Ib. Type of Well: ✓ Oil Well Gas Well Ot	NTEF AGEN	MENT L OR REENTER ER		OMB No Expires: Ja 5. Lease Serial No. NMNM0006531A 6. If Indian, Allotee 7. If Unit or CA Agr 8. Lease Name and LEALINIT	or Tribe eement, 1 Well No.	1137 , 2018 Name
2. Name of Operator LEGACY RESERVES OPERATING LP [240974] 3a. Address	3h P	Phone No. <i>(include area code</i>		200H 9. API-Well No. 30. 10. Field and Pool, d	-025-	45212
303 West Wall St., Ste 1800 Midland TX 79701	1)689-5287	' >	LEA (UPPER WO		
4. Location of Well (Report location clearly and in accordance w At surface NWNE / 140 FNL / 1740 FEL / LAT 32.5945 At proposed prod. zone SWNE / 2310 FNL / 2210 FEL / L	5004 /	LONG -103.5279787	295047	11. Sec., T. R. M. of SEC 117 T20S/R	Blk. and	Survey or Area
14. Distance in miles and direction from nearest town or post office 26 miles	ce*			12. County or Parish LEA	1	13. State NM
15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) 140 feet 18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease ft 50 feet	280 19. P	Proposed Depth	2559.68 20/BLM/	BIA Bond No. in file	his well	
applied for, on this lease, ft. 50 feet 21. Elevations (Show whether DF, KDB, RT, GL, etc.) 3665 feet	22.(A 08/27	Approximate date work will s 7/2018		23. Estimated durati 45 days	on	
 The following, completed in accordance with the requirements of (as applicable) 1. Well plat certified by a registered surveyor. 2. A Drilling Plan. 3. A Surface Use Plan (if the location is on National Forest Syster SUPO must be filed with the appropriate Forest Service Office) 	m Lanc	4. Bond to cover the Item 20 above). ds, the 5. Operator certifica	e operation ation.	lydraulic Fracturing r s unless covered by ar mation and/or plans as	n existing	bond on file (see
25. Signature (Electronic Submission) Title		Name (Printed/Typed) Shane Clark / Ph: (405)28	86-9326		Date 06/22/2	2018
Permitting Specialist Approved by (Signature) (Electronic Submission)		Name (Printed/Typed) Cody Layton / Ph: (575)2:	34-5959		Date 09/18/2	2018
Title Assistant Field Manager Lands & Minerals Application approval does not warrant or certify that the applican applicant to conduct operations thereon. Conditions of approval; if any, are attached.	t holds	Office CARLSBAD s legal or equitable title to the	ose rights	in the subject lease w	hich wou	ld entitle the
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, m of the United States any false, fictitious or fraudulent statements of					iny depar	tment or agency

GCP Rec 09/19/2018



KZ 09/19/2018

Approval Date: 09/18/2018



BUREAU OF LAND MANAGEMENT



Operator Certification

I hereby certify that I, or someone under my direct supervision, have inspected the drill site and access route proposed herein; that I am familiar with the conditions which currently exist; that I have full knowledge of state and Federal laws applicable to this operation; that the statements made in this APD package are, to the best of my knowledge, true and correct; and that the work associated with the operations proposed herein will be performed in conformity with this APD package and the terms and conditions under which it is approved. I also certify that I, or the company I represent, am responsible for the operations conducted under this application. These statements are subject to the provisions of 18 U.S.C. 1001 for the filing of false statements.

NAME: Shane Clark		Signed on: 06/22/2018
Title: Permitting Specialist		
Street Address: 1219 Clas	sen Drive	
City: Oklahoma City	State: OK	Zip: 73103
Phone: (405)286-9326		
Email address: sclark@rse	nergysolutions.com	
Field Represen	tative	
Representative Name:		
Street Address:		
City:	State:	Zip:
Phone:		
Email address:		

APD ID: 10400031426

Well Name: LEA UNIT

Well Type: OIL WELL

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Operator Name: LEGACY RESERVES OPERATING LP

Application Data Report

and the second second

Submission Date: 06/22/2018



1.

Well Number: 200H Well Work Type: Drill

Section 1 - General		
APD ID: 10400031426	Tie to previous NOS?	Submission Date: 06/22/2018
BLM Office: CARLSBAD	User: Shane Clark	Title: Permitting Specialist
Federal/Indian APD: FED	Is the first lease penetrated for	r production Federal or Indian? FED
Lease number: NMNM0006531A	Lease Acres: 280	
Surface access agreement in place	? Allotted? Res	ervation:
Agreement in place? NO	Federal or Indian agreement:	
Agreement number:		
Agreement name:		
Keep application confidential? YES		
Permitting Agent? YES	APD Operator: LEGACY RESE	RVES OPERATING LP
Operator letter of designation:	Authorization_Letter_for_Reagan_Smith_I	Lea 200H 20180619130758.pdf

Operator Info

Operator Organization Name:	LEGACY RESERVES OP	ERATING LP
Operator Address: 303 West	Wall St., Ste 1800	
Operator PO Box:		Zip: 79701
Operator City: Midland	State: TX	
Operator Phone: (432)689-528	37	
Operator Internet Address:		
Section 2 - We	Il Information	

Well in Master Development Plan? EXISTING	Mater Development Plan	name: Lea Unit Master Dev Plan						
Well in Master SUPO? NO	Master SUPO name:							
Well in Master Drilling Plan? NO	Master Drilling Plan name:							
Well Name: LEA UNIT	Well Number: 200H	Well API Number:						
Field/Pool or Exploratory? Field and Pool	Field Name: LEA	Pool Name: UPPER WOLFCAMP						

Is the proposed well in an area containing other mineral resources? USEABLE WATER, NATURAL GAS, OIL

Well Number: 200H

Describe other minerals:			
Is the proposed well in a Helium produ	uction area? N	Use Existing Well Pad? YES	New surface disturbance? N
Type of Well Pad: MULTIPLE WELL		Multiple Well Pad Name: LEA	Number: 7
Well Class: HORIZONTAL		UNIT 100H Number of Legs: 1	
Well Work Type: Drill			
Well Type: OIL WELL			
Describe Well Type:			
Well sub-Type: INFILL			
Describe sub-type:			
Distance to town: 26 Miles	Distance to ne	arest well: 50 FT Dista	nce to lease line: 140 FT
Reservoir well spacing assigned acres	s Measurement	: 2559.68 Acres	
Well plat: Lea_Unit_200H_Signed_C	102_04_10_18_	20180619141410.pdf	
Well work start Date: 08/27/2018		Duration: 45 DAYS	

Section 3 - Well Location Table

Survey Type: RECTANGULAR

Describe Survey Type:

Datum: NAD83

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Survey number:

	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD
SHL Leg #1	140	FNL	174 0	FEL	20S	34E	11	Aliquot NWNE	32.59450 04	- 103.5279 787	LEA	NEW MEXI CO	1	F	NMNM 000653 1A	366 5	0	0
KOP Leg #1	144	FNL	220 0	FEL	20S	34E	11	Aliquot NWNE	32.59451	- 103.5295	LEA	NEW MEXI CO		F	NMNM 000653 1A	- 765 9	113 50	113 24
PPP Leg #1	336	FNL	220 1	FEL	20S	34E	11	Aliquot NWNE	32.59398 3	- 103.5295	LEA	NEW MEXI CO	NEW MEXI CO	F	NMNM 000653 1A	- 813 5	120 99	118 00

Vertical Datum: NAVD88

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H

	NS-Foot	NS Indicator	EW-Foot	EW Indicator	Twsp	Range	Section	Aliquot/Lot/Tract	Latitude	Longitude	County	State	Meridian	Lease Type	Lease Number	Elevation	MD	TVD
PPP	0	FNL	220	FEL	20S	34E	14	Aliquot	32.58037	~	LEA	NEW	NEW	F	NMNM	-	167	118
Leg			0					NWNE	9	103.5295		MEXI			005343	813	60	00
#1										01		co	со		4	5		
EXIT	231	FNL	221	FEL	20S	34E	14	Aliquot	32.57402	-	LEA	NEW	NEW	F	NMNM	-	190	118
Leg	0		0					SWNE	91	103.5295		MEXI	MEXI		008026	813	73	00
#1										047		co	со		2	5		
BHL	231	FNL	221	FEL	20S	34E	14	Aliquot	32.57402	-	LEA	NEW	NEW	F	NMNM	-	190	118
Leg	0		0					SWNE	91	103.5295		MEXI	MEXI		008026	813	73	00
#1										047		co	со		2	5		



March 20, 2018

Bureau of Land Management Division of Oil and Gas 620 E. Greene Street Carlsbad, NM 88220-6292 Attn: Land Law Examiner

Re:

 Legacy Reserves Operating, L.P. Designation of Agent Lea Unit 200H 11-20S-34E NMPM Lea County, NM

To whom it may concern:

Legacy Reserves Operating, L.P. has contracted with Reagan Smith Energy Solutions, Inc. to assist in regulatory compliance associated with the Lea Unit 200H. Reagan Smith Energy Solutions, Inc. has the authority to act as Legacy Reserves Operating, L.P.'s agent to maintain regulatory compliance for the Lea Unit 200H. This includes the submittal of an APD, Communitization Agreement, Designations of Operator, Sundry Notices, and any other regulatory documents on behalf of Legacy Reserves Operating, L.P. in order to maintain regulatory compliance with the Bureau of Land Management in regard to the above referenced project.

Sincerely,

Matthew Dickson Legacy Reserves Operating, L.P.

DISTRICT I 1625 N. French Dr., Hobbs, NM 88240 Phone: (575) 393-6161 Fax: (575) 393-0720

DISTRICT II 611 S. Pirst SL., Artesia, NM 68210 Phone: (575) 748-1283 Fax: (575) 748-9720

DISTRICT III 1000 Rio Brazos Rd., Astec, NH 87410 Phone: (505) 334-6178 Fax: (505) 334-6170

DISTRICT IV 1220 S. St. Francis Dr., Santa Fe, NM 67505 Phone: (505) 476-3460 Faz: (505) 476-3462

State of New Mexico Energy, Minerals & Natural Resources Department OIL CONSERVATION DIVISION 1220 South St. Frances Dr. Santa Fe, NM 87505

Form C-102 Revised August 1, 2011 Submit one copy to appropriate District Office

□ AMENDED REPORT

23263

201740020

23263

W.Ø. Num.

Certificate No. Lindsay Gygax

Scale 1" = 2000'

API Number Pool Code Pool Name Well Number **Property** Code **Property** Name LEA UNIT 200H **Operator** Name OGRID No. Elevation LEGACY RESERVES OPERATING LP 3665' Surface Location UL or lot No. Feet from the North/South line Feet from the East/West line Section Township Range Lot Idn County NORTH 1740 В 11 20 S 34 E 140 EAST LEA Bottom Hole Location If Different From Surface UL or lot No. Section Range Lot Idn Feet from the North/South line Feet from the East/West line County Township 14 34 E NORTH EAST LEA G 20 S 2310 2210 **Dedicated** Acres Joint or Infill **Consolidation** Code Order No. NO ALLOWABLE WILL BE ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DIVISION S 67'45'28" W 140'-10--1740' SURFACE LOCATION OPERATOR CERTIFICATION 2210 506 ' **#200H (SL)**⊥ (NAD83) I hereby certify that the information contain d herein is true and cond Gr. El.: 3665' $\frac{\text{Plane Coordinate}}{X = 789,367.0}$ 200 the best of my knowledge and betief, and that this organization either come a working interest or unleased mineral interest in the land including Y = 580,949.0the proposed battom hole location or has a right to drill this well at this Geodetic (D.D.) 32.59450037' N location personnt to a contract with an owner of such a mineral or u First Take interest, or to a voluntary pooling agreement or a compulsary Point 103.52797866° W order heretofore entered by the division. follows Path FIRST TAKE POINT 11 £ Hoth H 7260' (NAD83) dep $\frac{\text{Plane Coordinate}}{X = 788,898.5}$ $\frac{Y = 580,757.4}{2}$ Signature Date ferent Т <u>Geodetic (D.D.)</u> 32.59398343' N <u>ا</u> ш Printed Name 103.52950471° W 0 6 15 E Ę 00.26 E-mail Address The L BOTTOM HOLE LOCATION į & LAST TAKE POINT SURVEYOR CERTIFICATION (NAD83) rgnsverse v Mexico North v gre S $\frac{Plone \ Coordinate}{X = 788,955.1} \\ Y = 573,497.7$ I hereby certify that the well location shown on this plat was plotted from field notes of actual surveys made by me or under my supervision, and that the Geodetic (D.D.) Vew M Zone, same is true and correct to the best of my belief. 32 57402905" N 2310 103.52949891° W December 20, 2017 the "N East Z ž Signature & Seal of Provellance Stations Date of Survey shown hereon Conform to th New Mexico Ev 1983. Distances s rface values. Last Take Point/ Bottom Hole Location 2210 -14

WELL LOCATION AND ACREAGE DEDICATION PLAT

) Plane Coordinate Mercator Grid an Coordinate System American Datum of mean horizontal s NOTE: ÷

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FMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Drilling Plan Data Report

