	12.524	
7,500.00	7,490.09	7,518.49	7,489.09	26.43	28.07	-90.59	-284.90	-567.00	660.29	606.89	53.39	12.367	
7,600.00	7,590.09	7,618.49	7,589.09	26.77	28.39	-90.59	-284.90	-567.00	660.29	606.23	54.06	12.214	
7,700.00	7,690.09	7,718.49	7,689.09	27.11	28.71	-90.59	-284.90	-567.00	660.29	605.56	54.73	12.065	
7,800.00	7,790.09	7,818.49	7,789.09	27.45	29.03	-90.59	-284.90	-567.00	660.29	604.89	55.40	11.919	
7,900.00	7,890.09	7,918.49	7,889.09	27.79	29.35	-90.59	-284.90	-567.00	660.29	604.21	56.07	11.776	
8,000.00	7,990.09	8,018.49	7,989.09	28.13	29.67	-90.59	-284.90	-567.00	660.29	603.54	56.74	11.636	
8,100.00	8,090.09	8,118.49	8,089.09	28.47	30.00	-90.59	-284.90	-567.00	660.29	602.87	57.42	11.500	
8,200.00	8,190.09	8,218.49	8,189.09	28.81	30.32	-90.59	-284.90	-567.00	660.29	602.19	58.09	11.366	
8,300.00	8,290.09	8,318.49	8,289.09	29.15	30.65	-90.59	-284.90	-567.00	660.29	601.52	58.77	11.235	
8,400.00	8,390.09	8,418.49	8,389.09	29.49	30.98	-90.59	-284.90	-567.00	660.29	600.84	59.45	11.107	
8,500.00	8,490.09	8,518.49	8,489.09	29.83	31.30	-90.59	-284.90	-567.00	660.29	600.16	60.12	10.982	
8,600.00	8,590.09	8,618.49	8,589.09	30.18	31.63	-90.59	-284.90	-567.00	660.29	599.48	60.80	10.859	
8,700.00	8,690.09	8,718.49	8,689.09	30.52	31.96	-90.59	-284.90	-567.00	660.29	598.80	61.48	10.739	
8,800.00	8,790.09	8,818.49	8,789.09	30.86	32.29	-90.59	-284.90	-567.00	660.29	598.12	62.16	10.622	
8,900.00	8,890.09	8,918.49	8,889.09	31.21	32.62	-90.59	-284.90	-567.00	660.29	597.44	62.85	10.506	
9,000.00	8,990.09	9,018.49	8,989.09	31.55	32.95	-90.59	-284.90	-567.00	660.29	596.76	63.53	10.394	
9,100.00	9,090.09	9,118.49	9,089.09	31.90	33.28	-90.59	-284.90	-567.00	660.29	596.07	64.21	10.283	
9,200.00	9,190.09	9,218.49	9,189.09	32.24	33.61	-90.59	-284.90	-567.00	660.29	595.39	64.89	10.175	
9,300.00	9,290.09	9,318.49	9,289.09	32.59	33.94	-90.59	-284.90	-567.00	660.29	594.71	65.58	10.069	
9,400.00	9,390.09	9,418.49	9,389.09	32.93	34.28	-90.59	-284.90	-567.00	660.29	594.02	66.26	9.965	
9,500.00	9,490.09	9,518.49	9,489.09	33.28	34.61	-90.59	-284.90	-567.00	660.29	593.34	66.95	9.862	
9,600.00	9,590.09	9,618.49	9,589.09	33.62	34.94	-90.59	-284.90	-567.00	660.29	592.65	67.64	9.762	
9,700.00	9,690.09	9,718.49	9,689.09	33.97	35.28	-90.59	-284.90	-567.00	660.29	591.96	68.32	9.664	
9,800.00	9,790.09	9,818.49	9,789.09	34.31	35.61	-90.59	-284.90	-567.00	660.29	591.28	69.01	9.568	
9,900.00	9,890.09	9,918.49	9,889.09	34.66	35.95	-90.59	-284.90	-567.00	660.29	590.59	69.70	9.473	
10,000.00	9,990.09	10,018.49	9,989.09	35.01	36.28	-90.59	-284.90	-567.00	660.29	589.90	70.39	9.381	
10,100.00	10,090.09	10,118.49	10,089.09	35.36	36.62	-90.59	-284.90	-567.00	660.29	589.21	71.08	9.290	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #202H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
10,200.00	10,190.09	10,218.49	10,189.09	35.70	36.95	-90.59	-284.90	-567.00	660.29	588.52	71.77	9.200	
10,300.00	10,290.09	10,318.49	10,289.09	36.05	37.29	-90.59	-284.90	-567.00	660.29	587.83	72.46	9.113	
10,400.00	10,390.09	10,418.49	10,389.09	36.40	37.63	-90.59	-284.90	-567.00	660.29	587.14	73.15	9.027	
10,500.00	10,490.09	10,518.49	10,489.09	36.75	37.97	-90.59	-284.90	-567.00	660.29	586.45	73.84	8.942	
10,600.00	10,590.09	10,618.49	10,589.09	37.09	38.30	-90.59	-284.90	-567.00	660.29	585.75	74.53	8.859	
10,700.00	10,690.09	10,718.49	10,689.09	37.44	38.64	-90.59	-284.90	-567.00	660.29	585.06	75.22	8.778	
10,800.00	10,790.09	10,818.49	10,789.09	37.79	38.98	-90.59	-284.90	-567.00	660.29	584.37	75.92	8.698	
10,900.00	10,890.09	10,918.49	10,889.09	38.14	39.32	-90.59	-284.90	-567.00	660.29	583.68	76.61	8.619	
11,000.00	10,990.09	11,018.49	10,989.09	38.49	39.66	-90.59	-284.90	-567.00	660.29	582.98	77.30	8.542	
11,100.00	11,090.09	11,118.49	11,089.09	38.84	40.00	-90.59	-284.90	-567.00	660.29	582.29	78.00	8.466	
11,200.00	11,190.09	11,218.49	11,189.09	39.19	40.34	-90.59	-284.90	-567.00	660.29	581.59	78.69	8.391	
11,300.00	11,290.09	11,318.49	11,289.09	39.54	40.68	-90.59	-284.90	-567.00	660.29	580.90	79.39	8.317	
11,400.00	11,390.09	11,418.49	11,389.09	39.89	41.02	-90.59	-284.90	-567.00	660.29	580.20	80.08	8.245	
11,500.00	11,490.09	11,518.49	11,489.09	40.24	41.36	-90.59	-284.90	-567.00	660.29	579.51	80.78	8.174	
11,600.00	11,590.09	11,618.49	11,589.09	40.59	41.70	-90.59	-284.90	-567.00	660.29	578.81	81.47	8.104	
11,654.03	11,644.11	11,672.59	11,643.11	40.78	41.88	-90.39	-282.55	-567.02	660.28	578.43	81.85	8.067	
11,700.00	11,690.09	11,717.94	11,688.08	40.94	42.03	-89.88	-276.66	-567.06	660.31	578.14	82.16	8.037	
11,800.00	11,790.09	11,811.87	11,778.94	41.29	42.30	-87.85	-253.28	-567.22	661.01	578.18	82.83	7.980	
11,824.15	11,814.24	11,833.23	11,798.99	41.37	42.36	-87.21	-245.91	-567.27	661.45	578.47	82.98	7.971	
11,850.00	11,840.08	11,855.63	11,819.69	41.46	42.42	-86.53	-237.39	-567.32	662.07	578.93	83.14	7.964	
11,900.00	11,889.86	11,898.18	11,858.05	41.63	42.52	-85.32	-218.98	-567.45	663.59	580.18	83.41	7.956	
11,950.00	11,939.08	11,939.82	11,894.16	41.79	42.61	-84.30	-198.28	-567.59	665.49	581.84	83.64	7.956	
12,000.00	11,987.34	11,980.63	11,928.01	41.94	42.69	-83.46	-175.48	-567.75	667.70	583.87	83.83	7.965	
12,050.00	12,034.28	12,020.72	11,959.59	42.09	42.76	-82.82	-150.81	-567.91	670.16	586.18	83.98	7.980	
12,100.00	12,079.55	12,060.16	11,988.90	42.23	42.83	-82.37	-124.43	-568.09	672.80	588.72	84.07	8.003	
12,150.00	12,122.80	12,100.00	12,016.60	42.36	42.88	-82.07	-95.81	-568.29	675.55	591.41	84.14	8.029	
12,200.00	12,163.71	12,137.41	12,040.74	42.48	42.92	-82.08	-67.24	-568.48	678.34	594.19	84.14	8.062	
12,250.00	12,201.95	12,175.35	12,063.26	42.59	42.95	-82.23	-36.72	-568.69	681.11	596.97	84.13	8.096	
12,300.00	12,237.24	12,212.90	12,083.52	42.70	42.98	-82.55	-5.11	-568.91	683.79	599.69	84.10	8.131	
12,350.00	12,269.31	12,250.00	12,101.46	42.81	43.00	-83.05	27.36	-569.13	686.33	602.28	84.05	8.165	
12,400.00	12,297.92	12,287.05	12,117.24	42.91	43.01	-83.69	60.87	-569.36	688.68	604.67	84.01	8.197	
12,450.00	12,322.85	12,323.74	12,130.70	43.02	43.02	-84.48	95.00	-569.59	690.79	606.81	83.98	8.226	
12,500.00	12,343.91	12,360.23	12,141.89	43.13	43.02	-85.39	129.72	-569.82	692.62	608.65	83.97	8.248	
12,550.00	12,360.93	12,396.55	12,150.81	43.24	43.03	-86.40	164.93	-570.06	694.13	610.14	83.99	8.264	
12,600.00	12,373.80	12,434.26	12,157.76	43.35	43.05	-87.38	201.98	-570.32	695.29	611.22	84.06	8.271	
12,624.15	12,378.49	12,453.89	12,160.70	43.40	43.07	-87.75	221.39	-570.45	695.63	611.51	84.12	8.269	
12,650.00	12,382.64	12,474.90	12,163.39	43.46	43.11	-88.15	242.23	-570.59	695.90	611.70	84.20	8.265	
12,700.00	12,388.69	12,515.51	12,167.30	43.58	43.20	-88.95	282.64	-570.87	696.29	611.92	84.37	8.253	
12,750.00	12,392.13	12,556.09	12,169.49	43.70	43.31	-89.76	323.16	-571.14	696.52	611.95	84.57	8.236	
12,790.82	12,393.00	12,589.66	12,170.00	43.81	43.41	-90.39	356.72	-571.37	696.60	611.84	84.76	8.218	
12,800.00	12,393.00	12,601.16	12,170.00	43.83	43.44	-90.39	365.90	-571.43	696.60	611.78	84.82	8.213	
12,900.00	12,393.00	12,701.16	12,170.00	44.14	43.77	-90.39	465.90	-572.11	696.59	611.18	85.41	8.156	
13,000.00	12,393.00	12,801.16	12,170.00	44.51	44.16	-90.39	565.90	-572.79	696.59	610.47	86.12	8.089	
13,100.00	12,393.00	12,901.16	12,170.00	44.93	44.59	-90.39	665.90	-573.48	696.58	609.65	86.94	8.012	
13,200.00	12,393.00	13,001.16	12,170.00	45.41	45.09	-90.39	765.89	-574.16	696.58	608.71	87.87	7.928	
13,300.00	12,393.00	13,101.16	12,170.00	45.95	45.63	-90.39	865.89	-574.84	696.57	607.68	88.90	7.836	
13,400.00	12,393.00	13,201.16	12,170.00	46.54	46.23	-90.39	965.89	-575.52	696.57	606.54	90.03	7.737	
13,500.00	12,393.00	13,301.16	12,170.00	47.18	46.87	-90.39	1,065.89	-576.20	696.56	605.30	91.26	7.633	
13,600.00	12,393.00	13,401.16	12,170.00	47.87	47.56	-90.39	1,165.89	-576.88	696.56	603.97	92.58	7.524	
13,700.00	12,393.00	13,501.16	12,170.00	48.60	48.30	-90.39	1,265.88	-577.56	696.55	602.56	94.00	7.410	
13,800.00	12,393.00	13,601.16	12,170.00	49.38	49.09	-90.39	1,365.88	-578.24	696.55	601.05	95.49	7.294	
13,900.00	12,393.00	13,701.16	12,170.00	50.21	49.91	-90.39	1,465.88	-578.92	696.54	599.47	97.07	7.175	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #202H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
14,000.00	12,393.00	13,801.16	12,170.00	51.07	50.78	-90.39	1,565.88	-579.61	696.54	597.81	98.73	7.055	
14,100.00	12,393.00	13,901.16	12,170.00	51.97	51.68	-90.39	1,665.87	-580.29	696.53	596.07	100.46	6.933	
14,200.00	12,393.00	14,001.16	12,170.00	52.91	52.62	-90.39	1,765.87	-580.97	696.52	594.26	102.26	6.811	
14,300.00	12,393.00	14,101.16	12,170.00	53.89	53.59	-90.39	1,865.87	-581.65	696.52	592.39	104.13	6.689	
14,400.00	12,393.00	14,201.16	12,170.00	54.89	54.60	-90.39	1,965.87	-582.33	696.51	590.46	106.06	6.567	
14,500.00	12,393.00	14,301.16	12,170.00	55.93	55.64	-90.39	2,065.86	-583.01	696.51	588.46	108.04	6.446	
14,600.00	12,393.00	14,401.16	12,170.00	57.00	56.71	-90.39	2,165.86	-583.69	696.50	586.41	110.09	6.327	
14,700.00	12,393.00	14,501.16	12,170.00	58.10	57.80	-90.39	2,265.86	-584.37	696.50	584.31	112.19	6.208	
14,800.00	12,393.00	14,601.16	12,170.00	59.22	58.92	-90.39	2,365.86	-585.05	696.49	582.16	114.34	6.092	
14,900.00	12,393.00	14,701.16	12,170.00	60.36	60.07	-90.39	2,465.86	-585.74	696.49	579.96	116.53	5.977	
15,000.00	12,393.00	14,801.16	12,170.00	61.53	61.24	-90.39	2,565.85	-586.42	696.48	577.71	118.77	5.864	
15,100.00	12,393.00	14,901.16	12,170.00	62.73	62.43	-90.39	2,665.85	-587.10	696.48	575.42	121.06	5.753	
15,200.00	12,393.00	15,001.16	12,170.00	63.94	63.65	-90.39	2,765.85	-587.78	696.47	573.09	123.38	5.645	
15,300.00	12,393.00	15,101.16	12,170.00	65.17	64.88	-90.39	2,865.85	-588.46	696.47	570.73	125.74	5.539	
15,400.00	12,393.00	15,201.16	12,170.00	66.42	66.13	-90.39	2,965.84	-589.14	696.46	568.33	128.14	5.435	
15,500.00	12,393.00	15,301.16	12,170.00	67.69	67.40	-90.39	3,065.84	-589.82	696.46	565.89	130.57	5.334	
15,600.00	12,393.00	15,401.16	12,170.00	68.97	68.68	-90.39	3,165.84	-590.50	696.45	563.42	133.03	5.235	
15,700.00	12,393.00	15,501.16	12,170.00	70.28	69.98	-90.39	3,265.84	-591.18	696.44	560.93	135.52	5.139	
15,800.00	12,393.00	15,601.16	12,170.00	71.59	71.30	-90.39	3,365.83	-591.87	696.44	558.40	138.04	5.045	
15,900.00	12,393.00	15,701.16	12,170.00	72.92	72.63	-90.39	3,465.83	-592.55	696.43	555.85	140.59	4.954	
16,000.00	12,393.00	15,801.16	12,170.00	74.26	73.97	-90.39	3,565.83	-593.23	696.43	553.27	143.16	4.865	
16,100.00	12,393.00	15,901.16	12,170.00	75.62	75.33	-90.39	3,665.83	-593.91	696.42	550.67	145.76	4.778	
16,200.00	12,393.00	16,001.16	12,170.00	76.99	76.69	-90.39	3,765.82	-594.59	696.42	548.04	148.38	4.694	
16,300.00	12,393.00	16,101.16	12,170.00	78.37	78.07	-90.39	3,865.82	-595.27	696.41	545.39	151.02	4.611	
16,400.00	12,393.00	16,201.16	12,170.00	79.75	79.46	-90.39	3,965.82	-595.95	696.41	542.73	153.68	4.532	
16,500.00	12,393.00	16,301.16	12,170.00	81.15	80.86	-90.39	4,065.82	-596.63	696.40	540.04	156.36	4.454	
16,600.00	12,393.00	16,401.16	12,170.00	82.56	82.27	-90.39	4,165.82	-597.31	696.40	537.33	159.06	4.378	
16,700.00	12,393.00	16,501.16	12,170.00	83.98	83.69	-90.39	4,265.81	-598.00	696.39	534.61	161.78	4.305	
16,800.00	12,393.00	16,601.16	12,170.00	85.41	85.12	-90.39	4,365.81	-598.68	696.39	531.87	164.52	4.233	
16,900.00	12,393.00	16,701.16	12,170.00	86.84	86.55	-90.39	4,465.81	-599.36	696.38	529.11	167.27	4.163	
17,000.00	12,393.00	16,801.16	12,170.00	88.29	87.99	-90.39	4,565.81	-600.04	696.37	526.34	170.03	4.096	
17,100.00	12,393.00	16,901.16	12,170.00	89.74	89.44	-90.39	4,665.80	-600.72	696.37	523.56	172.81	4.030	
17,143.70	12,393.00	16,942.54	12,170.00	90.37	90.00	-90.39	4,709.50	-601.02	696.37	522.45	173.92	4.004	
17,144.46	12,393.00	16,943.30	12,170.00	90.38	90.01	-90.39	4,710.26	-601.02	696.37	522.43	173.94	4.004 SF	

