OPER. OGRID NO. PROPERTY NO.

POOL CODE

EFF. DATE

FORM APPROVED OMB No. 1004-0136 Expires November 30, 2000

. Lease Serial No. NMNM63994 . If Indian, Allottee or Tribe Name

ALLEGA		,
1a. Type of Work: ☑ DRILL ☐ REENTER		7. If Unit or CA Agreement, Name and No.
	er Single Zone Multiple Zone KAREN COTTOM E-Mail: karen.cpttom@dvn.com	8. Lease Name and Well No. HORNET 6 FEDERAL 3 9. API Well No.
3a. Address 1500 MID-AMERICA TOWER 20 N. BROADWAY	3b. Prone No. (include area code) Ph; 405.228.7512	30 · 025 - 36599 10. Field and Pool, or Exploratory LIVINGSTON RIDGE
OKLAHOMA CITY, OK 73102	Fx: 405.552.4621	Delaware SE
4. Location of Well (Report location clearly and in accorded At surface SENE 1980FNL 660FEL	nce with any State requirements.*)	Sec., T., R., M., or Blk. and Survey or Area Sec 6 T23S R32E Mer NMP
At proposed prod. zone SENE 1980FNL 660FEL	Unit H	SME: BLM
14. Distance in miles and direction from nearest town or post 35 MILES W OF EUNICE NM	office*	12. County or Parish 13. State LEA NM
 Distance from proposed location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) 	16. No. of Acres in Lease 980.63	17. Spacing Unit dedicated to this well 40.00
 Distance from proposed location to nearest well, drilling, completed, applied for, on this lease, ft. 	19. Proposed Depth 8600 MD	20. BLM/BIA/Botter No. on file
21. Elevations (Show whether DF, KB, RT, GL, etc. 3520 GL	22. Approximate date work will start 02/09/2004	23. Estimated duration 7 4 5 DAYS
		ortheried Water Basin's
 The following, completed in accordance with the requirements of the control of the	Item 20 above). em Lands, the 5. Operator certification	ons unless covered by an examplified on file (see formation and/or plans as may be required by the
25. Signature (Electronic Submission)	Name (Printed/Typed) KAREN COTTOM	Date 01/08/2004
Title ENGINEERING TECHNICIAN		

FIELD MANAGER

CARLSBAD FIELD OFFICE

Application approval does not warrant or certify the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Conditions of approval, if any, are attached.

Name (Printed/Typed)

Office

APPROVAL FOR 1 YEAR

Date

FEB 2 3 2004

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

Additional Operator Remarks (see next page)

ESL'E A. THEISS

/s/ LESLIE A. THEISS

Electronic Submission #26665 verified by the BLM Well Information System
For DEVON ENERGY CORPORATION, sent to the Hobbs
DECLARED WATER BASING TO AFMSS for processing by ARMANDO LOPEZ on 01/08/2004 (04AL0009AE) CASING MUST BE CIRCULATED

general requirements and SPECIAL STIPULATIONS

** BLM REVISED ** BLM REVISED ** BLM REVISED **

. Additional Operator Remarks:

NO REMARK PROVIDED

DISTRICT I 1825 N. French Dr., Hobbs, NM 88240 DISTRICT II

DISTRICT IV

State of New Mexico

Form C-102 Revised March 17, 1999

Energy, Minerals and Natural Resources Department

Submit to Appropriate District Office

State Lease - 4 Copies Fee Lease - 3 Copies

DISTRICT III 1000 Rio Brezos Rd., Aztec, NM 87410

2040 South Pacheco, Sanis Fe, NM 67505

811 South First, Artesia, NM 88210

OIL CONSERVATION DIVISION

2040 South Pacheco

Santa Fe, New Mexico 87504-2088

D AMENDED REPORT

WELL LOCATION AND ACREAGE DEDICATION PLAT

API Number	Pool Code	Pool Name		
30-025-365	39380	Livingston Ridge; Delaware	SE SE	
Property Code		operty Name	Well Number	
33130	HORNET	"6" FEDERAL	3	
OGRID No.	Оре	erator Name	Elevation	
6137	DEVON ENERGY	PRODUCTION CO., L.P.	3520'	

Surface Location

1	UL or lot No.	Section	Township	Range	Lot ldn	Feet from the	North/South line	Feet from the	East/West line	County
	Н	6	23 S	32 E		1980	NORTH	660	EAST	LEA

Bottom Hole Location If Different From Surface

I	UL or lot No.	Section	Township	Range	Lot ldn	Feet from the	North/South line	Feet from the	East/West line	County
ſ	Dedicated Acres	Joint o	r Infill Co	nsolidation (Code Or	der No.				
۱	40		-					3		

NO ALLOWABLE WILL BE ASSIGNED TO THIS COMPLETION UNTIL ALL INTERESTS HAVE BEEN CONSOLIDATED OR A NON-STANDARD UNIT HAS BEEN APPROVED BY THE DIVISION

, 	OR A NON-STAN	DARD UNIT HAS BEEN	APPROVED BY TH	E DIVISION
				OPERATOR CERTIFICATION I hereby certify the the information contained herein is true and complete to the best of my knowledge and belief.
LOT 4 - 45.31 AC.	LOT 3 - 39.81 AC.	LOT 2 - 39.71 AC.	.] .00 .00 .00 .00 .00 .00 .00 .00 .00	Signature Linda B Guthrie
	 	} } !	3514.6' - 3519.4'	Printed Name Operations Associate Title 01/07/04
LOT 5 - 45.56 AC.	 		3519.2' 3520.7' at - N32*20'07.1"	SURVEYOR CERTIFICATION I hereby certify that the well location shown
		'Le 	ong – W103*42'26.8"	on this plat was plotted from field notes of actual surveys made by me or under my supervison, and that the same is true and correct to the best of my belief.
LOT 5 - 45.72 AC.	 	+		DECEMBER 22, 2003 Date Survey Signature to Seel of Professional Surveyor Professional Surveyor
	 			7977 (2) M. No. 38952
LOT 7 - 45.88 AC.	<u> </u>			Certification Gor Lines 7977