09/18/2018

APD ID: 10400031426

Submission Date: 06/22/2018

Highlightedidatar netlecisthetinost recentichangest

Operator Name: LEGACY RESERVES OPERATING LP **Well Name:** LEA UNIT

Well Number: 200H

Well Type: OIL WELL

Well Work Type: Drill

Show Final Text

Section 1 - Geologic Formations

Formation	- ·· ·· ·		True Vertical	1 1			Producing
ID	Formation Name	Elevation	Depth	Depth	Lithologies		Formation
1	MANZANITA	3665	0	0	DOLOMITE	USEABLE WATER	No
2	RUSTLER	1965	1700	1728		NONE	No
3	YATES	241	3424	3452	<u> </u>	NONE	No
4	SEVEN RIVERS	-144	3809	3837		NONE	No
5	QUEEN	-967	4632	4660		NONE	No
6	BELL CANYON	-1923	5588	5616		NONE	No
7	CHERRY CANYON	-2806	6471	6499		NONE	No
8	BRUSHY CANYON	-3442	7107	7135		NONE	No
9	BONE SPRING	-4526	8191	8219		NATURAL GAS, OIL	No
10	UPPER AVALON SHALE	-5117	8782	8810		NATURAL GAS,OIL	No
11	BONE SPRING 1ST	-5839	9504	9532	<u> </u>	NATURAL GAS,OIL	No
12	BONE SPRING 2ND	-6376	10041	10069		NATURAL GAS, OIL	No
13	BONE SPRING 3RD	-7034	10699	10727		NATURAL GAS, OIL	No
14	WOLFCAMP	-7344	11009	11085	<u> </u>	NATURAL GAS, OIL	Yes

Section 2 - Blowout Prevention

Well Name: LEA UNIT

Well Number: 200H

Pressure Rating (PSI): 5M

Rating Depth: 11800

Equipment: Ten thousand (10M) psi working pressure Blind Rams and Pipe Rams and a five thousand (5M) psi Annular Preventer will be installed on all casing. Three (3) chokes; two (2) hydraulic and one (1) manual, will be used. **Requesting Variance?** YES

Vanance requests A variance is regrested to use a SM annular on the 10 M BOP. A variance to the requirement of a right Seal (has connecting to the chicke the filled is requested. Speaklenting for the first hase are provided with BOP schematic in Shift seallon

Testing Procedure: A third party testing company will conduct pressure tests and record prior to drilling out below 13-3/8s" casing. The BOP, Choke, Choke Manifold, Top Drive Valves and Floor Safety Valves will be tested to 5000 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of working pressure (5,000 psi) prior to drilling below the 9-5/8" intermediate casing shoe. In addition, the BOP equipment will be tested after any repairs to the equipment as well as drilling out below any casing string. Pipe rams, blind rams, and annular preventer will be activated on each trip, and weekly BOP drills will be held with each crew. Floor Safety Valves that are full open and sized to fit Drill Pipe and Collars will be available on the rig floor in the open position when the Kelly is not in use.

Choke Diagram Attachment:

McVay_2_Choke_Manifold_Diagram_20180813105918.pdf

BOP Diagram Attachment:

McVay_2_BOP_Diagram_20180813105932.pdf

Casing ID	String Type	Hole Size	Csg Size	Condition	Standard	Tapered String	Top Set MD	Bottom Set MD	Top Set TVD	Bottom Set TVD	Top Set MSL	Bottom Set MSL	Calculated casing length MD	Grade	Weight	Joint Type	Collapse SF	Burst SF	Joint SF Type	Joint SF	Body SF Type	Body SF
1	SURFACE	17.5	13.375	NEW	API	N	0	1800	0	1794	-3665		1800	J-55	54.5	BUTT	1.42	3.5	DRY	4.3	DRY	4.3
2	INTERMED IATE	12.2 5	9.625	NEW	API	N	0	5600	0	5561	- 10136	- 11696		HCL -80	40	BUTT	1.97	1.34	DRY	2.99	DRY	2.99
3	INTERMED IATE	12.2 5	7.0	NEW	API	N	0	10700	0	10661			10700	HCP -110	32	BUTT	2.31	1.98	DRY	2.31	DRY	2.31
	PRODUCTI ON	8.75	4.5	NEW	API	N	10200	19073	10174	11800	-6137	- 15937		P- 110	13.5	BUTT	1.51	1.25	DRY	1.63	DRY	1.63

Section 3 - Casing

Casing Attachments

Casing Attachments

Casing ID: 1 String Type: SURFACE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Lea_Unit_200H_Drilling_Program_20180622132909.pdf

Casing ID: 2 String Type: INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Lea_Unit__200H_Drilling_Program_20180622132917.pdf

Casing ID: 3 String Type: INTERMEDIATE

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Lea_Unit__200H_Drilling_Program_20180622132925.pdf

Casing Attachments

Casing ID: 4

String Type: PRODUCTION

Inspection Document:

Spec Document:

Tapered String Spec:

Casing Design Assumptions and Worksheet(s):

Lea_Unit_200H_Drilling_Program_20180622132934.pdf

Section 4 - Cement

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String Type	Lead/Tail	Stage Tool Depth	Top MD	Bottom MD	Quantity(sx)	Yield	Density	Cu Ft	Excess%	Cement type	Additives
SURFACE	Lead		0	1600	1300	1.72	13.5	2236	100	Class C cement	4%Bentonite, 0.4 pps Defoamer, 0.125 pps Cellophane, 9.102 H2O GPS
SURFACE	Tail		1600	1800	200	1.32	14.8	264	60	Class C Neat	6.304 H2O GPS
INTERMEDIATE	Lead		0	5000	1700	1.94	12.6	3298	180	35:65 POZ-Class C	6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS
INTERMEDIATE	Tail		5000	5600	350	1.18	15.6	413	140	Class H	0.3% Fluidloss, 5.216 H2O GPS
INTERMEDIATE	Lead		0	5300	820	1.18	15.6	968	15	Class H	0.2% Retarder, 6.3 H2O GPS
INTERMEDIATE	Tail		5300	1070 0	550	1.62	12.6	891	30	PVL	1.3% Salt, 5% Expanding Cement, 0.5% Fluidloss, 0.3% Retarder, 0.1% Antisettling, 0.4 pps Defoamer, 8.621 H2O GPS
PRODUCTION	Lead		1020 0	1907 3	750	1.34	14.2	1005	30	50:50 POZ-Class H	5% Salt, 2% Bentonite, 0.5% Fluidloss, 0.2% Retarder, 0.2% Dispersant, 0.4pps

Page 4 of 7

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H



Section 5 - Circulating Medium

Mud System Type: Closed

Will an air or gas system be Used? NO

Description of the equipment for the circulating system in accordance with Onshore Order #2:

Diagram of the equipment for the circulating system in accordance with Onshore Order #2:

Describe what will be on location to control well or mitigate other conditions: In the event that circulation is lost (> 50%) while drilling the 12-1/4" intermediate hole in the Capitan Reef at +/-4000', we will plan to install a DV tool and external casing packer within 200' of the top depth where lost circulation occurred and will pump a two-stage cement job with the potential to add an additional DV tool for a three-stage cement job. If there is no lost circulation a single stage cementing procedure will be followed. Legacy plans to cement to surface regardless of whether a single stage, 2-stage or 3-stage procedure is implemented.

Describe the mud monitoring system utilized: A Pason PVT system will be rigged up prior to spudding this well. A volume monitoring system that measures, calculates, and displays readings from the mud system on the rig to alert the rig crew of impending gas kicks and lost circulation. In order to effectively run casing, the mud viscosity and fluid loss properties may be adjusted.

Circulating Medium Table

Top Depth	Bottom Depth	Mud Type	Min Weight (Ibs/gal)	Max Weight (Ibs/gal)	Density (lbs/cu ft)	Gel Strength (lbs/100 sqft)	На	Viscosity (CP)	Salinity (ppm)	Filtration (cc)	Additional Characteristics
5600	1070 0	OTHER : Cut brine	9	9.2							
1800	5600	OTHER : Brine	10	10							
0	1800	OTHER : Fresh Water	8.5	9							
1070 0	1180 0	OIL-BASED MUD	10.5	11							

Well Number: 200H

Section 6 - Test, Logging, Coring

List of production tests including testing procedures, equipment and safety measures:

Mud logging, H2S plan, BOP and choke plans all in place for testing, equipment, safety

List of open and cased hole logs run in the well:

CBL,GR,MWD,MUDLOG

Coring operation description for the well:

No coring planned

Section 7 - Pressure

Anticipated Bottom Hole Pressure: 6750

Anticipated Surface Pressure: 4154

Anticipated Bottom Hole Temperature(F): 205

Anticipated abnormal pressures, temperatures, or potential geologic hazards? YES

Describe:

Capitan Reef

Contingency Plans geoharzards description:

If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.

Contingency Plans geohazards attachment:

Hydrogen Sulfide drilling operations plan required? YES

Hydrogen sulfide drilling operations plan:

H2S_Contingency_Plan_Briefing_Areas_Alarm_Loc._Legacy_Lea_Unit_200H_20180622132552.pdf

Section 8 - Other Information

Proposed horizontal/directional/multi-lateral plan submission:

Lea_Unit_200H_Planning_Report_Plan_1_20180622132640.pdf

Lea_Unit__200H_Plot_Plan_1_20180622132651.pdf

Other proposed operations facets description:

Other proposed operations facets attachment:

Flex_Hose_Specs_20180619120636.pdf

Rig_Schematic_20180619120621.pdf

Lea_Unit_200H_GasCapturePlanFormAPD_20180622132616.pdf

Lea_Unit_200H_AC_Report_Plan_1_20180622132701.pdf

Other Variance attachment:





13-5/8" BOP Stack (10M)



DRILLING PROGRAM

Operator: LEGACY RESERVES OPERATING LP

Project Name: LEA UNIT 200H

Project Location:

Lea County, New Mexico

Prepared By:

Matt Dickson Drilling Engineer

Submitted To:

Bureau of Land Management Carlsbad Field Office

Please address inquiries, questions, scheduling of meetings and deficiency statements, if any, to Scott St. John and/or Monica Smith Griffin at the address shown below:

Reagan Smith Energy Solutions, Inc. 1219 Classen Drive Oklahoma City, OK 73103 405-286-9326

sstjohn@rsenergysolutions.com msmith@rsenergysolutions.com

1.0 Drilling Program

1.1 Estimated Formation Tops

FORMETON	TVD @	TVD	TVD @
FORMATION	<u>Surface Loc</u>	@ KB	<u>TD</u>
Rustler	1,700'	1,728'	1,728'
Yates	3,424'	3,452'	3,452'
Seven Rivers	3,809'	3,837'	3,837'
Queen	4,632'	4,660'	4,660'
Bell Canyon	5,588'	5,616'	5,616'
Cherry Canyon	6,471'	6,499'	6,499'
Brushy Canyon	7,107'	7,135'	7,135'
Bone Spring	8,191'	8,219'	8,219'
Avalon Shale	8,782'	8,810'	8,810'
1 st BS	9,504'	9,532'	9,532'
2 nd BS	10,041'	10,069'	10,069'
3 rd BS	10,699'	10,727'	10,727'
Wolfcamp	11,009'	11,037'	11,037'
Upper Wolfcamp	11,212'	11,240'	11,240'
Lower Wolfcamp	11,678'	11,698	11,800

Target Formation and Total Depth:

The total depth of the proposed well is approximately 19,100' MD located in the Upper Wolfcamp.

According to New Mexico EMNRD 19.15.15.9 NMAC a well shall be located no closer than 330' feet to a boundary of the unit.

1.2 Estimated Depths of Anticipated Fresh Water, Oil, and Gas

<u>Substance</u>	<u>Depth</u>
Fresh Water	0' to 250'
Base of Treatable Water	125'
Hydrocarbons	8,191' to TD

1.2.2 State Water Protection Compliance

Bureau of Land Management requires surface casing to be set at a minimum of 25' into the Rustler Anhydrite and above the salt section. Operator proposes to set the surface casing at a depth of 1800' (measured from the surface) and use 13-3/8" casing.

Special Capitan Reef requirements

If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.

1.3 Pressure Control Equipment

Ten thousand (10M) psi working pressure Blind Rams and Pipe Rams and a five thousand (5M) psi Annular Preventer will be installed on all casing. Three (3) chokes; two (2) hydraulic and one (1) manual, will be used.

A variance to the requirement of a rigid steel line connecting to the choke manifold is requested. Specifications for the flex hose are provided with BOP schematic in exhibit section.

A third party testing company will conduct pressure tests and record prior to drilling out below 13-3/8s" casing. The BOP, Choke, Choke Manifold, Top Drive Valves and Floor Safety Valves will be tested to 5000 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of working pressure (5,000 psi) prior to drilling below the 9-5/8" intermediate casing shoe.

In addition, the BOP equipment will be tested after any repairs to the equipment as well as drilling out below any casing string. Pipe rams, blind rams, and annular preventer will be activated on each trip, and weekly BOP drills will be held with each crew. Floor Safety Valves that are full open and sized to fit Drill Pipe and Collars will be available on the rig floor in the open position when the Kelly is not in use.