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #205H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
0.00	0.00	2.00	2.00	0.00	0.00	-90.56	-13.00	-1,320.00	1,320.06				
100.00	100.00	102.00	102.00	0.13	0.14	-90.56	-13.00	-1,320.00	1,320.06	1,319.80	0.26	5,010.169	
200.00	200.00	202.00	202.00	0.49	0.49	-90.56	-13.00	-1,320.00	1,320.06	1,319.08	0.98	1,346.427	
300.00	300.00	302.00	302.00	0.85	0.85	-90.56	-13.00	-1,320.00	1,320.06	1,318.37	1.70	777.715	
400.00	400.00	402.00	402.00	1.20	1.21	-90.56	-13.00	-1,320.00	1,320.06	1,317.65	2.41	546.767	
500.00	500.00	502.00	502.00	1.56	1.57	-90.56	-13.00	-1,320.00	1,320.06	1,316.93	3.13	421.577	
600.00	600.00	602.00	602.00	1.92	1.93	-90.56	-13.00	-1,320.00	1,320.06	1,316.22	3.85	343.035	
700.00	700.00	702.00	702.00	2.28	2.29	-90.56	-13.00	-1,320.00	1,320.06	1,315.50	4.57	289.162	
800.00	800.00	802.00	802.00	2.64	2.64	-90.56	-13.00	-1,320.00	1,320.06	1,314.78	5.28	249.914	
900.00	900.00	902.00	902.00	3.00	3.00	-90.56	-13.00	-1,320.00	1,320.06	1,314.07	6.00	220.047	
1,000.00	1,000.00	1,002.15	1,002.15	3.35	3.36	-90.56	-13.00	-1,320.00	1,320.06	1,313.35	6.72	196.551	
1,100.00	1,099.99	1,109.79	1,109.78	3.70	3.73	-90.57	-14.00	-1,319.67	1,320.03	1,312.61	7.42	177.834	
1,200.00	1,199.96	1,217.42	1,217.37	4.02	4.08	-90.59	-16.91	-1,318.69	1,319.96	1,311.86	8.10	162.862	
1,300.00	1,299.86	1,325.05	1,324.87	4.36	4.44	-90.62	-21.74	-1,317.08	1,319.85	1,311.05	8.80	150.011	
1,399.14	1,398.82	1,429.49	1,429.09	4.69	4.80	-90.65	-28.19	-1,314.92	1,319.73	1,310.24	9.49	139.067	CC
1,399.91	1,399.58	1,430.26	1,429.86	4.70	4.80	-90.65	-28.24	-1,314.90	1,319.73	1,310.23	9.50	138.990	
1,500.00	1,499.43	1,530.35	1,529.71	5.04	5.15	-90.65	-34.86	-1,312.69	1,319.73	1,309.54	10.19	129.565	
1,600.00	1,599.19	1,630.35	1,629.47	5.39	5.50	-90.65	-41.47	-1,310.47	1,319.73	1,308.85	10.88	121.252	
1,700.00	1,698.94	1,730.35	1,729.22	5.74	5.85	-90.65	-48.09	-1,308.26	1,319.74	1,308.15	11.59	113.876	
1,800.00	1,798.70	1,830.35	1,828.98	6.10	6.21	-90.65	-54.70	-1,306.05	1,319.74	1,307.44	12.30	107.297	
1,900.00	1,898.46	1,930.35	1,928.74	6.46	6.57	-90.65	-61.32	-1,303.83	1,319.75	1,306.73	13.02	101.401	
2,000.00	1,998.21	2,030.35	2,028.49	6.82	6.93	-90.65	-67.93	-1,301.62	1,319.75	1,306.02	13.73	96.092	
2,100.00	2,097.97	2,130.35	2,128.25	7.18	7.29	-90.65	-74.55	-1,299.41	1,319.75	1,305.30	14.46	91.291	
2,200.00	2,197.73	2,230.35	2,228.00	7.54	7.65	-90.65	-81.16	-1,297.19	1,319.76	1,304.58	15.18	86.929	
2,300.00	2,297.48	2,330.35	2,327.76	7.91	8.02	-90.65	-87.78	-1,294.98	1,319.76	1,303.85	15.91	82.953	
2,400.00	2,397.24	2,430.35	2,427.52	8.27	8.39	-90.65	-94.40	-1,292.77	1,319.77	1,303.13	16.64	79.315	
2,500.00	2,497.00	2,530.35	2,527.27	8.64	8.75	-90.65	-101.01	-1,290.55	1,319.77	1,302.40	17.37	75.974	
2,600.00	2,596.75	2,630.35	2,627.03	9.01	9.12	-90.65	-107.63	-1,288.34	1,319.78	1,301.67	18.10	72.896	
2,700.00	2,696.51	2,730.35	2,726.79	9.38	9.49	-90.65	-114.24	-1,286.13	1,319.78	1,300.94	18.84	70.053	
2,800.00	2,796.27	2,830.35	2,826.54	9.75	9.86	-90.65	-120.86	-1,283.91	1,319.78	1,300.21	19.58	67.419	
2,900.00	2,896.02	2,930.35	2,926.30	10.12	10.23	-90.65	-127.47	-1,281.70	1,319.79	1,299.47	20.31	64.972	
3,000.00	2,995.78	3,030.35	3,026.06	10.49	10.60	-90.65	-134.09	-1,279.48	1,319.79	1,298.74	21.05	62.694	
3,100.00	3,095.54	3,130.35	3,125.81	10.86	10.97	-90.65	-140.70	-1,277.27	1,319.80	1,298.01	21.79	60.567	
3,200.00	3,195.29	3,230.35	3,225.57	11.23	11.34	-90.65	-147.32	-1,275.06	1,319.80	1,297.27	22.53	58.578	
3,300.00	3,295.05	3,330.35	3,325.33	11.60	11.71	-90.65	-153.93	-1,272.84	1,319.80	1,296.53	23.27	56.713	
3,400.00	3,394.81	3,430.35	3,425.08	11.97	12.08	-90.65	-160.55	-1,270.63	1,319.81	1,295.80	24.01	54.962	
3,500.00	3,494.56	3,530.35	3,524.84	12.34	12.46	-90.65	-167.16	-1,268.42	1,319.81	1,295.06	24.76	53.314	
3,600.00	3,594.32	3,630.35	3,624.59	12.71	12.83	-90.65	-173.78	-1,266.20	1,319.82	1,294.32	25.50	51.762	
3,700.00	3,694.08	3,730.35	3,724.35	13.09	13.20	-90.65	-180.39	-1,263.99	1,319.82	1,293.58	26.24	50.296	
3,800.00	3,793.83	3,830.35	3,824.11	13.46	13.57	-90.66	-187.01	-1,261.78	1,319.82	1,292.84	26.98	48.910	
3,900.00	3,893.59	3,930.35	3,923.86	13.83	13.95	-90.66	-193.62	-1,259.56	1,319.83	1,292.10	27.73	47.597	
4,000.00	3,993.34	4,030.35	4,023.62	14.21	14.32	-90.66	-200.24	-1,257.35	1,319.83	1,291.36	28.47	46.353	
4,100.00	4,093.10	4,130.35	4,123.38	14.58	14.69	-90.66	-206.85	-1,255.14	1,319.84	1,290.62	29.22	45.171	
4,200.00	4,192.86	4,230.35	4,223.13	14.95	15.07	-90.66	-213.47	-1,252.92	1,319.84	1,289.88	29.96	44.048	
4,300.00	4,292.61	4,330.35	4,322.89	15.33	15.44	-90.66	-220.08	-1,250.71	1,319.85	1,289.14	30.71	42.979	
4,400.00	4,392.37	4,430.35	4,422.65	15.70	15.82	-90.66	-226.70	-1,248.50	1,319.85	1,288.39	31.46	41.960	
4,500.00	4,492.13	4,530.35	4,522.40	16.08	16.19	-90.66	-233.31	-1,246.28	1,319.85	1,287.65	32.20	40.988	
4,600.00	4,591.88	4,630.35	4,622.16	16.45	16.56	-90.66	-239.93	-1,244.07	1,319.86	1,286.91	32.95	40.059	
4,700.00	4,691.64	4,730.35	4,721.91	16.82	16.94	-90.66	-246.54	-1,241.86	1,319.86	1,286.17	33.69	39.172	
4,800.00	4,791.40	4,830.35	4,821.67	17.20	17.31	-90.66	-253.16	-1,239.64	1,319.87	1,285.42	34.44	38.322	
4,900.00	4,891.15	4,930.35	4,921.43	17.57	17.69	-90.66	-259.77	-1,237.43	1,319.87	1,284.68	35.19	37.509	
5,000.00	4,990.91	5,030.35	5,021.18	17.95	18.06	-90.66	-266.39	-1,235.22	1,319.87	1,283.94	35.94	36.729	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #205H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
5,100.00	5,090.67	5,130.35	5,120.94	18.32	18.44	-90.66	-273.00	-1,233.00	1,319.88	1,283.20	36.68	35.981	
5,103.96	5,094.62	5,134.31	5,124.89	18.34	18.45	-90.66	-273.27	-1,232.92	1,319.88	1,283.17	36.71	35.952	
5,200.00	5,190.42	5,228.35	5,218.70	18.70	18.80	-90.65	-279.42	-1,230.86	1,319.91	1,282.48	37.42	35.271	
5,205.01	5,195.42	5,233.02	5,223.37	18.72	18.82	-90.65	-279.71	-1,230.76	1,319.91	1,282.46	37.46	35.237	
5,300.00	5,290.23	5,321.73	5,311.94	19.07	19.15	-90.61	-284.44	-1,229.18	1,320.07	1,281.93	38.14	34.613	
5,400.00	5,390.13	5,415.11	5,405.24	19.43	19.49	-90.58	-288.02	-1,227.98	1,320.20	1,281.36	38.84	33.990	
5,500.00	5,490.09	5,508.49	5,498.59	19.79	19.82	-90.56	-290.15	-1,227.26	1,320.29	1,280.76	39.53	33.400	
5,600.00	5,590.09	5,601.99	5,592.09	20.13	20.14	-90.56	-290.85	-1,227.03	1,320.34	1,280.16	40.18	32.858	
5,604.91	5,595.00	5,606.91	5,597.00	20.15	20.15	-90.56	-290.85	-1,227.03	1,320.35	1,280.13	40.22	32.832	
5,700.00	5,690.09	5,701.99	5,692.09	20.46	20.46	-90.56	-290.85	-1,227.03	1,320.35	1,279.51	40.83	32.337	
5,800.00	5,790.09	5,801.99	5,792.09	20.78	20.78	-90.56	-290.85	-1,227.03	1,320.35	1,278.86	41.48	31.830	
5,900.00	5,890.09	5,901.99	5,892.09	21.11	21.11	-90.56	-290.85	-1,227.03	1,320.35	1,278.21	42.13	31.338	
6,000.00	5,990.09	6,001.99	5,992.09	21.43	21.44	-90.56	-290.85	-1,227.03	1,320.35	1,277.56	42.79	30.859	
6,100.00	6,090.09	6,101.99	6,092.09	21.76	21.76	-90.56	-290.85	-1,227.03	1,320.35	1,276.90	43.44	30.393	
6,200.00	6,190.09	6,201.99	6,192.09	22.09	22.09	-90.56	-290.85	-1,227.03	1,320.35	1,276.25	44.10	29.940	
6,300.00	6,290.09	6,301.99	6,292.09	22.42	22.42	-90.56	-290.85	-1,227.03	1,320.35	1,275.59	44.76	29.499	
6,400.00	6,390.09	6,401.99	6,392.09	22.75	22.75	-90.56	-290.85	-1,227.03	1,320.35	1,274.92	45.42	29.070	
6,500.00	6,490.09	6,501.99	6,492.09	23.08	23.08	-90.56	-290.85	-1,227.03	1,320.35	1,274.26	46.08	28.651	
6,600.00	6,590.09	6,601.99	6,592.09	23.41	23.42	-90.56	-290.85	-1,227.03	1,320.35	1,273.60	46.75	28.244	
6,700.00	6,690.09	6,701.99	6,692.09	23.74	23.75	-90.56	-290.85	-1,227.03	1,320.35	1,272.93	47.41	27.847	
6,800.00	6,790.09	6,801.99	6,792.09	24.08	24.08	-90.56	-290.85	-1,227.03	1,320.35	1,272.26	48.08	27.461	
6,900.00	6,890.09	6,901.99	6,892.09	24.41	24.42	-90.56	-290.85	-1,227.03	1,320.35	1,271.60	48.75	27.084	
7,000.00	6,990.09	7,001.99	6,992.09	24.75	24.75	-90.56	-290.85	-1,227.03	1,320.35	1,270.92	49.42	26.717	
7,100.00	7,090.09	7,101.99	7,092.09	25.08	25.09	-90.56	-290.85	-1,227.03	1,320.35	1,270.25	50.09	26.359	
7,200.00	7,190.09	7,201.99	7,192.09	25.42	25.42	-90.56	-290.85	-1,227.03	1,320.35	1,269.58	50.76	26.009	
7,300.00	7,290.09	7,301.99	7,292.09	25.75	25.76	-90.56	-290.85	-1,227.03	1,320.35	1,268.91	51.44	25.668	
7,400.00	7,390.09	7,401.99	7,392.09	26.09	26.10	-90.56	-290.85	-1,227.03	1,320.35	1,268.23	52.11	25.336	
7,500.00	7,490.09	7,501.99	7,492.09	26.43	26.43	-90.56	-290.85	-1,227.03	1,320.35	1,267.56	52.79	25.011	
7,600.00	7,590.09	7,601.99	7,592.09	26.77	26.77	-90.56	-290.85	-1,227.03	1,320.35	1,266.88	53.47	24.695	
7,700.00	7,690.09	7,701.99	7,692.09	27.11	27.11	-90.56	-290.85	-1,227.03	1,320.35	1,266.20	54.15	24.385	
7,800.00	7,790.09	7,801.99	7,792.09	27.45	27.45	-90.56	-290.85	-1,227.03	1,320.35	1,265.52	54.82	24.083	
7,900.00	7,890.09	7,901.99	7,892.09	27.79	27.79	-90.56	-290.85	-1,227.03	1,320.35	1,264.84	55.50	23.788	
8,000.00	7,990.09	8,001.99	7,992.09	28.13	28.13	-90.56	-290.85	-1,227.03	1,320.35	1,264.16	56.19	23.500	
8,100.00	8,090.09	8,101.99	8,092.09	28.47	28.47	-90.56	-290.85	-1,227.03	1,320.35	1,263.48	56.87	23.218	
8,200.00	8,190.09	8,201.99	8,192.09	28.81	28.81	-90.56	-290.85	-1,227.03	1,320.35	1,262.79	57.55	22.942	
8,300.00	8,290.09	8,301.99	8,292.09	29.15	29.16	-90.56	-290.85	-1,227.03	1,320.35	1,262.11	58.23	22.673	
8,400.00	8,390.09	8,401.99	8,392.09	29.49	29.50	-90.56	-290.85	-1,227.03	1,320.35	1,261.43	58.92	22.410	
8,500.00	8,490.09	8,501.99	8,492.09	29.83	29.84	-90.56	-290.85	-1,227.03	1,320.35	1,260.74	59.60	22.152	
8,600.00	8,590.09	8,601.99	8,592.09	30.18	30.18	-90.56	-290.85	-1,227.03	1,320.35	1,260.05	60.29	21.900	
8,700.00	8,690.09	8,701.99	8,692.09	30.52	30.53	-90.56	-290.85	-1,227.03	1,320.35	1,259.37	60.98	21.653	
8,800.00	8,790.09	8,801.99	8,792.09	30.86	30.87	-90.56	-290.85	-1,227.03	1,320.35	1,258.68	61.66	21.412	
8,900.00	8,890.09	8,901.99	8,892.09	31.21	31.21	-90.56	-290.85	-1,227.03	1,320.35	1,257.99	62.35	21.176	
9,000.00	8,990.09	9,001.99	8,992.09	31.55	31.56	-90.56	-290.85	-1,227.03	1,320.35	1,257.30	63.04	20.944	
9,100.00	9,090.09	9,101.99	9,092.09	31.90	31.90	-90.56	-290.85	-1,227.03	1,320.35	1,256.61	63.73	20.718	
9,200.00	9,190.09	9,201.99	9,192.09	32.24	32.25	-90.56	-290.85	-1,227.03	1,320.35	1,255.92	64.42	20.496	
9,300.00	9,290.09	9,301.99	9,292.09	32.59	32.59	-90.56	-290.85	-1,227.03	1,320.35	1,255.23	65.11	20.278	
9,400.00	9,390.09	9,401.99	9,392.09	32.93	32.94	-90.56	-290.85	-1,227.03	1,320.35	1,254.54	65.80	20.066	
9,500.00	9,490.09	9,501.99	9,492.09	33.28	33.28	-90.56	-290.85	-1,227.03	1,320.35	1,253.85	66.49	19.857	
9,600.00	9,590.09	9,601.99	9,592.09	33.62	33.63	-90.56	-290.85	-1,227.03	1,320.35	1,253.16	67.19	19.652	
9,700.00	9,690.09	9,701.99	9,692.09	33.97	33.97	-90.56	-290.85	-1,227.03	1,320.35	1,252.47	67.88	19.452	
9,800.00	9,790.09	9,801.99	9,792.09	34.31	34.32	-90.56	-290.85	-1,227.03	1,320.35	1,251.77	68.57	19.255	
9,900.00	9,890.09	9,901.99	9,892.09	34.66	34.67	-90.56	-290.85	-1,227.03	1,320.35	1,251.08	69.26	19.062	

