Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

30-025-36347

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: MEWBOURNE OIL CO.		Lease or Unit Name: SF "22" FED	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date: 11/20/03	Well No.: 1
Completion Date: 10/26/03	Total Depth: 13050	Plug Back TD: 12987	Elevation: 3760
Unit Ltr - Sec - TWP - Rge: 22 18S ~~27E~~ 32e			
Csg. Size: 8 3/4 / Wt.: 17 / d: / Set At: 13045	Perforations: From: 12554 To: 12656	County: Lea ~~EDDY~~	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At: 12464	Perforations: From: To:	Pool: LUSK MORROW NORTH	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At: 12340	Formation: MORROW	
Producing Thru: TUBING	Reservoir Temp.: 168	Mean Annual Temp.: 60	Baro. Press.-P_a: 13.2	Connection: SALES

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
12464	12464	0.677	1.32	6.411			3.068	FLG

	FLOW DATA				TUBING DATA		CASING DATA		
No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp.	Press p.s.i.g.	Temp.	Press p.s.i.g.	Temp.	Duration of Flow
SI					1050				
1	3.068 X .750	65	22	68	50				24 HRS
2									
3									
4									
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1	3.41	41.4	78.2	0.9924	1.215	1.048	250
2							
3							
4							
5							

No.	P_r	Temp. R	T_r	Z
1	0.79	528	1.45	0.911
2				
3				
4				
5				

Gas Liquid Hydrocarbon Ratio	2.083		Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	40.6		Deg.
Specific Gravity Separator Gas	0.677		XXXXXXX
Specific Gravity Flowing Fluid	XXXXX		GMIX = 1.907
Critical Pressure	662 P.S.I.A.	646	P.S.I.A.
Critical Temperature	364 R.	502	R

P_c 1063.2 P_c^2 1130.4

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		70.2	4.9	1125.5
2				
3				
4				
5				

(1) $\dfrac{P_c^2}{P_c^2 - P_w^2} =$ 1.004 (2) $\left[\dfrac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 1.004

$AOF = Q \left[\dfrac{P_c^2}{P_c^2 - P_w^2}\right]^n =$ 0.251

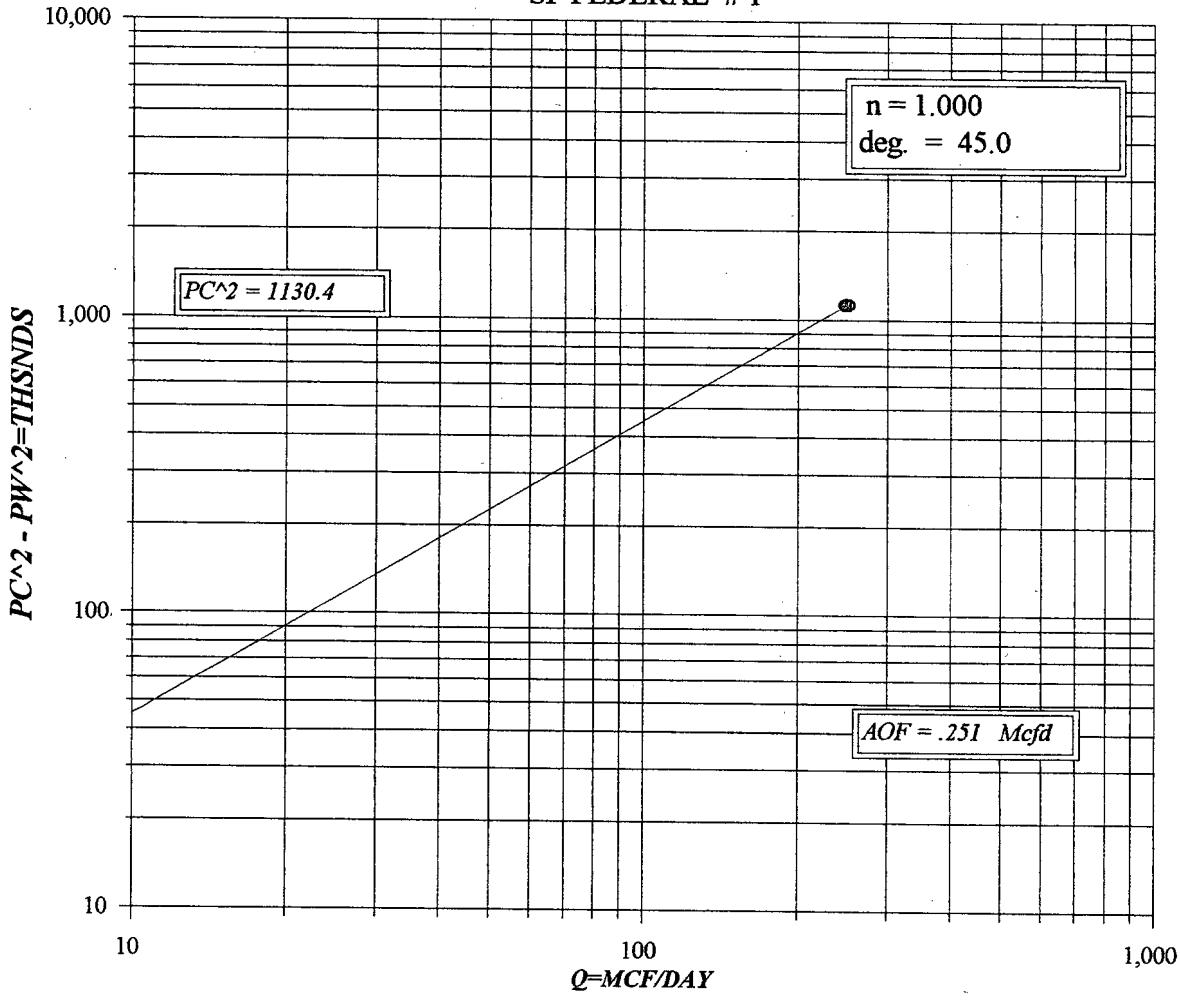
Absolute Open Flow	0.251	Mcfd @ 15.025	Angle of Slope ():	45	Slope n: 1