1.4 **Proposed Casing and Cementing Program**

Interval	Depth	Size	Weight/ft	Grade	Thread	Condition	Hole size	Wash out factor	Cement Yield
Conductor	120'	20"	94.00#	H-40		New	26"		Grout
Surface	1,800'	13-3/8"	54.50#	J-55	BTC	New	17-1/2"	100	1.72/1.32 cu. Ft/sk
Intermediate	5,600'	9-5/8"	47#	HCL-80	BTC	New	12-1/4"	150	1.94/1.18 cu. Ft/sk
Intermediate Liner	10,700	7"	32.00#	P-110HC	BTC	New	8-1/2"	30	1.62 cu. Ft/sk
Production	19,100'	4-1/2"	13.5#	P-110	BTC	New	6"	30	l.34 cu. Ft/sk

1.4.1 Proposed Casing Program

<u>Conductor</u>: 20", H-40# line pipe to a depth of 120'. Wall thickness of 0.250".

Surface Casing:

Тор	Bottom	Size	Weight/	Grade	Thread	Collapse	Internal	Body	Joint
			Ft			psi	Yld psi	Yld	Strength
								Strength	
Surface	1,800'	13- 3/8"	54.50	J-55	BTC	1130	2730	853,000	909,000

Intermediate Casing:

	TWCIII	culai	e Casiliq.	•					
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
-						psi	Yld psi	Yld	Strength
						-	_	Strength	_
Surface	5,600'	9-	47#	HCL-	BTC	5,740	6,870	1,086,000	1,122,000
		5/8"		80					
	Interm	<u>ediat</u>	e Liner:						
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
						psi	Yld psi	Yld	Strength
							_	Strength	
Surface	10,700	7"	32#	P-	BTC	11,890	12,450	1,025,000	1,053,000
				110HC				ſ	

Production Casing:

Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld Strength	Joint Strength
10,200	19,073	4- 1/2"	13.5#	P-110	BTC	10,690	12,420	422,000	443,000

1.4.2 Proposed Cement Program

Conductor: Grout to Surface (est. 8 cu. yds on backside)

<u>13-3/8" Surface:</u>

Surfece Casing Suing				
LEAD				
Top of MD	0			
Bottom of MD	1600			
Cement Type	Class C			
Additives	4%Bentonite, 0.4 pps Defoamer,			
	0.125 pps Cellophane, 9.102 H2O			
	GPS			
# of SKS	1300			
Yield (ft3/sk)	1.72			
Density (lbs/gal)	13.5			
Volume (ft3)	2236			
Excess (%)	100%			
	PAIL			
Top of MD	1600			
Bottom of MD	1800			
Cement Type	Class C Neat			
Additives	6.304 H2O GPS			
# of SKS	200			
Yield (ft3/sk)	1.32			
Density (lbs/gal)	14.8			
Volume (ft3)	264			
Excess (%)	60%			

9-5/8" Intermediate (No DV Tool):

Internediate Casing String					
LEAD					
Top of MD	0				
Bottom of MD	5000				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.542 H2O GPS				
# of SKS	1700				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	3298				
Excess (%)	180%				
T.	AIL				
Top of MD	5000				
Bottom of MD	5600				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	350				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	413				
Excess (%)	140%				

9-5/8" Intermediate (With 1 DV Tool):

lone	mnediate Casing Swing			
*Stage 1				
LEAD				
Top of MD	0			
Bottom of MD	5000			
Cement Type	35:65 POZ-Class C			
Additives	6% Bentonite, 0.5% Fluidloss,			
	0.15% Retarder, 0.4pps			
	Defoamer, 10.542 H2O GPS			
# of SKS	1700			
Yield (ft3/sk)	1.94			
Density (lbs/gal)	12.6			

Volume (ft3)	3298		
Excess (%)	180%		
	AIL		
Top of MD	500		
Bottom of MD	5600		
Cement Type	Class H		
Additives	0.3% Fluidloss, 5.216 H2O GPS		
# of SKS	350		
Yield (ft3/sk)	1.18		
Density (lbs/gal)	15.6		
Volume (ft3)	413		
Excess (%)	140%		
*Stage 2	······································		
Stage Tool Depth	+/- 3900'		
LE	AD		
Top of MD	0		
Bottom of MD	3500		
Cement Type	35:65 POZ-Class C		
Additives	6% Bentonite, 0.5% Fluidloss,		
	0.15% Retarder, 0.4pps		
	Defoamer, 10.543 H2O GPS		
# of SKS	1200		
Yield (ft3/sk)	1.94		
Density (lbs/gal)	12.6		
Volume (ft3)	2328		
Excess (%)	200%		
Tź	AIL		
Top of MD	3500		
Bottom of MD	3900		
Cement Type	Class H		
Additives	0.3% Fluidloss, 5.216 H2O GPS		
# of SKS	200		
Yield (ft3/sk)	1.18		
Density (lbs/gal)	15.6		
Volume (ft3)	236		
Excess (%)	100%		

9-5/8" Intermediate (With 2 DV Tools):

*Stage 1 LEAD Top of MD 0 Bottom of MD 5000 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 <t< th=""><th>holonadista</th><th>Casing Summ</th></t<>	holonadista	Casing Summ			
LEAD Top of MD 0 Bottom of MD 5000 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% Top of MD 5000 Bottom of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth Stage Tool Depth +/- 3900' LEAD 0 Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps					
Top of MD 0 Bottom of MD 5000 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Yolume (ft3) 413 Excess (%) 140% *Stage 2 140% Stage Tool Depth +/- 3900' LEAD 700 of MD 0 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94		AD			
Bottom of MD 5000 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5600 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 * Stage Tool Depth +/- 3900' LEAD Top of MD Top of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Vol					
Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth ±/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328					
Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
0.15% Retarder, 0.4pps Defoamer, 10.542 H2O GPS # of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth Kage 2 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 <td></td> <td></td>					
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# of SKS 1700 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	# of SKS				
Density (lbs/gal) 12.6 Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS 4 of SKS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
Volume (ft3) 3298 Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2					
Excess (%) 180% TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2					
TAIL Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2					
Top of MD 5000 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2					
Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 5 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL TAIL					
Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 5 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL TAIL					
Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	······································				
# of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2		••••••••••••••••••••••••••••••••••••••			
Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 *Stage 2 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL TAIL					
Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2 *Stage 2 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
Volume (ft3) 413 Excess (%) 140% *Stage 2	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			
Excess (%) 140% *Stage 2					
*Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
Stage Tool Depth +/- 3900' LEAD 0 Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
LEADTop of MD0Bottom of MD3500Cement Type35:65 POZ-Class CAdditives6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS# of SKS1200Yield (ft3/sk)1.94Density (lbs/gal)12.6Volume (ft3)2328Excess (%)200%TAIL		+/- 3900'			
Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%					
Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200%	Top of MD	0			
Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL		3500			
Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL	Cement Type	35:65 POZ-Class C			
0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL		6% Bentonite, 0.5% Fluidloss,			
Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL		0.15% Retarder, 0.4pps			
Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL					
Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL	# of SKS	1200			
Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL	Yield (ft3/sk)	1.94			
Volume (ft3) 2328 Excess (%) 200% TAIL	Density (lbs/gal)	12.6			
Excess (%) 200% TAIL		2328			
TAIL		200%			
Top of MD 3500					
	Top of MD	3500			

Bottom of MD	3900				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	200				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	236				
Excess (%)	100%				
*Stage 3					
Stage Tool Depth	+/- 1900'				
TAIL					
Top of MD	0				
Bottom of MD	1900				
Cement Type	Class C Neat				
Additives	6.304 H2O GPS				
# of SKS	700				
Yield (ft3/sk)	1.32				
Density (lbs/gal)	14.8				
Volume (ft3)	924				
Excess (%)	30%				

<u>7" Intermediate Liner:</u>

Inderanachata	Casing String					
LEAD						
Top of MD	0					
Bottom of MD	5300					
Cement Type	Class H					
Additives	0.2% Retarder, 6.3 H2O GPS					
# of SKS	820					
Yield (ft3/sk)	1.18					
Density (lbs/gal)	15.6					
Volume (ft3)	968					
Excess (%)	15%					
T	AIL					
Top of MD	5300					
Bottom of MD	10,700					
Cement Type	PVL					
Additives	1.3% Salt, 5% Expanding					
	Cement, 0.5% Fluidloss, 0.3%					
	Retarder, 0.1% Antisettling,					
	0.4 pps Defoamer, 8.621 H2O					

	GPS
# of SKS	550
Yield (ft3/sk)	1.62
Density (lbs/gal)	12.6
Volume (ft3)	891
Excess (%)	30%

4-1/2" Production Liner:

Production Casing String							
T	AIL						
Top of MD	10,200						
Bottom of MD	19,073						
Cement Type	50:50 POZ-Class H						
Additives	5% Salt, 2% Bentonite, 0.5%						
	Fluidloss, 0.2% Retarder, 0.2%						
	Dispersant, 0.4pps Defoamer,						
	6.088 H2O GPS						
# of SKS	750						
Yield (ft3/sk)	1.34						
Density (lbs/gal)	14.2						
Volume (ft3)	1005						
Excess (%)	30%						

Cement volumes are based on bringing cement to surface on all strings and TOC to $\sim 10,200'$ (top of liner) on production.

Operator reserves the right to change cement designs as hole conditions may warrant.

1.5 Proposed Mud Program

<u>Top</u> <u>TVD</u>	<u>Bottom</u> <u>TVD</u>	Туре	<u>Max Mud</u> <u>Weight for</u> <u>Hole Control</u> <u>Design</u>	<u>Viscosity</u> (sec/qt)
SURFACE	1,800	Fresh Water	9.0	28-38
1800	5,600	Brine	10.0	28-30
5,600	10,700	Cut Brine	9.2	28-30
10,700	TD	OBM	11.0	55-65

The operator must include the minimum design criteria, including casing loading assumptions and corresponding safety factors for burst, collapse, and tensions (body yield, and joint strength).

1.6 Casing Design

1.6.1 Drilling Design Analysis

Interval	Max	Anticipated	Estimated	Internal	Collapse	Joint	Body	Burst	Collpase	Tensile
	TVD	Mud	Max Pore	Yield	Strength	Strength	Strength	Safety	Safety	Safety
	(ft)	Weight	Pressure	Strength	(psi)	(lbs)	(lbs)	Factor	Factor (Min	Factor
		(ppg)	(psi)	(psi)				(Min 1.25)	1.25)	(Min 1.6)
Surface	1,800	8.5	780	2,730	1,130	909,000	853,000	3.5	1.42	4.3
Interm.	5,600	10	2,420	6,870	5,740	1,122,000	1,086,000	1.34	1.97	2.99
Interm.	10,700	9.0	4,730	12,450	11,890	1,053,000	1,025,000	1.98	2.31	2.31
Liner										
Prod.	11,800	11.5	5,880	12,420	10,690	443,000	422,000	1.25	1.51	1.63

Surface Casing Design Notes:

- Burst Design Assumptions: Calculations assume complete evacuation behind pipe.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Casing Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Liner w/ Tie-Back Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Production Design Notes:

- Burst Design Assumptions: Calculations assume surface frac pressure of 9500 psi along with a fluid gradient of 0.49psi/ft, with an external force equivalent to 0.44 psi/ft.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

*Notes:

- 1) Collapse DSF: If < 1.125 calculations are required.
- 2) Burst DSF: If < 1.0 calculations are required.
- 3) Body Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 4) Joint Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 5) Will an offset pressure variance request be requested to meet safety factors? Max. 0.22 psi/ft. Please indicate offset pressure variance requested.

Mud weight increases at shoe depths are for pressure control. Mud weight increases in the curve and lateral sections of the hole are for hole stability, not pressure control. Mud weight assumptions for casing load designs exceed anticipated maximum mud weight for balanced drilling in all hole sections. Expected mud weights in the Lower Wolfcamp Horizontal will be 0.5 to 1.0 ppg greater than formation pressure (i.e. overbalanced drilling.)

The Mud System will run as a closed loop system with PVT monitoring. All drill cuttings and liquid mud will be hauled to an approved NMOCD site for disposal or soil farm upon receiving appropriate approval.

1.7 Completion Program and Casing Design

Hydraulic fracturing will occur through the production casing. The burst design calculation assumes TOC at surface and therefore, the backside of the production casing is not evacuated. The maximum pumping pressure is 10,000 psi with a maximum proppant fluid weight of 9.5 ppg. The design safety factor for burst is 1.25.

Upon request, operator will provide proof of cement bonding by bond log. Operator is responsible for log interpretation and certification prior to frac treatment.

Upon request, operator will provide estimated fracture lengths, flowback storage, volumes of fluids and amount of sand to be used, and number of stages of frac procedure. Furthermore, a report of the annulus pressures before and after each stage of treatment may be requested by the BLM. The report may include chemical additives (other than proprietary), dissolved solids in frac fluid, and depth of perforations.

1.8 Evaluation Program

Required Testing, Logging, and Coring procedures noted below:

- Mud Logging/Gamma Ray/MWD.
- Cased hole CBL on production casing.

1.9 Downhole Conditions

Zones of possible lost circulation: Zones of possible abnormal pressure: Maximum bottom hole temperature: Maximum bottom hole pressure: Capitan Reef Lower Wolfcamp 205° F 6,750 psi or less.

1.10 Overview of Drilling Procedure

- Drill 17.5" surface hole to 1,800'; run 13.375" casing to 1,800' and cement to surface; install 10M stack, set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 12.25" intermediate hole to 5,600', run 9.625" casing and cement; set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 8-1/2" intermediate hole to approximately 10,700' and run 7" liner with a tie-back sleeve, and cement to top of liner set at +/- 5,300'.
- Drill 6" production hole to +/- 19,100'; run 4.5" liner from TD to +/- 10,200' and cement per cement program and test.
- Run 7" tie-back string from +/- 5300' to surface and cement per cement program, circulate cement to surface.