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #205H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
10,000.00	9,990.09	10,001.99	9,992.09	35.01	35.01	-90.56	-290.85	-1,227.03	1,320.35	1,250.39	69.96	18.873	
10,100.00	10,090.09	10,101.99	10,092.09	35.36	35.36	-90.56	-290.85	-1,227.03	1,320.35	1,249.69	70.65	18.688	
10,200.00	10,190.09	10,201.99	10,192.09	35.70	35.71	-90.56	-290.85	-1,227.03	1,320.35	1,249.00	71.35	18.506	
10,300.00	10,290.09	10,301.99	10,292.09	36.05	36.06	-90.56	-290.85	-1,227.03	1,320.35	1,248.30	72.04	18.327	
10,400.00	10,390.09	10,401.99	10,392.09	36.40	36.40	-90.56	-290.85	-1,227.03	1,320.35	1,247.61	72.74	18.152	
10,500.00	10,490.09	10,501.99	10,492.09	36.75	36.75	-90.56	-290.85	-1,227.03	1,320.35	1,246.91	73.44	17.979	
10,600.00	10,590.09	10,601.99	10,592.09	37.09	37.10	-90.56	-290.85	-1,227.03	1,320.35	1,246.21	74.13	17.811	
10,700.00	10,690.09	10,701.99	10,692.09	37.44	37.45	-90.56	-290.85	-1,227.03	1,320.35	1,245.52	74.83	17.645	
10,800.00	10,790.09	10,801.99	10,792.09	37.79	37.80	-90.56	-290.85	-1,227.03	1,320.35	1,244.82	75.53	17.482	
10,900.00	10,890.09	10,901.99	10,892.09	38.14	38.15	-90.56	-290.85	-1,227.03	1,320.35	1,244.12	76.23	17.322	
11,000.00	10,990.09	11,001.99	10,992.09	38.49	38.50	-90.56	-290.85	-1,227.03	1,320.35	1,243.42	76.92	17.164	
11,100.00	11,090.09	11,101.99	11,092.09	38.84	38.84	-90.56	-290.85	-1,227.03	1,320.35	1,242.72	77.62	17.010	
11,200.00	11,190.09	11,201.99	11,192.09	39.19	39.19	-90.56	-290.85	-1,227.03	1,320.35	1,242.02	78.32	16.858	
11,300.00	11,290.09	11,301.99	11,292.09	39.54	39.54	-90.56	-290.85	-1,227.03	1,320.35	1,241.33	79.02	16.709	
11,400.00	11,390.09	11,401.99	11,392.09	39.89	39.89	-90.56	-290.85	-1,227.03	1,320.35	1,240.63	79.72	16.562	
11,500.00	11,490.09	11,501.99	11,492.09	40.24	40.24	-90.56	-290.85	-1,227.03	1,320.35	1,239.93	80.42	16.418	
11,600.00	11,590.09	11,601.99	11,592.09	40.59	40.59	-90.56	-290.85	-1,227.03	1,320.35	1,239.23	81.12	16.277	
11,700.00	11,690.09	11,701.99	11,692.09	40.94	40.94	-90.56	-290.85	-1,227.03	1,320.35	1,238.53	81.82	16.137	
11,800.00	11,790.09	11,802.00	11,792.09	41.29	41.29	-90.56	-290.85	-1,227.03	1,320.35	1,237.83	82.52	16.000	
11,824.15	11,814.24	11,826.30	11,816.38	41.37	41.38	-90.53	-290.30	-1,227.04	1,320.34	1,237.66	82.69	15.968	
11,850.00	11,840.08	11,852.24	11,842.27	41.46	41.47	-90.48	-288.57	-1,227.05	1,320.34	1,237.47	82.87	15.933	
11,898.30	11,888.18	11,900.58	11,890.18	41.62	41.63	-90.39	-282.24	-1,227.09	1,320.34	1,237.15	83.19	15.872	
11,900.00	11,889.86	11,902.28	11,891.85	41.63	41.63	-90.39	-281.95	-1,227.09	1,320.34	1,237.14	83.20	15.870	
11,950.00	11,939.08	11,952.13	11,940.48	41.79	41.79	-90.29	-271.07	-1,227.17	1,320.34	1,236.83	83.52	15.809	
12,000.00	11,987.34	12,001.79	11,987.81	41.94	41.94	-90.21	-256.07	-1,227.27	1,320.35	1,236.53	83.82	15.753	
12,050.00	12,034.28	12,051.27	12,033.49	42.09	42.08	-90.13	-237.12	-1,227.40	1,320.36	1,236.25	84.10	15.699	
12,100.00	12,079.55	12,100.57	12,077.22	42.23	42.21	-90.06	-214.38	-1,227.55	1,320.37	1,236.00	84.37	15.649	
12,150.00	12,122.80	12,149.69	12,118.68	42.36	42.33	-90.01	-188.06	-1,227.73	1,320.38	1,235.76	84.63	15.602	
12,200.00	12,163.71	12,198.66	12,157.62	42.48	42.45	-89.97	-158.40	-1,227.93	1,320.40	1,235.53	84.87	15.558	
12,250.00	12,201.95	12,247.47	12,193.77	42.59	42.56	-89.94	-125.63	-1,228.16	1,320.42	1,235.32	85.10	15.516	
12,300.00	12,237.24	12,296.13	12,226.91	42.70	42.66	-89.93	-90.01	-1,228.40	1,320.44	1,235.11	85.33	15.475	
12,350.00	12,269.31	12,344.66	12,256.83	42.81	42.76	-89.94	-51.82	-1,228.66	1,320.46	1,234.92	85.54	15.436	
12,400.00	12,297.92	12,393.07	12,283.35	42.91	42.87	-89.96	-11.34	-1,228.94	1,320.48	1,234.72	85.76	15.398	
12,450.00	12,322.85	12,441.37	12,306.31	43.02	42.97	-90.00	31.14	-1,229.22	1,320.50	1,234.53	85.97	15.360	
12,500.00	12,343.91	12,489.57	12,325.58	43.13	43.07	-90.05	75.30	-1,229.52	1,320.52	1,234.34	86.18	15.323	
12,550.00	12,360.93	12,537.69	12,341.04	43.24	43.18	-90.11	120.85	-1,229.83	1,320.54	1,234.14	86.39	15.285	
12,600.00	12,373.80	12,585.73	12,352.61	43.35	43.28	-90.18	167.46	-1,230.15	1,320.55	1,233.94	86.61	15.247	
12,624.15	12,378.49	12,609.04	12,356.83	43.40	43.34	-90.22	190.39	-1,230.31	1,320.56	1,233.84	86.72	15.229	
12,650.00	12,382.64	12,634.25	12,360.68	43.46	43.39	-90.24	215.30	-1,230.48	1,320.56	1,233.73	86.83	15.208	
12,700.00	12,388.69	12,683.01	12,366.24	43.58	43.51	-90.30	263.73	-1,230.81	1,320.57	1,233.50	87.07	15.167	
12,750.00	12,392.13	12,731.75	12,369.32	43.70	43.63	-90.35	312.37	-1,231.14	1,320.57	1,233.25	87.31	15.124	
12,790.82	12,393.00	12,771.63	12,370.00	43.81	43.74	-90.39	352.24	-1,231.41	1,320.57	1,233.04	87.53	15.088	
12,800.00	12,393.00	12,780.80	12,370.00	43.83	43.77	-90.39	361.42	-1,231.47	1,320.57	1,232.99	87.58	15.079	
12,900.00	12,393.00	12,880.80	12,370.00	44.14	44.08	-90.39	461.41	-1,232.15	1,320.56	1,232.37	88.19	14.973	
13,000.00	12,393.00	12,980.80	12,370.00	44.51	44.45	-90.39	561.41	-1,232.83	1,320.56	1,231.63	88.93	14.850	
13,100.00	12,393.00	13,080.80	12,370.00	44.93	44.88	-90.39	661.41	-1,233.51	1,320.55	1,230.77	89.78	14.709	
13,200.00	12,393.00	13,180.80	12,370.00	45.41	45.36	-90.39	761.41	-1,234.19	1,320.55	1,229.80	90.74	14.553	
13,300.00	12,393.00	13,280.80	12,370.00	45.95	45.90	-90.39	861.40	-1,234.88	1,320.54	1,228.72	91.82	14.382	
13,400.00	12,393.00	13,380.80	12,370.00	46.54	46.49	-90.39	961.40	-1,235.56	1,320.53	1,227.54	93.00	14.200	
13,500.00	12,393.00	13,480.80	12,370.00	47.18	47.13	-90.39	1,061.40	-1,236.24	1,320.53	1,226.25	94.28	14.007	
13,600.00	12,393.00	13,580.80	12,370.00	47.87	47.83	-90.39	1,161.40	-1,236.92	1,320.52	1,224.86	95.66	13.804	
13,700.00	12,393.00	13,680.80	12,370.00	48.60	48.57	-90.39	1,261.39	-1,237.60	1,320.51	1,223.38	97.13	13.595	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #205H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
13,800.00	12,393.00	13,780.80	12,370.00	49.38	49.35	-90.39	1,361.39	-1,238.28	1,320.51	1,221.81	98.70	13.379	
13,900.00	12,393.00	13,880.80	12,370.00	50.21	50.17	-90.39	1,461.39	-1,238.96	1,320.50	1,220.16	100.35	13.160	
14,000.00	12,393.00	13,980.80	12,370.00	51.07	51.04	-90.39	1,561.39	-1,239.64	1,320.50	1,218.42	102.08	12.936	
14,100.00	12,393.00	14,080.80	12,370.00	51.97	51.95	-90.39	1,661.38	-1,240.32	1,320.49	1,216.61	103.88	12.711	
14,200.00	12,393.00	14,180.80	12,370.00	52.91	52.89	-90.39	1,761.38	-1,241.00	1,320.48	1,214.72	105.76	12.485	
14,300.00	12,393.00	14,280.80	12,370.00	53.89	53.87	-90.39	1,861.38	-1,241.68	1,320.48	1,212.76	107.71	12.259	
14,400.00	12,393.00	14,380.80	12,370.00	54.89	54.87	-90.39	1,961.38	-1,242.36	1,320.47	1,210.74	109.73	12.034	
14,500.00	12,393.00	14,480.80	12,370.00	55.93	55.91	-90.39	2,061.38	-1,243.04	1,320.46	1,208.66	111.81	11.810	
14,600.00	12,393.00	14,580.80	12,370.00	57.00	56.98	-90.39	2,161.37	-1,243.72	1,320.46	1,206.51	113.94	11.589	
14,700.00	12,393.00	14,680.80	12,370.00	58.10	58.08	-90.39	2,261.37	-1,244.40	1,320.45	1,204.32	116.14	11.370	
14,800.00	12,393.00	14,780.80	12,370.00	59.22	59.21	-90.39	2,361.37	-1,245.08	1,320.45	1,202.06	118.38	11.154	
14,900.00	12,393.00	14,880.80	12,370.00	60.36	60.35	-90.39	2,461.37	-1,245.76	1,320.44	1,199.76	120.68	10.942	
15,000.00	12,393.00	14,980.80	12,370.00	61.53	61.53	-90.39	2,561.36	-1,246.44	1,320.43	1,197.42	123.02	10.734	
15,100.00	12,393.00	15,080.80	12,370.00	62.73	62.72	-90.39	2,661.36	-1,247.13	1,320.43	1,195.03	125.40	10.530	
15,200.00	12,393.00	15,180.80	12,370.00	63.94	63.93	-90.39	2,761.36	-1,247.81	1,320.42	1,192.59	127.83	10.330	
15,300.00	12,393.00	15,280.80	12,370.00	65.17	65.17	-90.39	2,861.36	-1,248.49	1,320.42	1,190.12	130.29	10.134	
15,400.00	12,393.00	15,380.80	12,370.00	66.42	66.42	-90.39	2,961.35	-1,249.17	1,320.41	1,187.61	132.80	9.943	
15,500.00	12,393.00	15,480.80	12,370.00	67.69	67.69	-90.39	3,061.35	-1,249.85	1,320.40	1,185.07	135.34	9.756	
15,600.00	12,393.00	15,580.80	12,370.00	68.97	68.98	-90.39	3,161.35	-1,250.53	1,320.40	1,182.49	137.91	9.575	
15,700.00	12,393.00	15,680.80	12,370.00	70.28	70.28	-90.39	3,261.35	-1,251.21	1,320.39	1,179.88	140.51	9.397	
15,800.00	12,393.00	15,780.80	12,370.00	71.59	71.60	-90.39	3,361.35	-1,251.89	1,320.38	1,177.24	143.14	9.224	
15,900.00	12,393.00	15,880.80	12,370.00	72.92	72.93	-90.39	3,461.34	-1,252.57	1,320.38	1,174.58	145.80	9.056	
16,000.00	12,393.00	15,980.80	12,370.00	74.26	74.27	-90.39	3,561.34	-1,253.25	1,320.37	1,171.88	148.49	8.892	
16,100.00	12,393.00	16,080.80	12,370.00	75.62	75.63	-90.39	3,661.34	-1,253.93	1,320.37	1,169.16	151.20	8.732	
16,200.00	12,393.00	16,180.80	12,370.00	76.99	77.00	-90.39	3,761.34	-1,254.61	1,320.36	1,166.42	153.94	8.577	
16,300.00	12,393.00	16,280.80	12,370.00	78.37	78.38	-90.39	3,861.33	-1,255.29	1,320.35	1,163.66	156.70	8.426	
16,400.00	12,393.00	16,380.80	12,370.00	79.75	79.77	-90.39	3,961.33	-1,255.97	1,320.35	1,160.87	159.48	8.279	
16,500.00	12,393.00	16,480.80	12,370.00	81.15	81.17	-90.39	4,061.33	-1,256.65	1,320.34	1,158.07	162.27	8.136	
16,600.00	12,393.00	16,580.80	12,370.00	82.56	82.58	-90.39	4,161.33	-1,257.33	1,320.34	1,155.24	165.09	7.997	
16,700.00	12,393.00	16,680.80	12,370.00	83.98	84.00	-90.39	4,261.32	-1,258.01	1,320.33	1,152.40	167.93	7.862	
16,800.00	12,393.00	16,780.80	12,370.00	85.41	85.43	-90.39	4,361.32	-1,258.70	1,320.32	1,149.54	170.79	7.731	
16,900.00	12,393.00	16,880.80	12,370.00	86.84	86.86	-90.39	4,461.32	-1,259.38	1,320.32	1,146.66	173.66	7.603	
17,000.00	12,393.00	16,980.80	12,370.00	88.29	88.31	-90.39	4,561.32	-1,260.06	1,320.31	1,143.77	176.54	7.479	
17,100.00	12,393.00	17,080.80	12,370.00	89.74	89.76	-90.39	4,661.32	-1,260.74	1,320.30	1,140.86	179.45	7.358	
17,138.17	12,393.00	17,118.98	12,370.00	90.29	90.31	-90.39	4,699.49	-1,261.00	1,320.30	1,139.75	180.56	7.312	
17,143.70	12,393.00	17,119.49	12,370.00	90.37	90.32	-90.61	4,700.00	-1,261.00	1,320.31	1,139.67	180.64	7.309	
17,144.46	12,393.00	17,119.49	12,370.00	90.38	90.32	-90.64	4,700.00	-1,261.00	1,320.31	1,139.67	180.65	7.309	ES, SF