Remarks: * WELL MADE 5 BBLS OF 40.6 API GRAVITY CONDENSATE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

MEWBOURNE OIL CO.

SF FEDERAL # 1



C122D FORM IMPORTED FROM SYMPHONY ON 9-9-01

COMPANY :	MEWBOURNE OIL		LEASE	: SF "22"FED		WELL NO.	: 1						
UNIT :			SECTION	: 22		TOWNSHIP	: 18S						
L :	12464	H :	12464	L/H :	1	G/GMIX	: 0.677						
%CO2 :	1.32	%N2 :	6.411	H2S :			DATE	: 11/20/03					
d :	2.441	Fr :	0.010763	GH :	8197.0		RANGE	: 32E					
VOL 1 :	250	PSIA 1 :	63.2			RESV.TEMP	168.0						
VOL 2 :		PSIA 2 :											
VOL 3 :		PSIA 3 :				SHUT-IN PRES =	1063.2						
VOL 4 :		PSIA 4 :											
			PCR :	646									
			TCR :	502									

LINE		RATE 1		RATE 2		RATE 3		RATE 4	
		1ST	2ND	1ST	2ND	1ST	2ND	1ST	2ND
1	QM	0.250	0.250	0.000	0.000	0.000	0.000	0.000	0.000
2	TW	534	534	534	534	534	534	534	534
3	Ts	628.0	628.0	628.0	628.0	628.0	628.0	628.0	628.0
4	T	581.0	581.0	581.0	581.0	581.0	581.0	581.0	581.0
	PR (est)	0.10		0.00		0.00		0.00	
5	Z(est)	0.954	0.949	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
6	TZ	554.2	551.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
7	GH/TZ	14.791	14.872	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
8	eS	1.741	1.747	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
9	I-e-S	0.426	0.427	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
10	Pt	63.2	63.2	0.0	0.0	0.0	0.0	0.0	0.0
11	Pt2 /1000	4.0	4.0	0.0	0.0	0.0	0.0	0.0	0.0
12	Fr	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763	0.010763
13	Fc=FrTZ	5.965	5.932	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
14	FcQm	1.49	1.48	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
15	L/H(FcQm)2	2.2	2.2	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
16	Fw	0.946637	0.9402485	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
17	Pw2	4.9	4.9	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
18	Ps2	8.6	8.6	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
19	Ps	92.8	92.8	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
20	P	78.0	78.0	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
21	Pr	0.12	0.12	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
22	Tr	1.16	1.16	1.16	1.16	1.16	1.16	1.16	1.16
23	Z	0.949	0.949	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!

Pc =	1063.2	Pc2 =	1130.4	
Pt2 =	4.0	Pw =	70.2	
	0.0		#DIV/0!	
	0.0		#DIV/0!	
	0.0		#DIV/0!	
Pc2-Pw2=	1125.5	Pw2 =	4.9	
	#DIV/0!		#DIV/0!	
	#DIV/0!		#DIV/0!	
	#DIV/0!		#DIV/0!	
		n =	1.000	
Pc2/(Pc2-Pw2) =			1.004	
			#DIV/0!	
			#DIV/0!	
			#DIV/0!	
[Pc2/Pc2-Pw2]n =			1.004	
			#DIV/0!	
			#DIV/0!	
			#DIV/0!	
		AOF= Q	0.251	
			#DIV/0!	
			#DIV/0!	
			#DIV/0!	

FORM C122-D