1.11 Overview of Completion for Equipment Sizing

• A Sundry Notice will be submitted with the proposed completion procedure prior to the job.

DRILLING PROGRAM

Operator: LEGACY RESERVES OPERATING LP

> Project Name: LEA UNIT 200H

Project Location:

Lea County, New Mexico

Prepared By:

Matt Dickson Drilling Engineer

Submitted To:

Bureau of Land Management Carlsbad Field Office

Please address inquiries, questions, scheduling of meetings and deficiency statements, if any, to Scott St. John and/or Monica Smith Griffin at the address shown below:

Reagan Smith Energy Solutions, Inc. 1219 Classen Drive Oklahoma City, OK 73103 405-286-9326

sstjohn@rsenergysolutions.com msmith@rsenergysolutions.com

1.0 Drilling Program

1.1 Estimated Formation Tops

	TVD @	TVD	TVD @
FORMATION	<u>Surface Loc</u>	@ KB	<u>TD</u>
Rustler	1,700'	1,728'	1,728'
Yates	3,424'	3,452'	3,452'
Seven Rivers	3,809'	3,837'	3,837'
Queen	4,632'	4,660'	4,660'
Bell Canyon	5,588'	5,616'	5,616'
Cherry Canyon	6,471'	6,499'	6,499'
Brushy Canyon	7,107'	7,135'	7,135'
Bone Spring	8,191'	8,219'	8,219'
Avalon Shale	8,782'	8,810'	8,810'
1 st BS	9,504'	9,532'	9,532'
2 nd BS	10,041'	10,069'	10,069'
3 rd BS	10,699'	10,727'	10,727'
Wolfcamp	11,009'	11,037'	11,037'
Upper Wolfcamp	11,212'	11,240'	11,240'
Lower Wolfcamp	11,678'	11,698	11,800

Target Formation and Total Depth:

The total depth of the proposed well is approximately 19,100' MD located in the Upper Wolfcamp.

According to New Mexico EMNRD 19.15.15.9 NMAC a well shall be located no closer than 330' feet to a boundary of the unit.

1.2 Estimated Depths of Anticipated Fresh Water, Oil, and Gas

<u>Substance</u>	<u>Depth</u>
Fresh Water	0' to 250'
Base of Treatable Water	125'
Hydrocarbons	8,191' to TD

1.2.2 State Water Protection Compliance

Bureau of Land Management requires surface casing to be set at a minimum of 25' into the Rustler Anhydrite and above the salt section. Operator proposes to set the surface casing at a depth of 1800' (measured from the surface) and use 13-3/8" casing.

Special Capitan Reef requirements

If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.

1.3 Pressure Control Equipment

Ten thousand (10M) psi working pressure Blind Rams and Pipe Rams and a five thousand (5M) psi Annular Preventer will be installed on all casing. Three (3) chokes; two (2) hydraulic and one (1) manual, will be used.

A variance to the requirement of a rigid steel line connecting to the choke manifold is requested. Specifications for the flex hose are provided with BOP schematic in exhibit section.

A third party testing company will conduct pressure tests and record prior to drilling out below 13-3/8s" casing. The BOP, Choke, Choke Manifold, Top Drive Valves and Floor Safety Valves will be tested to 5000 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of working pressure (5,000 psi) prior to drilling below the 9-5/8" intermediate casing shoe.

In addition, the BOP equipment will be tested after any repairs to the equipment as well as drilling out below any casing string. Pipe rams, blind rams, and annular preventer will be activated on each trip, and weekly BOP drills will be held with each crew. Floor Safety Valves that are full open and sized to fit Drill Pipe and Collars will be available on the rig floor in the open position when the Kelly is not in use.

1.4 Proposed Casing and Cementing Program

Interval	Depth	Size	Weight/ft	Grade	Thread	Condition	Hole size	Wash out factor	Cement Yield
Conductor	120'	20"	94.00#	H-40		New	26"		Grout
Surface	1,800'	13-3/8"	54.50#	J-55	BTC	New	17-1/2"	100	1.72/1.32 cu. Ft/sk
Intermediate	5,600'	9-5/8"	47#	HCL-80	BTC	New	12-1/4"	150	1.94/1.18 cu. Ft/sk
Intermediate Liner	10,700	7"	32.00#	P-110HC	BTC	New	8-1/2"	30	1.62 cu. Ft/sk
Production	19,100'	4-1/2"	13.5#	P-110	BTC	New	6"	30	l.34 cu. Ft/sk

1.4.1 Proposed Casing Program

<u>**Conductor</u>**: 20", H-40# line pipe to a depth of 120'. Wall thickness of 0.250".</u>

Surface Casing:

Тор	Bottom	Size	Weight/ Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld	Joint Strength
					ĺ			Strength	
Surface	1,800'	13- 3/8"	54.50	J-55	BTC	1130	2730	853,000	909,000

Intermediate Casing:

	<u> </u>	Carac	<u>c ousing</u>						
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
			-			psi	Yld psi	Yld	Strength
						_		Strength	-
Surface	5,600'	9-	47#	HCL-	BTC	5,740	6,870	1,086,000	1,122,000
		5/8"		80					
	Intermediate Liner:								
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
_						psi	Yld psi	Yld	Strength
						-		Strength	_
Surface	10,700	7"	32#	P-	BTC	11,890	12,450	1,025,000	1,053,000
				110HC					

Production Casing:

Тор	Bottom	Size	Weight/Ft	Grade	Thread		Internal	Body	Joint
						psi	Yld psi	Yld	Strength
								Strength	
10,200	19,073	4-	13.5#	P-110	BTC	10,690	12,420	422,000	443,000
		1/2"							

1.4.2 Proposed Cement Program

Conductor: Grout to Surface (est. 8 cu. yds on backside)

13-3/8" Surface:

Studies Certing Studies							
LEAD							
Top of MD	0						
Bottom of MD	1600						
Cement Type	Class C						
Additives	4%Bentonite, 0.4 pps Defoamer,						
	0.125 pps Cellophane, 9.102 H2O						
	GPS						
# of SKS	1300						
Yield (ft3/sk)	1.72						
Density (lbs/gal)	13.5						
Volume (ft3)	2236						
Excess (%)	100%						
	TAIL						
Top of MD	1600						
Bottom of MD	1800						
Cement Type	Class C Neat						
Additives	6.304 H2O GPS						
# of SKS	200						
Yield (ft3/sk)	1.32						
Density (lbs/gal)	14.8						
Volume (ft3)	264						
Excess (%)	60%						

<u>9-5/8" Intermediate (No DV Tool):</u>

Internectiete Cesing String	
LEAD	
Top of MD	0
Bottom of MD	5000
Cement Type	35:65 POZ-Class C
Additives	6% Bentonite, 0.5% Fluidloss,
	0.15% Retarder, 0.4pps
	Defoamer, 10.542 H2O GPS
# of SKS	1700
Yield (ft3/sk)	1.94
Density (lbs/gal)	12.6
Volume (ft3)	3298
Excess (%)	180%
TAIL	
Top of MD	5000
Bottom of MD	5600
Cement Type	Class H
Additives	0.3% Fluidloss, 5.216 H2O GPS
# of SKS	350
Yield (ft3/sk)	1.18
Density (lbs/gal)	15.6
Volume (ft3)	413
Excess (%)	140%

9-5/8" Intermediate (With 1 DV Tool):

Internetiate Cashig Stidug	
*Stage 1	
LEAD	
Top of MD	0
Bottom of MD	5000
Cement Type	35:65 POZ-Class C
Additives	6% Bentonite, 0.5% Fluidloss,
	0.15% Retarder, 0.4pps
	Defoamer, 10.542 H2O GPS
# of SKS	1700
Yield (ft3/sk)	1.94
Density (lbs/gal)	12.6

Excess (%) 180% TAIL TAIL Top of MD 500 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O CPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	Volume (ft3)	3298
TAIL Top of MD 500 Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2		
Bottom of MD 5600 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2		
Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	Top of MD	500
Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	Bottom of MD	5600
# of SKS 350 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	Cement Type	Class H
Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	Additives	0.3% Fluidloss, 5.216 H2O GPS
Density (lbs/gal) 15.6 Volume (ft3) 413 Excess (%) 140% *Stage 2	# of SKS	350
Volume (ft3) 413 Excess (%) 140% *Stage 2	Yield (ft3/sk)	1.18
Excess (%) 140% *Stage 2 Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3500 Bottom of MD 3500 200% Stage 200% Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Stage 200% Stage 200% Top of MD 3900 Gement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236 236 Stage 200	Density (lbs/gal)	15.6
*Stage 2 Stage Tool Depth +/- 3900' LEAD Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Volume (ft3)	413
Stage Tool Depth +/- 3900' LEAD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Excess (%)	140%
LEADTop of MD0Bottom of MD3500Cement Type35:65 POZ-Class CAdditives6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS# of SKS1200Yield (ft3/sk)1.94Density (lbs/gal)12.6Volume (ft3)2328Excess (%)200%TAILTop of MD3500Bottom of MD3900Cement TypeClass HAdditives0.3% Fluidloss, 5.216 H2O GPS# of SKS200Yield (ft3/sk)1.18Density (lbs/gal)15.6Volume (ft3)236		
Top of MD 0 Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Stage Tool Depth	+/- 3900'
Bottom of MD 3500 Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236		
Cement Type 35:65 POZ-Class C Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Vield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Top of MD	0
Additives 6% Bentonite, 0.5% Fluidloss, 0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Bottom of MD	3500
0.15% Retarder, 0.4pps Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Cement Type	35:65 POZ-Class C
Defoamer, 10.543 H2O GPS # of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Additives	
# of SKS 1200 Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236		
Yield (ft3/sk) 1.94 Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236		Defoamer, 10.543 H2O GPS
Density (lbs/gal) 12.6 Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236		1200
Volume (ft3) 2328 Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Yield (ft3/sk)	1.94
Excess (%) 200% TAIL Top of MD 3500 Bottom of MD 3900 Cement Type Class H Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Density (lbs/gal)	12.6
TAILTop of MD3500Bottom of MD3900Cement TypeClass HAdditives0.3% Fluidloss, 5.216 H2O GPS# of SKS200Yield (ft3/sk)1.18Density (lbs/gal)15.6Volume (ft3)236	Volume (ft3)	2328
Top of MD3500Bottom of MD3900Cement TypeClass HAdditives0.3% Fluidloss, 5.216 H2O GPS# of SKS200Yield (ft3/sk)1.18Density (lbs/gal)15.6Volume (ft3)236	Excess (%)	200%
Bottom of MD3900Cement TypeClass HAdditives0.3% Fluidloss, 5.216 H2O GPS# of SKS200Yield (ft3/sk)1.18Density (lbs/gal)15.6Volume (ft3)236	TAIL	
Cement TypeClass HAdditives0.3% Fluidloss, 5.216 H2O GPS# of SKS200Yield (ft3/sk)1.18Density (lbs/gal)15.6Volume (ft3)236	Top of MD	3500
Additives 0.3% Fluidloss, 5.216 H2O GPS # of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Bottom of MD	3900
# of SKS 200 Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Cement Type	Class H
Yield (ft3/sk) 1.18 Density (lbs/gal) 15.6 Volume (ft3) 236	Additives	0.3% Fluidloss, 5.216 H2O GPS
Density (lbs/gal)15.6Volume (ft3)236	# of SKS	200
Volume (ft3) 236	Vield (ft3/sk)	1.18
Excess (%) 100%		
	Density (lbs/gal)	15.6
9-5/8" Intermediate (With 2 DV Tools):

ມີເຫັດຄະບານເປັນ	Cesing Stang				
*Stage 1	Charlonday Charles				
	AD				
Top of MD	0				
Bottom of MD	5000				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.542 H2O GPS				
# of SKS	1700				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	3298				
Excess (%)	180%				
	AIL				
Top of MD	5000				
Bottom of MD	5600				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	350				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	413				
Excess (%)	140%				
*Stage 2					
Stage Tool Depth	+/- 3900'				
	AD				
Top of MD	0				
Bottom of MD	3500				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.543 H2O GPS				
# of SKS	1200				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	2328				
Excess (%)	200%				
Т.	AIL				
Top of MD	3500				

.

Bottom of MD	3900				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	200				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	236				
Excess (%)	100%				
*Stage 3					
Stage Tool Depth	+/- 1900'				
T.	AIL				
Top of MD	0				
Bottom of MD	1900				
Cement Type	Class C Neat				
Additives	6.304 H2O GPS				
# of SKS	700				
Yield (ft3/sk)	1.32				
Density (lbs/gal)	14.8				
Volume (ft3)	924				
Excess (%)	30%				

<u>**7" Intermediate Liner:**</u>

hitermechaie Castug: String						
LEAD						
Top of MD	0					
Bottom of MD	5300					
Cement Type	Class H					
Additives	0.2% Retarder, 6.3 H2O GPS					
# of SKS	820					
Yield (ft3/sk)	1.18					
Density (lbs/gal)	15.6					
Volume (ft3)	968					
Excess (%)	15%					
Т	AIL					
Top of MD	5300					
Bottom of MD	10,700					
Cement Type	PVL					
Additives	1.3% Salt, 5% Expanding					
	Cement, 0.5% Fluidloss, 0.3%					
	Retarder, 0.1% Antisettling,					
	0.4 pps Defoamer, 8.621 H2O					

	GPS
# of SKS	550
Yield (ft3/sk)	1.62
Density (lbs/gal)	12.6
Volume (ft3)	891
Excess (%)	30%

4-1/2" Production Liner:

Production Casting String								
TAIL								
Top of MD	10,200							
Bottom of MD	19,073							
Cement Type	50:50 POZ-Class H							
Additives	5% Salt, 2% Bentonite, 0.5%							
	Fluidloss, 0.2% Retarder, 0.2%							
	Dispersant, 0.4pps Defoamer,							
	6.088 H2O GPS							
# of SKS	750							
Yield (ft3/sk)	1.34							
Density (lbs/gal)	14.2							
Volume (ft3)	1005							
Excess (%)	30%							

Cement volumes are based on bringing cement to surface on all strings and TOC to $\sim 10,200$ ' (top of liner) on production.