DRILLING PROGRAM

Devon Energy Production Company, LP Hornet 6 Federal #3

Surface Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM Bottom hole Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM

1. Geologic Name of Surface Formation

a. Permian

2. Estimated tops of geological markers:

a.	Rustler	460'
b.	Salt	830'
c.	Base of Salt	4300'
d.	Delaware	4560'
e.	Cherry Canyon	5550'
f.	Brushy Canyon	7180'
g.	Bone Spring LS	8450'

3. Estimated Depths of Anticipated Fresh Water, Oil or Gas

a. Cherry Canyon

5550'

Oil

No other formations are expected to yield oil, gas or fresh water in measurable volumes. The surface fresh water sands will be protected by setting 13 3/8" casing at 850' and circulating cement back to surface. Potash and salt will be protected by setting 8 5/8" casing at 4350' and circulating cement to surface. The Delaware intervals will be isolated by setting 5 ½" casing to total depth and circulating cement above the base of the 8 5/8" casing.

4. Casing Program:

<u>Hole Size</u>	<u>Interval</u>	OD Csg	<u>Weight</u>	<u>Collar</u>	<u>Grade</u>
25"	0' -40'	20"	Na	Na	Conductor
17 1/2"	0'-850'	13 3/8"	48#	ST&C	H-40
11"	0'-4350'	8 5/8"	32#	LT&C	J55
7 7/8"	0' - 8600'	5 ½"	15.5# & 17#	LT&C	J55

5. Cement & Setting Depth:

a. 20"	Conductor	Cement with ready-mix to surface.
b. 13 3/8	3" Surface	Cement to surface with 610 sx Poz C (35:65) + 2% Cacl2 followed by 250 sx Class C + 2% Cacl2
c. 8 5/8'	' Intermediate	Cement to surface with 1280 sx Poz C (35:65) + 5% Nacl2 followed by 300 sx 60:40 Class C + 5% Nacl2

d. $5\frac{1}{2}$ " Production Cement with 430 sx 35:65:6 + 3% Nacl2 + 0.25% retarder + 0.3% FL + LCM followed by 490 sx 60:40 + 1% Nacl2 + 0.5% Bonding agent + LCM

The above cement volumes could be revised pending the caliper measurement from the open hole logs. The top of cement is designed to reach above the 8 5/8" casing seat @ 4350'

6. Pressure Control Equipment:

The blowout preventor equipment (BOP) shown in Exhibit #1 will consist of a (3M system) double ram type (3000 psi WP) preventor and a bag-type (Hydril) preventor (3000 psi WP). Both units will be hydraulically operated and the ram type preventor will be equipped with blind rams on top and 4 ½" drill pipe rams on bottom. Both BOP's will be installed on the 13 3/8" surface casing and utilized continuously until total depth is reached. All BOP's and associated equipment will be tested to 1200 psi before drilling out the 13 3/8" casing shoe (70% of 48#, H-40 casing). Prior to drilling out the 8 5/8" casing shoe, the BOP's and Hydril will be tested as per BLM Drilling Operations Order #2.

Pipe rams will be operated and check each 24-hour period and each time the drill pipe is out of the hole. These functional tests will be documented on the daily drillers log. A 2" kill line and 3" choke line will be incorporated in the drilling spool below the ram-type BOP. Other accessory BOP equipment will include a Kelly cock, floor safety valve, choke lines and choke manifold having 3000 psi WP rating.

7. Proposed Mud Circulation System

<u>Depth</u>	Mud Wt.	<u>Visc</u>	Fluid Loss	Type System
0' - 850'	8.5-9.0	27-32	NC	Native spud mud
850' – 4350'	9.7-10.2	28-30	NC	Brine water
4350' - 8600'	8.4-8.9	28-34	25	Fresh water w/gel

The necessary mud products for weight addition and fluid loss control will be on location at all times.

8. Auxiliary Well Control and Monitoring Equipment:

- a. A Kelly cock will be in the drill string at all times.
- b. A full opening drill pipe stabbing valve having the appropriate connections will be on the rig floor at all times.
- c. Hydrogen Sulfide detection equipment will be in operations after drilling out the 13 3/8" casing shoe until the 8 5/8" casing is cemented. Breathing equipment will be on location upon drilling the 13 3/8' shoe until total depth is reached.

9. Logging, Coring, and Testing Program:

- a. Drill stem tests will be based on geological sample shows.
- b. The open hole electrical logging program will be:
 - i. Total Depth to Intermediate Casing Dual Laterolog-Micro Laterolog with SP and Gamma Ray. Compensated Neutron Z Density log with Gamma Ray and Caliper.
 - ii. Total Depth to Surface Compensated Neutron with Gamma Ray
 - iii. No coring program is planned

iv. Additional testing will be initiated subsequent to setting the 5 ½" production casing. Specific intervals will be targeted based on log evaluation, geological sample shows and drill stem tests.

10. Potential Hazards:

a. No abnormal pressures or temperatures are expected. No hydrogen sulfide or other hazardous gases or fluids have been encountered, reported or are known to exist at this depth in this area. All personnel will be familiar with all aspects of safe operation of equipment being used to drill this well. Estimated BHP 2900 psi and Estimated BHT 125°.

11. Anticipated Starting Date and Duration of Operations:

a. Road and location construction will begin after the BLM has approved the APD. Anticipated spud date will be as soon after BLM approval and as soon as a rig will be available. Move in operations and drilling is expected to take 32 days. If production casing is run then an additional 30 days will be needed to complete well and construct surface facilities and/or lay flow lines in order to place well on production.