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #221H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
0.00	0.00	1.00	1.00	0.00	0.00	-90.55	-13.00	-1,350.00	1,350.06				
100.00	100.00	101.00	101.00	0.13	0.13	-90.55	-13.00	-1,350.00	1,350.06	1,349.80	0.26	5,194.702	
200.00	200.00	201.00	201.00	0.49	0.49	-90.55	-13.00	-1,350.00	1,350.06	1,349.09	0.98	1,382.078	
300.00	300.00	301.00	301.00	0.85	0.85	-90.55	-13.00	-1,350.00	1,350.06	1,348.37	1.69	797.072	
400.00	400.00	401.00	401.00	1.20	1.21	-90.55	-13.00	-1,350.00	1,350.06	1,347.65	2.41	560.024	
500.00	500.00	501.00	501.00	1.56	1.57	-90.55	-13.00	-1,350.00	1,350.06	1,346.93	3.13	431.652	
600.00	600.00	601.00	601.00	1.92	1.92	-90.55	-13.00	-1,350.00	1,350.06	1,346.22	3.84	351.157	
700.00	700.00	701.00	701.00	2.28	2.28	-90.55	-13.00	-1,350.00	1,350.06	1,345.50	4.56	295.966	
800.00	800.00	801.00	801.00	2.64	2.64	-90.55	-13.00	-1,350.00	1,350.06	1,344.78	5.28	255.767	
900.00	900.00	901.00	901.00	3.00	3.00	-90.55	-13.00	-1,350.00	1,350.06	1,344.07	6.00	225.182	
1,000.00	1,000.00	1,001.00	1,001.00	3.35	3.36	-90.55	-13.00	-1,350.00	1,350.06	1,343.35	6.71	201.130	CC, ES
1,100.00	1,099.99	1,084.45	1,084.45	3.70	3.65	-90.53	-13.35	-1,350.51	1,350.95	1,343.61	7.34	184.040	
1,200.00	1,199.96	1,168.03	1,168.00	4.02	3.93	-90.47	-14.39	-1,352.03	1,353.59	1,345.64	7.95	170.293	
1,300.00	1,299.86	1,251.51	1,251.43	4.36	4.21	-90.37	-16.11	-1,354.56	1,357.98	1,349.42	8.56	158.617	
1,399.91	1,399.58	1,334.79	1,334.60	4.70	4.49	-90.22	-18.52	-1,358.07	1,364.12	1,354.94	9.18	148.598	
1,500.00	1,499.43	1,418.09	1,417.72	5.04	4.78	-90.07	-21.60	-1,362.59	1,371.74	1,361.94	9.81	139.900	
1,600.00	1,599.19	1,501.18	1,500.54	5.39	5.07	-89.95	-25.36	-1,368.09	1,380.56	1,370.13	10.43	132.314	
1,700.00	1,698.94	1,585.59	1,584.58	5.74	5.37	-89.87	-29.86	-1,374.68	1,390.57	1,379.50	11.07	125.587	
1,800.00	1,798.70	1,685.04	1,683.51	6.10	5.73	-89.83	-35.50	-1,382.93	1,401.07	1,389.30	11.78	118.977	
1,900.00	1,898.46	1,784.48	1,782.45	6.46	6.10	-89.79	-41.14	-1,391.18	1,411.57	1,399.09	12.48	113.063	
2,000.00	1,998.21	1,883.92	1,881.39	6.82	6.47	-89.75	-46.77	-1,399.43	1,422.08	1,408.88	13.20	107.750	
2,100.00	2,097.97	1,983.36	1,980.33	7.18	6.84	-89.71	-52.41	-1,407.68	1,432.58	1,418.67	13.91	102.955	
2,200.00	2,197.73	2,082.81	2,079.27	7.54	7.21	-89.68	-58.05	-1,415.93	1,443.08	1,428.45	14.63	98.608	
2,300.00	2,297.48	2,182.25	2,178.21	7.91	7.58	-89.64	-63.68	-1,424.18	1,453.59	1,438.23	15.36	94.652	
2,400.00	2,397.24	2,281.69	2,277.15	8.27	7.96	-89.61	-69.32	-1,432.43	1,464.10	1,448.01	16.08	91.039	
2,500.00	2,497.00	2,381.13	2,376.09	8.64	8.33	-89.57	-74.96	-1,440.68	1,474.60	1,457.79	16.81	87.726	
2,600.00	2,596.75	2,480.58	2,475.03	9.01	8.71	-89.54	-80.59	-1,448.93	1,485.11	1,467.57	17.54	84.679	
2,700.00	2,696.51	2,580.02	2,573.97	9.38	9.09	-89.50	-86.23	-1,457.18	1,495.61	1,477.35	18.27	81.869	
2,800.00	2,796.27	2,679.46	2,672.91	9.75	9.47	-89.47	-91.87	-1,465.43	1,506.12	1,487.12	19.00	79.269	
2,900.00	2,896.02	2,778.90	2,771.85	10.12	9.86	-89.43	-97.50	-1,473.68	1,516.63	1,496.90	19.73	76.856	
3,000.00	2,995.78	2,878.35	2,870.79	10.49	10.24	-89.40	-103.14	-1,481.93	1,527.14	1,506.67	20.47	74.613	
3,100.00	3,095.54	2,977.79	2,969.73	10.86	10.62	-89.37	-108.78	-1,490.18	1,537.65	1,516.45	21.20	72.521	
3,200.00	3,195.29	3,077.23	3,068.66	11.23	11.01	-89.34	-114.41	-1,498.43	1,548.16	1,526.22	21.94	70.567	
3,300.00	3,295.05	3,176.67	3,167.60	11.60	11.39	-89.31	-120.05	-1,506.68	1,558.67	1,535.99	22.68	68.737	
3,400.00	3,394.81	3,276.12	3,266.54	11.97	11.78	-89.28	-125.69	-1,514.93	1,569.18	1,545.76	23.41	67.021	
3,500.00	3,494.56	3,375.56	3,365.48	12.34	12.16	-89.24	-131.32	-1,523.18	1,579.69	1,555.54	24.15	65.407	
3,600.00	3,594.32	3,475.00	3,464.42	12.71	12.55	-89.21	-136.96	-1,531.43	1,590.20	1,565.31	24.89	63.887	
3,700.00	3,694.08	3,574.44	3,563.36	13.09	12.93	-89.18	-142.60	-1,539.68	1,600.71	1,575.08	25.63	62.454	
3,800.00	3,793.83	3,673.89	3,662.30	13.46	13.32	-89.15	-148.23	-1,547.93	1,611.22	1,584.85	26.37	61.100	
3,900.00	3,893.59	3,773.33	3,761.24	13.83	13.71	-89.13	-153.87	-1,556.18	1,621.74	1,594.63	27.11	59.819	
4,000.00	3,993.34	3,872.77	3,860.18	14.21	14.09	-89.10	-159.51	-1,564.43	1,632.25	1,604.40	27.85	58.605	
4,100.00	4,093.10	3,972.21	3,959.12	14.58	14.48	-89.07	-165.14	-1,572.68	1,642.76	1,614.17	28.59	57.453	
4,200.00	4,192.86	4,071.66	4,058.06	14.95	14.87	-89.04	-170.78	-1,580.93	1,653.28	1,623.94	29.34	56.358	
4,300.00	4,292.61	4,171.10	4,157.00	15.33	15.26	-89.01	-176.42	-1,589.18	1,663.79	1,633.71	30.08	55.317	
4,400.00	4,392.37	4,270.54	4,255.94	15.70	15.65	-88.99	-182.05	-1,597.43	1,674.31	1,643.49	30.82	54.326	
4,500.00	4,492.13	4,369.98	4,354.88	16.08	16.03	-88.96	-187.69	-1,605.68	1,684.82	1,653.26	31.56	53.381	
4,600.00	4,591.88	4,469.43	4,453.81	16.45	16.42	-88.93	-193.33	-1,613.93	1,695.34	1,663.03	32.31	52.478	
4,700.00	4,691.64	4,568.87	4,552.75	16.82	16.81	-88.91	-198.96	-1,622.18	1,705.85	1,672.80	33.05	51.616	
4,800.00	4,791.40	4,668.31	4,651.69	17.20	17.20	-88.88	-204.60	-1,630.43	1,716.37	1,682.58	33.79	50.791	
4,900.00	4,891.15	4,767.75	4,750.63	17.57	17.59	-88.85	-210.24	-1,638.68	1,726.88	1,692.35	34.54	50.002	
5,000.00	4,990.91	4,867.20	4,849.57	17.95	17.98	-88.83	-215.88	-1,646.93	1,737.40	1,702.12	35.28	49.245	
5,100.00	5,090.67	4,966.64	4,948.51	18.32	18.37	-88.80	-221.51	-1,655.18	1,747.92	1,711.89	36.02	48.520	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #221H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
5,200.00	5,190.42	5,066.08	5,047.45	18.70	18.76	-88.78	-227.15	-1,663.43	1,758.44	1,721.67	36.77	47.823	
5,205.01	5,195.42	5,071.06	5,052.40	18.72	18.78	-88.78	-227.43	-1,663.84	1,758.96	1,722.16	36.81	47.789	
5,300.00	5,290.23	5,165.55	5,146.42	19.07	19.15	-88.78	-232.79	-1,671.68	1,768.69	1,731.18	37.51	47.151	
5,400.00	5,390.13	5,265.07	5,245.43	19.43	19.54	-88.83	-238.43	-1,679.94	1,778.37	1,740.13	38.25	46.498	
5,500.00	5,490.09	5,364.60	5,344.46	19.79	19.93	-88.94	-244.07	-1,688.20	1,787.47	1,748.50	38.97	45.862	
5,600.00	5,590.09	5,464.11	5,443.47	20.13	20.32	-89.09	-249.71	-1,696.45	1,796.00	1,756.32	39.68	45.258	
5,604.91	5,595.00	5,469.00	5,448.33	20.15	20.34	-89.10	-249.99	-1,696.86	1,796.41	1,756.69	39.72	45.228	
5,700.00	5,690.09	5,563.61	5,542.46	20.46	20.71	-89.28	-255.35	-1,704.71	1,804.23	1,763.85	40.38	44.684	
5,800.00	5,790.09	5,663.10	5,641.45	20.78	21.10	-89.46	-260.99	-1,712.96	1,812.48	1,771.41	41.07	44.129	
5,900.00	5,890.09	5,762.60	5,740.44	21.11	21.49	-89.64	-266.63	-1,721.22	1,820.74	1,778.98	41.77	43.592	
6,000.00	5,990.09	5,862.09	5,839.43	21.43	21.88	-89.82	-272.27	-1,729.47	1,829.03	1,786.56	42.46	43.072	
6,100.00	6,090.09	5,968.83	5,945.63	21.76	22.30	-90.01	-278.28	-1,738.27	1,837.29	1,794.09	43.20	42.534	
6,200.00	6,190.09	6,104.57	6,080.90	22.09	22.82	-90.21	-284.71	-1,747.68	1,844.24	1,800.18	44.06	41.862	
6,300.00	6,290.09	6,240.79	6,216.86	22.42	23.32	-90.35	-289.34	-1,754.46	1,849.23	1,804.34	44.90	41.189	
6,400.00	6,390.09	6,377.31	6,353.29	22.75	23.81	-90.44	-292.15	-1,758.57	1,852.26	1,806.54	45.72	40.515	
6,500.00	6,490.09	6,514.00	6,489.96	23.08	24.28	-90.47	-293.13	-1,760.00	1,853.31	1,806.79	46.52	39.842	
6,600.00	6,590.09	6,615.12	6,591.09	23.41	24.60	-90.47	-293.13	-1,760.00	1,853.31	1,806.13	47.18	39.283	
6,700.00	6,690.09	6,715.12	6,691.09	23.74	24.92	-90.47	-293.13	-1,760.00	1,853.31	1,805.47	47.84	38.741	
6,800.00	6,790.09	6,815.12	6,791.09	24.08	25.24	-90.47	-293.13	-1,760.00	1,853.31	1,804.81	48.50	38.212	
6,900.00	6,890.09	6,915.12	6,891.09	24.41	25.56	-90.47	-293.13	-1,760.00	1,853.31	1,804.15	49.16	37.697	
7,000.00	6,990.09	7,015.12	6,991.09	24.75	25.88	-90.47	-293.13	-1,760.00	1,853.31	1,803.48	49.83	37.194	
7,100.00	7,090.09	7,115.12	7,091.09	25.08	26.20	-90.47	-293.13	-1,760.00	1,853.31	1,802.82	50.49	36.703	
7,200.00	7,190.09	7,215.12	7,191.09	25.42	26.53	-90.47	-293.13	-1,760.00	1,853.31	1,802.15	51.16	36.224	
7,300.00	7,290.09	7,315.12	7,291.09	25.75	26.85	-90.47	-293.13	-1,760.00	1,853.31	1,801.48	51.83	35.756	
7,400.00	7,390.09	7,415.12	7,391.09	26.09	27.18	-90.47	-293.13	-1,760.00	1,853.31	1,800.81	52.50	35.300	
7,500.00	7,490.09	7,515.12	7,491.09	26.43	27.51	-90.47	-293.13	-1,760.00	1,853.31	1,800.14	53.17	34.854	
7,600.00	7,590.09	7,615.12	7,591.09	26.77	27.83	-90.47	-293.13	-1,760.00	1,853.31	1,799.47	53.85	34.419	
7,700.00	7,690.09	7,715.12	7,691.09	27.11	28.16	-90.47	-293.13	-1,760.00	1,853.31	1,798.79	54.52	33.994	
7,800.00	7,790.09	7,815.12	7,791.09	27.45	28.49	-90.47	-293.13	-1,760.00	1,853.31	1,798.12	55.19	33.578	
7,900.00	7,890.09	7,915.12	7,891.09	27.79	28.82	-90.47	-293.13	-1,760.00	1,853.31	1,797.44	55.87	33.172	
8,000.00	7,990.09	8,015.12	7,991.09	28.13	29.15	-90.47	-293.13	-1,760.00	1,853.31	1,796.76	56.55	32.775	
8,100.00	8,090.09	8,115.12	8,091.09	28.47	29.48	-90.47	-293.13	-1,760.00	1,853.31	1,796.09	57.22	32.386	
8,200.00	8,190.09	8,215.12	8,191.09	28.81	29.81	-90.47	-293.13	-1,760.00	1,853.31	1,795.41	57.90	32.007	
8,300.00	8,290.09	8,315.12	8,291.09	29.15	30.14	-90.47	-293.13	-1,760.00	1,853.31	1,794.73	58.58	31.635	
8,400.00	8,390.09	8,415.12	8,391.09	29.49	30.48	-90.47	-293.13	-1,760.00	1,853.31	1,794.05	59.26	31.272	
8,500.00	8,490.09	8,515.12	8,491.09	29.83	30.81	-90.47	-293.13	-1,760.00	1,853.31	1,793.37	59.95	30.917	
8,600.00	8,590.09	8,615.12	8,591.09	30.18	31.14	-90.47	-293.13	-1,760.00	1,853.31	1,792.68	60.63	30.569	
8,700.00	8,690.09	8,715.12	8,691.09	30.52	31.48	-90.47	-293.13	-1,760.00	1,853.31	1,792.00	61.31	30.228	
8,800.00	8,790.09	8,815.12	8,791.09	30.86	31.81	-90.47	-293.13	-1,760.00	1,853.31	1,791.32	61.99	29.895	
8,900.00	8,890.09	8,915.12	8,891.09	31.21	32.15	-90.47	-293.13	-1,760.00	1,853.31	1,790.63	62.68	29.568	
9,000.00	8,990.09	9,015.12	8,991.09	31.55	32.48	-90.47	-293.13	-1,760.00	1,853.31	1,789.95	63.36	29.249	
9,100.00	9,090.09	9,115.12	9,091.09	31.90	32.82	-90.47	-293.13	-1,760.00	1,853.31	1,789.26	64.05	28.935	
9,200.00	9,190.09	9,215.12	9,191.09	32.24	33.16	-90.47	-293.13	-1,760.00	1,853.31	1,788.57	64.74	28.628	
9,300.00	9,290.09	9,315.12	9,291.09	32.59	33.49	-90.47	-293.13	-1,760.00	1,853.31	1,787.89	65.42	28.328	
9,400.00	9,390.09	9,415.12	9,391.09	32.93	33.83	-90.47	-293.13	-1,760.00	1,853.31	1,787.20	66.11	28.033	
9,500.00	9,490.09	9,515.12	9,491.09	33.28	34.17	-90.47	-293.13	-1,760.00	1,853.31	1,786.51	66.80	27.744	
9,600.00	9,590.09	9,615.12	9,591.09	33.62	34.51	-90.47	-293.13	-1,760.00	1,853.31	1,785.82	67.49	27.461	
9,700.00	9,690.09	9,715.12	9,691.09	33.97	34.85	-90.47	-293.13	-1,760.00	1,853.31	1,785.13	68.18	27.183	
9,800.00	9,790.09	9,815.12	9,791.09	34.31	35.19	-90.47	-293.13	-1,760.00	1,853.31	1,784.44	68.87	26.910	
9,900.00	9,890.09	9,915.12	9,891.09	34.66	35.53	-90.47	-293.13	-1,760.00	1,853.31	1,783.75	69.56	26.643	
10,000.00	9,990.09	10,015.12	9,991.09	35.01	35.87	-90.47	-293.13	-1,760.00	1,853.31	1,783.06	70.25	26.381	
10,100.00	10,090.09	10,115.12	10,091.09	35.36	36.21	-90.47	-293.13	-1,760.00	1,853.31	1,782.37	70.94	26.124	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #221H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
10,200.00	10,190.09	10,215.12	10,191.09	35.70	36.55	-90.47	-293.13	-1,760.00	1,853.31	1,781.68	71.64	25.871	
10,300.00	10,290.09	10,315.12	10,291.09	36.05	36.89	-90.47	-293.13	-1,760.00	1,853.31	1,780.98	72.33	25.624	
10,400.00	10,390.09	10,415.12	10,391.09	36.40	37.23	-90.47	-293.13	-1,760.00	1,853.31	1,780.29	73.02	25.380	
10,500.00	10,490.09	10,515.12	10,491.09	36.75	37.57	-90.47	-293.13	-1,760.00	1,853.31	1,779.60	73.72	25.141	
10,600.00	10,590.09	10,615.12	10,591.09	37.09	37.91	-90.47	-293.13	-1,760.00	1,853.31	1,778.90	74.41	24.907	
10,700.00	10,690.09	10,715.12	10,691.09	37.44	38.26	-90.47	-293.13	-1,760.00	1,853.31	1,778.21	75.10	24.677	
10,800.00	10,790.09	10,815.12	10,791.09	37.79	38.60	-90.47	-293.13	-1,760.00	1,853.31	1,777.51	75.80	24.450	
10,900.00	10,890.09	10,915.12	10,891.09	38.14	38.94	-90.47	-293.13	-1,760.00	1,853.31	1,776.82	76.49	24.228	
11,000.00	10,990.09	11,015.12	10,991.09	38.49	39.29	-90.47	-293.13	-1,760.00	1,853.31	1,776.12	77.19	24.010	
11,100.00	11,090.09	11,115.12	11,091.09	38.84	39.63	-90.47	-293.13	-1,760.00	1,853.31	1,775.42	77.89	23.795	
11,200.00	11,190.09	11,215.12	11,191.09	39.19	39.97	-90.47	-293.13	-1,760.00	1,853.31	1,774.73	78.58	23.584	
11,300.00	11,290.09	11,315.12	11,291.09	39.54	40.32	-90.47	-293.13	-1,760.00	1,853.31	1,774.03	79.28	23.377	
11,400.00	11,390.09	11,415.12	11,391.09	39.89	40.66	-90.47	-293.13	-1,760.00	1,853.31	1,773.33	79.98	23.173	
11,500.00	11,490.09	11,515.12	11,491.09	40.24	41.01	-90.47	-293.13	-1,760.00	1,853.31	1,772.64	80.67	22.973	
11,600.00	11,590.09	11,615.12	11,591.09	40.59	41.35	-90.47	-293.13	-1,760.00	1,853.31	1,771.94	81.37	22.776	
11,700.00	11,690.09	11,715.12	11,691.09	40.94	41.70	-90.47	-293.13	-1,760.00	1,853.31	1,771.24	82.07	22.582	
11,800.00	11,790.09	11,815.12	11,791.09	41.29	42.04	-90.47	-293.13	-1,760.00	1,853.31	1,770.54	82.77	22.391	
11,824.15	11,814.24	11,839.28	11,815.24	41.37	42.12	-90.47	-293.13	-1,760.00	1,853.31	1,770.37	82.94	22.346	
11,850.00	11,840.08	11,865.11	11,841.08	41.46	42.21	-90.48	-293.13	-1,760.00	1,853.31	1,770.19	83.12	22.297	
11,900.00	11,889.86	11,914.90	11,890.86	41.63	42.38	-90.62	-293.13	-1,760.00	1,853.32	1,769.87	83.46	22.206	
11,950.00	11,939.08	11,964.11	11,940.08	41.79	42.55	-90.89	-293.13	-1,760.00	1,853.38	1,769.59	83.79	22.120	
12,000.00	11,987.34	12,012.37	11,988.34	41.94	42.72	-91.29	-293.13	-1,760.00	1,853.54	1,769.43	84.11	22.038	
12,050.00	12,034.28	12,059.00	12,035.96	42.09	42.85	-91.80	-292.50	-1,760.09	1,853.99	1,769.61	84.38	21.971	
12,100.00	12,079.55	12,083.82	12,059.67	42.23	42.97	-92.38	-289.94	-1,760.47	1,855.00	1,770.37	84.63	21.919	
12,150.00	12,122.80	12,118.63	12,094.15	42.36	43.08	-93.01	-285.26	-1,761.17	1,856.60	1,771.73	84.87	21.875	
12,200.00	12,163.71	12,153.94	12,128.77	42.48	43.19	-93.68	-278.40	-1,762.19	1,858.81	1,773.70	85.10	21.842	
12,250.00	12,201.95	12,189.81	12,163.43	42.59	43.30	-94.39	-269.29	-1,763.54	1,861.63	1,776.31	85.33	21.818	
12,300.00	12,237.24	12,226.34	12,198.06	42.70	43.41	-95.12	-257.83	-1,765.24	1,865.09	1,779.54	85.54	21.803	
12,350.00	12,269.31	12,263.60	12,232.56	42.81	43.51	-95.86	-243.91	-1,767.31	1,869.17	1,783.41	85.75	21.797	
12,400.00	12,297.92	12,301.74	12,266.84	42.91	43.61	-96.59	-227.40	-1,769.76	1,873.88	1,787.91	85.96	21.799	
12,450.00	12,322.85	12,340.87	12,300.78	43.02	43.70	-97.31	-208.15	-1,772.62	1,879.20	1,793.04	86.17	21.809	
12,500.00	12,343.91	12,381.16	12,334.26	43.13	43.79	-98.00	-185.98	-1,775.92	1,885.14	1,798.77	86.37	21.827	
12,550.00	12,360.93	12,422.82	12,367.13	43.24	43.87	-98.64	-160.68	-1,779.68	1,891.66	1,805.09	86.56	21.853	
12,600.00	12,373.80	12,466.08	12,399.20	43.35	43.94	-99.20	-131.98	-1,783.94	1,898.73	1,811.97	86.76	21.886	
12,624.15	12,378.49	12,487.63	12,414.34	43.40	43.98	-99.45	-116.80	-1,786.19	1,902.34	1,815.49	86.85	21.904	
12,650.00	12,382.64	12,511.37	12,430.33	43.46	44.01	-99.68	-99.45	-1,788.77	1,906.32	1,819.37	86.95	21.926	
12,700.00	12,388.69	12,559.85	12,460.66	43.58	44.07	-100.01	-62.06	-1,794.33	1,914.29	1,827.16	87.14	21.969	
12,750.00	12,392.13	12,611.98	12,489.58	43.70	44.12	-100.19	-19.18	-1,800.70	1,922.56	1,835.23	87.33	22.015	
12,790.82	12,393.00	12,657.51	12,511.53	43.81	44.16	-100.20	20.26	-1,806.56	1,929.46	1,841.96	87.50	22.052	
12,800.00	12,393.00	12,668.15	12,516.20	43.83	44.16	-100.18	29.72	-1,807.96	1,931.01	1,843.48	87.53	22.060	
12,900.00	12,393.00	12,785.32	12,556.79	44.14	44.30	-99.85	138.31	-1,824.09	1,947.67	1,859.67	88.00	22.131	
13,000.00	12,393.00	12,904.51	12,582.95	44.51	44.63	-99.34	253.24	-1,841.17	1,963.64	1,875.03	88.61	22.161	
13,100.00	12,393.00	13,028.63	12,594.60	44.93	45.04	-98.62	375.39	-1,859.31	1,978.51	1,889.15	89.37	22.139	
13,200.00	12,393.00	13,306.04	12,595.00	45.41	46.18	-93.46	651.07	-1,889.28	1,989.14	1,898.24	90.90	21.882	
13,300.00	12,393.00	13,511.94	12,595.00	45.95	47.25	-90.39	856.86	-1,894.78	1,990.40	1,897.99	92.41	21.539	
13,400.00	12,393.00	13,611.94	12,595.00	46.54	47.83	-90.39	956.86	-1,895.47	1,990.40	1,896.83	93.57	21.272	
13,500.00	12,393.00	13,711.94	12,595.00	47.18	48.47	-90.39	1,056.86	-1,896.15	1,990.39	1,895.56	94.83	20.989	
13,600.00	12,393.00	13,811.94	12,595.00	47.87	49.15	-90.39	1,156.85	-1,896.83	1,990.39	1,894.20	96.19	20.693	
13,700.00	12,393.00	13,911.94	12,595.00	48.60	49.87	-90.39	1,256.85	-1,897.52	1,990.39	1,892.75	97.64	20.385	
13,800.00	12,393.00	14,011.94	12,595.00	49.38	50.64	-90.39	1,356.85	-1,898.20	1,990.38	1,891.21	99.18	20.069	
13,900.00	12,393.00	14,111.94	12,595.00	50.21	51.45	-90.39	1,456.85	-1,898.88	1,990.38	1,889.58	100.80	19.746	
14,000.00	12,393.00	14,211.94	12,595.00	51.07	52.30	-90.39	1,556.84	-1,899.57	1,990.38	1,887.87	102.51	19.417	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #221H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
14,100.00	12,393.00	14,311.94	12,595.00	51.97	53.18	-90.39	1,656.84	-1,900.25	1,990.37	1,886.08	104.29	19.085	
14,200.00	12,393.00	14,411.94	12,595.00	52.91	54.11	-90.39	1,756.84	-1,900.93	1,990.37	1,884.22	106.15	18.751	
14,300.00	12,393.00	14,511.94	12,595.00	53.89	55.06	-90.39	1,856.84	-1,901.62	1,990.37	1,882.30	108.07	18.417	
14,400.00	12,393.00	14,611.94	12,595.00	54.89	56.05	-90.39	1,956.83	-1,902.30	1,990.36	1,880.30	110.06	18.084	
14,500.00	12,393.00	14,711.94	12,595.00	55.93	57.07	-90.39	2,056.83	-1,902.98	1,990.36	1,878.25	112.11	17.753	
14,600.00	12,393.00	14,811.94	12,595.00	57.00	58.12	-90.39	2,156.83	-1,903.66	1,990.36	1,876.13	114.22	17.425	
14,700.00	12,393.00	14,911.94	12,595.00	58.10	59.20	-90.39	2,256.83	-1,904.35	1,990.35	1,873.96	116.39	17.101	
14,800.00	12,393.00	15,011.94	12,595.00	59.22	60.30	-90.39	2,356.82	-1,905.03	1,990.35	1,871.74	118.61	16.780	
14,900.00	12,393.00	15,111.94	12,595.00	60.36	61.43	-90.39	2,456.82	-1,905.71	1,990.34	1,869.46	120.88	16.465	
15,000.00	12,393.00	15,211.94	12,595.00	61.53	62.58	-90.39	2,556.82	-1,906.40	1,990.34	1,867.14	123.20	16.156	
15,100.00	12,393.00	15,311.94	12,595.00	62.73	63.76	-90.39	2,656.82	-1,907.08	1,990.34	1,864.78	125.56	15.852	
15,200.00	12,393.00	15,411.94	12,595.00	63.94	64.95	-90.39	2,756.82	-1,907.76	1,990.33	1,862.38	127.96	15.554	
15,300.00	12,393.00	15,511.94	12,595.00	65.17	66.17	-90.39	2,856.81	-1,908.45	1,990.33	1,859.93	130.40	15.263	
15,400.00	12,393.00	15,611.94	12,595.00	66.42	67.40	-90.39	2,956.81	-1,909.13	1,990.33	1,857.45	132.88	14.978	
15,500.00	12,393.00	15,711.94	12,595.00	67.69	68.66	-90.39	3,056.81	-1,909.81	1,990.32	1,854.93	135.40	14.700	
15,600.00	12,393.00	15,811.94	12,595.00	68.97	69.92	-90.39	3,156.81	-1,910.50	1,990.32	1,852.38	137.94	14.429	
15,700.00	12,393.00	15,911.94	12,595.00	70.28	71.21	-90.39	3,256.80	-1,911.18	1,990.32	1,849.79	140.52	14.164	
15,800.00	12,393.00	16,011.94	12,595.00	71.59	72.51	-90.39	3,356.80	-1,911.86	1,990.31	1,847.18	143.13	13.905	
15,900.00	12,393.00	16,111.94	12,595.00	72.92	73.82	-90.39	3,456.80	-1,912.55	1,990.31	1,844.54	145.77	13.654	
16,000.00	12,393.00	16,211.94	12,595.00	74.26	75.15	-90.39	3,556.80	-1,913.23	1,990.31	1,841.87	148.43	13.409	
16,100.00	12,393.00	16,311.94	12,595.00	75.62	76.49	-90.39	3,656.79	-1,913.91	1,990.30	1,839.18	151.12	13.170	
16,200.00	12,393.00	16,411.94	12,595.00	76.99	77.85	-90.39	3,756.79	-1,914.60	1,990.30	1,836.46	153.84	12.938	
16,300.00	12,393.00	16,511.94	12,595.00	78.37	79.21	-90.39	3,856.79	-1,915.28	1,990.30	1,833.72	156.58	12.711	
16,400.00	12,393.00	16,611.94	12,595.00	79.75	80.59	-90.39	3,956.79	-1,915.96	1,990.29	1,830.96	159.33	12.491	
16,500.00	12,393.00	16,711.94	12,595.00	81.15	81.98	-90.39	4,056.79	-1,916.65	1,990.29	1,828.18	162.11	12.277	
16,600.00	12,393.00	16,811.94	12,595.00	82.56	83.37	-90.39	4,156.78	-1,917.33	1,990.29	1,825.38	164.91	12.069	
16,700.00	12,393.00	16,911.94	12,595.00	83.98	84.78	-90.39	4,256.78	-1,918.01	1,990.28	1,822.55	167.73	11.866	
16,800.00	12,393.00	17,011.94	12,595.00	85.41	86.19	-90.39	4,356.78	-1,918.70	1,990.28	1,819.72	170.56	11.669	
16,900.00	12,393.00	17,111.94	12,595.00	86.84	87.62	-90.39	4,456.78	-1,919.38	1,990.27	1,816.86	173.41	11.477	
17,000.00	12,393.00	17,211.94	12,595.00	88.29	89.05	-90.39	4,556.77	-1,920.06	1,990.27	1,813.99	176.28	11.290	
17,100.00	12,393.00	17,311.94	12,595.00	89.74	90.47	-90.39	4,656.77	-1,920.75	1,990.27	1,811.13	179.14	11.110	
17,141.78	12,393.00	17,353.71	12,595.00	90.35	91.04	-90.39	4,698.55	-1,921.03	1,990.27	1,809.99	180.27	11.040	SF
17,143.70	12,393.00	17,349.17	12,595.00	90.37	90.97	-90.58	4,694.00	-1,921.00	1,990.28	1,810.02	180.26	11.041	
17,144.46	12,393.00	17,349.17	12,595.00	90.38	90.97	-90.60	4,694.00	-1,921.00	1,990.28	1,810.01	180.27	11.040	