Operator reserves the right to change cement designs as hole conditions may warrant.

1.5 Proposed Mud Program

<u>Top</u> <u>TVD</u>	Bottom TVD	<u>Туре</u>	<u>Max Mud</u> <u>Weight for</u> <u>Hole Control</u> <u>Design</u>	<u>Viscosity</u> (sec/qt)
SURFACE	1,800	Fresh Water	9.0	28-38
1800	5,600	Brine	10.0	28-30
5,600	10,700	Cut Brine	9.2	28-30
10,700	TD	OBM	11.0	55-65

The operator must include the minimum design criteria, including casing loading assumptions and corresponding safety factors for burst, collapse, and tensions (body yield, and joint strength).

1.6 Casing Design

1.6.1 Drilling Design Analysis

Interval	Max	Anticipated	Estimated	Internal	Collapse	Joint	Body	Burst	Collpase	Tensile
	TVD	Mud	Max Pore	Yield	Strength	Strength	Strength	Safety	Safety	Safety
	(ft)	Weight	Pressure	Strength	(psi)	(lbs)	(lbs)	Factor	Factor (Min	Factor
		(ppg)	(psi)	(psi)				(Min 1.25)	1.25)	(Min 1.6)
Surface	1,800	8.5	780	2,730	1,130	909,000	853,000	3.5	1.42	4.3
Interm.	5,600	10	2,420	6,870	5,740	1,122,000	1,086,000	1.34	1.97	2.99
Interm.	10,700	9.0	4,730	12,450	11,890	1,053,000	1,025,000	1.98	2.31	2.31
Liner	1									· · · · ·
Prod.	11,800	11.5	5,880	12,420	10,690	443,000	422,000	1.25	1.51	1.63

Surface Casing Design Notes:

- Burst Design Assumptions: Calculations assume complete evacuation behind pipe.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Casing Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Liner w/ Tie-Back Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Production Design Notes:

- Burst Design Assumptions: Calculations assume surface frac pressure of 9500 psi along with a fluid gradient of 0.49psi/ft, with an external force equivalent to 0.44 psi/ft.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

*Notes:

- 1) Collapse DSF: If < 1.125 calculations are required.
- 2) Burst DSF: If < 1.0 calculations are required.
- 3) Body Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- Joint Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 5) Will an offset pressure variance request be requested to meet safety factors? Max. 0.22 psi/ft. Please indicate offset pressure variance requested.

Mud weight increases at shoe depths are for pressure control. Mud weight increases in the curve and lateral sections of the hole are for hole stability, not pressure control. Mud weight assumptions for casing load designs exceed anticipated maximum mud weight for balanced drilling in all hole sections. Expected mud weights in the Lower Wolfcamp Horizontal will be 0.5 to 1.0 ppg greater than formation pressure (i.e. overbalanced drilling.)

The Mud System will run as a closed loop system with PVT monitoring. All drill cuttings and liquid mud will be hauled to an approved NMOCD site for disposal or soil farm upon receiving appropriate approval.

1.7 Completion Program and Casing Design

Hydraulic fracturing will occur through the production casing. The burst design calculation assumes TOC at surface and therefore, the backside of the production casing is not evacuated. The maximum pumping pressure is 10,000 psi with a maximum proppant fluid weight of 9.5 ppg. The design safety factor for burst is 1.25.

Upon request, operator will provide proof of cement bonding by bond log. Operator is responsible for log interpretation and certification prior to frac treatment.

Upon request, operator will provide estimated fracture lengths, flowback storage, volumes of fluids and amount of sand to be used, and number of stages of frac procedure. Furthermore, a report of the annulus pressures before and after each stage of treatment may be requested by the BLM. The report may include chemical additives (other than proprietary), dissolved solids in frac fluid, and depth of perforations.

1.8 Evaluation Program

Required Testing, Logging, and Coring procedures noted below:

- Mud Logging/Gamma Ray/MWD.
- Cased hole CBL on production casing.

1.9 Downhole Conditions

Zones of possible lost circulation: Zones of possible abnormal pressure: Maximum bottom hole temperature: Maximum bottom hole pressure: Capitan Reef Lower Wolfcamp 205° F 6,750 psi or less.

1.10 Overview of Drilling Procedure

- Drill 17.5" surface hole to 1,800'; run 13.375" casing to 1,800' and cement to surface; install 10M stack, set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 12.25" intermediate hole to 5,600', run 9.625" casing and cement; set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 8-1/2" intermediate hole to approximately 10,700' and run 7" liner with a tie-back sleeve, and cement to top of liner set at +/- 5,300'.
- Drill 6" production hole to +/- 19,100'; run 4.5" liner from TD to +/- 10,200' and cement per cement program and test.
- Run 7" tie-back string from +/- 5300' to surface and cement per cement program, circulate cement to surface.

1.11 Overview of Completion for Equipment Sizing

• A Sundry Notice will be submitted with the proposed completion procedure prior to the job.

DRILLING PROGRAM

Operator: LEGACY RESERVES OPERATING LP

Project Name: LEA UNIT 200H

Project Location:

Lea County, New Mexico

Prepared By:

Matt Dickson Drilling Engineer

Submitted To:

Bureau of Land Management Carlsbad Field Office

Please address inquiries, questions, scheduling of meetings and deficiency statements, if any, to Scott St. John and/or Monica Smith Griffin at the address shown below:

Reagan Smith Energy Solutions, Inc. 1219 Classen Drive Oklahoma City, OK 73103 405-286-9326

sstjohn@rsenergysolutions.com msmith@rsenergysolutions.com

1.0 Drilling Program

-

1.1 Estimated Formation Tops

FORMETION	TVD @	TVD	TVD @		
FORMATION	<u>Surface Loc</u>	@ KB	<u>TD</u>		
Rustler	1,700'	1,728'	1,728'		
Yates	3,424'	3,452'	3,452'		
Seven Rivers	3,809'	3,837'	3,837'		
Queen	4,632'	4,660'	4,660'		
Bell Canyon	5,588'	5,616'	5,616'		
Cherry Canyon	6,471'	6,499'	6,499'		
Brushy Canyon	7,107'	7,135'	7,135'		
Bone Spring	8,191'	8,219'	8,219'		
Avalon Shale	8,782'	8,810'	8,810'		
l st BS	9,504'	9,532'	9,532'		
2 nd BS	10,041'	10,069'	10,069'		
3 rd BS	10,699'	10,727'	10,727'		
Wolfcamp	11,009'	11,037'	11,037'		
Upper Wolfcamp	11,212'	11,240'	11,240'		
Lower Wolfcamp	11,678'	11,698	11,800		

Target Formation and Total Depth:

The total depth of the proposed well is approximately 19,100' MD located in the Upper Wolfcamp.

According to New Mexico EMNRD 19.15.15.9 NMAC a well shall be located no closer than 330' feet to a boundary of the unit.

1.2 Estimated Depths of Anticipated Fresh Water, Oil, and Gas

Substance	<u>Depth</u>
Fresh Water	0' to 250'
Base of Treatable Water	125'
Hydrocarbons	8,191' to TD

1.2.2 State Water Protection Compliance

Bureau of Land Management requires surface casing to be set at a minimum of 25' into the Rustler Anhydrite and above the salt section. Operator proposes to set the surface casing at a depth of 1800' (measured from the surface) and use 13-3/8" casing.

Special Capitan Reef requirements

If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.

1.3 Pressure Control Equipment

Ten thousand (10M) psi working pressure Blind Rams and Pipe Rams and a five thousand (5M) psi Annular Preventer will be installed on all casing. Three (3) chokes; two (2) hydraulic and one (1) manual, will be used.

A variance to the requirement of a rigid steel line connecting to the choke manifold is requested. Specifications for the flex hose are provided with BOP schematic in exhibit section.

A third party testing company will conduct pressure tests and record prior to drilling out below 13-3/8s" casing. The BOP, Choke, Choke Manifold, Top Drive Valves and Floor Safety Valves will be tested to 5000 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of working pressure (5,000 psi) prior to drilling below the 9-5/8" intermediate casing shoe.

In addition, the BOP equipment will be tested after any repairs to the equipment as well as drilling out below any casing string. Pipe rams, blind rams, and annular preventer will be activated on each trip, and weekly BOP drills will be held with each crew. Floor Safety Valves that are full open and sized to fit Drill Pipe and Collars will be available on the rig floor in the open position when the Kelly is not in use.

1.4 Proposed Casing and Cementing Program

Interval	Depth	Size	Weight/ft	Grade	Thread	Condition	Hole size	Wash out factor	Cement Yield
Conductor	120'	20"	94.00#	H-40		New	26"		Grout
Surface	1,800'	13-3/8"	54.50#	J-55	BTC	New	17-1/2"	100	1.72/1.32 cu. Ft/sk
Intermediate	5,600'	9-5/8"	47#	HCL-80	BTC	New	12-1/4"	150	1.94/1.18 cu. Ft/sk
Intermediate Liner	10,700	7"	32.00#	P-110HC	BTC	New	8-1/2"	30	1.62 cu. Ft/sk
Production	19,100'	4-1/2"	13.5#	P-110	BTC	New	6"	30	1.34 cu. Ft/sk

1.4.1 Proposed Casing Program

Conductor: 20", H-40# line pipe to a depth of 120'. Wall thickness of 0.250".

Surface Casing:

		<u> </u>							
Тор	Bottom	Size	Weight/ Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld	Joint Strength
								Strength	
Surface	1,800'	13- 3/8"	54.50	J-55	BTC	1130	2730	853,000	909,000

Intermediate Casing:

	THETH	culai	<u>e Casiliy</u>	•							
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint		
-						psi	Yld psi	Yld	Strength		
						-	-	Strength	_		
Surface	5,600'	9-	47#	HCL-	BTC	5,740	6,870	1,086,000	1,122,000		
		5/8"		80							
	Intermediate Liner:										
Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint		
-			-			psi	Yld psi	Yld	Strength		
								Strength			
Surface	10,700	7"	32#	P-	BTC	11,890	12,450	1,025,000	1,053,000		
				110HC			1				

Production Casing:

Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld	Joint Strength
								Strength	
10,200	19,073	4- 1/2"	13.5#	P-110	BTC	10,690	12,420	422,000	443,000

.

1.4.2 Proposed Cement Program

<u>Conductor:</u> Grout to Surface (est. 8 cu. yds on backside)

13-3/8" Surface:

Studies Casing Studie						
LEAD						
Top of MD	0					
Bottom of MD	1600					
Cement Type	Class C					
Additives	4%Bentonite, 0.4 pps Defoamer,					
	0.125 pps Cellophane, 9.102 H2O					
	GPS					
# of SKS	1300					
Yield (ft3/sk)	1.72					
Density (lbs/gal)	13.5					
Volume (ft3)	2236					
Excess (%)	100%					
Т	AIL					
Top of MD	1600					
Bottom of MD	1800					
Cement Type	Class C Neat					
Additives	6.304 H2O GPS					
# of SKS	200					
Yield (ft3/sk)	1.32					
Density (lbs/gal)	14.8					
Volume (ft3)	264					
Excess (%)	60%					

9-5/8" Intermediate (No DV Tool):

Intermediate Castug String							
LEAD							
Top of MD	0						
Bottom of MD	5000						
Cement Type	35:65 POZ-Class C						
Additives	6% Bentonite, 0.5% Fluidloss,						
	0.15% Retarder, 0.4pps						
	Defoamer, 10.542 H2O GPS						
# of SKS	1700						
Yield (ft3/sk)	1.94						
Density (lbs/gal)	12.6						
Volume (ft3)	3298						
Excess (%)	180%						
<u> </u>	AIL						
Top of MD	5000						
Bottom of MD	5600						
Cement Type	Class H						
Additives	0.3% Fluidloss, 5.216 H2O GPS						
# of SKS	350						
Yield (ft3/sk)	1.18						
Density (lbs/gal)	15.6						
Volume (ft3)	413						
Excess (%)	140%						

9-5/8" Intermediate (With 1 DV Tool):

	murediate Casing String
*Stage 1	
	LEAD
Top of MD	0
Bottom of MD	5000
Cement Type	35:65 POZ-Class C
Additives	6% Bentonite, 0.5% Fluidloss,
	0.15% Retarder, 0.4pps
	Defoamer, 10.542 H2O GPS
# of SKS	1700
Yield (ft3/sk)	1.94
Density (lbs/gal)	12.6