SURFACE USE PLAN

Devon Energy Production Company, LP

Hornet 6 Federal #3

Surface Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM Bottom hole Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM

1. Existing Roads:

- a. The well site and elevation plat for the proposed are reflected on Exhibit 2. The well was staked by Basin Surveys.
- b. All roads into the location are depicted on Exhibit 3.
- c. Directions to Location: From the junction of US Hwy 62/180 and Co. Rd H-29, go south on H-29 for 15.8 miles to a lease road; thence east on lease road for 1.2 mile to a "Y", go left at "Y" and continue east for 0.9 mile to a water line and lease road; thence northerly on lease road for approximately 0.5 mile to a proposed lease road.

2. Access Road

- a. Exhibit #3 shows the existing lease road. Approximately 238' of new access road will be constructed. It will be constructed as follows:
- b. The maximum width of the road will be 15'. It will be crowned and made of 6" of rolled and compacted caliche. Water will be deflected, as necessary, to avoid accumulation and prevent surface erosion.
- c. Surface material will be native caliche. This material will be obtained from a BLM approved pit nearest in proximity to the location. The average grade will be approximately 1%.
- d. No cattle guards, grates or fence cuts will be required. No turnouts are planned.

3. Proposed Facilities

- a. In the event the well is found productive, a tank battery would be constructed and the necessary production equipment will be installed at the well site.
- b. If necessary, the well will be operated by means of an electric prime mover. Electric power poles will be set along side of the access road.
- c. The tank battery, all connections and all lines will adhere to API standards.
- d. The well will be operated by means of a gas driven prime mover. No power will be required.
- e. If the well is productive, rehabilitation plans are as follows:
 - i. The reserve pit will be back-filled after the contents of the pit are dry (within 120 days after completion, weather permitting).
 - ii. The original topsoil from the well site will be returned to the location. The drill site will then be contoured as close as possible to the original state.

4. Methods of Handling Waste Material:

- a. Drill cuttings will be disposed of in the reserve pits.
- b. All trash, junk and other waste material will be contained in trash cages or trash bins to prevent scattering. When the job is completed all contents will be removed and disposed of in an approved sanitary landfill.
- c. The supplier, including broken sacks, will pick up salts remaining after completion of well.
- d. Wastewater from living quarters will be drained into hole with a minimum of 10'. These holes will be covered during drilling and will be back filled when the well is completed. A Porto-john will be provided for the rig crews. This equipment will be properly maintained during the drilling and completion operations and will be removed when all operations are complete

e. Remaining drilling fluids will be allowed to evaporate in the reserve pits until the pits are dry enough to be broken out for further drying. If the drilling fluids do not evaporate in a reasonable time they will be hauled off by transports to a state approved disposal site. Later pits will be broken out to speed dry. Water produced during completion will be put in reserve pits. Oil and condensate produced will be put in a storage tank and sold.

5. Well Site Layout

- a. Exhibit D Shows the proposed well site layout.
- b. This exhibit indicated proposed location of reserve and sump pits and living facilities.
- c. Mud pits in the active circulating system will be steel pits & the reserve pits is proposed to be unlined unless subsurface condition encountered during pit construction indicate that lining is needed for lateral containment of fluids.
- d. If needed, the reserve pit is to be lined with polyethylene. The pit liner will be 6 mils thick. Pit liner will extend a minimum 2' over the reserve pits dikes where the liner will be anchored down.
- e. The reserve pit will be fenced on three sides with four strands of barbed wire during drilling and completion phases. The fourth side will be fenced after all drilling operations have ceased. If the well is a producer, the reserve pit fence will be torn down. The reserve pit and those areas of the location not essential to production facilities will be reclaimed and seeded per BLM requirements.

6. Other Information:

- a. The area surrounding the well site is grassland. The topsoil is very sandy in nature. The vegetation is moderately sparse with native prairie grass, sagebrush, yucca and miscellaneous weeds.
- b. The surface and minerals are owned by the US Government and is administered by the Bureau of Land Management. The surface is of limited use except for the grazing of livestock and the production of oil and gas.
- c. An archaeological survey will be submitted to the Bureau of Land Management
- d. There are no dwellings within 2 miles of location.

Operators Representative:

The Devon Energy Production Company, L.P. representatives responsible for ensuring compliance of the surface use plan are listed below.

James Blount Operations Engineer Advisor

Don Mayberry Superintendent

Devon Energy Production Company, L.P. 20 North Broadway, Suite 1500 Oklahoma City, OK 73102-8260

Devon Energy Production Company, L.P. Post Office Box 250 Artesia, NM 88211-0250

(405) 228-4301 (office) (405) 834-9207 (Cellular) (505) 748-3371 (office) (505) 746-4945 (home)

Certification

I hereby certify that I, or persons under my direct supervision, have inspected the proposed drill site and access road; that I am familiar with the conditions that presently exist; that the statements made in this plan are, to the

best of my knowledge, true and correct; and that the work associated with the operations proposed herein wil	11
be performed by Devon Energy Production Company, L.P. and its contractors and subcontractors in conform	iity
with this plan and the terms and conditions under which it is approved.	

signed: Lakal

Date: January 7, 2004

Linda Guthrie
Operations Associate

Attachment to Exhibit #1 NOTES REGARDING BLOWOUT PREVENTERS

Devon Energy Production Company, LP

Hornet 6 Federal #3

Surface Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM Bottom hole Location: 1980' FNL & 660' FEL, Unit Letter H, Sec 6 T23S R32E, Lea, NM