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #226H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
0.00	0.00	0.00	0.00	0.00	0.00	-90.00	0.00	-30.00	30.00				
100.00	100.00	100.00	100.00	0.13	0.13	-90.00	0.00	-30.00	30.00	29.74	0.26	117.047	
200.00	200.00	200.00	200.00	0.49	0.49	-90.00	0.00	-30.00	30.00	29.03	0.97	30.825	
300.00	300.00	300.00	300.00	0.85	0.85	-90.00	0.00	-30.00	30.00	28.31	1.69	17.749	
400.00	400.00	400.00	400.00	1.20	1.20	-90.00	0.00	-30.00	30.00	27.59	2.41	12.463	
500.00	500.00	500.00	500.00	1.56	1.56	-90.00	0.00	-30.00	30.00	26.88	3.12	9.603	
600.00	600.00	600.00	600.00	1.92	1.92	-90.00	0.00	-30.00	30.00	26.16	3.84	7.810	CC
700.00	700.00	699.98	699.98	2.28	2.26	-91.66	-0.87	-30.02	30.03	25.49	4.54	6.613	
800.00	800.00	799.90	799.86	2.64	2.59	-96.61	-3.49	-30.06	30.26	25.03	5.23	5.787	ES
900.00	900.00	899.70	899.56	3.00	2.93	-104.57	-7.84	-30.14	31.15	25.22	5.93	5.256	
1,000.00	1,000.00	999.73	998.99	3.35	3.28	-114.69	-13.91	-30.25	33.31	26.68	6.63	5.025	
1,100.00	1,099.99	1,100.88	1,098.56	3.70	3.63	-123.17	-20.86	-30.37	36.64	29.32	7.32	5.004	
1,200.00	1,199.96	1,200.98	1,198.21	4.02	3.99	-127.79	-27.82	-30.50	40.04	32.03	8.00	5.002	
1,300.00	1,299.86	1,301.04	1,297.91	4.36	4.35	-129.54	-34.78	-30.62	42.99	34.30	8.69	4.945	
1,399.91	1,399.58	1,401.16	1,397.55	4.70	4.72	-129.02	-41.74	-30.75	45.33	35.94	9.39	4.827	
1,500.00	1,499.43	1,501.09	1,497.37	5.04	5.08	-127.57	-48.71	-30.87	47.39	37.29	10.10	4.693	
1,600.00	1,599.19	1,601.12	1,597.10	5.39	5.45	-126.23	-55.67	-31.00	49.47	38.66	10.81	4.576	
1,700.00	1,698.94	1,698.85	1,696.83	5.74	5.81	-125.01	-62.64	-31.12	51.58	40.06	11.52	4.478	
1,800.00	1,798.70	1,801.18	1,796.56	6.10	6.19	-123.88	-69.60	-31.25	53.71	41.46	12.25	4.384	
1,900.00	1,898.46	1,901.21	1,896.29	6.46	6.56	-122.84	-76.57	-31.37	55.86	42.88	12.98	4.305	
2,000.00	1,998.21	2,001.23	1,996.01	6.82	6.93	-121.88	-83.53	-31.50	58.03	44.32	13.70	4.234	
2,100.00	2,097.97	2,101.26	2,095.74	7.18	7.30	-120.99	-90.50	-31.62	60.21	45.77	14.44	4.171	
2,200.00	2,197.73	2,201.29	2,195.47	7.54	7.67	-120.16	-97.46	-31.74	62.40	47.24	15.17	4.114	
2,300.00	2,297.48	2,301.32	2,295.20	7.91	8.04	-119.38	-104.42	-31.87	64.61	48.71	15.90	4.062	
2,400.00	2,397.24	2,401.35	2,394.93	8.27	8.42	-118.66	-111.39	-31.99	66.83	50.19	16.64	4.016	
2,500.00	2,497.00	2,501.37	2,494.66	8.64	8.79	-117.99	-118.35	-32.12	69.06	51.68	17.38	3.973	
2,600.00	2,596.75	2,601.40	2,594.39	9.01	9.16	-117.35	-125.32	-32.24	71.30	53.18	18.12	3.935	
2,700.00	2,696.51	2,701.43	2,694.12	9.38	9.54	-116.76	-132.28	-32.37	73.54	54.68	18.86	3.899	
2,800.00	2,796.27	2,801.46	2,793.85	9.75	9.91	-116.20	-139.25	-32.49	75.80	56.19	19.60	3.867	
2,900.00	2,896.02	2,901.49	2,893.58	10.12	10.29	-115.67	-146.21	-32.62	78.06	57.71	20.35	3.836	
3,000.00	2,995.78	3,001.51	2,993.30	10.49	10.66	-115.17	-153.17	-32.74	80.32	59.23	21.09	3.809	
3,100.00	3,095.54	3,101.54	3,093.03	10.86	11.04	-114.70	-160.14	-32.87	82.59	60.76	21.83	3.783	
3,200.00	3,195.29	3,201.57	3,192.76	11.23	11.41	-114.26	-167.10	-32.99	84.87	62.29	22.58	3.759	
3,300.00	3,295.05	3,301.60	3,292.49	11.60	11.79	-113.84	-174.07	-33.12	87.15	63.83	23.32	3.737	
3,400.00	3,394.81	3,401.63	3,392.22	11.97	12.16	-113.43	-181.03	-33.24	89.44	65.37	24.07	3.716	
3,500.00	3,494.56	3,501.65	3,491.95	12.34	12.54	-113.05	-188.00	-33.36	91.73	66.91	24.82	3.696	
3,600.00	3,594.32	3,601.68	3,591.68	12.71	12.91	-112.69	-194.96	-33.49	94.03	68.46	25.56	3.678	
3,700.00	3,694.08	3,701.71	3,691.41	13.09	13.29	-112.35	-201.92	-33.61	96.32	70.01	26.31	3.661	
3,800.00	3,793.83	3,801.74	3,791.14	13.46	13.66	-112.02	-208.89	-33.74	98.63	71.57	27.06	3.645	
3,900.00	3,893.59	3,901.77	3,890.87	13.83	14.04	-111.71	-215.85	-33.86	100.93	73.12	27.81	3.630	
4,000.00	3,993.34	4,001.80	3,990.59	14.21	14.42	-111.41	-222.82	-33.99	103.24	74.68	28.56	3.615	
4,100.00	4,093.10	4,101.82	4,090.32	14.58	14.79	-111.12	-229.78	-34.11	105.55	76.24	29.31	3.602	
4,200.00	4,192.86	4,201.85	4,190.05	14.95	15.17	-110.85	-236.75	-34.24	107.86	77.81	30.05	3.589	
4,300.00	4,292.61	4,301.88	4,289.78	15.33	15.54	-110.59	-243.71	-34.36	110.18	79.37	30.80	3.577	
4,400.00	4,392.37	4,401.91	4,389.51	15.70	15.92	-110.33	-250.67	-34.49	112.49	80.94	31.55	3.565	
4,500.00	4,492.13	4,501.94	4,489.24	16.08	16.30	-110.09	-257.64	-34.61	114.81	82.51	32.30	3.554	
4,600.00	4,591.88	4,598.04	4,588.97	16.45	16.66	-109.86	-264.60	-34.74	117.14	84.10	33.04	3.545	
4,700.00	4,691.64	4,698.66	4,689.39	16.82	17.03	-109.35	-270.93	-34.85	119.22	85.43	33.79	3.528	
4,800.00	4,791.40	4,799.32	4,789.95	17.20	17.40	-108.07	-275.50	-34.93	120.73	86.19	34.54	3.495	
4,900.00	4,891.15	4,899.88	4,890.47	17.57	17.76	-106.04	-278.30	-34.98	121.77	86.49	35.29	3.451	
5,000.00	4,990.91	5,000.28	4,990.86	17.95	18.10	-103.25	-279.34	-35.00	122.53	86.52	36.01	3.403	
5,100.00	5,090.67	5,100.09	5,090.67	18.32	18.42	-100.02	-279.35	-35.00	123.37	86.66	36.71	3.360	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #226H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
5,200.00	5,190.42	5,200.16	5,190.42	18.70	18.74	-96.85	-279.35	-35.00	124.59	87.19	37.41	3.331	
5,205.01	5,195.42	5,204.84	5,195.42	18.72	18.75	-96.69	-279.35	-35.00	124.66	87.22	37.44	3.330	
5,300.00	5,290.23	5,300.35	5,290.23	19.07	19.06	-94.09	-279.35	-35.00	125.99	87.90	38.10	3.307	
5,400.00	5,390.13	5,400.45	5,390.13	19.43	19.38	-92.15	-279.35	-35.00	127.17	88.40	38.78	3.280	
5,500.00	5,490.09	5,500.49	5,490.09	19.79	19.70	-90.99	-279.35	-35.00	127.96	88.51	39.45	3.243	
5,600.00	5,590.09	5,600.49	5,590.09	20.13	20.03	-90.58	-279.35	-35.00	128.26	88.14	40.11	3.197	
5,604.91	5,595.00	5,604.42	5,595.00	20.15	20.04	-90.58	-279.35	-35.00	128.26	88.11	40.14	3.195	
5,700.00	5,690.09	5,700.49	5,690.09	20.46	20.35	-90.58	-279.35	-35.00	128.26	87.49	40.76	3.146	
5,800.00	5,790.09	5,800.49	5,790.09	20.78	20.68	-90.58	-279.35	-35.00	128.26	86.84	41.41	3.097	
5,900.00	5,890.09	5,900.49	5,890.09	21.11	21.00	-90.58	-279.35	-35.00	128.26	86.19	42.07	3.049	
6,000.00	5,990.09	6,000.49	5,990.09	21.43	21.33	-90.58	-279.35	-35.00	128.26	85.53	42.72	3.002	
6,100.00	6,090.09	6,100.49	6,090.09	21.76	21.66	-90.58	-279.35	-35.00	128.26	84.88	43.38	2.957	
6,200.00	6,190.09	6,200.49	6,190.09	22.09	21.99	-90.58	-279.35	-35.00	128.26	84.22	44.04	2.912	
6,300.00	6,290.09	6,300.49	6,290.09	22.42	22.32	-90.58	-279.35	-35.00	128.26	83.56	44.70	2.869	
6,400.00	6,390.09	6,400.49	6,390.09	22.75	22.65	-90.58	-279.35	-35.00	128.26	82.90	45.36	2.827	
6,500.00	6,490.09	6,500.49	6,490.09	23.08	22.99	-90.58	-279.35	-35.00	128.26	82.23	46.03	2.787	
6,600.00	6,590.09	6,600.49	6,590.09	23.41	23.32	-90.58	-279.35	-35.00	128.26	81.57	46.69	2.747	
6,700.00	6,690.09	6,700.49	6,690.09	23.74	23.65	-90.58	-279.35	-35.00	128.26	80.90	47.36	2.708	
6,800.00	6,790.09	6,800.49	6,790.09	24.08	23.99	-90.58	-279.35	-35.00	128.26	80.23	48.03	2.671	
6,900.00	6,890.09	6,900.49	6,890.09	24.41	24.32	-90.58	-279.35	-35.00	128.26	79.56	48.70	2.634	
7,000.00	6,990.09	7,000.49	6,990.09	24.75	24.66	-90.58	-279.35	-35.00	128.26	78.89	49.37	2.598	
7,100.00	7,090.09	7,100.49	7,090.09	25.08	25.00	-90.58	-279.35	-35.00	128.26	78.22	50.04	2.563	
7,200.00	7,190.09	7,200.49	7,190.09	25.42	25.33	-90.58	-279.35	-35.00	128.26	77.54	50.71	2.529	
7,300.00	7,290.09	7,300.49	7,290.09	25.75	25.67	-90.58	-279.35	-35.00	128.26	76.87	51.39	2.496	
7,400.00	7,390.09	7,400.49	7,390.09	26.09	26.01	-90.58	-279.35	-35.00	128.26	76.19	52.06	2.463	
7,500.00	7,490.09	7,500.49	7,490.09	26.43	26.35	-90.58	-279.35	-35.00	128.26	75.51	52.74	2.432	
7,600.00	7,590.09	7,600.49	7,590.09	26.77	26.69	-90.58	-279.35	-35.00	128.26	74.84	53.42	2.401	
7,700.00	7,690.09	7,700.49	7,690.09	27.11	27.03	-90.58	-279.35	-35.00	128.26	74.16	54.10	2.371	
7,800.00	7,790.09	7,800.49	7,790.09	27.45	27.37	-90.58	-279.35	-35.00	128.26	73.48	54.78	2.341	
7,900.00	7,890.09	7,900.49	7,890.09	27.79	27.71	-90.58	-279.35	-35.00	128.26	72.80	55.46	2.313	
8,000.00	7,990.09	8,000.49	7,990.09	28.13	28.05	-90.58	-279.35	-35.00	128.26	72.11	56.14	2.284	
8,100.00	8,090.09	8,100.49	8,090.09	28.47	28.39	-90.58	-279.35	-35.00	128.26	71.43	56.83	2.257	
8,200.00	8,190.09	8,200.49	8,190.09	28.81	28.74	-90.58	-279.35	-35.00	128.26	70.75	57.51	2.230	
8,300.00	8,290.09	8,300.49	8,290.09	29.15	29.08	-90.58	-279.35	-35.00	128.26	70.06	58.19	2.204	
8,400.00	8,390.09	8,400.49	8,390.09	29.49	29.42	-90.58	-279.35	-35.00	128.26	69.38	58.88	2.178	
8,500.00	8,490.09	8,500.49	8,490.09	29.83	29.77	-90.58	-279.35	-35.00	128.26	68.69	59.56	2.153	
8,600.00	8,590.09	8,600.49	8,590.09	30.18	30.11	-90.58	-279.35	-35.00	128.26	68.01	60.25	2.129	
8,700.00	8,690.09	8,700.49	8,690.09	30.52	30.45	-90.58	-279.35	-35.00	128.26	67.32	60.94	2.105	
8,800.00	8,790.09	8,800.49	8,790.09	30.86	30.80	-90.58	-279.35	-35.00	128.26	66.63	61.63	2.081	
8,900.00	8,890.09	8,900.49	8,890.09	31.21	31.14	-90.58	-279.35	-35.00	128.26	65.94	62.32	2.058	
9,000.00	8,990.09	9,000.49	8,990.09	31.55	31.49	-90.58	-279.35	-35.00	128.26	65.25	63.00	2.036	
9,100.00	9,090.09	9,100.49	9,090.09	31.90	31.83	-90.58	-279.35	-35.00	128.26	64.56	63.69	2.014	
9,200.00	9,190.09	9,200.49	9,190.09	32.24	32.18	-90.58	-279.35	-35.00	128.26	63.87	64.38	1.992	
9,300.00	9,290.09	9,300.49	9,290.09	32.59	32.52	-90.58	-279.35	-35.00	128.26	63.18	65.08	1.971	
9,400.00	9,390.09	9,400.49	9,390.09	32.93	32.87	-90.58	-279.35	-35.00	128.26	62.49	65.77	1.950	
9,500.00	9,490.09	9,500.49	9,490.09	33.28	33.22	-90.58	-279.35	-35.00	128.26	61.80	66.46	1.930	
9,600.00	9,590.09	9,600.49	9,590.09	33.62	33.56	-90.58	-279.35	-35.00	128.26	61.10	67.15	1.910	
9,700.00	9,690.09	9,700.49	9,690.09	33.97	33.91	-90.58	-279.35	-35.00	128.26	60.41	67.85	1.890	
9,800.00	9,790.09	9,800.49	9,790.09	34.31	34.26	-90.58	-279.35	-35.00	128.26	59.72	68.54	1.871	
9,900.00	9,890.09	9,900.49	9,890.09	34.66	34.60	-90.58	-279.35	-35.00	128.26	59.02	69.23	1.853	
10,000.00	9,990.09	10,000.49	9,990.09	35.01	34.95	-90.58	-279.35	-35.00	128.26	58.33	69.93	1.834	
10,100.00	10,090.09	10,100.49	10,090.09	35.36	35.30	-90.58	-279.35	-35.00	128.26	57.63	70.62	1.816	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #226H - Wellbore #1 - Design #2 — **Offset Site Error:** 0.00 usft

Survey Program: 0-MWD — **Offset Well Error:** 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
10,200.00	10,190.09	10,200.49	10,190.09	35.70	35.65	-90.58	-279.35	-35.00	128.26	56.94	71.32	1.798	
10,300.00	10,290.09	10,300.49	10,290.09	36.05	36.00	-90.58	-279.35	-35.00	128.26	56.24	72.01	1.781	
10,400.00	10,390.09	10,400.49	10,390.09	36.40	36.34	-90.58	-279.35	-35.00	128.26	55.55	72.71	1.764	
10,500.00	10,490.09	10,500.49	10,490.09	36.75	36.69	-90.58	-279.35	-35.00	128.26	54.85	73.41	1.747	
10,600.00	10,590.09	10,600.49	10,590.09	37.09	37.04	-90.58	-279.35	-35.00	128.26	54.15	74.10	1.731	
10,700.00	10,690.09	10,700.49	10,690.09	37.44	37.39	-90.58	-279.35	-35.00	128.26	53.45	74.80	1.715	
10,800.00	10,790.09	10,800.49	10,790.09	37.79	37.74	-90.58	-279.35	-35.00	128.26	52.76	75.50	1.699	
10,900.00	10,890.09	10,900.49	10,890.09	38.14	38.09	-90.58	-279.35	-35.00	128.26	52.06	76.20	1.683	
11,000.00	10,990.09	11,000.49	10,990.09	38.49	38.44	-90.58	-279.35	-35.00	128.26	51.36	76.90	1.668	
11,100.00	11,090.09	11,100.49	11,090.09	38.84	38.79	-90.58	-279.35	-35.00	128.26	50.66	77.60	1.653	
11,200.00	11,190.09	11,200.49	11,190.09	39.19	39.14	-90.58	-279.35	-35.00	128.26	49.96	78.30	1.638	
11,300.00	11,290.09	11,300.49	11,290.09	39.54	39.49	-90.58	-279.35	-35.00	128.26	49.26	78.99	1.624	
11,400.00	11,390.09	11,400.49	11,390.09	39.89	39.84	-90.58	-279.35	-35.00	128.26	48.56	79.69	1.609	
11,500.00	11,490.09	11,500.49	11,490.09	40.24	40.19	-90.58	-279.35	-35.00	128.26	47.86	80.39	1.595	
11,600.00	11,590.09	11,600.49	11,590.09	40.59	40.54	-90.58	-279.35	-35.00	128.26	47.16	81.10	1.582	
11,700.00	11,690.09	11,700.49	11,690.09	40.94	40.89	-90.58	-279.35	-35.00	128.26	46.46	81.80	1.568	
11,800.00	11,790.09	11,800.49	11,790.09	41.29	41.24	-90.58	-279.35	-35.00	128.26	45.76	82.50	1.555	
11,824.15	11,814.24	11,823.66	11,814.24	41.37	41.32	-90.58	-279.35	-35.00	128.26	45.59	82.66	1.552	
11,850.00	11,840.08	11,849.50	11,840.08	41.46	41.41	-90.84	-279.35	-35.00	128.26	45.42	82.84	1.548	
11,900.00	11,889.86	11,900.71	11,889.86	41.63	41.59	-92.82	-279.35	-35.00	128.37	45.17	83.20	1.543	SF
11,950.00	11,939.08	11,948.50	11,939.08	41.79	41.76	-96.70	-279.35	-35.00	129.04	45.51	83.53	1.545	
12,000.00	11,987.34	11,996.76	11,987.34	41.94	41.93	-102.36	-279.35	-35.00	131.11	47.25	83.86	1.563	
12,050.00	12,034.28	12,048.50	12,039.03	42.09	42.11	-108.80	-277.59	-34.76	135.00	50.86	84.13	1.605	
12,100.00	12,079.55	12,102.47	12,092.55	42.23	42.29	-114.59	-270.89	-33.85	139.90	55.68	84.22	1.661	
12,150.00	12,122.80	12,158.20	12,146.90	42.36	42.46	-119.59	-258.76	-32.21	145.58	61.60	83.97	1.734	
12,200.00	12,163.71	12,215.78	12,201.53	42.48	42.63	-123.75	-240.80	-29.77	151.78	68.50	83.28	1.823	
12,250.00	12,201.95	12,275.29	12,255.78	42.59	42.80	-127.07	-216.63	-26.50	158.22	76.18	82.04	1.929	
12,300.00	12,237.24	12,336.77	12,308.86	42.70	42.96	-129.54	-185.94	-22.34	164.64	84.42	80.22	2.052	
12,350.00	12,269.31	12,400.22	12,359.83	42.81	43.12	-131.18	-148.56	-17.27	170.77	92.95	77.82	2.194	
12,400.00	12,297.92	12,465.59	12,407.66	42.91	43.27	-131.91	-104.45	-11.29	176.35	101.44	74.91	2.354	
12,450.00	12,322.85	12,532.78	12,451.20	43.02	43.42	-131.61	-53.79	-4.42	181.14	109.53	71.61	2.530	
12,500.00	12,343.91	12,601.60	12,489.29	43.13	43.57	-129.99	2.96	3.27	184.93	116.81	68.12	2.715	
12,550.00	12,360.93	12,671.80	12,520.78	43.24	43.72	-126.50	65.09	11.69	187.53	122.83	64.70	2.898	
12,600.00	12,373.80	12,737.02	12,543.34	43.35	43.86	-123.21	125.70	19.91	189.22	126.99	62.22	3.041	
12,624.15	12,378.49	12,766.33	12,551.96	43.40	43.92	-122.30	153.45	23.67	190.41	129.09	61.32	3.105	
12,650.00	12,382.64	12,797.78	12,560.25	43.46	44.00	-121.06	183.51	27.75	191.84	131.43	60.41	3.176	
12,700.00	12,388.69	12,858.96	12,573.50	43.58	44.15	-117.39	242.69	35.77	194.47	135.60	58.88	3.303	
12,750.00	12,392.13	12,920.55	12,582.94	43.70	44.31	-111.06	303.00	43.94	196.87	139.18	57.69	3.413	
12,790.82	12,393.00	12,971.11	12,587.75	43.81	44.45	-102.34	352.87	50.70	198.63	141.61	57.02	3.483	
12,800.00	12,393.00	12,982.52	12,588.46	43.83	44.48	-99.70	364.14	52.23	198.96	142.04	56.91	3.496	
12,900.00	12,393.00	13,092.24	12,590.00	44.14	44.81	-83.39	472.91	66.44	198.21	141.87	56.34	3.518	
13,000.00	12,393.00	13,191.12	12,590.00	44.51	45.16	-85.37	571.31	76.12	197.33	141.11	56.22	3.510	
13,100.00	12,393.00	13,290.61	12,590.00	44.93	45.57	-87.36	670.59	82.43	197.05	140.63	56.42	3.493	
13,200.00	12,393.00	13,390.46	12,590.00	45.41	46.04	-89.34	770.40	85.30	197.00	140.23	56.78	3.470	
13,300.00	12,393.00	13,509.55	12,590.00	45.95	46.66	-90.36	870.39	85.09	197.00	139.75	57.25	3.441	
13,304.02	12,393.00	13,505.54	12,590.00	45.97	46.64	-90.36	874.40	85.06	197.00	139.75	57.25	3.441	
13,400.00	12,393.00	13,609.55	12,590.00	46.54	47.24	-90.36	970.38	84.41	197.00	139.28	57.72	3.413	
13,500.00	12,393.00	13,709.55	12,590.00	47.18	47.87	-90.36	1,070.38	83.73	197.00	138.77	58.24	3.383	
13,600.00	12,393.00	13,809.55	12,590.00	47.87	48.55	-90.35	1,170.38	83.05	197.00	138.22	58.79	3.351	
13,700.00	12,393.00	13,909.55	12,590.00	48.60	49.27	-90.35	1,270.38	82.37	197.00	137.63	59.37	3.318	
13,800.00	12,393.00	14,009.55	12,590.00	49.38	50.04	-90.35	1,370.38	81.69	197.00	137.01	60.00	3.284	
13,900.00	12,393.00	14,109.55	12,590.00	50.21	50.86	-90.35	1,470.37	81.02	197.00	136.35	60.65	3.248	

CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Offset Design Brad Dyer 35-22S-32E AR - #226H - Wellbore #1 - Design #2

Offset Site Error: 0.00 usft

Survey Program: 0-MWD

Offset Well Error: 0.00 usft

Reference Measured Depth (usft)	Reference Vertical Depth (usft)	Offset Measured Depth (usft)	Offset Vertical Depth (usft)	Semi Major Axis Reference (usft)	Semi Major Axis Offset (usft)	Azimuth from North (°)	Offset Wellbore Centre +N/-S (usft)	Offset Wellbore Centre +E/-W (usft)	Distance Between Centres (usft)	Distance Between Ellipses (usft)	Minimum Separation (usft)	Separation Factor	Warning
14,000.00	12,393.00	14,209.55	12,590.00	51.07	51.71	-90.35	1,570.37	80.34	197.00	135.66	61.34	3.212	
14,100.00	12,393.00	14,309.55	12,590.00	51.97	52.60	-90.35	1,670.37	79.66	197.00	134.94	62.06	3.174	
14,200.00	12,393.00	14,409.55	12,590.00	52.91	53.53	-90.35	1,770.37	78.98	197.00	134.19	62.82	3.136	
14,300.00	12,393.00	14,509.55	12,590.00	53.89	54.49	-90.35	1,870.36	78.30	197.00	133.40	63.60	3.098	
14,400.00	12,393.00	14,609.55	12,590.00	54.89	55.49	-90.34	1,970.36	77.62	197.00	132.59	64.41	3.059	
14,500.00	12,393.00	14,709.55	12,590.00	55.93	56.51	-90.34	2,070.36	76.94	197.00	131.75	65.25	3.019	
14,600.00	12,393.00	14,809.55	12,590.00	57.00	57.57	-90.34	2,170.36	76.26	197.00	130.89	66.11	2.980	
14,700.00	12,393.00	14,909.55	12,590.00	58.10	58.65	-90.34	2,270.35	75.59	197.00	130.00	67.01	2.940	
14,800.00	12,393.00	15,009.55	12,590.00	59.22	59.77	-90.34	2,370.35	74.91	197.00	129.08	67.92	2.900	
14,900.00	12,393.00	15,109.55	12,590.00	60.36	60.90	-90.34	2,470.35	74.23	197.00	128.14	68.86	2.861	
15,000.00	12,393.00	15,209.55	12,590.00	61.53	62.06	-90.33	2,570.35	73.55	197.00	127.18	69.82	2.821	
15,100.00	12,393.00	15,309.55	12,590.00	62.73	63.24	-90.33	2,670.35	72.87	197.00	126.20	70.81	2.782	
15,200.00	12,393.00	15,409.55	12,590.00	63.94	64.45	-90.33	2,770.34	72.19	197.00	125.19	71.81	2.743	
15,300.00	12,393.00	15,509.55	12,590.00	65.17	65.67	-90.32	2,870.34	71.51	197.00	124.17	72.84	2.705	
15,400.00	12,393.00	15,609.55	12,590.00	66.42	66.91	-90.32	2,970.34	70.83	197.00	123.12	73.88	2.667	
15,500.00	12,393.00	15,709.55	12,590.00	67.69	68.17	-90.32	3,070.34	70.16	197.00	122.06	74.94	2.629	
15,600.00	12,393.00	15,809.55	12,590.00	68.97	69.45	-90.31	3,170.33	69.48	197.00	120.98	76.02	2.591	
15,700.00	12,393.00	15,909.55	12,590.00	70.28	70.74	-90.31	3,270.33	68.80	197.00	119.88	77.12	2.555	
15,800.00	12,393.00	16,009.55	12,590.00	71.59	72.04	-90.30	3,370.33	68.12	197.00	118.77	78.23	2.518	
15,900.00	12,393.00	16,109.55	12,590.00	72.92	73.37	-90.29	3,470.33	67.44	197.00	117.64	79.36	2.482	
16,000.00	12,393.00	16,209.55	12,590.00	74.26	74.70	-90.28	3,570.32	66.76	197.00	116.50	80.50	2.447	
16,100.00	12,393.00	16,309.55	12,590.00	75.62	76.05	-90.27	3,670.32	66.08	197.00	115.34	81.66	2.413	
16,200.00	12,393.00	16,390.45	12,590.00	76.99	77.15	-90.26	3,770.32	65.41	197.00	114.29	82.72	2.382	
16,300.00	12,393.00	16,509.55	12,590.00	78.37	78.78	-90.25	3,870.32	64.73	197.00	112.99	84.01	2.345	
16,400.00	12,393.00	16,609.55	12,590.00	79.75	80.16	-90.23	3,970.32	64.05	197.00	111.79	85.21	2.312	
16,500.00	12,393.00	16,709.55	12,590.00	81.15	81.55	-90.20	4,070.31	63.37	197.00	110.59	86.41	2.280	
16,600.00	12,393.00	16,809.55	12,590.00	82.56	82.96	-90.17	4,170.31	62.69	197.00	109.37	87.63	2.248	
16,700.00	12,393.00	16,909.55	12,590.00	83.98	84.37	-90.12	4,270.31	62.01	197.00	108.14	88.86	2.217	
16,800.00	12,393.00	17,009.55	12,590.00	85.41	85.79	-90.04	4,370.31	61.33	197.00	106.90	90.10	2.186	
16,900.00	12,393.00	17,109.55	12,590.00	86.84	87.22	-89.89	4,470.30	60.65	197.00	105.64	91.36	2.156	
17,000.00	12,393.00	17,209.55	12,590.00	88.29	88.65	-89.55	4,570.30	59.98	197.00	104.38	92.62	2.127	
17,100.00	12,393.00	17,290.45	12,590.00	89.74	89.82	-87.63	4,670.30	59.30	197.00	103.23	93.77	2.101	
17,143.70	12,393.00	17,334.15	12,590.00	90.37	90.40	0.00	4,714.00	59.00	197.00	102.79	94.21	2.091	
17,144.46	12,393.00	17,334.91	12,590.00	90.38	90.41	0.00	4,714.76	58.99	197.00	102.78	94.22	2.091	

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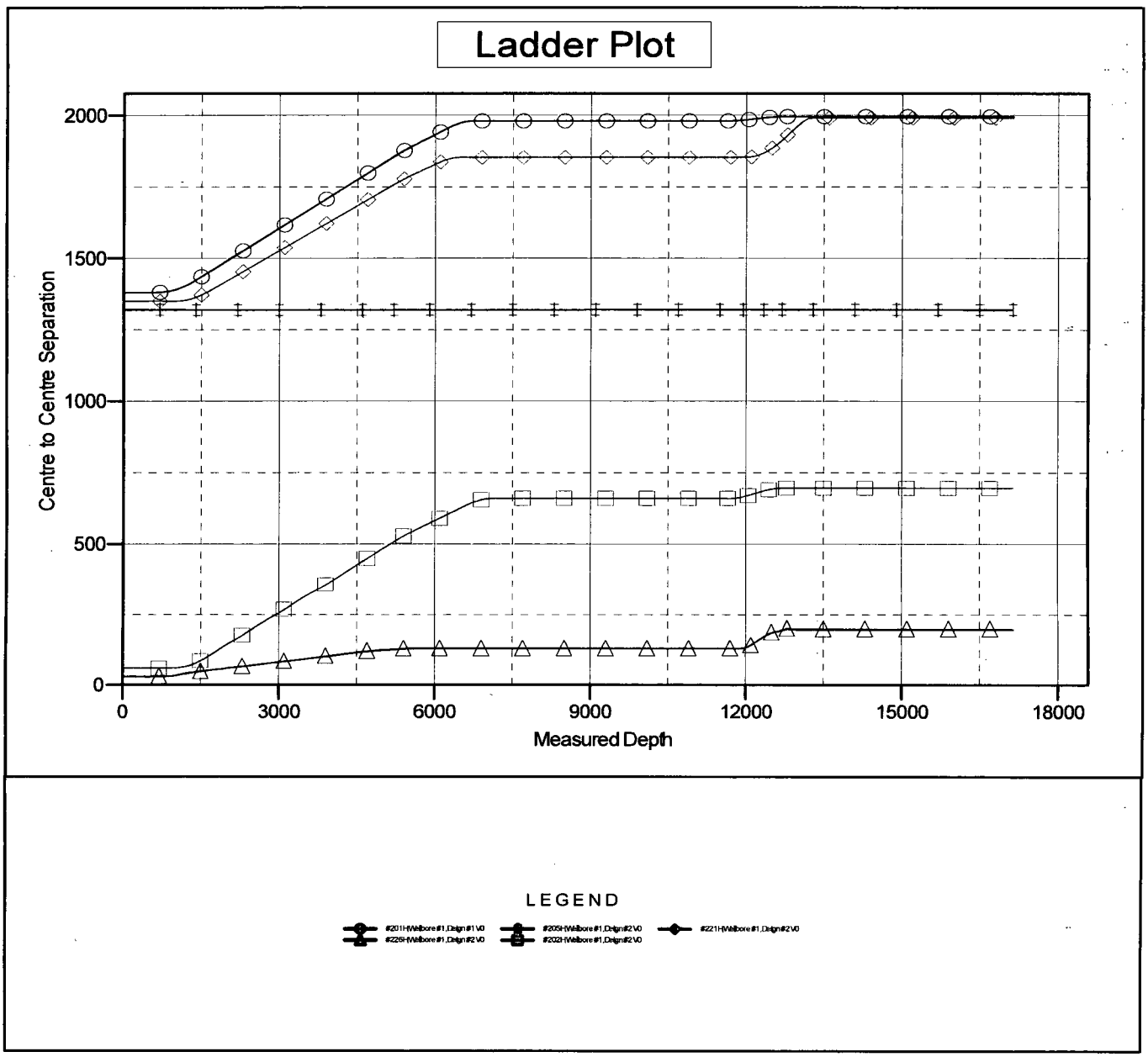
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Reference Depths are relative to WELL @ 3760.50usft (Patterson 282) Coordinates are relative to: #206H
Offset Depths are relative to Offset Datum Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30
Central Meridian is 104° 20' 0.000 W Grid Convergence at Surface is: 0.37°

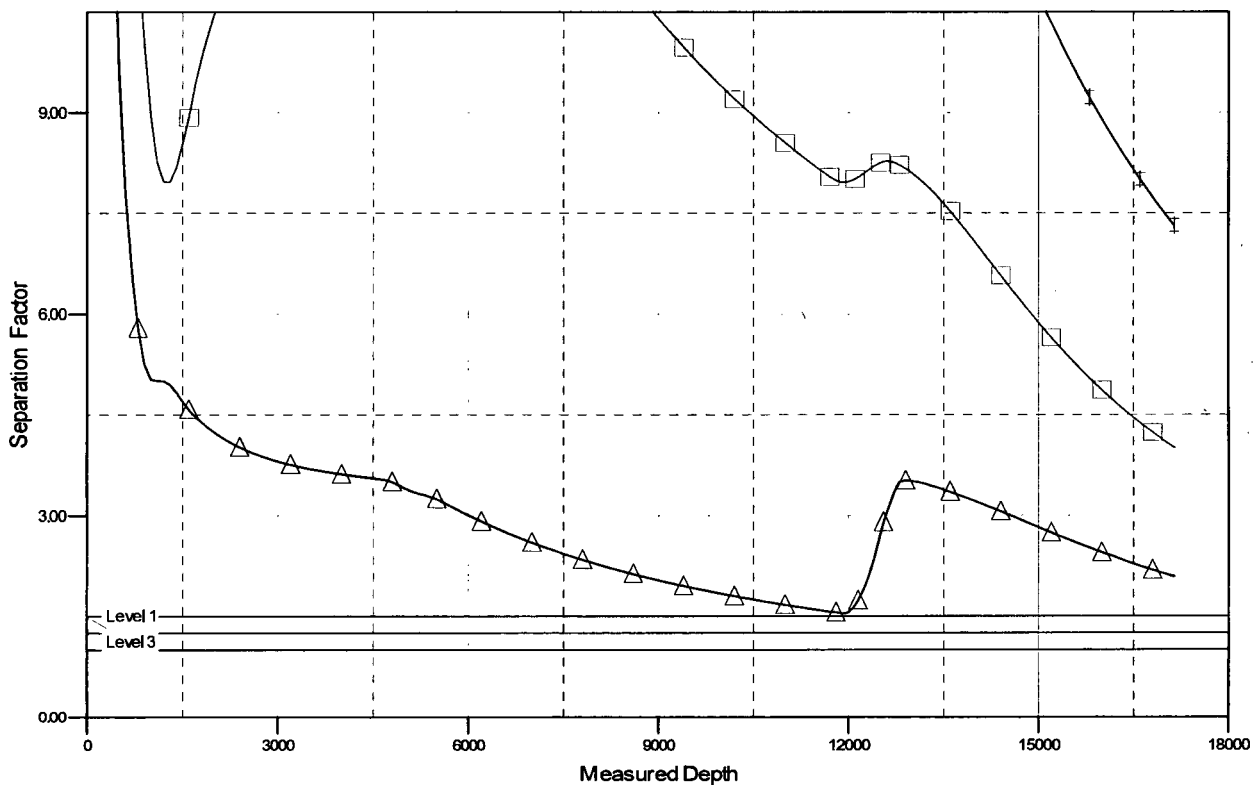


CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation

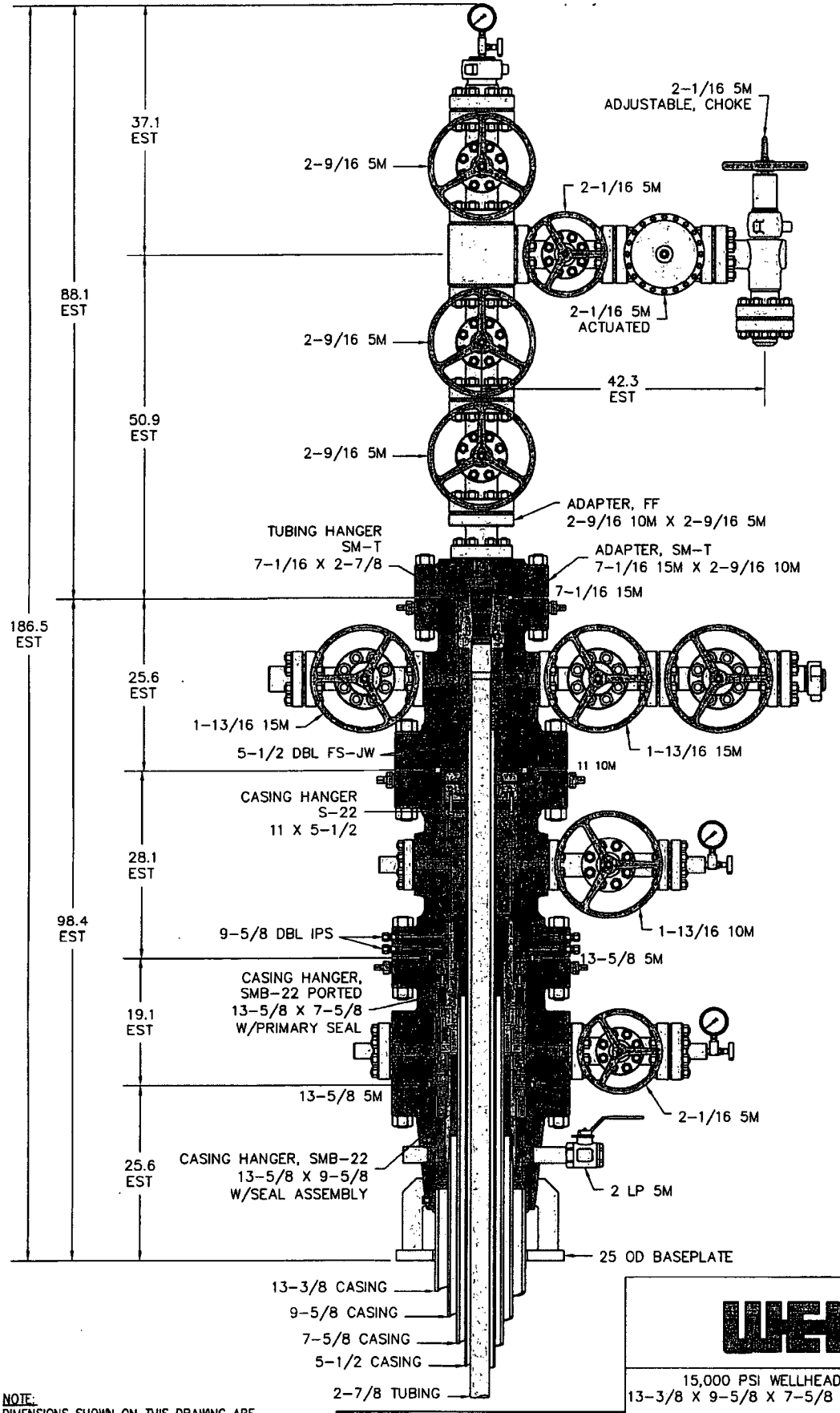
Company:	Matador Resources	**Local Co-ordinate Reference:**	Well #206H
Project:	Lea County, New Mexico (NAD 27)	**TVD Reference:**	WELL @ 3760.50usft (Patterson 282)
Reference Site:	Brad Dyer 35-22S-32E AR	**MD Reference:**	WELL @ 3760.50usft (Patterson 282)
Site Error:	0.00 usft	**North Reference:**	Grid
Reference Well:	#206H	**Survey Calculation Method:**	Minimum Curvature
Well Error:	0.00 usft	**Output errors are at**	2.00 sigma
Reference Wellbore	Wellbore #1	**Database:**	EDM Conroe
Reference Design:	Design #2	**Offset TVD Reference:**	Offset Datum

Reference Depths are relative to WELL @ 3760.50usft (Patterson 282) Coordinates are relative to: #206H
Offset Depths are relative to Offset Datum Coordinate System is US State Plane 1927 (Exact solution), New Mexico East 30
Central Meridian is 104° 20' 0.000 W Grid Convergence at Surface is: 0.37°

Separation Factor Plot



CC - Min centre to center distance or covergent point, SF - min separation factor, ES - min ellipse separation



NOTE:
DIMENSIONS SHOWN ON THIS DRAWING ARE ESTIMATES ONLY AND CAN VARY SIGNIFICANTLY DEPENDING ON RAW MATERIAL LENGTHS.
NO GUARANTEE OF STACKUP HEIGHT IS IMPLIED.
DIMENSIONS SHOWN SHOULD BE CONSIDERED FOR REFERENCE PURPOSES ONLY.

WEIR

15,000 PSI WELLHEAD ASSEMBLY
13-3/8 X 9-5/8 X 7-5/8 X 5-1/2 X 2-7/8

DRAWN BY:	SCALE	DATE	REV
RPL	1-11	06OCT17	
CHECKED BY:	DRAWING NO.		
APPROVED BY:	P-22401		

Surface Use Plan

1. ROAD DIRECTIONS & DESCRIPTIONS (See MAPS 1 – 5)

From the junction of US 285 and US 62/180 in Carlsbad...
Go NE 32.8 miles on US 62/180 to the equivalent of Mile Post 67.8
Then turn right and go East 6.5 miles on paved NM 176
Then turn right and go South 0.6 mile on a caliche road to a junction
Then bear right and go SW 1.6 mile on a caliche road
Then bear left and go SE 2.2 miles on a caliche road
Then bear right and go South7.5 miles on a caliche road
Then turn right and go West 1.5 miles on a caliche road
Then turn left and go South 1.75 miles on a caliche road
Then turn right and go W 1280.7' cross-country to the proposed pad

Non-state roads will be maintained as needed to Gold Book standards. This includes pulling ditches, preserving the crown, and cleaning culverts. This will be done at least once a year, and more often as needed.

2. ROAD TO BE BUILT OR UPGRADED (See MAPS 4 & 5)

The 1280.7' of new resource road will be crowned and ditched, have a 14' wide driving surface, and be surfaced with caliche. A 3" O. D. poly surface flowline on the west side of the existing road will be padded. Maximum disturbed width = 30'. Maximum grade = 2%. Maximum cut or fill = 1'. No culvert, cattle guard, or vehicle turn out is needed. Upgrading will consist of filling potholes with caliche.

3. EXISTING WELLS (See MAP 6)

Existing oil, injection, SWD, and P & A wells are within a mile. No gas or water well is within a mile radius.

4. PROPOSED PRODUCTION FACILITIES (See MAPS 7 - 9)

Production equipment will be located on the south and west sides of the pad. A 3-phase overhead raptor-safe power line will be built south and east 2,924.64' from an existing power pole at OXY's Red Tank 35 Federal 3 SWD. No pipeline plans have been finalized at this time.

5. WATER SUPPLY (See MAP 10)

Water will be trucked from an existing water station on private land. Berry's water station (CP 00802) is in NWNE 2-21s-33e.

6. CONSTRUCTION MATERIALS & METHODS (See MAPS 11 - 14)

NM One Call (811) will be notified before construction starts. Top ≈6" of soil and brush will be stockpiled north of the pad. V-door will face south. Closed loop drilling system will be used. Caliche will be hauled from an existing caliche pit on private (Berry) land in E2NE4 35-20s-34e.

7. WASTE DISPOSAL

All trash will be placed in a portable trash cage. It will be hauled to the Lea County landfill. There will be no trash burning. Contents (drill cuttings, mud, salts, and other chemicals) of the mud tanks will be hauled to R360's state approved (NM-01-0006) disposal site at Halfway. Human waste will be disposed of in chemical toilets and hauled to the Hobbs wastewater treatment plant.

8. ANCILLARY FACILITIES

There will be no airstrip or camp. Camper trailers will be on location for the company man, tool pusher, and mud logger.

9. WELL SITE LAYOUT (See MAP 11)

Also see Rig Layout diagram for depictions of the well pad, trash cage, access onto the location, parking, living facilities, and rig orientation.

10. RECLAMATION (See MAPS 15 & 16)

Interim reclamation will be completed within 6 months of completing the well. Interim reclamation will consist of shrinking the pad ≈12% (0.45 acre) by removing caliche and reclaiming a 140' x 140' area in the southeast corner of the pad. This will leave 3.20 acres for production equipment (e. g., tank battery, heater-treaters, separators,

flare/CBU, pump jacks), and tractor-trailer turn around. Disturbed areas will be contoured to match pre-construction grades. Soil and brush will be evenly spread over disturbed areas and harrowed on the contour. Disturbed areas will be seeded in accordance with the surface owners' requirements.

Enough stockpiled topsoil will be retained to cover the remainder of the pad when the well is plugged. Once the last well is plugged, then the rest of the pad and 1280.7' of new road will be similarly reclaimed within 6 months of plugging. Noxious weeds will be controlled.

Land use:

2924.64' x 15' power line = 1.01 acre
1280.7' x 30' road = 0.88 acre
+ 370' x 430' pad = 3.65 acres
5.54 acres short term
- 2924.64' x 15' power line = 1.01 acre
- 0.45 acre interim reclamation
4.08 acres long term (0.88 ac. road + 3.20 ac. pad)

11. SURFACE OWNER

All construction will be on BLM. BLM office is the Carlsbad Field Office, 620 E. Greene, Carlsbad NM 88220. Phone is 575 234-5972.

12. OTHER INFORMATION

On site inspection was held with Vance Wolf (BLM) on November 13, 2017. Lone Mountain will file an archaeology report.

CERTIFICATION

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U. S. C. 1001 for the filing of false statements. Executed this 27th day of March, 2018.

Brian Wood, Consultant
Permits West, Inc.
37 Verano Loop, Santa Fe, NM 87508
(505) 466-8120 FAX: (505) 466-9682 Cellular: (505) 699-2276

Field representative will be:
Sam Pryor, Senior Staff Landman
Matador Production Company

5400 LBJ Freeway, Suite 1500
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