Volume (ft3)	3298			
Excess (%)	180%			
	AIL			
Top of MD	500			
Bottom of MD	5600			
Cement Type	Class H			
Additives	0.3% Fluidloss, 5.216 H2O GPS			
# of SKS	350			
Yield (ft3/sk)	1.18			
Density (lbs/gal)	15.6			
Volume (ft3)	413			
Excess (%)	140%			
*Stage 2				
Stage Tool Depth	+/- 3900'			
LE	AD			
Top of MD	0			
Bottom of MD	3500			
Cement Type	35:65 POZ-Class C			
Additives	6% Bentonite, 0.5% Fluidloss,			
	0.15% Retarder, 0.4pps			
	Defoamer, 10.543 H2O GPS			
# of SKS	1200			
Yield (ft3/sk)	1.94			
Density (lbs/gal)	12.6			
Volume (ft3)	2328			
Excess (%)	200%			
T <i>I</i>	AIL			
Top of MD	3500			
Bottom of MD	3900			
Cement Type	Class H			
Additives	0.3% Fluidloss, 5.216 H2O GPS			
# of SKS	200			
Yield (ft3/sk)	1.18			
Density (lbs/gal)	15.6			
Volume (ft3)	236			

9-5/8" Intermediate (With 2 DV Tools):

liniammadiata	Cosing Shing				
*Stage 1	(*************************************				
	AD				
Top of MD	0				
Bottom of MD	5000				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.542 H2O GPS				
# of SKS	1700				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	3298				
Excess (%)	180%				
T2	AIL				
Top of MD	5000				
Bottom of MD	5600				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	350				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	413				
Excess (%)	140%				
*Stage 2					
Stage Tool Depth	+/- 3900'				
	AD				
Top of MD	0				
Bottom of MD	3500				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.543 H2O GPS				
# of SKS	1200				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	2328				
Excess (%)	200%				
	AIL				
Top of MD	3500				

Bottom of MD	3900				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	200				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	236				
Excess (%)	100%				
*Stage 3					
Stage Tool Depth +/- 1900'					
TAIL					
Top of MD	0				
Bottom of MD	1900				
Cement Type	Class C Neat				
Additives	6.304 H2O GPS				
# of SKS	700				
Yield (ft3/sk)	1.32				
Density (lbs/gal)	14.8				
Volume (ft3)	924				
Excess (%)	30%				

<u>**7" Intermediate Liner:**</u>

Internediate	Casing String
LE	AD
Top of MD	0
Bottom of MD	5300
Cement Type	Class H
Additives	0.2% Retarder, 6.3 H2O GPS
# of SKS	820
Yield (ft3/sk)	1.18
Density (lbs/gal)	15.6
Volume (ft3)	968
Excess (%)	15%
	AIL
Top of MD	5300
Bottom of MD	10,700
Cement Type	PVL
Additives	1.3% Salt, 5% Expanding
	Cement, 0.5% Fluidloss, 0.3%
	Retarder, 0.1% Antisettling,
	0.4 pps Defoamer, 8.621 H2O

	GPS
# of SKS	550
Yield (ft3/sk)	1.62
Density (lbs/gal)	12.6
Volume (ft3)	891
Excess (%)	30%

4-1/2" Production Liner:

Fueduction	Cesing Subag						
TAIL							
Top of MD	10,200						
Bottom of MD	19,073						
Cement Type	50:50 POZ-Class H						
Additives	5% Salt, 2% Bentonite, 0.5%						
	Fluidloss, 0.2% Retarder, 0.2%						
	Dispersant, 0.4pps Defoamer,						
	6.088 H2O GPS						
# of SKS	750						
Yield (ft3/sk)	1.34						
Density (lbs/gal)	14.2						
Volume (ft3)	1005						
Excess (%)	30%						

Cement volumes are based on bringing cement to surface on all strings and TOC to $\sim 10,200'$ (top of liner) on production.

Operator reserves the right to change cement designs as hole conditions may warrant.

1.5 Proposed Mud Program

<u>Top</u> TVD			<u>Max Mud</u> <u>Weight for</u> <u>Hole Control</u> <u>Design</u>	<u>Viscosity</u> (sec/qt)	
SURFACE	1,800	Fresh Water	9.0	28-38	
1800	5,600	Brine	10.0	28-30	
5,600	10,700	Cut Brine	9.2	28-30	
10,700	TD	OBM	11.0	55-65	

The operator must include the minimum design criteria, including casing loading assumptions and corresponding safety factors for burst, collapse, and tensions (body yield, and joint strength).

1.6 Casing Design

1.6.1 Drilling Design Analysis

Interval	Max	Anticipated	Estimated	Internal	Collapse	Joint	Body	Burst	Collpase	Tensile
	TVD	Mud	Max Pore	Yield	Strength	Strength	Strength	Safety	Safety	Safety
	(ft)	Weight	Pressure	Strength	(psi)	(lbs)	(lbs)	Factor	Factor (Min	Factor
		(ppg)	(psi)	(psi)				(Min 1.25)	1.25)	(Min 1.6)
Surface	1,800	8.5	780	2,730	1,130	909,000	853,000	3.5	1.42	4.3
Interm.	5,600	10	2,420	6,870	5,740	1,122,000	1,086,000	1.34	1.97	2.99
Interm.	10,700	9.0	4,730	12,450	11,890	1,053,000	1,025,000	1.98	2.31	2.31
Liner			•							
Prod.	11,800	11.5	5,880	12,420	10,690	443,000	422,000	1.25	1.51	1.63

Surface Casing Design Notes:

- Burst Design Assumptions: Calculations assume complete evacuation behind pipe.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Casing Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Liner w/ Tie-Back Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Production Design Notes:

- Burst Design Assumptions: Calculations assume surface frac pressure of 9500 psi along with a fluid gradient of 0.49psi/ft, with an external force equivalent to 0.44 psi/ft.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

*Notes:

- 1) Collapse DSF: If < 1.125 calculations are required.
- 2) Burst DSF: If < 1.0 calculations are required.
- 3) Body Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 4) Joint Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 5) Will an offset pressure variance request be requested to meet safety factors? Max. 0.22 psi/ft. Please indicate offset pressure variance requested.

Mud weight increases at shoe depths are for pressure control. Mud weight increases in the curve and lateral sections of the hole are for hole stability, not pressure control. Mud weight assumptions for casing load designs exceed anticipated maximum mud weight for balanced drilling in all hole sections. Expected mud weights in the Lower Wolfcamp Horizontal will be 0.5 to 1.0 ppg greater than formation pressure (i.e. overbalanced drilling.)

The Mud System will run as a closed loop system with PVT monitoring. All drill cuttings and liquid mud will be hauled to an approved NMOCD site for disposal or soil farm upon receiving appropriate approval.

1.7 Completion Program and Casing Design

Hydraulic fracturing will occur through the production casing. The burst design calculation assumes TOC at surface and therefore, the backside of the production casing is not evacuated. The maximum pumping pressure is 10,000 psi with a maximum proppant fluid weight of 9.5 ppg. The design safety factor for burst is 1.25.

Upon request, operator will provide proof of cement bonding by bond log. Operator is responsible for log interpretation and certification prior to frac treatment.

Upon request, operator will provide estimated fracture lengths, flowback storage, volumes of fluids and amount of sand to be used, and number of stages of frac procedure. Furthermore, a report of the annulus pressures before and after each stage of treatment may be requested by the BLM. The report may include chemical additives (other than proprietary), dissolved solids in frac fluid, and depth of perforations.

1.8 Evaluation Program

Required Testing, Logging, and Coring procedures noted below:

- Mud Logging/Gamma Ray/MWD.
- Cased hole CBL on production casing.

1.9 Downhole Conditions

Zones of possible lost circulation: Zones of possible abnormal pressure: Maximum bottom hole temperature: Maximum bottom hole pressure: Capitan Reef Lower Wolfcamp 205° F 6,750 psi or less.

1.10 Overview of Drilling Procedure

- Drill 17.5" surface hole to 1,800'; run 13.375" casing to 1,800' and cement to surface; install 10M stack, set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 12.25" intermediate hole to 5,600', run 9.625" casing and cement; set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 8-1/2" intermediate hole to approximately 10,700' and run 7" liner with a tie-back sleeve, and cement to top of liner set at +/- 5,300'.
- Drill 6" production hole to +/- 19,100'; run 4.5" liner from TD to +/- 10,200' and cement per cement program and test.
- Run 7" tie-back string from +/- 5300' to surface and cement per cement program, circulate cement to surface.

1.11 Overview of Completion for Equipment Sizing

• A Sundry Notice will be submitted with the proposed completion procedure prior to the job.

DRILLING PROGRAM

Operator: LEGACY RESERVES OPERATING LP

> Project Name: LEA UNIT 200H

Project Location: Lea County, New Mexico

Prepared By: Matt Dickson

Drilling Engineer

Submitted To:

Bureau of Land Management Carlsbad Field Office

Please address inquiries, questions, scheduling of meetings and deficiency statements, if any, to Scott St. John and/or Monica Smith Griffin at the address shown below:

Reagan Smith Energy Solutions, Inc. 1219 Classen Drive Oklahoma City, OK 73103 405-286-9326

sstjohn@rsenergysolutions.com msmith@rsenergysolutions.com

1.0 Drilling Program

1.1 Estimated Formation Tops

FORMATION	TVD @	TVD	TVD @
FORMATION	Surface Loc	@ KB	<u>TD</u>
Rustler	1,700'	1,728'	1,728'
Yates	3,424'	3,452'	3,452'
Seven Rivers	3,809'	3,837'	3,837'
Queen	4,632'	4,660'	4,660'
Bell Canyon	5,588'	5,616'	5,616'
Cherry Canyon	6,471'	6,499'	6,499'
Brushy Canyon	7,107'	7,135'	7,135'
Bone Spring	8,191'	8,219'	8,219'
Avalon Shale	8,782'	8,810'	8,810'
l st BS	9,504'	9,532'	9,532'
2 nd BS	10,041'	10,069'	10,069'
3 rd BS	10,699'	10,727'	10,727'
Wolfcamp	11,009'	11,037'	11,037'
Upper Wolfcamp	11,212'	11,240'	11,240'
Lower Wolfcamp	11,678'	11,698	11,800

Target Formation and Total Depth:

The total depth of the proposed well is approximately 19,100' MD located in the Upper Wolfcamp.

According to New Mexico EMNRD 19.15.15.9 NMAC a well shall be located no closer than 330' feet to a boundary of the unit.

1.2 Estimated Depths of Anticipated Fresh Water, Oil, and Gas

Substance	<u>Depth</u>
Fresh Water	0' to 250'
Base of Treatable Water	125'
Hydrocarbons	8,191' to TD

1.2.2 State Water Protection Compliance

Bureau of Land Management requires surface casing to be set at a minimum of 25' into the Rustler Anhydrite and above the salt section. Operator proposes to set the surface casing at a depth of 1800' (measured from the surface) and use 13-3/8" casing.

Special Capitan Reef requirements

If lost circulation (50% or greater) occurs below the Base of the Salt, the operator shall switch to fresh water mud to protect the Capitan Reef and use fresh water mud until setting the intermediate casing. The appropriate BLM office is to be notified for a PET to witness the switch to fresh water.

1.3 Pressure Control Equipment

Ten thousand (10M) psi working pressure Blind Rams and Pipe Rams and a five thousand (5M) psi Annular Preventer will be installed on all casing. Three (3) chokes; two (2) hydraulic and one (1) manual, will be used.

A variance to the requirement of a rigid steel line connecting to the choke manifold is requested. Specifications for the flex hose are provided with BOP schematic in exhibit section.

A third party testing company will conduct pressure tests and record prior to drilling out below 13-3/8s" casing. The BOP, Choke, Choke Manifold, Top Drive Valves and Floor Safety Valves will be tested to 5000 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of full working pressure (10,000 psi) prior to drilling below the 9-5/8s" intermediate casing shoe. The Annular Preventer will be tested to 2500 psi prior to drilling below the 13-3/8s" surface casing shoe and to 100% of working pressure (5,000 psi) prior to drilling below the 9-5/8" intermediate casing shoe.

In addition, the BOP equipment will be tested after any repairs to the equipment as well as drilling out below any casing string. Pipe rams, blind rams, and annular preventer will be activated on each trip, and weekly BOP drills will be held with each crew. Floor Safety Valves that are full open and sized to fit Drill Pipe and Collars will be available on the rig floor in the open position when the Kelly is not in use.