- 1. Drilling nipple will be constructed so it can be removed mechanically without the aid of a welder. The minimum internal diameter will equal BOP bore.
- 2. Wear ring will be properly installed in head.
- 3. Blowout preventer and all associated fittings will be in operable condition to withstand a minimum 3000 psi working pressure.
- 4. All fittings will be flanged.
- 5. A full bore safety valve tested to a minimum 3000 psi WP with proper thread connections will be available on the rotary rig floor at all times.
- 6. All choke lines will be anchored to prevent movement.
- 7. All BOP equipment will be equal to or larger in bore than the internal diameter of the last casing string.
- 8. Will maintain a kelly cock attached to the kelly.
- 9. Hand wheels and wrenches will be properly installed and tested for safe operation.
- 10. Hydraulic floor control for blowout preventer will be located as near in proximity to driller's controls as possible.
- 11. All BOP equipment will meet API standards and include a minimum 40 gallon accumulator having two independent means of power to initiate closing operation.

UNITED STATES DEPARTMENT OF THE INTERIOR

Bureau of Land Management Roswell Field Office 2909 West Second Street Roswell, New Mexico 88201-1287

Statement Accepting Responsibility for Operations

Devon Energy Production Company, LP

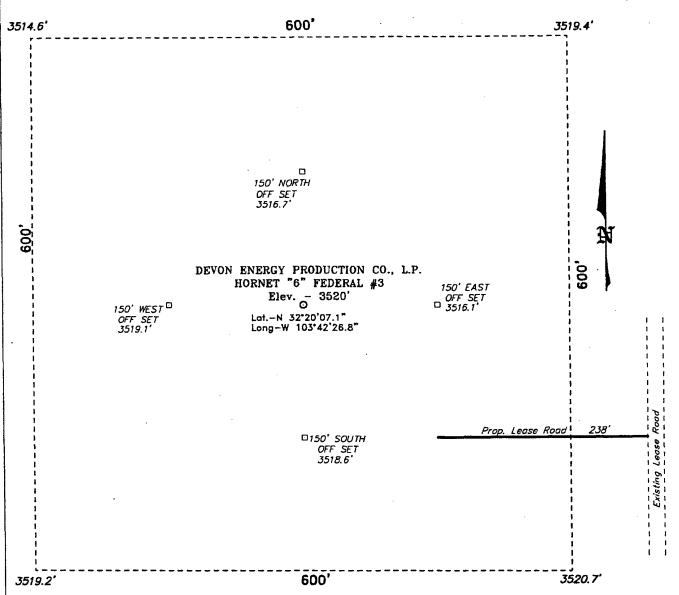
20 North Broadway, Suite 1500

City, State: Zip Code:	Oklahoma City, Oklahoma 73102-8260
<u> </u>	applicable terms, conditions, stipulations and restrictions concerning leased land or portion thereof, as described below.
Lease No.:	NMNM63994
Legal Description of Land:	40 acres 6-T23S-R32E
Formation(s):	Delaware/Bone Spring
Bond Coverage:	Nationwide
BLM Bond File No.:	CO-1104
Authorized Signature:	Linda Guthrie
Title:	Operations Associate
Date:	January 7, 2004

Operator Name:

Street or Box:

SECTION 6, TOWNSHIP 23 SOUTH, RANGE 32 EAST, N.M.P.M., LEA COUNTY, NEW MEXICO.



Directions to Location:

12-23-2003

FROM THE JUNCTION OF US HWY 62/180 AND CO. RD. H-29, GO SOUTH ON H-29 FOR 15.8 MILES TO A LEASE ROAD; THENCE EAST ON LEASE ROAD FOR 1.2 MILE TO A "Y", GO LEFT AT "Y" AND CONTINUE EAST FOR 0.9 MILE TO A WATER LINE AND LEASE ROAD; THENCE NORTHERLY ON LEASE ROAD FOR APPROX. 0.5 TO A PROPOSED LEASE ROAD.

BASIN SURVEYS P.O. BOX 1786-HOBBS, NEW MEXICO

Disk: KJG CD#4 -

3885A.DWG

W.O. Number: 3885 Drawn By: **K. GOAD**

100 0 100 200 FEET

SCALE: 1" = 100'

DEVON ENERGY PROD. CO., L.P.

: HORNET "6" FED. No. 3 / Well Pod Topo

THE HORNET "6" FED. No. 3 LOCATED 1980' FROM

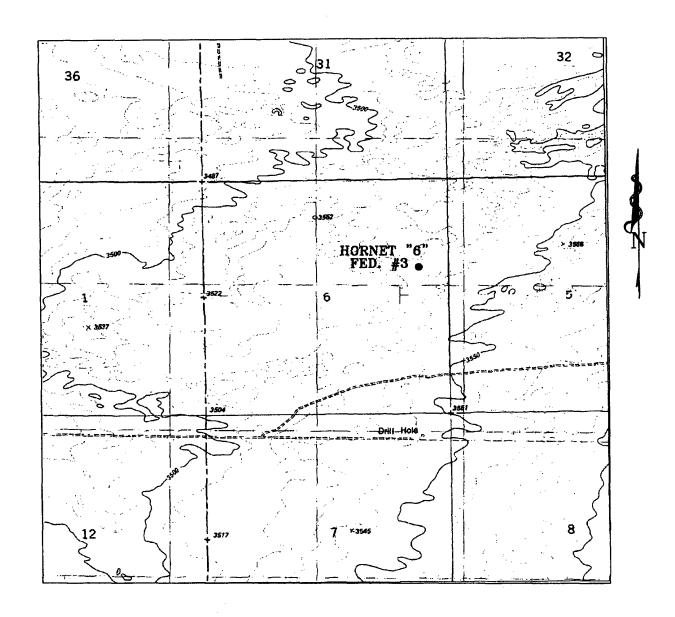
THE NORTH LINE AND 660' FROM THE EAST LINE OF

SECTION 6, TOWNSHIP 23 SOUTH, RANGE 32 EAST,

N.M.P.M., LEA COUNTY, NEW MEXICO.

Sheets

Survey Date: 12-22-2003 Sheet 1 of 1



HORNET "6" FEDERAL #3 1980' FNL AND 660' FEL Section 6, Township 23 South, Range 32 East, N.M.P.M., Lea County, New Mexico.



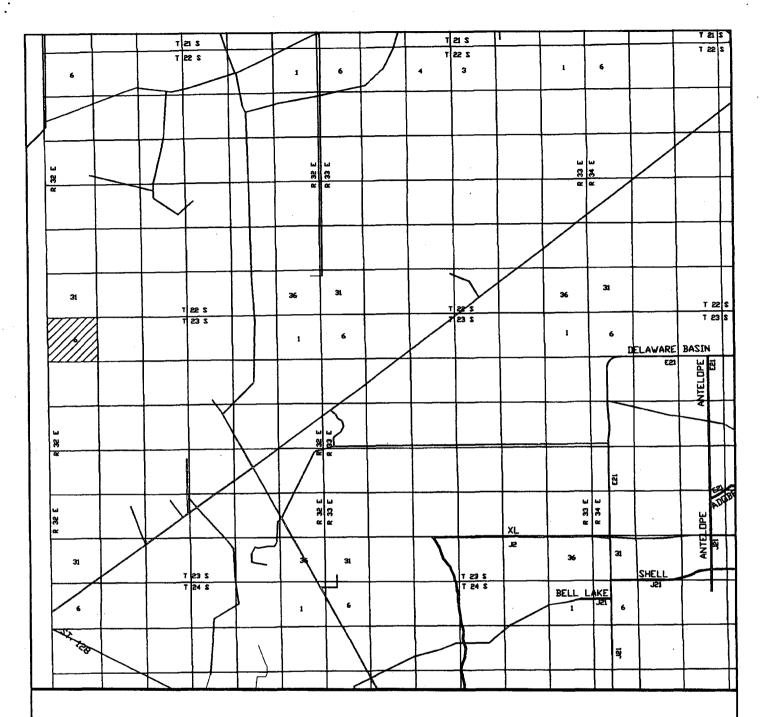
focused on excellence in the oilfield

P.O. Box 1786 1120 N. West County Rd. Hobbs, New Mexico 88241 (505) 393-7316 - Office (505) 392-3074 - Fax

basinsurveys.com

W.O. Number:	3885ÅA - KJG CD#4
Survey Date:	12-22-2003
Scale: 1" = 20	000'
Date: 12-23-	-2003

DEVON ENERGY PROD. CO., L.P.



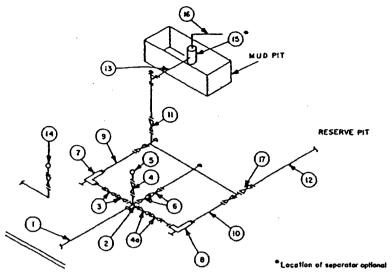
HORNET "6" FEDERAL #3
1980' FNL AND 660' FEL
Section 6, Township 23 South, Range 32 East,
N.M.P.M., Lea County, New Mexico.



P.O. Box 1786 1120 N. West County Rd. Hobbs, New Mexico 88241 (505) 393-7316 - Office (505) 392-3074 - Fax basinsurveys.com

W.O. Number:	3885AA - KJG CD#4
Survey Date:	12-22-2003
Scale: 1" = 2	MILES
Date: 12-23-	-2003

DEVON ENERGY PROD. CO., L.P.



BEYOND	SUBST	RUCTUR	ŧ
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			MINI	MUM REOL	HREMENTS	3				
			3,000 MWP						10,000 MWF	
No.		I.D.	NOMINAL	RATING	1.0.	NOMINAL	PLATING	I.D.	NOMINAL	RATING
1	Line from drilling spool		3*	3,000		3"	5,000		3*	10,000
2	Cross 3"x3"x3"x2"			3,000			5,000			
	Cross 3"x3"x3"x3"									10,000
3	Valves(1) Gate □ Plug □(2)	3-1/8"		3,000	3-1/8*	·	5,000	3-1/8*		10,000
4	Valve Gate □ Plug □(2)	1-13/16*	·	3,000	1-13/16*		5,000	1-13/16*		10,000
4a	Valves(1)	2-1/16"		3,000	2-1/16*		5,000	3-1/8"		10,000
5	Pressure Gauge			3,000	•		5,000			10,000
6	Valves Gate □ Plug □(2)	3-1/8"		3,000	3-1/8*		5,000	3-1/8"		10,000
7	Adjustable Choke(3)	2*		3,000	2*		5,000	2*		10,000
8	Adjustable Choke	1"		3,000	1"		5,000	2-		10,000
9	Line		3*	3,000		3"	5,000		3″	10,000
10	Line		2*	3,000		2"	5,000		3-	10,000
11	Valves Gate □ Plug □(2)	3-1/8"		3,000	3-1/8*		5,000	3-1/8"		10,000
12	Lines		3*	1,000		3″	1,000		3*	2,000
13	Lines	1	3*	1,000		3*	1,000		3*	2,000
14	Remote reading compound standpipe pressure gauge			3,000			5,000	-		10,000
15	Gas Separator		2'x5'			2'x5'			2'x5'	
16	Line	1	4*	1,000		4*	1,000		4"	2,000
17	Valves Gate □ Plug □(2)	3-1/8"		3,000	3-1/8"		5.000	3-1/8*		10,000

- (1) Only one required in Class 3M.
- (2) Gate valves only shall be used for Class 10M.
- (3) Remote operated hydraulic choke required on 5,000 psi and 10,000 psi for drilling.

EQUIPMENT SPECIFICATIONS AND INSTALLATION INSTRUCTIONS

- 1. All connections in choke manifold shall be welded, studded, flanged or Cameron clamp of comparable rating.
- 2. All flanges shall be API 6B or 6BX and ring gaskets shall be API RX or BX. Use only BX for 10 MWP.
- 3. All fines shall be securely anchored.
- 4. Chokes shall be equipped with tungsten carbide seats and needles, and replacements shall be available.
- 5. Choke manifold pressure and standpipe pressure gauges shall be available at the choke manifold to assist in regulating chokes. As an alternate with automatic chokes, a choke manifold pressure gauge shall be located on the rig floor in conjunction with the standpipe pressure gauge.
- Line from drilling spool to choke manifold should be as straight as possible. Lines downstream from chokes shall make turns by large bends or 90° bends using bull plugged tees.
- 7. Discharge lines from chokes, choke bypass and from top of gas separator should vent as far as practical from the well.

CONFIGURATION

1,000 psl Working Pressure

3 MWP

STACK REQUIREMENTS

No.	llem		Mın. I.D.	Min. Nominal
1	Flowline			
2	Fill up line			2"
3	Drilling nipple			
4	Annular preventer			
5	Two single or one dual hyd operated rams			
6a	Drilling spool with 2" min. I 3" min choke line outlets			
6b	2" min. kill line and 3" min outlets in ram. (Alternate to			
7	Valve	3-1/8"		
8	Gale valve-power operate	ad	3-1/8*	·
9	Line to choke manifold			3*
10	Valves	Gate 🗅 Plug 🖸	2-1/16"	
11	Check valve	2-1/16"		
12	Casing head			
13	Valve	Gate D Plug D	1-13/16*	
14	Pressure gauge with needl			
15	Kill line to rig mud pump m	aniloid		2*

. (D. F	Ø . ·
(
••		
	. ANKULAR PREVENTER	
		1
	BLIND RAUS	
•		<u> </u>
_	PIPE RAMS	
		<u> </u>
(B)·		(D-i-[]
	DRILLING	
	SPOOL I	San mile
. (1)	5	
	CASING	XIII La
	7	- March
	(E) CASING	® W

		OPTIONAL		
16	Flanged valve	:	1-13/16"	

CONTRACTOR'S OPTION TO FURNISH:

- 1.All equipment and connections above bradenhead or casinghead. Working pressure of preventers to be 3,000 psi, minimum.
- 2. Automatic accumulator (80 gallon, minimum) capable of closing BOP in 30 seconds or less and, holding them closed against full rated working pressure.
- BOP controls, to be located near drillers position.
- 4. Kelly equipped with Kelly cock.
- 5. Inside blowout prevventer or its equivalent on derrick floor at all times with proper threads to fit pipe being used.
- 6.Kelly saver-sub equipped with rubber casing protector at all times.
- 7-Plug type blowout preventer tester.
- 8.Extra sat pipe rams to ili drili pipe in use on location at all times.
- 9. Type RX ring gaskets in place of Type R.

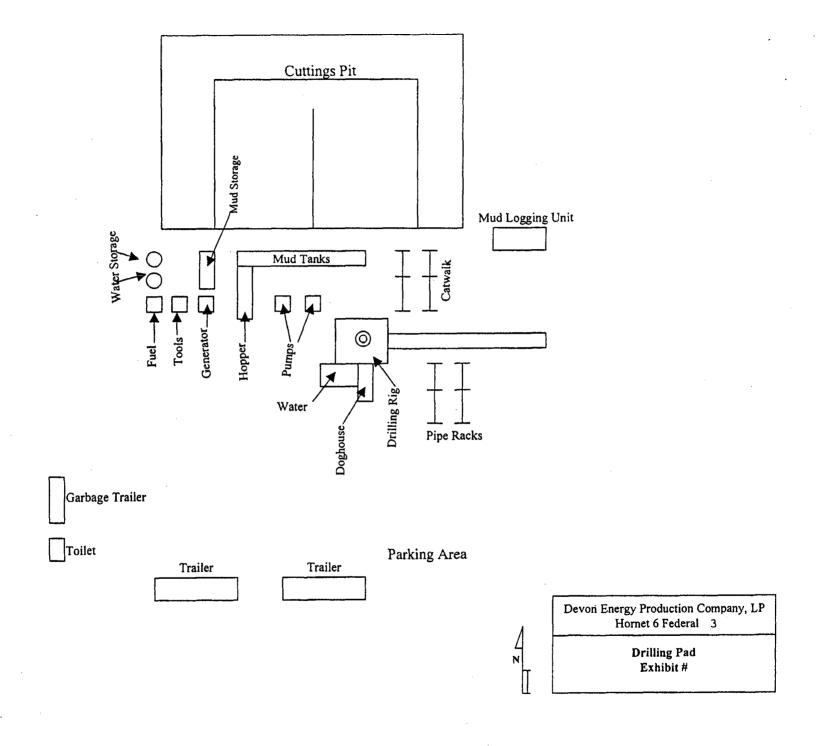
MEC TO FURNISH:

- Bradenhead or casinghead and side valves.
- 2.Wear bushing, if required.

GENERAL NOTES:

- Deviations from this drawing may be made only with the express permission of MEC's Drilling Manager.
- 2.All connections, valves, fittings, piping, etc., subject to well or pump pressure must be flanged (sultable clamp connections acceptable) and have minimum working pressure equal to rated working pressure of preventers up through chore. Valves must be full opening and sultable for high pressure mud service.
- Controls to be of standard design and each marked, showing opening and closing position.
- 4. Chokes will be positioned so as not to hamper or delay changing of choke beans. Replaceable parts for adjustable choke, other bean sizes, retainers, and choke wrenches to be conveniently located for immediate use.
- All valves to be equipped with handwheels or handles ready for immediate use.
- 5. Choke lines must be sultably anchored.

- 7. Handwheels and extensions to be connected and ready for use.
- Valves adjacent to drilling apool to be kept open. Use outside valves except for emergency.
- 9.All seamless steel control piping (3000 psi working pressure) to have flexible joints to avoid stress. Hoses will be permitted.
- Casinghead connections shall not be used except in case of emergency.
- 11.Do not use kill line for routine fill-up operations.



Well name:
Operator:
String type:

New Mexico

Hornet 6 Fed 3

Surface 3

New Mexico

Burst	Design parameters: Collapse Mud weight: 9.000 ppg Design is based on evacuated pipe.			Minimun Collapse: Design fac	•	tors: 1.125	Environme H2S conside Surface tem Bottom hole Temperature Minimum se	No 75 °F 82 °F 1.40 °F/100ft 500 ft		
Max anticipated surface pressure:						ctor	1.00		ouon longui.	000 K
Description Pressure Pressu	Burst			•						
Internal gradient: Calculated BHP 500 psi 8 Round STC: 1.80 (J) 8 Round LTC: 1.80 (B) 8		anticipated :	surface							
Calculated BHP 500 psi 8 Round STC: 1.80 (J) 8 Round LTC: 1.80 (J) No backup mud specified. Buttress: 1.60 (J) Premium: 1.50 (J) Body yield: 1.60 (B) Re subsequent strings: Next setting depth: 2.200 ft Next mud weight: 9.000 ppg Neutral point: 434 ft Next mud weight: 1.029 psi Fracture mud wt: 19.250 ppg Fracture depth: 500 ft Injection pressure Run Segment Size Weight Grade Finish Depth Depth Diameter (ft) (in) (lbs/ft) (ft) (in) (lbs/ft) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Load Strength Design Load Strength Design (psi) (psi) Factor (kips) (kips) Factor	pı	ressure:								
No backup mud specified. Buttress:								Non-directional string.		
No backup mud specified. Buttress: 1.60 (J) Premium: 1.50 (J) Body yield: 1.60 (B) Re subsequent strings: Next setting depth: 2,200 ft Next mud weight: 9.000 ppg Neutral point: 434 ft Next mud weight: 1,029 psi Fracture mud wt: 19.250 ppg Fracture depth: 500 ft Injection pressure 500 psi Run Segment Nominal End True Vert Measured Drift Est. Seq Length Size Weight Grade Finish Depth Depth Diameter Cost (ft) (in) (lbs/ft) (ft) (ft) (in) (\$) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Tension Seq Load Strength Design Load Strength Design Load Strength Design (psi) (psi) Factor (kips) (kips) Factor	Calc	ulated BHP		500 psi			٠,,			
Premium: 1.50 (J) Body yield: 1.60 (B) Re subsequent strings: Next setting depth: 9.000 ppg Neutral point: 434 ft Next setting BHP: 1,029 psi Fracture depth: 500 ft Injection pressure 500 psi Run Segment Nominal End True Vert Measured Drift Injection pressure 500 psi Run Size Weight Grade Finish Depth Depth Diameter Cost (ft) (in) (lbs/ft) (ft) (ft) (in) (\$\$) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Tension Seq Load Strength Design Factor						_1C:				
Body yield: 1.60 (B) Re subsequent strings: Next setting depth: 2,200 ft Tension is based on air weight. Neutral point: 434 ft Next mud weight: 9.000 ppg Neutral point: 434 ft Next mud weight: 9.000 ppg Fracture mud wt: 19.250 ppg Fracture depth: 500 ft Injection pressure 500 psi Run Segment Nominal End True Vert Measured Drift Est. Seq Length Size Weight Grade Finish Depth Depth Diameter Cost (ft) (in) (lbs/ft) (ft) (ft) (in) (\$\$) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Tension Seq Load Strength Design Load Strength Design Load Strength Design (psi) (psi) Factor (psi) (psi) Factor (kips) (kips) Factor	NO D	eckup mud	specified.		• •					
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Tension is based on air weight. Neutral point: 434 ft Next mud weight: Next setting BHP: 1,029 psi Fracture mud wt: Injection pressure 800 psi Run Segment Seq Length Size Weight (ft) (in) (lbs/ft) 1 500 13.375 Run Collapse Collapse Load Strength Design Factor (kips) Kext mud weight: Next					Body yield	3:	1.60 (B)	•	_	0.000.0
Neutral point: A34 ft										
Run Segment Nominal End True Vert Measured Drift Est. Seq Length Size Weight Grade Finish Depth Depth Diameter Cost (ft) (in) (lbs/ft) (ft) (ft) (in) (\$\$) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Tension Seq Load Strength Design Load Strength Design Load Strength Design (psi) (psi) Factor (psi) (psi) Factor (kips) (kips) Factor									_	
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Run Segment Nominal End True Vert Measured Drift Est. Seq Length Size Weight Grade Finish Depth Depth Diameter Cost (ft) (in) (lbs/ft) (ft) (ft) (in) (\$) 1 500 13.375 48.00 H-40 ST&C 500 500 12.59 6201 Run Collapse Collapse Collapse Burst Burst Burst Tension Tension Tension Seq Load Strength Design Load Strength Design Load Strength Design (psi) (psi) Factor (psi) (psi) Factor (kips) (kips) Factor										
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SeqLength (ft)Size (in)Weight (lbs/ft)GradeFinish (ft)Depth (ft)Depth (ft)Diameter (in)Cost (s)150013.37548.00H-40ST&C50050012.596201RunCollapseCollapseBurstBurstBurstTensionTensionTensionSeqLoadStrengthDesignLoadStrengthDesignLoadStrengthDesign(psi)(psi)Factor(psi)Factor(kips)(kips)Factor								injection	pressure	out psi
SeqLength (ft)Size (in)Weight (lbs/ft)GradeFinish (m)Depth (ft)Depth (ft)Diameter (ft)Cost (in)150013.37548.00H-40ST&C50050012.596201RunCollapseCollapseBurstBurstBurstTensionTensionTensionSeqLoadStrengthDesignLoadStrengthDesignLoadStrengthDesign(psi)(psi)Factor(psi)(psi)Factor(kips)(kips)Factor	Run	Seament		Nominal		End	True Vert	Measured	Drift	Est.
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Seq Load Strength Design Load Strength Design Load Strength Design (psi) (psi) Factor (psi) (psi) Factor (kips) Factor	Run	Collapse	Collapse	e Collapse	Burst	Burst	Burst	Tension	Tension	Tension
(psi) (psi) Factor (psi) (psi) Factor (kips) (kips) Factor		•	•	•						
they they they they they			-	-		•	_		•	•
	1	•• •			., .	** *		· · ·		

Devon Energy

Date: October 2,2003 Oklahoma City, Oklahoma

Remarks:

Collapse is based on a vertical depth of 500 ft, a mud weight of 9 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Well name: Hornet 6 Fed 3

Operator: Devon Energy
String type: Intermediate

Location: New Mexico

,									
Design	paramete	rs:		Minimum	design fac	tors:	Environme		
Collaps	e			Collapse:			H2S conside	ered?	No
Mud	weight:	11	0.000 ppg	Design fac	tor	1.125	Surface tem	perature:	75 °F
Desi	gn is based	on evacuate	ed pipe.					temperature:	135 °F
							Temperature		1.40 °F/100ft
	•						Minimum se	ction length:	500 ft
				Burst:		4.00			
				Design fac	tor	1.00			
Burst									
	anticipated		010 pci				•		
pressure: 2,919 psi Internal gradient: 0.120 psi/ft				Tension:			Non-directio	nat string	
Calculated BHP 3,435 psi			8 Round S	STC:	1.80 (J)	Non-directional string.			
Calculated Diff. 3,435 psi			8 Round L		1.80 (J)				
No backup mud specified.			Buttress:		1.60 (J)				
			Premium: 1.50 (J)						
				Body yield: 1.60 (B)			Re subsequ	ent strings:	
							Next setting depth: 8,400 f		
					based on air	-	Next mu	9.000 ppg 3,927 psi	
				Neutral po	Neutral point: 3,661 ft			Next setting BHP:	
								mud wt:	19.250 ppg
			•				Fracture	•	4,300 ft
							injection	pressure	4,300 psi
Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost
	(ft)	(in)	(lbs/ft)			(ft)	(ft)	(in)	(\$)
1	4300	8.625	32.00	J-55	LT&C	4 3 €D'	4352	7.875	34652
				• ••		1000	130		0.002
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension
Seq	Load	Strength	Design	Load	Strength	Design	Load	Strength	Design
	(psi)	(psi)	Factor	(psi)	(psi)	Factor	(kips)	(kips)	Factor
1	2234	2530	1.13	3435	3930	1.14	137.6	417	3.03 J

Devon Energy

Date: October 2,2003 Oklahoma City, Oklahoma

Remarks:

Collapse is based on a vertical depth of 4300 ft, a mud weight of 10 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Well name:

Hornet 6 Fed 3

Operator:

Devon Energy

String type:

Production

Location:

New Mexico

Design parameters:

Collapse

9.000 ppg

Mud weight: Design is based on evacuated pipe. Minimum design factors:

Collapse: Design factor

1.125

Environment: H2S considered?

Surface temperature: Bottom hole temperature: 193 °F

No 75 °F

Temperature gradient:

1.40 °F/100ft

Burst:

Design factor

1.00

Minimum section length:

500 ft

Burst

Max anticipated surface

No backup mud specified.

pressure: Internal gradient: Calculated BHP

2,919 psi 0.120 psi/ft

3,927 psi

Tension: 8 Round STC:

8 Round LTC: Buttress:

Premium: Body yield: 1.50 (J) 1.60 (B)

1.80 (J) 1.80 (J)

1.60 (J)

Tension is based on air weight. Neutral point: 7,235 ft

Estimated cost:

30,210 (\$)

Non-directional string.

Run	Segment		Nominal		End	True Vert	Measured	Drift	Est.
Seq	Length	Size	Weight	Grade	Finish	Depth	Depth	Diameter	Cost
	(ft)	(in)	(lbs/ft)			(ft)	(ft)	(in)	(\$)
3	600	5.5	17.00	J-55	LT&C	600	600	4.767	2325
2	6800	5.5	15.50	J-55	LT&C	7400	7400	4.825	24011
1	1000	5.5	17.00	J-55	LT&C	8600	8600	4.767	3874
Run	Collapse	Collapse	Collapse	Burst	Burst	Burst	Tension	Tension	Tension
Seq	Load	Strength	Design	Load	Strength	Design	Load	Strength	Design
	(psi)	(psi)	Factor	(psi)	(psi)	Factor	(kips)	(kips)	Factor
3	281	3893	13.88	2991	5320	1.78	132.6	247	1.86 J
2	3460	3968	1.15	3807	4810	1.26	122.4	217	1.77 J
1	3927	4910	1.25	3927	5320	1.35	17	247	14.53 J

Devon Energy

Date: October 2,2003 Oklahoma City, Oklahoma

Collapse is based on a vertical depth of 8400 ft, a mud weight of 9 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