1.4 Proposed Casing and Cementing Program

Interval	Depth	Size	Weight/ft	Grade	Thread	Condition	Hole size	Wash out factor	Cement Yield
Conductor	120'	20"	94.00#	H-40		New	26"		Grout
Surface	1,800'	13-3/8"	54.50#	J-55	BTC	New	17-1/2"	100	1.72/1.32 cu. Ft/sk
Intermediate	5,600'	9-5/8"	47#	HCL-80	BTC	New	12-1/4"	150	1.94/1.18 cu. Ft/sk
Intermediate Liner	10,700	7"	32.00#	P-110HC	BTC	New	8-1/2"	30	l.62 cu. Ft/sk
Production	19,100'	4-1/2"	13.5#	P-110	BTC	New	6"	30	l.34 cu. Ft/sk

1.4.1 Proposed Casing Program

<u>**Conductor</u>**: 20", H-40# line pipe to a depth of 120'. Wall thickness of 0.250".</u>

<u>Surface Casing</u>:

		0.000							
Тор	Bottom	Size	Weight/ Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld Strength	Joint Strength
Surface	1,800'	13- 3/8"	54.50	J-55	BTC	1130	2730	853,000	909,000

Intermediate Casing:

Surface 5,600' 9- 5/8'' 47# HCL- 80 BTC 5,740 6,870 1,04 Intermediate Liner: 80 9 47# 100										
Surface 5,600' 9- 5/8'' 47# 80 HCL- 80 BTC 5,740 6,870 1,04 Intermediate Liner: 80 9- 47# 100	Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
Surface 5,600' 9- 5/8'' 47# 80 HCL- 80 BTC 5,740 6,870 1,08 Intermediate Liner: 80				-			psi	Yld psi	Yld	Strength
5/8" 80 Intermediate Liner:							_	_	Strength	-
Intermediate Liner:	Surface	5,600'	9-	47#	HCL-	BTC	5,740	6,870	1,086,000	1,122,000
			5/8"		80					
Top Bottom Size Weight/Ft Grade Thread Collapse Internal E		Intermediate Liner:								
	Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse	Internal	Body	Joint
psi Yld psi				-			psi	Yld psi	Yld	Strength
Str									Strength	
	Surface	10,700	7"	32#	P-	BTC	11,890	12,450	1,025,000	1,053,000

Production Casing:

Тор	Bottom	Size	Weight/Ft	Grade	Thread	Collapse psi	Internal Yld psi	Body Yld Strength	Joint Strength
10,200	19,073	4- 1/2"	13.5#	P-110	BTC	10,690	12,420	422,000	443,000

110HC

1.4.2 Proposed Cement Program

<u>Conductor:</u> Grout to Surface (est. 8 cu. yds on backside)

<u>13-3/8" Surface:</u>

Studes Casing Subag					
L	LEAD				
Top of MD	0				
Bottom of MD	1600				
Cement Type	Class C				
Additives	4%Bentonite, 0.4 pps Defoamer,				
	0.125 pps Cellophane, 9.102 H2O				
	GPS				
# of SKS	1300				
Yield (ft3/sk)	1.72				
Density (lbs/gal)	13.5				
Volume (ft3)	2236				
Excess (%)	100%				
7	'AIL				
Top of MD	1600				
Bottom of MD	1800				
Cement Type	Class C Neat				
Additives	6.304 H2O GPS				
# of SKS	200				
Yield (ft3/sk)	1.32				
Density (lbs/gal)	14.8				
Volume (ft3)	264				
Excess (%)	60%				

9-5/8" Intermediate (No DV Tool):

Intermodiate Casing String					
LEAD					
Top of MD	0				
Bottom of MD	5000				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.542 H2O GPS				
# of SKS	1700				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	3298				
Excess (%)	180%				
Т	AIL				
Top of MD	5000				
Bottom of MD	5600				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	350				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	413				
Excess (%)	140%				

9-5/8" Intermediate (With 1 DV Tool):

l liga	enmedicite Casho: Sudag
*Stage 1	
	LEAD
Top of MD	0
Bottom of MD	5000
Cement Type	35:65 POZ-Class C
Additives	6% Bentonite, 0.5% Fluidloss,
	0.15% Retarder, 0.4pps
	Defoamer, 10.542 H2O GPS
# of SKS	1700
Yield (ft3/sk)	1.94
Density (lbs/gal)	12.6

Volume (ft3)	3298
Excess (%)	180%
	TAIL
Top of MD	500
Bottom of MD	5600
Cement Type	Class H
Additives	0.3% Fluidloss, 5.216 H2O GPS
# of SKS	350
Yield (ft3/sk)	1.18
Density (lbs/gal)	15.6
Volume (ft3)	413
Excess (%)	140%
*Stage 2	
Stage Tool Depth	+/- 3900'
	LEAD
Top of MD	0
Bottom of MD	3500
Cement Type	35:65 POZ-Class C
Additives	6% Bentonite, 0.5% Fluidloss,
	0.15% Retarder, 0.4pps
	Defoamer, 10.543 H2O GPS
# of SKS	1200
Yield (ft3/sk)	1.94
Density (lbs/gal)	12.6
Volume (ft3)	2328
Excess (%)	200%
	TAIL
Top of MD	3500
Bottom of MD	3900
Cement Type	Class H
Additives	0.3% Fluidloss, 5.216 H2O GPS
# of SKS	200
Yield (ft3/sk)	1.18
Density (lbs/gal)	15.6
Volume (ft3)	236
Excess (%)	100%

9-5/8" Intermediate (With 2 DV Tools):

	Casing Shing				
*Stage 1					
	AD				
Top of MD	0				
Bottom of MD	5000				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.542 H2O GPS				
# of SKS	1700				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	3298				
Excess (%)	180%				
TAIL					
Top of MD	5000				
Bottom of MD	5600				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	350				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	413				
Excess (%)	140%				
*Stage 2					
Stage Tool Depth	+/- 3900'				
LE	AD				
Top of MD	0				
Bottom of MD	3500				
Cement Type	35:65 POZ-Class C				
Additives	6% Bentonite, 0.5% Fluidloss,				
	0.15% Retarder, 0.4pps				
	Defoamer, 10.543 H2O GPS				
# of SKS	1200				
Yield (ft3/sk)	1.94				
Density (lbs/gal)	12.6				
Volume (ft3)	2328				
Excess (%)	200%				
	AIL				
Top of MD	3500				

Bottom of MD	3900				
Cement Type	Class H				
Additives	0.3% Fluidloss, 5.216 H2O GPS				
# of SKS	200				
Yield (ft3/sk)	1.18				
Density (lbs/gal)	15.6				
Volume (ft3)	236				
Excess (%)	100%				
*Stage 3					
Stage Tool Depth	+/- 1900'				
Т	TAIL				
Top of MD	0				
Bottom of MD	1900				
Cement Type	Class C Neat				
Additives	6.304 H2O GPS				
# of SKS	700				
Yield (ft3/sk)	1.32				
Density (lbs/gal)	14.8				
Volume (ft3)	924				
Excess (%)	30%				

<u>7" Intermediate Liner:</u>

Intermediate Caring String			
LEAD			
Top of MD	0		
Bottom of MD	5300		
Cement Type	Class H		
Additives	0.2% Retarder, 6.3 H2O GPS		
# of SKS	820		
Yield (ft3/sk)	1.18		
Density (lbs/gal)	15.6		
Volume (ft3)	968		
Excess (%)	15%		
T/	AIL		
Top of MD	5300		
Bottom of MD	10,700		
Cement Type	PVL		
Additives	1.3% Salt, 5% Expanding		
	Cement, 0.5% Fluidloss, 0.3%		
Retarder, 0.1% Antisettlir			
	0.4 pps Defoamer, 8.621 H2O		

	GPS
# of SKS	550
Yield (ft3/sk)	1.62
Density (lbs/gal)	12.6
Volume (ft3)	891
Excess (%)	30%

4-1/2" Production Liner:

Prôduction Casting Studig			
TAIL			
Top of MD	10,200		
Bottom of MD	19,073		
Cement Type	pe 50:50 POZ-Class H		
Additives	5% Salt, 2% Bentonite, 0.5%		
	Fluidloss, 0.2% Retarder, 0.2%		
	Dispersant, 0.4pps Defoamer,		
	6.088 H2O GPS		
# of SKS	750		
Yield (ft3/sk)	1.34		
Density (lbs/gal)	14.2		
Volume (ft3)	1005		
Excess (%)	30%		

Cement volumes are based on bringing cement to surface on all strings and TOC to $\sim 10,200$ ' (top of liner) on production.

Operator reserves the right to change cement designs as hole conditions may warrant.

1.5 Proposed Mud Program

Top TVD	<u>Bottom</u> <u>TVD</u>	Туре	<u>Max Mud</u> <u>Weight for</u> <u>Hole Control</u> <u>Design</u>	<u>Viscosity</u> (sec/qt)
SURFACE	1,800	Fresh Water	9.0	28-38
1800	5,600	Brine	10.0	28-30
5,600	10,700	Cut Brine	9.2	28-30
10,700	TD	OBM	11.0	55-65

The operator must include the minimum design criteria, including casing loading assumptions and corresponding safety factors for burst, collapse, and tensions (body yield, and joint strength).

1.6 Casing Design

1.6.1 Drilling Design Analysis

Interval	Max	Anticipated	Estimated	Internal	Collapse	Joint	Body	Burst	Collpase	Tensile
	TVD	Mud	Max Pore	Yield	Strength	Strength	Strength	Safety	Safety	Safety
	(ft)	Weight	Pressure	Strength	(psi)	(lbs)	(lbs)	Factor	Factor (Min	Factor
		(ppg)	(psi)	(psi)				(Min 1.25)	1.25)	(Min 1.6)
Surface	1,800	8.5	780	2,730	1,130	909,000	853,000	3.5	1.42	4.3
Interm.	5,600	10	2,420	6,870	5,740	1,122,000	1,086,000	1.34	1.97	2.99
Interm.	10,700	9.0	4,730	12,450	11,890	1,053,000	1,025,000	1.98	2.31	2.31
Liner										
Prod.	11,800	11.5	5,880	12,420	10,690	443,000	422,000	1.25	1.51	1.63

Surface Casing Design Notes:

- Burst Design Assumptions: Calculations assume complete evacuation behind pipe.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Casing Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Intermediate Liner w/ Tie-Back Design Notes:

- Burst Design Assumptions: Calculations assume a .7psi/ft shoe test, and 0.22 psi/ft gas gradient.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

Production Design Notes:

- Burst Design Assumptions: Calculations assume surface frac pressure of 9500 psi along with a fluid gradient of 0.49psi/ft, with an external force equivalent to 0.44 psi/ft.
- Collapse Design Assumptions: Calculations assume complete evacuation inside pipe.
- Tension Design Assumptions: Calculations include 100,000 lb. max overpull and do not consider the effects of buoyancy, with string held in tension.

*Notes:

- 1) Collapse DSF: If < 1.125 calculations are required.
- 2) Burst DSF: If < 1.0 calculations are required.
- 3) Body Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 4) Joint Tensile DSF: If < 1.6 (dry) or < 1.8 (buoyant) calculations are required.
- 5) Will an offset pressure variance request be requested to meet safety factors? Max. 0.22 psi/ft. Please indicate offset pressure variance requested.

Mud weight increases at shoe depths are for pressure control. Mud weight increases in the curve and lateral sections of the hole are for hole stability, not pressure control. Mud weight assumptions for casing load designs exceed anticipated maximum mud weight for balanced drilling in all hole sections. Expected mud weights in the Lower Wolfcamp Horizontal will be 0.5 to 1.0 ppg greater than formation pressure (i.e. overbalanced drilling.)

The Mud System will run as a closed loop system with PVT monitoring. All drill cuttings and liquid mud will be hauled to an approved NMOCD site for disposal or soil farm upon receiving appropriate approval.

1.7 Completion Program and Casing Design

Hydraulic fracturing will occur through the production casing. The burst design calculation assumes TOC at surface and therefore, the backside of the production casing is not evacuated. The maximum pumping pressure is 10,000 psi with a maximum proppant fluid weight of 9.5 ppg. The design safety factor for burst is 1.25.

Upon request, operator will provide proof of cement bonding by bond log. Operator is responsible for log interpretation and certification prior to frac treatment.

Upon request, operator will provide estimated fracture lengths, flowback storage, volumes of fluids and amount of sand to be used, and number of stages of frac procedure. Furthermore, a report of the annulus pressures before and after each stage of treatment may be requested by the BLM. The report may include chemical additives (other than proprietary), dissolved solids in frac fluid, and depth of perforations.

1.8 Evaluation Program

Required Testing, Logging, and Coring procedures noted below:

- Mud Logging/Gamma Ray/MWD.
- Cased hole CBL on production casing.

1.9 Downhole Conditions

Zones of possible lost circulation: Zones of possible abnormal pressure: Maximum bottom hole temperature: Maximum bottom hole pressure: Capitan Reef Lower Wolfcamp 205° F 6,750 psi or less.

1.10 Overview of Drilling Procedure

- Drill 17.5" surface hole to 1,800'; run 13.375" casing to 1,800' and cement to surface; install 10M stack, set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 12.25" intermediate hole to 5,600', run 9.625" casing and cement; set isolation plug and test BOPE and casing independently to regulatory requirements.
- Drill 8-1/2" intermediate hole to approximately 10,700' and run 7" liner with a tie-back sleeve, and cement to top of liner set at +/- 5,300'.
- Drill 6" production hole to +/- 19,100'; run 4.5" liner from TD to +/- 10,200' and cement per cement program and test.
- Run 7" tie-back string from +/- 5300' to surface and cement per cement program, circulate cement to surface.

1.11 Overview of Completion for Equipment Sizing

• A Sundry Notice will be submitted with the proposed completion procedure prior to the job.



U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

SUPO Data Report

APD ID: 10400031426

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Type: OIL WELL

Submission Date: 06/22/2018

Well Number: 200H Well Work Type: Drill Alghildiwed deter Gleci's the most fecent changes

Show Final Text

Section 1 - Existing Roads

Will existing roads be used? YES

Existing Road Map:

200H_Location_Verification_Map_03_21_18_20180622133016.pdf

Existing Road Purpose: ACCESS, FLUID TRANSPORT

Row(s) Exist? YES

ROW ID(s)

ID:

Do the existing roads need to be improved? NO

Existing Road Improvement Description:

Existing Road Improvement Attachment:

Section 2 - New or Reconstructed Access Roads

Will new roads be needed? NO

Section 3 - Location of Existing Wells

Existing Wells Map? YES

Attach Well map:

One_Mile_Radius_Plat_20180622133041.pdf

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H

Existing Wells description:

Section 4 - Location of Existing and/or Prop	osed Production Facilities
Submit or defer a Proposed Production Facilities plan? DEFER	
Estimated Production Facilities description: Existing production facilit	ies will be utilized.
Section 5 - Location and Types of Water Sup	oly
Water Source Table	
Water source use type: INTERMEDIATE/PRODUCTION CASING, STIMULATION, SURFACE CASING Describe type:	Water source type: GW WELL
Source latitude:	Source longitude:
Source datum:	
Water source permit type: WATER WELL	
Source land ownership: PRIVATE	
Water source transport method: TRUCKING	
Source transportation land ownership: FEDERAL	
Water source volume (barrels): 10000	Source volume (acre-feet): 1.288931
Source volume (gal): 420000	
Water source use type: STIMULATION	Water source type: RAW PRODUCED
Describe type:	
Source latitude: 32.695213	Source longitude: -103.371185
Source datum: NAD83	
Water source permit type: PRIVATE CONTRACT	
Source land ownership: PRIVATE	
Water source transport method: TRUCKING	
Source transportation land ownership: STATE	
Water source volume (barrels): 3000	Source volume (acre-feet): 0.3866793
Source volume (gal): 126000	

Operator Name: LEGACY RESERVES OPERATING LP Well Name: LEA UNIT

Well Number: 200H

Water source and transportation map:

Lea_Unit_Water_Sources_Lower_20180622134757.pdf Water_Transportation_Plat_20180622134835.pdf Water source comments:

New water well? NO

New Water Well Info

Well latitude:	Well Longitude:	Well datum:
Well target aquifer:		
Est. depth to top of aquifer(ft):	Est thickness of aquife	r:
Aquifer comments:		
Aquifer documentation:		
Well depth (ft):	Well casing type:	
Well casing outside diameter (in.):	Well casing inside diamet	er (in.):
New water well casing?	Used casing source:	
Drilling method:	Drill material:	
Grout material:	Grout depth:	
Casing length (ft.):	Casing top depth (ft.):	
Well Production type:	Completion Method:	
Water well additional information:		
State appropriation permit:		
Additional information attachment:		

Section 6 - Construction Materials

Construction Materials description: CONSTRUCTION MATERIALS: CALICHE WILL BE USED TO CONSTRUCT THISWELL PAD Any construction material that may be required for surfacing of the drill pad will be from a contractor having a permitted source of materials within the general area. No construction materials will be removed from Federal lands without prior approval from the appropriate surface management agency. See attached for source information. **Construction Materials source location attachment:**

Section 7 - Methods for Handling Waste

Waste type: DRILLING

Waste content description: Drilling fluids (flowback, water, cuttings)

Amount of waste: 20000 barrels

Waste disposal frequency : Daily

Safe containment description: Drilling fluids will be contained in steel mud tanks.

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H

Safe containmant attachment:

Waste disposal type: HAUL TO COMMERCIAL Disposal location ownership: PRIVATE FACILITY

Disposal type description:

Disposal location description: NMOCD approved disposal site in Halfway, NM.

Reserve Pit

Reserve Pit being used? NO

.

Temporary disposal of produced water into reserve pit?

Reserve pit length (ft.)

Reserve pit depth (ft.)

Reserve pit volume (cu. yd.)

Is at least 50% of the reserve pit in cut?

Reserve pit liner

Reserve pit liner specifications and installation description

Cuttings Area

Reserve pit width (ft.)

Cuttings Area being used? NO

Are you storing cuttings on location? YES

Description of cuttings location Drill cuttings will be held in roll-off style mud boxes and taken to an NMOCD approved disposal site in Halfway, NM.

Cuttings area length (ft.)	Cuttings area width (ft.)

Cuttings area depth (ft.)

Cuttings area volume (cu. yd.)

Is at least 50% of the cuttings area in cut?

WCuttings area liner

Cuttings area liner specifications and installation description

Section 8 - Ancillary Facilities

Are you requesting any Ancillary Facilities?: NO

Ancillary Facilities attachment:

Comments:

Operator Name: LEGACY RESERVES OPERATING LP **Well Name:** LEA UNIT

Well Number: 200H

Section 9 - Well Site Layout

Well Site Layout Diagram:

200H_Well_Pad_Plat_03_21_18_20180622135255.pdf

Comments:

Section 10 - Plans for Surface Reclamation

Type of disturbance: No New Surface Disturbance Multiple Well Pad Name: LEA UNIT 100H

Multiple Well Pad Number: 7

Recontouring attachment:

Drainage/Erosion control construction: To mitigate erosion and protect the natural drainage areas, erosion control methods (e.g. cut and fill ratios of 3:1) will be implemented during the construction and production phases of this project. The slopes of the well pad may be reserved or replanted per agreement with the landowner. Erosion mitigation such as silt fences and hay bales will be located as necessary around the well pad.

Drainage/Erosion control reclamation: • The original landform will be restored for all disturbed areas including well pads, production facilities, roads, pipelines, and utility corridors. • A self-sustaining, vigorous, diverse, native (or otherwise approved) plant community will be established on the site, with a density sufficient to control erosion and invasion by non-native plants and to re-establish wildlife habitat or forage production. At a minimum, the established plant community will consist of species included in the seed mix and/or desirable species occurring in the surrounding natural vegetation. • Erosion features are equal to or less than surrounding area and erosion control is sufficient so that water naturally infiltrates into the soil and gullying, headcutting, slumping, and deep or excessive rills (greater than 3 inches) are not observed. • The site will be free of State- or county-listed noxious weeds, oil field debris and equipment, and contaminated soil. Invasive and non-native weeds are controlled.

Well pad proposed disturbance	Well pad interim reclamation (acres):	Well pad long term disturbance
(acres): 0 Road proposed disturbance (acres): 0		(acres): Road long term disturbance (acres):
Powerline proposed disturbance (acres): 0 Pipeline proposed disturbance (acres): 0 Other proposed disturbance (acres): 0	Powerline interim reclamation (acres): 0 Pipeline interim reclamation (acres): Other interim reclamation (acres):	Powerline long term disturbance (acres): 0 Pipeline long term disturbance (acres): Other long term disturbance (acres):
Total proposed disturbance: 0	Total interim reclamation:	Total long term disturbance:

Disturbance Comments: Existing pipeline & lease road will be utilized.

Reconstruction method: Final reclamation to achieve restoration of the original landform and a natural vegetative community. The original landform will be restored for all disturbed areas including well pads, production facilities, roads, pipelines, and utility corridors.

Topsoil redistribution: Topsoil will be redistributed after the well pad has been returned to original contours, or as close as practical.

Soil treatment: No soil treatment will be needed.

Existing Vegetation at the well pad:

Existing Vegetation at the well pad attachment:

Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H

Existing Vegetation Community at the road: Existing Vegetation Community at the road attachment: Existing Vegetation Community at the pipeline: Existing Vegetation Community at the pipeline attachment:

Existing Vegetation Community at other disturbances: Existing Vegetation Community at other disturbances attachment:

Non native seed used? NO

Non native seed description:

Seedling transplant description:

Will seedlings be transplanted for this project? NO

Seedling transplant description attachment:

Will seed be harvested for use in site reclamation? NO Seed harvest description: Seed harvest description attachment:

Seed Management

Seed Table

Seed type:

Seed name:

Source name:

Source phone:

Seed cultivar:

Seed use location:

PLS pounds per acre:

Proposed seeding season:

Seed source:

Source address:

Total pounds/Acre:

Seed Summary Seed Type Pounds/Acre

Seed reclamation attachment:

Operator Contact/Responsible Official Contact Info

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Operator Name: LEGACY RESERVES OPERATING LP

Well Name: LEA UNIT

Well Number: 200H

First Name: Scott

Phone: (405)286-9326

Last Name: St. John

Email: sstjohn@rsenergysolutions.com

Seedbed prep:

Seed BMP:

Seed method:

Existing invasive species? NO

Existing invasive species treatment description:

Existing invasive species treatment attachment:

Weed treatment plan description: Weeds will be mowed regularly to prevent them from becoming dominant within the project area

Weed treatment plan attachment:

Monitoring plan description: The project location will be periodically monitored by Legacy Reserves Operating, LP's staff that are responsible for infrastructure maintenance. **Monitoring plan attachment:**

Success standards: Develop sufficient plant and root coverage to maximize erosion and sediment control.

Pit closure description: No pit will be utilized for this project.

Pit closure attachment:

Section 11 - Surface Ownership

Disturbance type: WELL PAD

Describe:

Surface Owner: BUREAU OF LAND MANAGEMENT

Other surface owner description:

BIA Local Office:

BOR Local Office:

COE Local Office:

DOD Local Office:

NPS Local Office:

State Local Office:

Military Local Office:

USFWS Local Office:

Other Local Office:

USFS Region:

USFS Forest/Grassland:

USFS Ranger District:

Well Number: 200H

Section 12 - Other Information

Right of Way needed? NO

Use APD as ROW?

ROW Type(s):

ROW Applications

SUPO Additional Information:

Use a previously conducted onsite? YES

Previous Onsite information: An onsite was previously conducted for the existing Lea Unit #54H, Lea Unit #55H, and Lea Unit #56H pad. The Lea Unit 200H is located on this same well pad.

Other SUPO Attachment



Section 1 - General

Would you like to address long-term produced water disposal? NO

Section 2 - Lined Pits Would you like to utilize Lined Pit PWD options? NO **Produced Water Disposal (PWD) Location:** PWD surface owner: Lined pit PWD on or off channel: Lined pit PWD discharge volume (bbl/day): Lined pit specifications: Pit liner description: Pit liner manufacturers information: Precipitated solids disposal: Decribe precipitated solids disposal: Precipitated solids disposal permit: Lined pit precipitated solids disposal schedule: Lined pit precipitated solids disposal schedule attachment: Lined pit reclamation description: Lined pit reclamation attachment: Leak detection system description: Leak detection system attachment: Lined pit Monitor description: Lined pit Monitor attachment: Lined pit: do you have a reclamation bond for the pit? Is the reclamation bond a rider under the BLM bond? Lined pit bond number: Lined pit bond amount: Additional bond information attachment:

PWD disturbance (acres):

PWD Data Report

09/18/201

Section 3 - Unlined Pits

Would you like to utilize Unlined Pit PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Unlined pit PWD on or off channel:

Unlined pit PWD discharge volume (bbl/day):

Unlined pit specifications:

Precipitated solids disposal:

Decribe precipitated solids disposal:

Precipitated solids disposal permit:

Unlined pit precipitated solids disposal schedule:

Unlined pit precipitated solids disposal schedule attachment:

Unlined pit reclamation description:

Unlined pit reclamation attachment:

Unlined pit Monitor description:

Unlined pit Monitor attachment:

Do you propose to put the produced water to beneficial use?

Beneficial use user confirmation:

Estimated depth of the shallowest aquifer (feet):

Does the produced water have an annual average Total Dissolved Solids (TDS) concentration equal to or less than that of the existing water to be protected?

TDS lab results:

Geologic and hydrologic evidence:

State authorization:

Unlined Produced Water Pit Estimated percolation:

Unlined pit: do you have a reclamation bond for the pit?

Is the reclamation bond a rider under the BLM bond?

Unlined pit bond number:

Unlined pit bond amount:

Additional bond information attachment:

Section 4 - Injection

Would you like to utilize Injection PWD options? NO

Produced Water Disposal (PWD) Location:

PWD surface owner:

Injection PWD discharge volume (bbl/day):

Injection well mineral owner:

PWD disturbance (acres):

PWD disturbance (acres):

Injection well type: Injection well number: Assigned injection well API number? Injection well new surface disturbance (acres): Minerals protection information: Mineral protection attachment: Underground Injection Control (UIC) Permit? UIC Permit attachment:

Section 5 - Surface Discharge

Would you like to utilize Surface Discharge PWD options? NO

 Produced Water Disposal (PWD) Location:

 PWD surface owner:
 PWD disturbance (acres):

 Surface discharge PWD discharge volume (bbl/day):
 Surface Discharge NPDES Permit?

 Surface Discharge NPDES Permit attachment:
 Surface Discharge site facilities information:

 Surface discharge site facilities map:
 Section 6 - Other

Would you like to utilize Other PWD options? NO

Produced Water Disposal (PWD) Location: PWD surface owner: Other PWD discharge volume (bbl/day): Other PWD type description: Other PWD type attachment: Have other regulatory requirements been met? Other regulatory requirements attachment:

PWD disturbance (acres):

Injection well name: Injection well API number:

FMSS

U.S. Department of the Interior BUREAU OF LAND MANAGEMENT

Bond Information

Federal/Indian APD: FED

BLM Bond number: NMB001015

BIA Bond number:

Do you have a reclamation bond? NO

Is the reclamation bond a rider under the BLM bond?

Bond Info Data Report

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Is the reclamation bond BLM or Forest Service?

BLM reclamation bond number:

Forest Service reclamation bond number:

Forest Service reclamation bond attachment:

Reclamation bond number:

Reclamation bond amount:

Reclamation bond rider amount:

Additional reclamation bond information attachment: